REPORT



WALKER AGGREGATES INC.

NIAGARA FALLS, ONTARIO

UPPER'S QUARRY: ACOUSTIC ASSESSMENT REPORT

RWDI #1603157 January 11, 2024

SUBMITTED TO

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VERSION HISTORY

| Index | Date | Description | Prepared by | Reviewed by |
|-------|-------------------|----------------------------------|---------------------|----------------|
| 1 | September 4, 2020 | Acoustic Assessment Report | Ray Li | Khalid Hussein |
| 2 | October 28, 2021 | Additional Modelling | Ray Li | Slavi Grozev |
| 3 | August 2, 2023 | Response to Peer Review Comments | Slavi Grozev | Slavi Grozev |
| 4 | January 11, 2024 | Response to Peer Review Comments | Caelan Weber-Martin | Slavi Grozev |

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1 INTRODUCTION

Walker Aggregates Inc. (WAI) has retained RWDI AIR Inc. (RWDI) to complete an Acoustic Assessment Report (AAR) for the Upper's Quarry (the Quarry) in Niagara Falls, Ontario.

This assessment is completed in respect of an application under the Aggregate Resources Act. Based on the Ministry of Natural Resources Policy #A.R. 2.01.09 (MNR, 2006), a detailed noise assessment is required since there are noise-sensitive lands within 150 m of the Quarry. The Aggregate Resources Act recommends referencing the Ontario Ministry of the Environment and Climate Change (MOECC) guidelines for stationary sources of sound. This AAR is completed using the applicable Ontario Ministry of the Environment, Conservation and Parks (MECP), previously known as the Ministry of the Environment and Climate Change (MOECC), guidance documents (MOECC, 2012 and 1995). Documents in this report still reference the MOECC.

Quarry operations will not include large sources of vibration. Therefore, an assessment of vibration impact is not required. Blasting is outside of the scope of this assessment and is addressed separately in the blast impact analysis by Explotech. The results of the acoustic assessment indicate that sound levels produced at the proposed quarry will comply with the applicable guidelines with the implementation of noise control recommendations summarized in **Section 6**.

2 FACILITY DESCRIPTION

The proposed Upper's Quarry is located on Part of Lots 119, 120, 136 and 137, and Part of the Road Allowance between Lots 120 and 136 (geographic township of Stamford) in the City of Niagara Falls, Regional Municipality of Niagara. Sensitive land uses adjacent to Upper's is shown on zoning maps in **Appendix A**.

2.1 Proposed Extraction Scenario

The layout of the site and phases for the Proposed Extraction Scenario can be found in **Figure 1**. Two municipal road allowances separate the proposed quarry site into three extraction areas:

- i. North Extraction Area: extraction area north of Upper's Lane;
- ii. Mid Extraction Area: extraction area south of Upper's Lane and north of the unopened road allowance between Township Lots 120 & 136 in the former Township of Stamford, now in the City of Niagara Falls ("unopened road allowance"); and
- iii. South Extraction Area: extraction area south of the unopened road allowance.

The proposed extraction scenario avoids extraction within the road allowances. Operations at the proposed quarry will consist of overburden stripping; berm construction; drilling, blasting, extraction, transportation, processing, washing, stockpiling, and shipping of aggregate; and rehabilitation. The annual production limit will be 1,800,000 tonnes of aggregate per year, however during several phases of operation, the maximum annual tonnage will be lower due to operational constraints.

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Clearing of overburden and berm construction will take place prior to drilling and blasting in each phase. At the start of extraction operations, four sinking cuts will be required to allow extraction to begin. Two sinking cuts are required in Phase 1A (one in the Mid Extraction Area, one in the South Extraction Area), one sinking cut is required in 2A.

During the sinking cuts and early phases of operation, the primary crusher is integrated into a single processing plant located near the working face. In later phases, the primary crusher will split from the single integrated plant and start to follow the working face. The processing plant, which contains the secondary and tertiary crushers, will remain close to the quarry entrance. The processing plant will be located at varying elevations, beginning at the top of rock during the sinking cut portion of operations, and moving to the first bench and then the final quarry floor as space becomes available.

Shot rock will be loaded by front-end loaders into the primary crusher adjacent of the working face. Conveyors will then transport the products from the primary crusher to the processing plant, where it will be further processed, washed and stockpiled, prior to loading into highway shipping trucks by front-end loaders.

Phases 1A, 2A, and 3 will be extracted in two benches down to the Quarry floor, which is at elevations of 141 to 149 metres above sea level (masl). The quarry floor has a gradual downward slope from the northeast corner (149 masl) to the southwest corner (141 masl). The first bench is between 175 to 178 masl and the second bench is between 160 to 162 masl. Phases 1B and 2B will be extracted to an elevation of 155 masl. They will then be backfilled with clay material up to approximately 176 to 177 masl for the watercourse realignment.

In addition to aggregate extraction and processing, the site will also include an asphalt plant (AP), to be located in mid-extraction area Phase 1A, capable of producing 4,900 tonnes per day of hot-mix asphalt (HMA). Operations include the receipt and drying of washed aggregate, receipt and storage of asphalt cement, mixing and storage of HMA, and loading highway trucks for shipment to the job site. The asphalt plant will become operational once Phases 1A and 1B have been fully extracted. This will allow room for the asphalt plant to be put in place.

The hours of operation at the Quarry for the Proposed Extraction Scenario are:

- Drilling and extraction at the working face: Monday to Saturday 0700 1900h;
- Aggregate processing at the primary crusher: Monday to Saturday 0700 1900h;
- Conveyor to the mobile crusher plants: Monday to Saturday 0700 1900h;
- Aggregate processing at the processing plant: Monday to Saturday 0700 1900h;
- Aggregate shipping from processing plant stockpile: 24 hours per day, 7 days a week;
- Hauling aggregates from processing plant stockpiles to the asphalt plant: 24 hours per day, 7 days a week;
- Asphalt plant: 24 hours per day, 7 days a week;
- HMA shipping from asphalt plant: 24 hours per day, 7 days a week; and
- Asphalt cement (AC) and reclaimed asphalt pavement (RAP) receiving at the asphalt plant: 24 hours per day, 7 days a week.



2.2 Modelled Phases

The receptors surrounding the Quarry will experience the most impact from the Quarry during different phases. Therefore, the modelled scenarios are selected based on the worst-case extraction location for the different receptors.

The modelled phases for the Proposed Extraction Scenario are:

- Phase 1A Sinking Cut (P1A_Sinkcut*):
 - o Sinking cut in Mid Extraction Area
- Phase 1A South Sinking Cut (P1AS_Sinkcut*):
 - o Sinking cut in South Extraction Area
- Phase 2A Sinking Cut (P2A_Sinkcut*):
 - Sinking cut in North Extraction Area
- Phase 3A (P3A*):
 - Extraction in northern portion of Phase 3A, with AP operational
- Phase 3B Northeast (P3B_NE*):
 - Extraction in the northeastern corner of North Extraction Area, with AP operational
- Phase 4 Southeast (P4_SE*):
 - o Extraction in southeastern corner of Mid Extraction Area, with AP operational
- Phase 5 East (P5_E*):
 - Extraction in eastern corner of South Extraction Area, with AP operational

Sinking cut in Phase 3A was also assessed but was deemed to be less impactful than Phase 2A sinking cut. Phase 3B sinking cut is expected to have similar impacts. Therefore sinking cuts in Phases 3A/3B were not evaluated further. The operation overviews of the modelled scenarios are shown in **Figures 2a** through **2g**.

3 NOISE SOURCE SUMMARY

A summary of significant sound sources is provided in **Table 1**, including sound power levels, location, sound characteristics, operating duration, and vehicle route assumptions. Sound power levels for the proposed sources are based on historical measurement data on file at RWDI. The overview of the locations of the modelled sources are shown in **Figures 2a** through **2g**. Detailed examples of the significant source locations are shown in **Figures 2h** and **2i**.

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3.1 Continuous Sources

The continuous sources modelled are:

- Working Face (WF) and Primary Crusher (PC) sources (daytime only, 0700 to 1900h):
 - One (1) silenced drill working on the 1st bench;
 - One (1) loader working on the 2nd bench;
 - Dumping of rocks into primary crusher;
 - One (1) primary crusher; and
 - One (1) primary screen.
- Conveyor from Working Face Primary Crusher to Processing Plant (daytime only, 0700 to 1900h).
- Processing Plant (PP) sources:
 - Two (2) secondary crushers (daytime only, 0700 to 1900h);
 - Two (2) secondary & tertiary screens (daytime only, 0700 to 1900h);
 - Two (2) tertiary crushers (daytime only, 0700 to 1900h);
 - One (1) loader working at piles (24h/day); and
 - Two (2) idling shipping trucks (24h/day).
- Asphalt Plant (AP) sources (operating continuously, 24 hours per day):
 - Two (2) loaders working;
 - Two (2) idling trucks;
 - One (1) compressor vent;
 - One (1) dust collector blower motor;
 - One (1) dust collector blower stack;
 - One (1) elevator motor;
 - One (1) conveyor motor;
 - One (1) oven motor;
 - One (1) pug mill door (pressure relief noise through the door); and
 - One (1) pug mill motor.
- Internal Haul Truck Routes:
 - Haul roads between PP and AP for aggregates (24h/day).
- Shipping Truck Routes (24h/day):
 - Shipping of aggregate from PP stockpiles to offsite;
 - Shipping of HMA from AP to offsite; and
 - Receiving of AC and RAP at AP.

Trucks with water spray system have an insignificant acoustical effect when compared to all other sources on site and thus were not included in the final list of notable sources of noise.

All continuous sources are assumed to be operating constantly in their respective operating periods. During the sinking cut, only one (1) secondary and one (1) tertiary crusher will be deployed. As the Quarry progresses to later phases, two (2) sets of secondary and tertiary crushers will be deployed at the processing plant. Asphalt plant noise sources were based on the existing asphalt plant at Walker Brothers Quarry and Asphalt Plant in Niagara Falls.

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Shipping truck traffic modelled using moving point source calculation method. Shipping trucks on site are expected to travel at a mean speed of approximately 20 km/h. The number of vehicle trips per hour are calculated based on peak daily production rate and typical vehicle payload and are shown in **Table 1**.

3.2 Impulsive Sources

The only impulsive source considered in this study is the impulses associated with the asphalt plant silos (ASPH_imp_silo), which could operate up to 24 hours a day. As per NPC-300, the sound limits are based on the number of impulses per hour. Nine (9) or more impulses are anticipated to occur at a worst-case hour during daytime, evening, and nighttime.

3.3 Construction Sources

Temporary construction noise from the Quarry is anticipated for short periods throughout its lifespan. Activities considered to be construction noise include overburden removal and berm creation. Details on construction noise assessment are provided in **Section 5**.

3.4 Identifiable Source Characteristics

Continuous sources that warrant adjustment due to tonal, cyclically varying, quasi-steady impulsive or beating sound characteristics receive additional consideration in accordance with MOECC NPC-104 guidelines (MOECC, 1978). These guidelines specify that a penalty is applicable for tonal, cyclically varying, or quasi-steady impulsive sound characteristics. No sources were identified to exhibit tonal, cyclically varying, quasi-steady impulsive or beating sound characteristics per NPC-103.

4 POINTS OF RECEPTION

Sound levels from sources at the Quarry were determined at points of reception (PORs) located on noise sensitive land uses. Noise sensitive land uses are defined in the MOECC's environmental guideline, Publication NPC-300 (MOECC, 2013), as the property of a person that accommodates a dwelling, a noise sensitive commercial building or a noise sensitive institutional building. In some cases, a vacant lot may be considered noise sensitive provided it is zoned to allow a sensitive use.

A noise sensitive land use may have one or more POR. PORs for an acoustic assessment are those locations where sound from the facility is received and assessed against the applicable limits. Sound levels may be assessed at the façade of the building and/or outdoor areas, depending on the type of sensitive land use assessed. Outdoor PORs are only assessed for dwellings and are not assessed for commercial and institutional noise sensitive land uses.

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4.1 Surrounding Noise Sensitive Land Uses

Representative receptors with noise-sensitive land uses were identified from zoning maps and aerial photography of the area surrounding the facility. Zoning information for the area surrounding the Quarry is provided in **Appendix A**. These receptors are:

- **R1**, Residence at 10148 Beaverdams Rd;
- **R2**, Residence at 9722 Beaverdams Rd;
- **R3**, Residence at 9602 Beaverdams Rd;
- **R4**, Residence at 5584 Beechwood Rd;
- **R5**, Residence at 5769 Beechwood Rd; and
- **R6**, Residence at 9944 Lundy's Ln.

Receptors R1 and R4 are owned by WAI. As a conservative measure, these receptors have been included in the assessment. There is a neighboring church on the southwest corner of the intersection of Upper's Lane and Beechwood Rd, approximately 60 m from the Quarry boundary. WAI has a special agreement in place with the Church to avoid noise disturbance. Therefore, the Church was not assessed as a noise sensitive receptor.

Zoning maps are included in **Appendix B**. Lands surrounding the subject lands and west of Thorold Townline Road are within the City of Thorold and are subject to Zoning By-law 60-2019. Lands surrounding the subject lands and east of Thorold Townline Road are within the City of Niagara Falls and are subject to Zoning By-law 79-200.

It is noted that the lands west of Thorold Townline Road and 500 m of the bedrock resource area (including the subject lands) are identified as "Aggregate Resource Buffer Lands" by the City of Thorold's Rolling Meadows Secondary Plan and any future development of those lands are subject to policy B.8.12.3 of the Rolling Meadows Secondary Plan. The policy is included in **Appendix B**. Furthermore, these lands are currently vacant of any sensitive land use and are currently zoned:

- Future Development (FD); or
- Environmental Protection Two (EP2).

A noise sensitive land use is not permitted to be developed as-of-right in these zones and any development of sensitive land uses within these zones would need to be rezoned to a Residential zone (or similar) to permit the development of a sensitive land use and subject to policy B.8.12.2 of the Secondary Plan. Given this, the vacant properties west of Thorold Townline Road would not be considered a noise sensitive zoned lot according to NPC-300.

4.2 Modelled Points of Reception

Two PORs were used to assess the sound level at residential receptors (**R1** through **R6**): the façade POR and the outdoor POR. The façade PORs are placed at the closest window facing the Quarry. For two-storey residences, the façade POR is modelled 4.5 m above ground. For one-storey residence, the POR is modelled 1.5 m above ground. All outdoor PORs are modelled at a height of 1.5 m.

The locations of the modelled PORs are shown in **Figure 1**. The location of the PORs are also shown on the zoning map **Figure A.1** in **Appendix A**.

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5 ASSESSMENT CRITERIA

The assessment criteria for sound levels at the receptors is the higher of either the exclusion limit per NPC-300 or the minimum background sound level that occurs or is likely to occur. The exclusion limit is the highest sound level limit that may be used for a receptor when the background sound level is lower than the exclusion limit.

The sound from the facility was assessed during a given worst-case hour occurring in three time periods in NPC 300:

- Daytime, 0700 1900h;
- **Evening**, 1900 2300h; and
- Nighttime, 2300 0700h.

The outdoor location is only assessed during daytime and evening periods and may have a different evening sound level limit than the corresponding façade depending on the Class. The type of acoustic environment, or "Class", defines the set of sound level limits based on the level of urbanization.

- **Class 1**, an acoustical environment which is typical of a major population centre that is dominated by sounds of human activity and traffic.
- **Class 2**, an acoustical environment which is dominated by sounds of human activity and traffic during the daytime (07:00 19:00) and defined by the environmental and infrequent human activity at night (19:00 07:00).
- **Class 3**, an acoustical environment defined by the environmental and infrequent human activity.

Different types of sources are also assessed separately. There are separate assessment criteria for continuous sources vs. impulsive sources.

5.1 Exclusion Limits for Continuous Sources

The exclusion limits are determined from the level of urbanization, or 'Class', at the noise-sensitive land use. The acoustic environment surround the Quarry is characterized primarily by CN rail to the south and road traffic surrounding the site. Noise sensitive land uses for the receptors are therefore in a Class 2 acoustical environment, which is typical of a suburban area that is dominated by sounds of human activity and road traffic. As such, the MOECC Publication NPC-300 Class 2 exclusion limits apply to PORs in this study. The exclusion limits for each POR are shown in **Tables 3a** through **3g**.

5.2 Exclusion Limits for Impulsive Sources

The effect of impulsive sources of sound is evaluated separately from that of continuous sources. The sound level limits for impulsive sources are determined by the number of impulses expected to occur during a worst-case hour.

Since there is only one impulsive source on site (ASPH_imp_silo), it is evaluated against the limit associated with the number of impulses per hour for this individual source. There is expected to be nine or more impulses per hour. Therefore, the strictest Class 2 impulsive limits apply. The worst-case impulsive sound level impacts and associated limits for each POR are summarized in **Tables 3h**.

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5.3 Construction Limits

Overburden-clearing and berm construction are considered short-term construction activities and are not examined explicitly in this assessment. Construction activities are generally temporary in nature and is not part of the day-to-day operation of the site. The sound level due to temporary construction events are not generally assessed at the surrounding receptors.

The following best practice recommendations have been provided in order to minimize the potential for construction noise impacts:

- Construction should be limited to the time periods allowed by the locally applicable bylaws. If construction activities are required outside of these hours, WAI must seek permits / exemptions directly from the municipalities in advance.
- Ensure that all internal combustion engines are fitted with appropriate muffler systems.
- WAI operating procedures should contain a provision that any initial noise complaint will trigger verification that the general noise control measures agreed to are in effect.
- In the event of verified noise complaints, all construction equipment should be verified to comply with MOECC NPC-115 guidelines, as outlined below.
- In the event of verified noise complaints, alternative noise control measured may be required, where reasonably available. In selecting appropriate noise control and mitigation measures, consideration should be given to the technical, administrative, and economic feasibility of the various alternatives.

All construction equipment must meet the sound emission standards defined in MOECC publication NPC-115 (MOECC, 1977). The applicable guidelines for sound emissions from construction equipment are:

- For equipment manufactured after January 1, 1981:
 - o 83 dBA at 15 m for equipment under 75 kW; and
 - \circ 85 dBA at 15 m for equipment 75 kW or larger.
- For equipment manufactured January 1, 1979 to December 31, 1980:
 - \circ ~~ 85 dBA at 15 m for equipment under 75 kW; and
 - o 88 dBA at 15 m for equipment 75 kW or larger.



6 NOISE CONTROL RECOMMENDATIONS

The following recommendations are provided in order to meet the applicable compliance criteria:

- 1. Minimum 3 m tall perimeter berms shall be constructed around the Quarry as shown in **Figure 1**. The perimeter berms shall be constructed as soon as possible during site preparation prior to extraction to provide additional noise attenuation, particularly around the north and south perimeters of the site during work near R1 and R6, while also serving to provide for visual screening.
- 2. The primary crusher shall stay within 30 m of the working face to maximize shielding effect of the Quarry terrain.
- 3. Material extracted from the South Extraction Area shall be processed in the Mid Extraction Area.
- 4. While processing in Phase 4, the licensee shall maintain an 8 m tall barrier at a radius of 40 m to the southeast of the processing plant secondary crushers as shown in **Figures 2f** and **2g**. The barrier can be material stockpiles, noise walls, or a combination of both. The barrier shall extend long enough to shield R4 and R5 from the secondary crushers. If crushers need to be moved for operational reasons, the barrier must be extended to block the additional line-of-sight to both R4 and R5. The 40m radius from the barrier to the processing plant secondary crushers must also be maintained.

Although construction noise is not part of the assessment, RWDI recommends the following best practices to minimize potential for construction noise impacts and complaints:

- 5. All construction equipment shall meet the sound emission standards defined in MECP Publication NPC-115.
- 6. Construction will be limited to time periods allowed by the City's applicable by-laws. If construction activities are required outside of these hours, the licensee will seek permits / exemptions directly from the City in advance.
- 7. All internal combustion engines will be fitted with appropriate muffler systems.
- 8. The licensee's operating procedures will contain a provision that any initial complaint will trigger verification that the general noise control measures agreed to on this Plan are in effect.
- 9. In the presences of persistent noise complaints, all construction equipment will be verified to comply with MECP's NPC-115 guidelines.
- 10. In the presence of persistent noise complaints and subject to the results of a field investigation, alternative noise control measures may be required, where reasonably available. In selecting appropriate noise control and mitigation measures, consideration will be given to the technical, administrative, and economic feasibility of the various alternatives.

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7 IMPACT ASSESSMENT

The Quarry sound emissions were modelled based on the operating scenarios as described in **Section 2**. The sound levels at surrounding PORs are calculated by modelling the sound propagation from the significant sources at the Quarry. The modelled sound levels at the PORs were assessed against the applicable limits.

Modelling of sound level propagation to the PORs was completed using Cadna/A, a commercially available implementation of the ISO 9613 (ISO, 1994b and ISO, 1996) algorithms. Cadna/A is produced by Datakustik GmbH. The modelling took into account the following factors:

- Source sound power level;
- Distance attenuation;
- Source-receptor geometry including heights, elevations, and topography;
- Barrier effects of terrains, berms, and surrounding buildings;
- Duration of events;
- Ground and air (atmospheric) attenuation; and
- Meteorological effects on sound propagation.

Sample calculations showing step-by-step calculation parameters is included in **Appendix C**. Key modelling parameters are also summarized in **Appendix C**.

Ground absorption surrounding the Quarry is modelled as 0.8, to account for the predominantly soft ground. Ground absorption within the Quarry boundary is modelled as 0.2 to account for the hard rock surfaces.

Existing terrain surrounding the quarry was extracted from the Southwestern Ontario Orthophotography Project (SWOOP) 2015 Digital Elevation Model (MNRF, 2015).

The individual contribution of each source at the modelled PORs are presented for Proposed Phase 1A Sinking Cut and Proposed Phase 4 Southeast in **Tables 2a** and **2b**, respectively, as representative sample results.

The predicted sound levels at PORs were assessed using applicable sound level limits, as shown in **Tables 3a** to **3g** for continuous sources, and **Table 3h** for impulsive source. The predicted sound levels at each POR complies with the applicable NPC-300 exclusion limits for all scenarios.

Predicted sound level contours (isopleths of equal sound level) for continuous sources were generated for the worst-case operating scenario for the modelled phases described in **Section 2**. The sound level contours are shown in **Figures 3a** through **3n**.

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8 ALTERNATE EXTRACTION SCENARIO

In the event that Walker obtains permission from the City of Niagara Falls, extraction will include the two road allowances bisecting the proposed quarry site:

- i. Upper's Lane, between the North Extraction Area and the Mid Extraction Area; and
- ii. the unopened road allowance between Lots 120 and 136, between the Mid Extraction Area and the South Extraction Area.

The assessment results and recommendations for the alternate extraction scenario are included in **Appendix D**.

9 CONCLUSIONS

An assessment of the sound levels from the Upper's Quarry operation was completed by modelling the contribution of the significant sources at the representative receptors. The sound levels due the Quarry are predicted to comply with MOECC NPC-300 Class 2 exclusion limits at the representative receptors with the implementation of the mitigation measures described in **Section 6**.

10 STATEMENT OF LIMITATIONS

This report entitled Walker Aggregates Inc. – Upper's Quarry: Acoustic Assessment Report was prepared by RWDI AIR Inc. ("RWDI") for Walker Aggregates Inc. ("Client"). The findings and conclusions presented in this report have been prepared for the Client and are specific to the project described herein ("Project"). The conclusions and recommendations contained in this report are based on the information available to RWDI when this report was prepared. Because the contents of this report may not reflect the final design of the Project or subsequent changes made after the date of this report, RWDI recommendations provided in this report have been correctly interpreted in the final design of the Project.

The conclusions and recommendations contained in this report have also been made for the specific purpose(s) set out herein. Should the Client or any other third party utilize the report and/or implement the conclusions and recommendations contained therein for any other purpose or project without the involvement of RWDI, the Client or such third party assumes any and all risk of any and all consequences arising from such use and RWDI accepts no responsibility for any liability, loss, or damage of any kind suffered by Client or any other third party arising therefrom.

Finally, it is imperative that the Client and/or any party relying on the conclusions and recommendations in this report carefully review the stated assumptions contained herein and to understand the different factors which may impact the conclusions and recommendations provided.

UPPER'S QUARRY: ACOUSTIC ASSESSMENT REPORT WALKER AGGREGATES INC.

RWDI#1603157 January 11, 2024



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TABLES



Table 1: Noise Source Summary - Proposed Extraction Scenario Upper's Quarry, 1603157

| Upper's Quarry, 1603157 | | | | | | Upper's Quarry | , 1603157 | | | | | | | | | | | | | |
|-------------------------------------|--|---|-----------------------------------|-----------------------------------|--|----------------|----------------------|------------------------------------|---|---|--------------------------------------|-----------------|---------------|-------|----------|-------------|-------|---------------|------------------|------------------|
| | | | | | | | | | | | | | | | | | | | | |
| Notes to Table: | | | | | | | | | | | | | | | | | | | | |
| 1. | Wherever possible, the Source ID matches the identifiers used in the I | ESDM repor | t. | | | | 6. Source | ype indicates (| Cadna/A modellin | ng methodology. For | Point, Line, and Area source | ces, PWLs rep | resent | | | | | | | |
| 2. | Sound Power Level of Source, in dBA, not including sound characteri NPC-104. | istic adjustm | ents per | | | | the over point sc | all level for the arce, and PWL | e entire source. V is calculated fro | Where source type is m a single-vehicle pa | Mobile Equipment, the sour assby. | ce is modelled | 1 as a moving | | | | | | | |
| 3. | Source Location: O = Outside of building, including the roof, I = Insic | le of buildin | g. | | | | 7. Sound I - Man | ower Level Da Manufacturer | ita Source: 's Data | | - EC = Engineering Calc | based on spec | ifications | | | | | | | |
| 4. | Sound Characteristic, per NPC-104: | | | | | | - Mea = - Hist = | Measured Dir Historical Dat | ectly a on File at RWI | DI | - Same ### = same type a | is source no. # | <i>\##</i> | | | | | | | |
| | - S = Steady - Q = Quasi-Steady Impulsive | - I = Impu - B = Buzz | lsive | -T = Tonal - C = Cyclic | | | 8 For load | er dumping int | o primary crushe | er, it is assumed each | dump takes approximately | 10s | | | | | | | | |
| 5. | Noise control measures currently in place or specified in construction - S = Silencer/Muffler - A = Acoustic lining, plenum - B = Barrier/Berm | drawings: - L = Lagg - E = Acou | ing Istic enclosure | - O = Other - U = Uncontrolled | | | | | | | | | | | | | | | | |
| | Where noise control measures are specified in construction drawings octave band sound power levels include the effects of the noise contro recommended in the mitigation section of this report are not included | or were four ol measures. in this table | nd on existing o Noise control | equipment, measures | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | 6 | с r | | Operating Tir | e during Wors | st-case hour for |
| Source ID ^[1] | Source Description | Power | Source Location ³ | Sound Characteristics [4] | Noise Control Measures ^[5] | | if availab (dB) | e | ata | Source Type ^[6] | PWL Data Source ^[7] | Above | Height Ab. | Above | for p | point sourc | es | Vahiala Passi | OINT Sources, OR | Speed for Line |
| | | Level | | (0.0.1.D.T.O) | | | | 1000 0000 | | | | | Graue | Graue | | (, | 7 | Deutime | Sources | Ninhttime |
| | | (dBA) | (1 or O) | (8,Q,I,B,T,C) | (S,A,B,L,E,O,U) | 31.5 63 | 125 250 500 | 1000 2000 | 4000 8000 | | | (m) | (m) | (m) | X | Ŷ | Z | Daytime | Evening | Nighttime |
| | | | | | | | Point Sourc | es | | | | | | | | | | | | |
| P1A_Sinkcut_PC_CrusherDump | P1A_Sinkcut, PC loader dumping into crusher | 123 | 0 | S | U | 115.4 120.3 | 122.2 120.0 118.3 | 118.5 116.6 | 5 111.1 102.3 | Point | Hist | - | - | 3.0 | 648673 4 | 772848 | 180.0 | 30 dumps/hr | - | - |
| P1A_Sinkcut_PC_Ldr | P1A_Sinkcut, PC Loader | 106 | 0 | S | U | 102.4 111.2 | 104.7 101.4 99.9 | 99.2 97.5 | 97.7 98.5 | Point | Hist | - | - | 2.5 | 648672 4 | 772850 | 179.5 | 60 min | - | - |
| P1A_Sinkcut_PC_PrimaryCrush | P1A_Sinkcut, PC Primary Crusher | 118 | 0 | S | U | 108.9 119.8 | 115.0 118.7 114.6 | 112.2 109.6 | 5 104.4 99.6 | Point | Hist | | - | 3.0 | 648675 4 | 772847 | 180.0 | 60 min | - | - |
| P1A_Sinkcut_PC_PrimaryScreen | P1A_Sinkcut, PC Primary Screen | 114 | 0 | S | U | 111.4 113.6 | 111.5 111.1 110.9 | 106.9 106.5 | 5 105.2 101.7 | Point | Hist | | - | 3.0 | 648676 4 | 772845 | 180.0 | 60 min | - | - |
| PIA_Sinkcut_PP_Ldr | PIA_Sinkcut, PP Loader | 106 | 0 | S | U | 102.4 111.2 | 104.7 101.4 99.9 | 99.2 97.5 | 97.7 98.5 | Point | Hist | - | - | 2.5 | 648802 4 | 772799 | 179.5 | 60 min | 60 min | 60 min |
| PIA_Sinkcut_PP_SecondaryCrush | PIA_Sinkcut, PP Secondary Crusher | 115 | 0 | S | U | 102.3 108.9 | 111.7 110.8 109.6 | 100.0 107.4 | 104.6 99.0 | Point | Hist | | - | 3.0 | 648791 4 | 772793 | 180.0 | 60 min | - | - |
| PIA_Sinkcut_PP_SecondaryTeruaryScr | PIA_Sinkcut, PP Secondary & Tertiary Screen | 00 | 0 | 5 | U | 102.4 106.5 | 07.1 00.0 06.0 | 02.8 01.2 | 886 820 | Point | Hist | | - | 3.0 | 648793 4 | 772700 | 180.0 | 60 min | - | - |
| P1A_Sinkcut_PP_TertiaryCrush | PIA_Sinkcut, PP Ternary Crusher | 99 | | s | U | 103.4 106.7 | 97.1 99.9 96.0 | 92.8 91.3 | 81.6 73.8 | Point | Hist | | - | 3.0 | 648794 4 | 772810 | 180.0 | 60 min | - 60 min | |
| PIA Sinkeut PP Trk2 | P1A Sinkeut PP Idling Truck | 96 | 0 | 5 | U | 101.7 98.9 | 94.6 90.2 90.5 | 92.8 90.1 | 81.6 73.8 | Point | Hist | | | 3.0 | 648807 4 | 772811 | 180.0 | 60 min | 60 min | 60 min |
| PIA Sinkeut WF Drill | P1A Sinkeut WF Drill | 110 | 0 | s | U | 96.8 101.2 | 99.3 96.9 102.5 | 104.3 104.4 | 102.0 99.5 | Point | Hist | | - | 2.5 | 648631 4 | 772870 | 179.5 | 60 min | - | - |
| PIAS Sinkcut PC CrusherDump | PIAS Sinkcut, PC loader dumping into crusher | 123 | 0 | S | U | 115.4 120.3 | 122.2 120.0 118.3 | 118.5 116.6 | 5 111.1 102.3 | Point | Hist | - 1 | - | 3.0 | 648618 4 | 772517 | 180.0 | 30 dumps/hr | | - |
| P1AS Sinkcut PC Ldr | PIAS Sinkcut, PC Loader | 106 | 0 | S | U | 102.4 111.2 | 104.7 101.4 99.9 | 99.2 97.5 | 97.7 98.5 | Point | Hist | 1 - | - | 2.5 | 648618 4 | 772516 | 179.5 | 60 min | | - |
| P1AS_Sinkcut_PC_PrimaryCrush | P1AS_Sinkcut, PC Primary Crusher | 118 | 0 | S | U | 108.9 119.8 | 115.0 118.7 114.6 | 112.2 109.6 | 5 104.4 99.6 | Point | Hist | - 1 | - | 3.0 | 648619 4 | 772520 | 180.0 | 60 min | - | - |
| P1AS_Sinkcut_PC_PrimaryScreen | P1AS_Sinkcut, PC Primary Screen | 114 | 0 | S | U | 111.4 113.6 | 111.5 111.1 110.9 | 106.9 106.5 | 5 105.2 101.7 | Point | Hist | - 1 | - | 3.0 | 648619 4 | 772523 | 180.0 | 60 min | - | - |
| P1AS_Sinkcut_PP_Ldr | P1AS_Sinkcut, PP Loader | 106 | 0 | S | U | 102.4 111.2 | 104.7 101.4 99.9 | 99.2 97.5 | 97.7 98.5 | Point | Hist | - | - | 2.5 | 648705 4 | 772726 | 179.5 | 60 min | 60 min | 60 min |
| P1AS_Sinkcut_PP_SecondaryCrush | P1AS_Sinkcut, PP Secondary Crusher | 115 | 0 | S | U | 102.3 108.9 | 111.7 110.8 109.6 | 110.5 107.4 | 104.6 99.0 | Point | Hist | - | - | 3.0 | 648705 4 | 772706 | 180.0 | 60 min | - | - |
| P1AS_Sinkcut_PP_SecondaryTertiarySc | PIAS_Sinkcut, PP Secondary & Tertiary Screen | 114 | 0 | S | U | 111.4 113.6 | 111.5 111.1 110.9 | 106.9 106.5 | 5 105.2 101.7 | Point | Hist | - | - | 3.0 | 648705 4 | 772708 | 180.0 | 60 min | - | - |
| P1AS_Sinkcut_PP_TertiaryCrush | P1AS_Sinkcut, PP Tertiary Crusher | 99 | 0 | S | U | 103.4 106.7 | 97.1 99.9 96.0 | 92.8 91.3 | 88.6 83.9 | Point | Hist | - | - | 3.0 | 648706 4 | 772710 | 180.0 | 60 min | - | - |
| P1AS_Sinkcut_PP_Trk1 | P1AS_Sinkcut, PP Idling Truck | 96 | 0 | S | U | 101.7 98.9 | 94.6 90.2 90.5 | 92.8 90.1 | 81.6 73.8 | Point | Hist | - | - | 3.0 | 648703 4 | 772742 | 180.0 | 60 min | 60 min | 60 min |
| P1AS_Sinkcut_PP_Trk2 | P1AS_Sinkcut, PP Idling Truck | 96 | 0 | S | U | 101.7 98.9 | 94.6 90.2 90.5 | 92.8 90.1 | 81.6 73.8 | Point | Hist | | - | 3.0 | 648707 4 | 772743 | 180.0 | 60 min | 60 min | 60 min |
| P1AS_Sinkcut_WF_Drill | PIAS_Sinkcut, WF Drill | 110 | 0 | S | U | 96.8 101.2 | 99.3 96.9 102.5 | 104.3 104.4 | 102.0 99.5 | Point | Hist | | - | 2.5 | 648633 4 | 772485 | 179.5 | 60 min | - | |
| P2A_Sinkcut_PC_CrusherDump | P2A_Sinkcut, PC loader dumping into crusher | 123 | 0 | S | U | 115.4 120.3 | 122.2 120.0 118.3 | 118.5 116.6 | 07.7 | Point | Hist | - | - | 3.0 | 648657 4 | 7/3006 | 180.0 | 30 dumps/hr | - | |
| P2A_Sinkout_PC_Ldr | P2A Sinkout, PC Loader | 106 | 0 | S | | 102.4 111.2 | 104.7 101.4 99.9 | 99.2 97.5 | 97.7 98.5 | Point | Hist | | - | 2.5 | 648657 4 | 772007 | 179.5 | 60 min | - | |
| P2A_Sinkout_PC_PrimaryCrush | P2A Sinkout, PC Primary Crusher | 118 | | <u>s</u> | U | 108.9 119.8 | 115.0 118.7 114.6 | 106.0 106.6 | 104.4 99.6 | Point | Hist | ┨┝─── | | 3.0 | 648657 4 | 772009 | 180.0 | 60 min | - | |
| P2A_Sinkcut_FC_FrinaryScreen | P2A_Sinkeut, PC Filinary Screen | 104 | 0 | 5 | U | 102.4 111.2 | 104.7 101.4 00.0 | 00.2 07.5 | 07.7 08.5 | Point | Hist | | - | 2.5 | 648602 4 | 772005 | 170.5 | 60 min | | |
| P2A Sinkeut PP SecondaryCrush | P2A_Sinkcut_PP_Secondary_Crusher | 115 | 0 | 5 | U | 102.4 111.2 | 111.7 110.8 109.6 | 110.5 107.4 | 97.7 98.3 | Point | Hist | | | 3.0 | 648685 4 | 773094 | 180.0 | 60 min | - | |
| P2A Sinkeut PP SecondaryTertiaryScr | eer P2A_Sinkcut_PP Secondary & Tertiary Screen | 113 | 0 | S | U | 111.4 113.6 | 111.7 110.8 109.0 | 106.9 106.5 | 104.0 99.0 | Point | Hist | | | 3.0 | 648685 4 | 773095 | 180.0 | 60 min | | - |
| P2A Sinkeut PP TertiaryCrush | P2A Sinkcut PP Tertiary Crusher | 99 | 0 | S | U | 103.4 106.7 | 97.1 99.9 96.0 | 92.8 91.3 | 88.6 83.9 | Point | Hist | | - | 3.0 | 648686 4 | 773095 | 180.0 | 60 min | | - |
| P2A Sinkeut PP Trk1 | P2A Sinkcut, PP Idling Truck | 96 | 0 | s | U | 101.7 98.9 | 94.6 90.2 90.5 | 92.8 90.1 | 81.6 73.8 | Point | Hist | - | - | 3.0 | 648698 4 | 773094 | 180.0 | 60 min | 60 min | 60 min |
| P2A Sinkcut PP Trk2 | P2A Sinkcut, PP Idling Truck | 96 | 0 | S | U | 101.7 98.9 | 94.6 90.2 90.5 | 92.8 90.1 | 81.6 73.8 | Point | Hist | 1 - | - | 3.0 | 648696 4 | 773094 | 180.0 | 60 min | 60 min | 60 min |
| P2A_Sinkcut_WF_Drill | P2A_Sinkcut, WF Drill | 110 | 0 | S | U | 96.8 101.2 | 99.3 96.9 102.5 | 104.3 104.4 | 102.0 99.5 | Point | Hist | 1 - | - | 2.5 | 648630 4 | 773018 | 179.5 | 60 min | - | - |
| P3A_PC_CrusherDump | P3A, PC loader dumping into crusher | 123 | 0 | S | U | 115.4 120.3 | 122.2 120.0 118.3 | 118.5 116.6 | 5 111.1 102.3 | Point | Hist | - | - | 3.0 | 648874 4 | 773392 | 164.0 | 60 dumps/hr | - | - |
| P3A_PC_Ldr | P3A, PC Loader | 106 | 0 | S | U | 102.4 111.2 | 104.7 101.4 99.9 | 99.2 97.5 | 97.7 98.5 | Point | Hist |] | - | 2.5 | 648872 4 | 773395 | 163.5 | 60 min | - | - |
| P3A_PC_PrimaryCrush | P3A, PC Primary Crusher | 118 | 0 | S | U | 108.9 119.8 | 115.0 118.7 114.6 | 112.2 109.6 | 5 104.4 99.6 | Point | Hist | - | - | 3.0 | 648875 4 | 773391 | 164.0 | 60 min | - | - |
| P3A_PC_PrimaryScreen | P3A, PC Primary Screen | 114 | 0 | S | U | 111.4 113.6 | 111.5 111.1 110.9 | 106.9 106.5 | 5 105.2 101.7 | Point | Hist | - | - | 3.0 | 648875 4 | 773391 | 164.0 | 60 min | - | - |
| P3A_PP_Ldr | P3A, PP Loader | 106 | 0 | S | U | 102.4 111.2 | 104.7 101.4 99.9 | 99.2 97.5 | 97.7 98.5 | Point | Hist | - | - | 2.5 | 648708 4 | 773140 | 147.5 | 60 min | 60 min | 60 min |
| P3A_PP_SecondaryCrush1 | P3A, PP Secondary Crusher | 115 | 0 | S | U | 102.3 108.9 | 111.7 110.8 109.6 | 110.5 107.4 | 104.6 99.0 | Point | Hist | | - | 3.0 | 648709 4 | 773151 | 148.0 | 60 min | - | |
| P3A_PP_SecondaryCrush2 | P3A, PP Secondary Crusher | 115 | 0 | S | U | 102.3 108.9 | 111.7 110.8 109.6 | 110.5 107.4 | 104.6 99.0 | Point | Hist | - | - | 3.0 | 648710 4 | 773151 | 148.0 | 60 min | | |
| P3A_PP_SecondaryTertiaryScreen1 | P3A, PP Secondary & Tertiary Screen | 114 | 0 | S | U | 111.4 113.6 | 111.5 111.1 110.9 | 106.9 106.5 | 105.2 101.7 | Point | Hist | | - | 3.0 | 648710 4 | 773149 | 148.0 | 60 min | - | |
| P3A_PP_SecondaryTertiaryScreen2 | P3A, PP Secondary & Tertiary Screen | 114 | 0 | S | U | 111.4 113.6 | 111.5 111.1 110.9 | 106.9 106.5 | 5 105.2 101.7 | Point | Hist | - | - | 3.0 | 648710 4 | 773149 | 148.0 | 60 min | - | |

Table 1: Additional Data

Table 1: Noise Source Summary - Proposed Extraction Scenario Upper's Quarry, 1603157

| Notes to Table: | | | | |
|-----------------|----|---|--|---|
| | 1. | Wherever possible, the Source ID matches the identifiers used in the | ESDM report. | |
| | 2. | Sound Power Level of Source, in dBA, not including sound character NPC-104. | istic adjustments per | |
| | 3. | Source Location: O = Outside of building, including the roof, I = Inside | de of building. | |
| | 4. | Sound Characteristic, per NPC-104: - S = Steady - Q = Quasi-Steady Impulsive | - I = Impulsive - B = Buzzing | - T = Tonal - C = Cyclic |
| | 5. | Noise control measures currently in place or specified in construction - S = Silencer/Muffler - A = Acoustic lining, plenum - B = Barrier/Berm Where noise control measures are specified in construction drawings octave band sound power levels include the effects of the noise contro recommended in the mitigation section of this report are not included | drawings: - L = Lagging - E = Acoustic enclosure or were found on existing e ol measures. Noise control in this table | - O = Other - U = Uncontrolled equipment, measures |

Table 1: Additional Data

7.

8

Upper's Quarry, 1603157

- Source type indicates Cadna/A modelling methodology. For Point, Line, and Area sources, PWLs represent the overall level for the entire source. Where source type is Mobile Equipment, the source is modelled as a moving point source, and PWL is calculated from a single-vehicle passby. 6.
 - Sound Power Level Data Source: Man = Manufacturer's Data Mea = Measured Directly Hist = Historical Data on File at RWDI

EC = Engineering Calc based on specifications
 Same ### = same type as source no. ###

For loader dumping into primary crusher, it is assumed each dump takes approximately 10s

| | | | | | | | | | | | | | | | | Operating Tin | e during Wors | st-case hour for |
|------------------------------------|--|----------------------|--------------|---------------------|-----------------|---|---|----------------------------|--------------------------------|--------|------------|--------|--------|-----------------|-------|---------------|----------------------------|------------------|
| | | Sound | Source | Sound | Noise Control | | 1/1 Octave Band Sound Power Level Data | | | Height | Local Roof | Height | Sou | rce Co-ordina | ites | 1 | oint Sources, [[] | 8] |
| Source ID ^[1] | Source Description | Power | Location [3] | Characteristics [4] | Monsuras [5] | | if available | Source Type ^[6] | PWL Data Source ^[7] | Above | Height Ab. | Above | f | or point source | es | | OR | |
| | | Level ^[2] | Location | Characteristics | wicasures | | (dB) | | | Roof | Grade | Grade | | (m) | | Vehicle Passb | y per Hour & S | Speed for Line |
| | | | | | | | | | | | | | | | | | Sources | |
| | | (dBA) | (I or O) | (S,Q,I,B,T,C) | (S,A,B,L,E,O,U) | Ŀ | <u>31.5 63 125 250 500 1000 2000 4000 8000</u> | | | (m) | (m) | (m) | X | Y | Z | Daytime | Evening | Nighttime |
| P3A_PP_TertiaryCrush1 | P3A, PP Tertiary Crusher | 99 | 0 | S | U | 1 | 103.4 106.7 97.1 99.9 96.0 92.8 91.3 88.6 83.9 | Point | Hist | - | - | 3.0 | 648709 | 4773148 | 148.0 | 60 min | - | - |
| P3A_PP_TertiaryCrush2 | P3A, PP Tertiary Crusher | 99 | 0 | S | U | 1 | 103.4 106.7 97.1 99.9 96.0 92.8 91.3 88.6 83.9 | Point | Hist | - | - | 3.0 | 648710 | 4773148 | 148.0 | 60 min | - | - |
| P3A_PP_Trk1 | P3A, PP Idling Truck | 96 | 0 | S | U | 1 | 101.7 98.9 94.6 90.2 90.5 92.8 90.1 81.6 73.8 | Point | Hist | - | - | 3.0 | 648709 | 4773130 | 148.0 | 60 min | 60 min | 60 min |
| P3A_PP_Trk2 | P3A, PP Idling Truck | 96 | 0 | S | U | 1 | 101.7 98.9 94.6 90.2 90.5 92.8 90.1 81.6 73.8 | Point | Hist | - | - | 3.0 | 648706 | 4773131 | 148.0 | 60 min | 60 min | 60 min |
| P3A_WF_Drill | P3A, WF Drill | 110 | 0 | S | U | | 96.8 101.2 99.3 96.9 102.5 104.3 104.4 102.0 99.5 | Point | Hist | - | - | 2.5 | 648850 | 4773416 | 177.5 | 60 min | - | - |
| P3B_NE_PC_CrusherDump | P3B_NE, PC loader dumping into crusher | 123 | 0 | S | U | 1 | 115.4 120.3 122.2 120.0 118.3 118.5 116.6 111.1 102.3 | Point | Hist | - | - | 3.0 | 649442 | 4773420 | 164.5 | 60 dumps/hr | - | - |
| P3B_NE_PC_Ldr | P3B_NE, PC Loader | 106 | 0 | S | U | 1 | 102.4 111.2 104.7 101.4 99.9 99.2 97.5 97.7 98.5 | Point | Hist | - | - | 2.5 | 649443 | 4773421 | 164.0 | 60 min | - | - |
| P3B_NE_PC_PrimaryCrush | P3B_NE, PC Primary Crusher | 118 | 0 | S | U | 1 | 108.9 119.8 115.0 118.7 114.6 112.2 109.6 104.4 99.6 | Point | Hist | - | - | 3.0 | 649441 | 4773419 | 164.5 | 60 min | - | - |
| P3B_NE_PC_PrimaryScreen | P3B_NE, PC Primary Screen | 114 | 0 | S | U | 1 | 111.4 113.6 111.5 111.1 110.9 106.9 106.5 105.2 101.7 | Point | Hist | - | - | 3.0 | 649440 | 4773419 | 164.5 | 60 min | - | - |
| P3B_NE_PP_Ldr | P3B_NE, PP Loader | 106 | 0 | S | U | 1 | 102.4 111.2 104.7 101.4 99.9 99.2 97.5 97.7 98.5 | Point | Hist | - | - | 2.5 | 648896 | 4773262 | 150.5 | 60 min | 60 min | 60 min |
| P3B_NE_PP_SecondaryCrush1 | P3B_NE, PP Secondary Crusher | 115 | 0 | S | U | 1 | 102.3 108.9 111.7 110.8 109.6 110.5 107.4 104.6 99.0 | Point | Hist | - | - | 3.0 | 648908 | 4773261 | 151.0 | 60 min | - | - |
| P3B_NE_PP_SecondaryCrush2 | P3B_NE, PP Secondary Crusher | 115 | 0 | S | U | 1 | 102.3 108.9 111.7 110.8 109.6 110.5 107.4 104.6 99.0 | Point | Hist | - | - | 3.0 | 648908 | 4773260 | 151.0 | 60 min | - | - |
| P3B_NE_PP_SecondaryTertiaryScreen1 | P3B_NE, PP Secondary & Tertiary Screen | 114 | 0 | S | U | 1 | 111.4 113.6 111.5 111.1 110.9 106.9 106.5 105.2 101.7 | Point | Hist | - | - | 3.0 | 648907 | 4773261 | 151.0 | 60 min | - | - |
| P3B_NE_PP_SecondaryTertiaryScreen2 | P3B_NE, PP Secondary & Tertiary Screen | 114 | 0 | S | U | 1 | 111.4 113.6 111.5 111.1 110.9 106.9 106.5 105.2 101.7 | Point | Hist | - | - | 3.0 | 648907 | 4773260 | 151.0 | 60 min | - | - |
| P3B_NE_PP_TertiaryCrush1 | P3B_NE, PP Tertiary Crusher | 99 | 0 | S | U | 1 | 103.4 106.7 97.1 99.9 96.0 92.8 91.3 88.6 83.9 | Point | Hist | - | - | 3.0 | 648906 | 4773261 | 151.0 | 60 min | - | - |
| P3B_NE_PP_TertiaryCrush2 | P3B_NE, PP Tertiary Crusher | 99 | 0 | S | U | 1 | 103.4 106.7 97.1 99.9 96.0 92.8 91.3 88.6 83.9 | Point | Hist | - | - | 3.0 | 648906 | 4773260 | 151.0 | 60 min | - | - |
| P3B_NE_PP_Trk1 | P3B_NE, PP Idling Truck | 96 | 0 | S | U | 1 | 101.7 98.9 94.6 90.2 90.5 92.8 90.1 81.6 73.8 | Point | Hist | - | - | 3.0 | 648884 | 4773262 | 151.0 | 60 min | 60 min | 60 min |
| P3B_NE_PP_Trk2 | P3B_NE, PP Idling Truck | 96 | 0 | S | U | 1 | 101.7 98.9 94.6 90.2 90.5 92.8 90.1 81.6 73.8 | Point | Hist | - | - | 3.0 | 648884 | 4773264 | 151.0 | 60 min | 60 min | 60 min |
| P3B_NE_WF_Drill | P3B_NE, WF Drill | 110 | 0 | S | U | | 96.8 101.2 99.3 96.9 102.5 104.3 104.4 102.0 99.5 | Point | Hist | - | - | 2.5 | 649462 | 4773462 | 177.5 | 60 min | - | - |
| P4_SE_PC_CrusherDump | P4_SE, PC loader dumping into crusher | 123 | 0 | S | U | 1 | 115.4 120.3 122.2 120.0 118.3 118.5 116.6 111.1 102.3 | Point | Hist | - | - | 3.0 | 649481 | 4772802 | 164.5 | 60 dumps/hr | - | - |
| P4_SE_PC_Ldr | P4_SE, PC Loader | 106 | 0 | S | U | 1 | 102.4 111.2 104.7 101.4 99.9 99.2 97.5 97.7 98.5 | Point | Hist | - | - | 2.5 | 649484 | 4772801 | 164.0 | 60 min | - | - |
| P4_SE_PC_PrimaryCrush | P4_SE, PC Primary Crusher | 118 | 0 | S | U | 1 | 108.9 119.8 115.0 118.7 114.6 112.2 109.6 104.4 99.6 | Point | Hist | - | - | 3.0 | 649480 | 4772803 | 164.5 | 60 min | - | - |
| P4_SE_PC_PrimaryScreen | P4_SE, PC Primary Screen | 114 | 0 | S | U | 1 | 111.4 113.6 111.5 111.1 110.9 106.9 106.5 105.2 101.7 | Point | Hist | - | - | 3.0 | 649479 | 4772804 | 164.5 | 60 min | - | - |
| P4_SE_PP_Ldr | P4_SE, PP Loader | 106 | 0 | S | U | | 102.4 111.2 104.7 101.4 99.9 99.2 97.5 97.7 98.5 | Point | Hist | - | - | 2.5 | 649152 | 4772897 | 148.5 | 60 min | 60 min | 60 min |
| P4_SE_PP_SecondaryCrush1 | P4_SE, PP Secondary Crusher | 115 | 0 | S | U | 1 | 102.3 108.9 111.7 110.8 109.6 110.5 107.4 104.6 99.0 | Point | Hist | - | - | 3.0 | 649166 | 4772899 | 149.0 | 60 min | - | - |
| P4_SE_PP_SecondaryCrush2 | P4_SE, PP Secondary Crusher | 115 | 0 | S | U | 1 | 102.3 108.9 111.7 110.8 109.6 110.5 107.4 104.6 99.0 | Point | Hist | - | - | 3.0 | 649166 | 4772898 | 149.0 | 60 min | - | - |
| P4_SE_PP_SecondaryTertiaryScreen1 | P4_SE, PP Secondary & Tertiary Screen | 114 | 0 | S | U | | 111.4 113.6 111.5 111.1 110.9 106.9 106.5 105.2 101.7 | Point | Hist | - | - | 3.0 | 649165 | 4772899 | 149.0 | 60 min | - | - |
| P4_SE_PP_SecondaryTertiaryScreen2 | P4_SE, PP Secondary & Tertiary Screen | 114 | 0 | S | U | 1 | 111.4 113.6 111.5 111.1 110.9 106.9 106.5 105.2 101.7 | Point | Hist | - | - | 3.0 | 649165 | 4772898 | 149.0 | 60 min | - | - |
| P4_SE_PP_TertiaryCrush1 | P4_SE, PP Tertiary Crusher | 99 | 0 | S | U | 1 | 103.4 106.7 97.1 99.9 96.0 92.8 91.3 88.6 83.9 | Point | Hist | - | - | 3.0 | 649163 | 4772898 | 149.0 | 60 min | - | - |
| P4_SE_PP_TertiaryCrush2 | P4_SE, PP Tertiary Crusher | 99 | 0 | S | U | | 103.4 106.7 97.1 99.9 96.0 92.8 91.3 88.6 83.9 | Point | Hist | - | - | 3.0 | 649164 | 4772897 | 149.0 | 60 min | - | - |
| P4_SE_PP_Trk1 | P4_SE, PP Idling Truck | 96 | 0 | S | U | | 101.7 98.9 94.6 90.2 90.5 92.8 90.1 81.6 73.8 | Point | Hist | - | - | 3.0 | 649143 | 4772895 | 149.0 | 60 min | 60 min | 60 min |
| P4_SE_PP_Trk2 | P4_SE, PP Idling Truck | 96 | 0 | S | U | | 101.7 98.9 94.6 90.2 90.5 92.8 90.1 81.6 73.8 | Point | Hist | - | - | 3.0 | 649142 | 47/2897 | 149.0 | 60 min | 60 min | 60 min |
| P4_SE_WF_Drill | P4_SE, WF Drill | 110 | 0 | S | U | E | 96.8 101.2 99.3 96.9 102.5 104.3 104.4 102.0 99.5 | Point | Hist | - | - | 2.5 | 649523 | 4772782 | 180.5 | 60 min | - | - |
| P5_E_PC_CrusherDump | P5_E, PC loader dumping into crusher | 123 | | S | U | | <u>115.4</u> <u>120.3</u> <u>122.2</u> <u>120.0</u> <u>118.3</u> <u>118.5</u> <u>116.6</u> <u>111.1</u> <u>102.3</u> | Point | Hist | - | - | 3.0 | 649208 | 4//2601 | 163.0 | 60 dumps/hr | - | |
| P5_E_PC_Ldr | P5_E, PC Loader | 106 | 0 | S | U | | 102.4 111.2 104.7 101.4 99.9 99.2 97.5 97.7 98.5 | Point | Hist | - | - | 2.5 | 649211 | 4772602 | 162.5 | 60 min | - | - |
| P5_E_PC_PrimaryCrush | P5_E, PC Primary Crusher | 118 | 0 | s | U | | 108.9 119.8 115.0 118.7 114.6 112.2 109.6 104.4 99.6 | Point | Hist | - | - | 3.0 | 649204 | 4772601 | 163.0 | 60 min | - | - |
| P5_E_PC_PrimaryScreen | P5_E, PC Primary Screen | 114 | 0 | S | U | | 111.4 113.6 111.5 111.1 110.9 106.9 106.5 105.2 101.7 | Point | Hist | - | - | 3.0 | 649200 | 47/2601 | 163.0 | 60 min | - | |
| P5_E_PP_Ldr | P5_E, PP Loader | 106 | 0 | S | U | Ľ | 102.4 111.2 104.7 101.4 99.9 99.2 97.5 97.7 98.5 | Point | Hist | - | - | 2.5 | 649153 | 47/2896 | 148.5 | 60 min | 60 min | 60 min |
| P5_E_PP_SecondaryCrush1 | P5_E, PP Secondary Crusher | 115 | 0 | s | U | | 102.3 108.9 111.7 110.8 109.6 110.5 107.4 104.6 99.0 | Point | Hist | - | - | 3.0 | 649170 | 4772897 | 149.0 | 60 min | - | - |
| P5_E_PP_SecondaryCrush2 | P5_E, PP Secondary Crusher | 115 | | S | U | | 102.3 108.9 111.7 110.8 109.6 110.5 107.4 104.6 99.0 | Point | Hist | - | - | 3.0 | 649170 | 4772896 | 149.0 | 60 min | - | |
| PS_E_PP_SecondaryTertiaryScreen1 | P5_E, PP Secondary & Tertiary Screen | 114 | | S | U | | 111.4 113.6 111.5 111.1 110.9 106.9 106.5 105.2 101.7 | Point | Hist | - | - | 3.0 | 649168 | 4772897 | 149.0 | 60 min | - | |
| PS_E_PP_SecondaryTertiaryScreen2 | P5_E, PP Secondary & Tertiary Screen | 114 | | s | U | | <u>111.4</u> <u>113.6</u> <u>111.5</u> <u>111.1</u> <u>110.9</u> <u>106.9</u> <u>106.5</u> <u>105.2</u> <u>101.7</u> | Point | Hist | - | - | 3.0 | 649168 | 4772896 | 149.0 | 60 min | - | - |
| P5_E_PP_TertiaryCrush1 | P5_E, PP Tertiary Crusher | 99 | 0 | S ~ | U | | 103.4 106.7 97.1 99.9 96.0 92.8 91.3 88.6 83.9 | Point | Hist | - | - | 3.0 | 649166 | 4772897 | 149.0 | 60 min | - | |
| P5_E_PP_TertiaryCrush2 | P5_E, PP Tertiary Crusher | 99 | 0 | S | U | | 103.4 106.7 97.1 99.9 96.0 92.8 91.3 88.6 83.9 101.7 00.0 04.6 00.0 02.8 91.3 88.6 83.9 | Point | Hist | - | - | 3.0 | 649166 | 4772896 | 149.0 | 60 min | - | - |
| PS_E_PP_Trkl | P5_E, PP Idling Truck | 96 | | S | U | | 101.7 98.9 94.6 90.2 90.5 92.8 90.1 81.6 73.8 101.7 00.0 04.6 00.2 00.5 02.0 00.1 81.6 73.8 | Point | Hist | - | - | 3.0 | 649137 | 4772894 | 149.0 | 60 min | 60 min | 60 min |
| PS_E_PP_1rk2 | P5_E, PP Idling Truck | 96 | 0 | S | U | | 101./ 98.9 94.6 90.2 90.5 92.8 90.1 81.6 73.8 | Point | Hist | - | - | 3.0 | 649137 | 4772897 | 149.0 | 60 min | 60 min | 60 min |
| P3_E_wF_Drill | P5_E, WF Drill | 110 | 0 | s | U | | 90.8 101.2 99.3 96.9 102.5 104.3 104.4 102.0 99.5 | Point | Hist | - | - | 2.5 | 649269 | 4/72608 | 177.5 | 60 min | - | - |

| Page 2 of 3 |
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Table 1: Noise Source Summary - Proposed Extraction Scenario Upper's Quarry, 1603157

| Notes to Table: | | | |
|-----------------|--|--|-----------------------|
| 1. | Wherever possible, the Source ID matches the id | entifiers used in the ESDM report. | |
| 2. | Sound Power Level of Source, in dBA, not inclu NPC-104. | ding sound characteristic adjustments per | |
| 3. | Source Location: O = Outside of building, include | ling the roof, I = Inside of building. | |
| 4. | Sound Characteristic, per NPC-104: | | |
| | - S = Steady | - I = Impulsive | - T = Tonal |
| | - Q = Quasi-Steady Impulsive | - B = Buzzing | - C = Cyclic |
| 5. | Noise control measures currently in place or spec | cified in construction drawings: | |
| | - S = Silencer/Muffler | -L = Lagging | - O = Other |
| | A = Acoustic lining, plenum | -E = Acoustic enclosure | - U = Uncontrolled |
| | - B = Barrier/Berm | | |
| | Where noise control measures are specified in co octave band sound power levels include the effec recommended in the mitigation section of this re | onstruction drawings or were found on existing e ets of the noise control measures. Noise control n port are not included in this table. | quipment, neasures |

Table 1: Additional Data Upper's Quarry, 1603157

8

- Source type indicates Cadna/A modelling methodology. For Point, Line, and Area sources, PWLs represent the overall level for the entire source. Where source type is Mobile Equipment, the source is modelled as a moving point source, and PWL is calculated from a single-vehicle passby. 6.
- Sound Power Level Data Source: Man = Manufacturer's Data Mea = Measured Directly Hist = Historical Data on File at RWDI 7.

EC = Engineering Calc based on specifications
 Same ### = same type as source no. ###

For loader dumping into primary crusher, it is assumed each dump takes approximately 10s

| Source ID ^[1] | Source Description | Sound Power Level ^[2] | Source Location ^[3] | Sound Characteristics ^[4] | Noise Control Measures ^[5] | | 1/1 O | Octave B | and Sound Po if available (dB) | ower Lev e | rel Data | | Source Type | ^{6]} PWL Data Source ^[7] | Height Above Roof | Local Roof Height Ab. Grade | Height Above Grade | | Source Co-ord for point sou (m) | inates rces | Operating Ti Vehicle Pass | me during Wor Point Sources, OR by per Hour & Sources | st-case hour for [8] |
|-----------------------------|--|--|-----------------------------------|---|--|------|--------------|----------|--------------------------------------|---------------|----------|-----------|-------------|--|-------------------------|-----------------------------------|--------------------------|--------|---------------------------------------|----------------|------------------------------|---|-------------------------|
| | | (dBA) | (I or O) | (S,Q,I,B,T,C) | (S,A,B,L,E,O,U) | 31.5 | 5 63 12 | 25 2 | 50 500 | 1000 | 2000 40 | 000 800 |) | | (m) | (m) | (m) | X | Y | Z | Daytime | Evening | Nighttime |
| ASPH_comp | Asphalt Plant - Compressor Vent | 96 | 0 | S | U | 91.4 | 4 88.5 99 | 9.4 9 | 6.2 93.0 | 90.2 | 87.4 84 | 4.9 81.3 | Point | Hist | - | - | 0.6 | 648875 | 4772829 | 143.6 | 60 min | 60 min | 60 min |
| ASPH_DC_m | Asphalt Plant - Dust Collector Blower (motor) | 105 | 0 | S | U | 110. | .8 113.6 10 | 05.4 10 | 4.1 102.2 | 99.8 | 94.9 93 | 3.4 91.5 | Point | Hist | - | - | 2.0 | 648856 | 4772826 | 145.0 | 60 min | 60 min | 60 min |
| ASPH_DC_s | Asphalt Plant - Dust Collector Blower (stack) | 110 | 0 | S | U | 125. | .3 126.2 11 | 7.0 11 | 0.0 105.8 | 103.5 | 98.5 93 | 3.6 86.1 | Point | Hist | 0.1 | 20.0 | 20.1 | 648855 | 4772826 | 163.1 | 60 min | 60 min | 60 min |
| ASPH_elev | Asphalt Plant - Elevator Motor | 100 | 0 | S | U | 95.7 | 7 97.7 95 | 5.1 9: | 5.2 97.8 | 95.5 | 91.5 87 | 7.3 77.2 | Point | Hist | - | - | 19.0 | 648861 | 4772835 | 162.0 | 60 min | 60 min | 60 min |
| ASPH_IDLE_TRK1 | Asphalt Plant - Idling Truck | 96 | 0 | S | U | 101. | .7 98.9 94 | 4.6 9 | 0.2 90.5 | 92.8 | 90.1 81 | 1.6 73.8 | Point | Hist | - | - | 3.5 | 648880 | 4772826 | 146.5 | 60 min | 60 min | 60 min |
| ASPH_IDLE_TRK2 | Asphalt Plant - Idling Truck | 96 | 0 | S | U | 101. | .7 98.9 94 | 4.6 9 | 0.2 90.5 | 92.8 | 90.1 81 | 1.6 73.8 | Point | Hist | | - | 3.5 | 648880 | 4772825 | 146.5 | 60 min | 60 min | 60 min |
| ASPH_imp_silo | Asphalt Plant - Silo - Impulsive | 127 | 0 | I | U | 122. | 0 127.9 114 | 4.5 10 | 7.6 106.6 | 108.5 | 117.9 12 | 22.3 123. | 2 Point | Hist | 1.0 | 21.0 | 22.0 | 648888 | 4772842 | 165.0 | 60 min | 60 min | 60 min |
| ASPH_Ldr_Act1 | Asphalt Plant - Loader Activity | 102 | 0 | S | U | 103. | .6 109.2 104 | 04.1 9 | 9.2 97.3 | 95.8 | 94.2 93 | 3.1 88.0 | Point | Hist | | - | 2.5 | 648870 | 4772830 | 145.5 | 60 min | 60 min | 60 min |
| ASPH_Ldr_Act2 | Asphalt Plant - Loader Activity | 102 | 0 | S | U | 103. | .6 109.2 104 | 04.1 9 | 9.2 97.3 | 95.8 | 94.2 93 | 3.1 88.0 | Point | Hist | - | - | 2.5 | 648864 | 4772827 | 145.5 | 60 min | 60 min | 60 min |
| ASPH_motor | Asphalt Plant - Conveyor motor, gravel hitting metal plate | 107 | 0 | S | U | 100. | .5 102.5 94 | 4.2 9: | 5.5 98.9 | 103.0 | 102.0 95 | 5.1 91.4 | Point | Hist | | - | 4.0 | 648854 | 4772834 | 147.0 | 60 min | 60 min | 60 min |
| ASPH_oven | Asphalt Plant - Oven Motor | 102 | 0 | S | U | 111. | 4 110.7 104 | 04.0 10 | 0.1 98.3 | 97.8 | 93.9 91 | 1.9 89.9 | Point | Hist | - | - | 5.8 | 648858 | 4772832 | 148.8 | 60 min | 60 min | 60 min |
| ASPH_pugdoor | Asphalt Plant - Pug Mill door (pressure relief noise) | 107 | 0 | S | U | 114. | .6 112.8 109 | 9.9 10 | 6.3 105.2 | 101.2 | 96.8 94 | 4.9 93.4 | Point | Hist | - | - | 4.0 | 648863 | 4772834 | 147.0 | 60 min | 60 min | 60 min |
| ASPH_pugmill | Asphalt Plant - Pug Mill Motor | 105 | 0 | S | U | 0.0 | 105.0 104 | 04.6 10 | 0.8 94.8 | 94.7 | 96.6 99 | 9.5 99.3 | Point | Hist | - | - | 5.0 | 648870 | 4772837 | 148.0 | 60 min | 60 min | 60 min |
| | | | | | | | | T | ine Source | s | | | | | | | | | | | | | |
| P1A Sinkeyt Conveyor | P1A Sinkeut Conveyor | 83 | 0 | s | II | 74 5 | 5 75 5 79 | 90 7 | 73 788 | 70.2 | 75.6 69 | 01 584 | Line | Hist | | | 3.5 | | | - | 60 min | | <u> </u> |
| P1A Sinkcut RD SHP Aggr Em | P1A Sinkcut Aggregate Shipping from PP Empty | 104 | 0 | s | U | 107 | 7 110 2 10 | 183 9 | 99 994 | 98.6 | 96.7 93 | 3.6 91.6 | Line | Hist | | · · | 3.5 | | - | | 4/hr 20kph | 4/hr 20kph | 4/hr 20kph |
| P1A Sinkcut RD SHP Ager Fu | PIA Sinkeut Aggregate Shipping from PP Full | 104 | 0 | s | U | 107 | 7 110.2 10 | 83 9 | 99 994 | 98.6 | 96.7 93 | 3.6 91.6 | Line | Hist | | - | 3.5 | | - | - | 4/hr 20kph | 4/hr 20kph | 4/hr 20kph |
| PIAS Sinkcut Conveyor | PIAS Sinkeut Conveyor | 83 | 0 | s | U | 74 4 | 5 75 5 79 | 9.0 7 | 73 788 | 79.2 | 75.6 69 | 91 58 4 | Line | Hist | | - | 3.5 | | | - | 60 min | | - |
| PIAS Sinkcut RD SHP Ager Em | PIAS Sinkeut Aggregate Shipping from PP Empty | 104 | 0 | s | U | 107 | 7 110 2 10 | 083 9 | 99 994 | 98.6 | 96.7 93 | 3.6 91.6 | Line | Hist | | - | 3.5 | | - | - | 4/hr 20kph | 4/hr 20kph | 4/hr 20kph |
| PIAS Sinkcut RD SHP Ager Fu | PIAS Sinkcut, Aggregate Shipping from PP, Full | 104 | 0 | s | U | 107. | 7 110.2 10 | 08.3 9 | 9.9 99.4 | 98.6 | 96.7 93 | 3.6 91.6 | Line | Hist | - | - | 3.5 | | - | - | 4/hr. 20kph | 4/hr. 20kph | 4/hr. 20kph |
| P2A Sinkcut Conveyor | P2A Sinkcut Conveyor | 83 | 0 | s | U | 74.5 | 5 75.5 79 | 9.0 7 | 7.3 78.8 | 79.2 | 75.6 69 | 9.1 58.5 | Line | Hist | - | - | 3.5 | | - | - | 60 min | - | - |
| P2A Sinkcut RD SHP Ager Em | P2A Sinkcut, Aggregate Shipping from PP. Empty | 104 | 0 | S | U | 107. | 7 110.2 108 | 8.3 9 | 9.9 99.4 | 98.6 | 96.7 93 | 3.6 91.6 | Line | Hist | 1 _ | - | 3.5 | | _ | - | 4/hr. 20kph | 4/hr. 20kph | 4/hr. 20kph |
| P2A Sinkcut RD SHP Aggr Fu | P2A Sinkcut, Aggregate Shipping from PP, Full | 104 | 0 | S | U | 107. | 7 110.2 108 | 8.3 9 | 9.9 99.4 | 98.6 | 96.7 93 | 3.6 91.6 | Line | Hist | 1 - | - | 3.5 | - | - | - | 4/hr, 20kph | 4/hr, 20kph | 4/hr, 20kph |
| P3A Conveyor | P3A. Conveyor | 83 | 0 | s | U | 74.5 | 5 75.5 79 | 9.0 7 | 7.3 78.8 | 79.2 | 75.6 69 | 9.1 58.5 | Line | Hist | - 1 | - | 3.5 | - | - | - | 60 min | - | - |
| P3A RD Haul PP AP Em | P3A, Aggregate Haul road b/w PP and AP, Empty | 108 | 0 | s | U | 110. | 2 113.9 109 | 9.7 10 | 5.1 104.6 | 102.7 | 101.6 92 | 2.5 89.4 | Line | Hist | 1 - | - | 3.5 | - | - | - | 3/hr, 20kph | 3/hr, 20kph | 3/hr, 20kph |
| P3A RD Haul PP AP Fu | P3A, Aggregate Haul road b/w PP and AP, Full | 112 | 0 | S | U | 108. | .8 108.3 109 | 9.9 10 | 9.0 106.2 | 108.2 | 104.3 98 | 8.4 94.8 | Line | Hist | - 1 | - | 3.5 | - | - | - | 3/hr, 20kph | 3/hr, 20kph | 3/hr, 20kph |
| P3A RD SHP Aggr Em | P3A, Aggregate Shipping from PP, Empty | 104 | 0 | S | U | 107. | 7 110.2 108 | 8.3 9 | 9.9 99.4 | 98.6 | 96.7 93 | 3.6 91.6 | Line | Hist | 1 - | - | 3.5 | - | - | - | 12/hr, 20kph | 12/hr, 20kph | 12/hr, 20kph |
| P3A RD SHP Aggr Fu | P3A, Aggregate Shipping from PP, Full | 104 | 0 | S | U | 107. | 7 110.2 108 | 8.3 9 | 9.9 99.4 | 98.6 | 96.7 93 | 3.6 91.6 | Line | Hist | - 1 | - | 3.5 | - | - | - | 12/hr, 20kph | 12/hr, 20kph | 12/hr, 20kph |
| P3B NE Conveyor | P3B NE, Conveyor | 83 | 0 | S | U | 74.5 | 5 75.5 79 | 9.0 7 | 7.3 78.8 | 79.2 | 75.6 69 | 9.1 58.5 | Line | Hist | - 1 | - | 3.5 | - | - | - | 60 min | - | - |
| P3B NE RD Haul PP AP Em | P3B NE, Aggregate Haul road b/w PP and AP, Empty | 108 | 0 | S | U | 110. | 2 113.9 109 | 9.7 10 | 5.1 104.6 | 102.7 | 101.6 92 | 2.5 89.4 | Line | Hist | - 1 | - | 3.5 | - | - | - | 3/hr, 20kph | 3/hr, 20kph | 3/hr, 20kph |
| P3B NE RD Haul PP AP Fu | P3B NE, Aggregate Haul road b/w PP and AP, Full | 112 | 0 | S | U | 108. | 8 108.3 109 | 9.9 10 | 9.0 106.2 | 108.2 | 104.3 98 | 8.4 94.8 | Line | Hist | - 1 | - | 3.5 | - | - | - | 3/hr, 20kph | 3/hr, 20kph | 3/hr, 20kph |
| P3B_NE_RD_SHP_Aggr_Em | P3B_NE, Aggregate Shipping from PP, Empty | 104 | 0 | S | U | 107. | 7 110.2 108 | 8.3 9 | 9.9 99.4 | 98.6 | 96.7 93 | 3.6 91.6 | Line | Hist | 1 - | - | 3.5 | - | - | - | 12/hr, 20kph | 12/hr, 20kph | 12/hr, 20kph |
| P3B_NE_RD_SHP_Aggr_Fu | P3B_NE, Aggregate Shipping from PP, Full | 104 | 0 | S | U | 107. | .7 110.2 10 | 08.3 9 | 9.9 99.4 | 98.6 | 96.7 93 | 3.6 91.6 | Line | Hist | - | - | 3.5 | - | - | - | 12/hr, 20kph | 12/hr, 20kph | 12/hr, 20kph |
| P4_SE_Conveyor | P4_SE, Conveyor | 83 | 0 | S | U | 74.5 | 5 75.5 79 | 9.0 7 | 7.3 78.8 | 79.2 | 75.6 69 | 9.1 58.5 | Line | Hist | - | - | 3.5 | - | - | - | 60 min | - | - |
| P4_SE_RD_Haul_PP_AP_Em | P4 SE, Aggregate Haul road b/w PP and AP, Empty | 108 | 0 | S | U | 110. | 2 113.9 109 | 9.7 10 | 5.1 104.6 | 102.7 | 101.6 92 | 2.5 89.4 | Line | Hist | - 1 | - | 3.5 | - | - | - | 3/hr, 20kph | 3/hr, 20kph | 3/hr, 20kph |
| P4_SE_RD_Haul_PP_AP_Fu | P4 SE, Aggregate Haul road b/w PP and AP, Full | 112 | 0 | S | U | 108. | .8 108.3 109 | 9.9 10 | 9.0 106.2 | 108.2 | 104.3 98 | 8.4 94.8 | Line | Hist | - | - | 3.5 | - | - | - | 3/hr, 20kph | 3/hr, 20kph | 3/hr, 20kph |
| P4_SE_RD_SHP_Aggr_Em | P4_SE, Aggregate Shipping from PP, Empty | 104 | 0 | S | U | 107. | 7 110.2 108 | 08.3 9 | 9.9 99.4 | 98.6 | 96.7 93 | 3.6 91.6 | Line | Hist | - | - | 3.5 | - | - | - | 12/hr, 20kph | 12/hr, 20kph | 12/hr, 20kph |
| P4_SE_RD_SHP_Aggr_Fu | P4_SE, Aggregate Shipping from PP, Full | 104 | 0 | S | U | 107. | .7 110.2 103 | 08.3 9 | 9.9 99.4 | 98.6 | 96.7 93 | 3.6 91.6 | Line | Hist | - | - | 3.5 | - | - | - | 12/hr, 20kph | 12/hr, 20kph | 12/hr, 20kph |
| P5_E_Conveyor | P5_E, Conveyor | 83 | 0 | S | U | 74.5 | 5 75.5 79 | 9.0 7 | 7.3 78.8 | 79.2 | 75.6 69 | 9.1 58.5 | Line | Hist | - | - | 3.5 | - | - | - | 60 min | - | - |
| P5_E_RD_Haul_PP_AP_Em | P5 E, Aggregate Haul road b/w PP and AP, Empty | 108 | 0 | S | U | 110. | .2 113.9 109 | 9.7 10 | 5.1 104.6 | 102.7 | 101.6 92 | 2.5 89.4 | Line | Hist | - | - | 3.5 | - | - | - | 3/hr, 20kph | 3/hr, 20kph | 3/hr, 20kph |
| P5_E_RD_Haul_PP_AP_Fu | P5 E, Aggregate Haul road b/w PP and AP, Full | 112 | 0 | S | U | 108. | .8 108.3 109 | 9.9 10 | 9.0 106.2 | 108.2 | 104.3 98 | 8.4 94.8 | Line | Hist | | - | 3.5 | - | - | - | 3/hr, 20kph | 3/hr, 20kph | 3/hr, 20kph |
| P5_E_RD_SHP_Aggr_Em | P5_E, Aggregate Shipping from PP, Empty | 104 | 0 | S | U | 107. | 7 110.2 108 | 8.3 9 | 9.9 99.4 | 98.6 | 96.7 93 | 3.6 91.6 | Line | Hist | | - | 3.5 | - | - | - | 12/hr, 20kph | 12/hr, 20kph | 12/hr, 20kph |
| P5_E_RD_SHP_Aggr_Fu | P5_E, Aggregate Shipping from PP, Full | 104 | 0 | S | U | 107. | 7 110.2 108 | 8.3 9 | 9.9 99.4 | 98.6 | 96.7 93 | 3.6 91.6 | Line | Hist | | - | 3.5 | | - | - | 12/hr, 20kph | 12/hr, 20kph | 12/hr, 20kph |
| AP_RD_SHP_AC_RAP_Em | AP, AC and RAP shipped from Offsite, Empty | 104 | 0 | S | U | 107. | 7 110.2 108 | 8.3 9 | 9.9 99.4 | 98.6 | 96.7 93 | 3.6 91.6 | Line | Hist | | - | 3.5 | - | - | - | 6/hr, 20kph | 6/hr, 20kph | 6/hr, 20kph |
| AP_RD_SHP_AC_RAP_Fu | AP, AC and RAP shipped from Offsite, Full | 104 | 0 | S | U | 107. | 7 110.2 108 | 8.3 9 | 9.9 99.4 | 98.6 | 96.7 93 | 3.6 91.6 | Line | Hist | | - | 3.5 | - | - | - | 6/hr, 20kph | 6/hr, 20kph | 6/hr, 20kph |
| AP_RD_SHP_HMA_Em | AP, HMA product shipping, Empty | 104 | 0 | S | U | 107. | 7 110.2 108 | 8.3 9 | 9.9 99.4 | 98.6 | 96.7 93 | 3.6 91.6 | Line | Hist | | - | 3.5 | - | - | - | 6/hr, 20kph | 6/hr, 20kph | 6/hr, 20kph |
| AP_RD_SHP_HMA_Fu | AP, HMA product shipping, Full | 104 | 0 | S | U | 107. | 7 110.2 108 | 8.3 9 | 9.9 99.4 | 98.6 | 96.7 93 | 3.6 91.6 | Line | Hist | | - | 3.5 | - | - | - | 6/hr, 20kph | 6/hr, 20kph | 6/hr, 20kph |

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Table 2a: Point of Reception Noise Impact (Sample Calculation for Proposed Phase 1A Sinking Cut) Upper's Quarry, 16

Notes to Table: "Table A2" in Appendix A of Basic CCofA Guide. 1. "Continuous" noise sources includes operating time corrections and sum of steady, quasi-steady impulsive, tonal, eyelical and buzzing noise sources, with appropriate penalties applied, in accordance with documents NPC-104 and NPC-300. 2. Wherever possible, the Source ID matches the identifiers used in the ESDM report. Sound Level units: - dBA = 1-hour energy equivalent sound level (L_{ud}, (1-hr)), in terms of A-Weighted decibels. - dBA = Logarithmic mean impulsive noise level (L_{tdd}, in terms of A-Weighted decibels incorporating an impulsive time weighting. 3. Noise and vibration receptors representative of worst-case potential impacts have been selected. For the purposes of noise and vibration impact assessment, the following land uses (existing or zoned for future use) have been considered: - portunent, seasonal, or retrait evidences - hostigkin and clinics - naming / retrainment homes - naming / retrainment homes - charches and places of working ---

| Point of Reception ID R1f | Point of Reception ID R10 | Point of Reception ID R2f | Point of Reception ID R20 | Point of Reception ID R3f | Point of Reception ID R30 | Point of Reception ID R4f | Point of Reception ID R40 | Point of Reception ID R5f | Point of Reception ID R50 | Point of Reception ID R6f | Point of Reception ID R60 |
|--|--|---|---|---|---|--|--|--|--|--------------------------------------|--|
| Point of Reception Description | Point of Reception Description | Point of Reception Description | Point of Reception Description | Point of Reception Description | Point of Reception Description | Point of Reception Description | Point of Reception Description | Point of Reception Description | Point of Reception Description | Point of Reception Description | Point of Reception Description |
| Facade of dwelling (10148 Beaverdams Rd) | Outdoor area of dwelling (10148 Beaverdams Rd) | Facade of dwelling (9722 Beaverdams Rd) | Outdoor area of dwelling (9722 Beaverdams Rd) | Facade of dwelling (9602 Beaverdams Rd) | Outdoor area of dwelling (9602 Beaverdams Rd) | Facade of dwelling (5584 Beechwood Rd) | Outdoor area of dwelling (5584 Beechwood Rd) | Facade of dwelling (5769 Beechwood Rd) | Outdoor area of dwelling (5769 Beechwood Rd) | Facade of dwelling (9944 Lundy's Ln) | Outdoor area of dwelling (9944 Lundy's Ln) |
| Point of Reception Coordinates | Point of Reception Coordinates | Point of Reception Coordinates | Point of Reception Coordinates | Point of Reception Coordinates | Point of Reception Coordinates | Point of Reception Coordinates | Point of Reception Coordinates | Point of Reception Coordinates | Point of Reception Coordinates | Point of Reception Coordinates | Point of Reception Coordinates |
| X Y Z | X Y Z | X Y Z | X Y Z | X Y Z | X Y Z | X Y Z | X Y Z | X Y Z | X Y Z | X Y Z | X Y Z |
| 648766 4773660 181.91 | 648766 4773629 179,5 | 649394 4773728 184.5 | 649391 4773698 178.69 | 649571 4773645 184.4 | 649553 4773620 179.77 | 649611 4772698 190.5 | 649594 4772727 186.76 | 649553 4772408 189.5 | 649532 4772429 185.95 | 649084 4771672 186.5 | 649070 4771693 182.43 |

| | 6 B 1 J | | Point of Reception | 11 | | Point of Reception | n 2 | 1 | oint of Reception | 3 | F | oint of Reception | 4 | P | oint of Reception | 5 | 1 | Point of Reception | 6 | | Point of Reception | 7 | F | Point of Reception | 18 | P | oint of Reception | 9 | Pe | oint of Reception | 10 |
|--|--|----------|--------------------|----------------------|----------|--------------------|----------------------|----------|-------------------|----------------------|----------|-------------------|----------------------|----------|-------------------|----------------------|----------|--------------------|-----------|----------|--------------------|----------------------|----------|--------------------|----------------------|----------|-------------------|-----------|----------|-------------------|----------------------|
| Source ID 1-1 | Source Description | Distance | Sound Level | Units ^[3] | Distance | Sound Level | Units ^[3] | Distance | Sound Level | Units ^[3] | Distance | Sound Level | Units ^[3] | Distance | Sound Level | Units ^[3] | Distance | Sound Level | Units [3] | Distance | Sound Level | Units ^[3] | Distance | Sound Level | Units ^[3] | Distance | Sound Level | Units [3] | Distance | Sound Level | Units ^[3] |
| | | (m) | at PoR | (dBA) | (m) | at PoR | (dBA) | (m) | at PoR | (dBA) | (m) | at PoR | (dBA) | (m) | at PoR | (dBA) | (m) | at PoR | (dBA) | (m) | at PoR | (dBA) | (m) | at PoR | (dBA) | (m) | at PoR | (dBA) | (m) | at PoR | (dBA) |
| P1A Sinkcut PC CrusherDump | P1A Sinkcut, PC loader dumping into crusher | 817 | 37 | dBA | 786 | 37 | dBA | 1137 | 37 | dBA | 1112 | 32 | dBA | 1200 | 36 | dBA | 1170 | 31 | dBA | 949 | 39 | dBA | 929 | 34 | dBA | 984 | 39 | dBA | 956 | 34 | dBA |
| P1A_Sinkcut_PC_Ldr | P1A_Sinkcut, PC Loader | 815 | 29 | dBA | 785 | 29 | dBA | 1137 | 25 | dBA | 1112 | 24 | dBA | 1200 | 29 | dBA | 1170 | 24 | dBA | 951 | 31 | dBA | 930 | 26 | dBA | 985 | 31 | dBA | 957 | 26 | dBA |
| P1A Sinkcut PC PrimaryCrush | P1A Sinkcut, PC Primary Crusher | 818 | 43 | dBA | 788 | 42 | dBA | 1138 | 43 | dBA | 1113 | 38 | dBA | 1200 | 43 | dBA | 1170 | 37 | dBA | 948 | 46 | dBA | 927 | 40 | dBA | 982 | 45 | dBA | 954 | 40 | dBA |
| P1A Sinkcut PC PrimaryScreen | P1A Sinkcut, PC Primary Screen | 819 | 38 | dBA | 789 | 37 | dBA | 1138 | 39 | dBA | 1113 | 33 | dBA | 1200 | 38 | dBA | 1170 | 32 | dBA | 946 | 41 | dBA | 926 | 35 | dBA | 980 | 40 | dBA | 952 | 35 | dBA |
| P1A Sinkcut PP Ldr | P1A Sinkcut, PP Loader | 861 | 28 | dBA | 831 | 28 | dBA | 1102 | 30 | dBA | 1075 | 25 | dBA | 1143 | 29 | dBA | 1112 | 24 | dBA | 815 | 33 | dBA | 795 | 28 | dBA | 847 | 28 | dBA | 819 | 28 | dBA |
| P1A Sinkcut PP SecondaryCrush | P1A Sinkcut, PP Secondary Crusher | 867 | 43 | dBA | 837 | 38 | dBA | 1112 | 40 | dBA | 1086 | 34 | dBA | 1155 | 39 | dBA | 1124 | 34 | dBA | 825 | 43 | dBA | 805 | 38 | dBA | 853 | 38 | dBA | 825 | 38 | dBA |
| P1A_Sinkcut_PP_SecondaryTertiaryScreen | P1A_Sinkcut, PP Secondary & Tertiary Screen | 869 | 42 | dBA | 838 | 37 | dBA | 1113 | 39 | dBA | 1086 | 33 | dBA | 1155 | 38 | dBA | 1124 | 33 | dBA | 823 | 42 | dBA | 804 | 37 | dBA | 852 | 37 | dBA | 824 | 36 | dBA |
| P1A Sinkcut PP TertiaryCrush | P1A Sinkcut, PP Tertiary Crusher | 870 | 28 | dBA | 839 | 23 | dBA | 1113 | 25 | dBA | 1086 | 20 | dBA | 1155 | 25 | dBA | 1124 | 19 | dBA | 822 | 28 | dBA | 803 | 23 | dBA | 850 | 23 | dBA | 822 | 23 | dBA |
| P1A_Sinkcut_PP_Trk1 | P1A_Sinkcut, PP Idling Truck | 850 | 25 | dBA | 820 | 20 | dBA | 1091 | 22 | dBA | 1064 | 17 | dBA | 1133 | 21 | dBA | 1102 | 16 | dBA | 814 | 25 | dBA | 794 | 20 | dBA | 850 | 25 | dBA | 822 | 20 | dBA |
| P1A Sinkcut PP Trk2 | P1A Sinkcut, PP Idling Truck | 850 | 25 | dBA | 819 | 20 | dBA | 1089 | 22 | dBA | 1062 | 17 | dBA | 1131 | 21 | dBA | 1101 | 16 | dBA | 812 | 25 | dBA | 792 | 20 | dBA | 848 | 25 | dBA | 820 | 20 | dBA |
| P1A Sinkcut WF Drill | P1A Sinkcut, WF Drill | 801 | 33 | dBA | 771 | 32 | dBA | 1148 | 28 | dBA | 1124 | 28 | dBA | 1218 | 27 | dBA | 1188 | 27 | dBA | 995 | 35 | dBA | 973 | 30 | dBA | 1031 | 34 | dBA | 1003 | 29 | dBA |
| P1A_Sinkcut_Conveyor | P1A_Sinkcut, Conveyor | varies | 32 | dBA | varies | 28 | dBA | varies | 29 | dBA | varies | 24 | dBA | varies | 28 | dBA | varies | 23 | dBA | varies | 32 | dBA | varies | 26 | dBA | varies | 31 | dBA | varies | 26 | dBA |
| P1A Sinkcut RD SHP Aggr Em | P1A Sinkcut, Aggregate Shipping from PP, Empty | varies | 22 | dBA | varies | 18 | dBA | varies | 18 | dBA | varies | 13 | dBA | varies | 17 | dBA | varies | 12 | dBA | varies | 20 | dBA | varies | 15 | dBA | varies | 19 | dBA | varies | 16 | dBA |
| P1A Sinkcut RD SHP Aggr Fu | P1A Sinkcut, Aggregate Shipping from PP, Full | varies | 22 | dBA | varies | 18 | dBA | varies | 18 | dBA | varies | 13 | dBA | varies | 17 | dBA | varies | 12 | dBA | varies | 20 | dBA | varies | 15 | dBA | varies | 19 | dBA | varies | 16 | dBA |

Point of Reception ID R60

| 1 | Point of Reception | 11 | 1 | Point of Reception | 12 |
|-----------------|-----------------------|-------------------------------|-----------------|-----------------------|------------------------------|
| Distance (m) | Sound Level at PoR | Units ^[3] (dBA) | Distance (m) | Sound Level at PoR | Units ^{[2} (dBA) |
| 1246 | 36 | dBA | 1221 | 31 | dBA |
| 1248 | 28 | dBA | 1223 | 23 | dBA |
| 1244 | 42 | dBA | 1219 | 37 | dBA |
| 1242 | 38 | dBA | 1217 | 32 | dBA |
| 1162 | 24 | dBA | 1138 | 24 | dBA |
| 1158 | 39 | dBA | 1134 | 34 | dBA |
| 1157 | 38 | dBA | 1133 | 33 | dBA |
| 1155 | 24 | dBA | 1131 | 19 | dBA |
| 1172 | 21 | dBA | 1148 | 16 | dBA |
| 1172 | 16 | dBA | 1148 | 16 | dBA |
| 1280 | 31 | dBA | 1256 | 26 | dBA |
| varies | 28 | dBA | varies | 23 | dBA |
| varies | 16 | dBA | varies | 13 | dBA |
| varies | 16 | dBA | varies | 13 | dBA |

Table 2b: Point of Reception Noise Impact (Sample Calculation for Proposed Phase 4 Southeast) Uppers Quary, 1603157

- Notes to Table: "Table A2" in Appendix A of Basic CCofA Guide. 1. "Continuous" noise sources includes operating time corrections and sum of steady, quasi-steady impulsive, tonal, cyclical and buzzing noise sources, with appropriate penalties applied, in accordance with documents NPC-104 and NPC-300.
 - 2. Wherever possible, the Source ID matches the identifiers used in the ESDM report.
- 3.
- ---
- Sound Level units: BBA = 1-hour energy equivalent sound level (L_{un}(1-hr)), in terms of A-Weighted decibels. BBA = Logarithmic mean impulsive noise level (L_{unk}), in terms of A-Weighted decibels incorporating an impulsive time weighting. Noise and vibration receptors representative of worst-case potential impacts have been selected. For the purposes of noise and vibration impact assessment, the following hand uses (existing or zoned for future use) have been considered: bretch, motive and examproads barbeth, motive and examproads nursing / retirement homes unchest and places of worship

| Poin | int of Receptio R1f | n ID | | Point of Recep R10 | tion ID | | Point of Recep R2f | tion ID | | Point of Recept R20 | tion ID | | Point of Recep R3f | tion ID | | Point of Reception R30 | n ID | | Point of Recep R4f | tion ID | | Point of Recepti R40 | on ID | | Point of Recept R5f | ion ID | |
|------|------------------------|-----------------|-----------|-----------------------|-------------------|----------------|-----------------------|--------------------|----------|------------------------|--------------------|----------------|-----------------------|-------------------|----------|------------------------|------------------|---------------|-----------------------|-------------------|---------|-------------------------|------------------|--------------|------------------------|-------------------|---------|
| Poin | int of Receptio | n Description | | Point of Recep | tion Description | | Point of Recep | tion Description | | Point of Recept | tion Description | | Point of Recep | tion Description | | Point of Reception | n Description | | Point of Recept | tion Description | | Point of Recepti | on Description | | Point of Recept | ion Description | - |
| Fac | cade of dwellir | ıg (10148 Beave | rdams Rd) | Outdoor area o | f dwelling (10148 | Beaverdams Rd) | Facade of dwe | lling (9722 Beaver | dams Rd) | Outdoor area o | f dwelling (9722 I | Beaverdams Rd) | Facade of dwe | ling (9602 Beaver | dams Rd) | Outdoor area of | dwelling (9602 B | eaverdams Rd) | Facade of dwel | ling (5584 Beechw | ood Rd) | Outdoor area of | dwelling (5584 B | eechwood Rd) | Facade of dwel | ling (5769 Beechw | əod Rd) |
| Poin | int of Receptio | n Coordinates | | Point of Recep | tion Coordinates | | Point of Recept | tion Coordinates | | Point of Recept | tion Coordinates | | Point of Recept | tion Coordinates | | Point of Reception | n Coordinates | | Point of Recept | tion Coordinates | | Point of Recepti | on Coordinates | | Point of Recept | ion Coordinates | - |
| | X Y Z | | | X | Y | Z | X | Y | Z | X | Y | Z | x | Y | Z | x | Y | z | x | Y | Z | x | Y | z | x | Y | Z |
| | 648766 | 4773660 | 181.91 | 648766 | 4773629 | 179.5 | 649394 | 4773728 | 184.5 | 649391 | 4773698 | 178.69 | 649571 | 4773645 | 184.4 | 649553 | 4773620 | 179.77 | 649611 | 4772698 | 190.5 | 649594 | 4772727 | 186.76 | 649553 | 4772408 | 189.5 |
| | | | | | | | | | | | | | | | | | | | | | | | | | | | |

| | | | Point of Rec | eption 1 | | Point of Recep | tion 2 | | Point of F | eception 3 | | Point of Rec | ception 4 | | Point o | of Reception 5 | ; | | Point of Reception | 6 | P | oint of Reception | n 7 | | Point of Reception | n 8 | P | oint of Reception | 1.9 | 1 | oint of Reception | n 10 | F | oint of Reception | 11 | P | oint of Reception | 12 |
|-----------------------------------|--|----------|--------------|----------------|----------|----------------|----------|--------------------|------------|----------------------------|----------|--------------|-------------|---------------------|----------|----------------|----------------------|----------|--------------------|----------------------|----------|-------------------|----------------------|----------|--------------------|----------------------|----------|-------------------|----------------------|----------|-------------------|----------------------|----------|-------------------|-----------|----------|-------------------|----------------------|
| Source ID 1-1 | Source Description | Distance | Sound L | evel Units [3] | Distance | Sound Lev | el Units | ^[3] Dis | ance Soun | Level Units ^[3] | Distance | Sound 1 | Level Units | ^[3] Dist | tance So | und Level | Units ^[3] | Distance | Sound Level | Units ^[3] | Distance | Sound Level | Units ^[3] | Distance | Sound Level | Units ^[3] | Distance | Sound Level | Units ^[3] | Distance | Sound Level | Units ^[3] | Distance | Sound Level | Units [3] | Distance | Sound Level | Units ^[3] |
| | | (m) | at Po | R (dBA) | (m) | at PoR | (dBA | a (| m) at | PoR (dBA) | (m) | at Pe | oR (dBA | (I) (I | m) | at PoR | (dBA) | (m) | at PoR | (dBA) | (m) | at PoR | (dBA) | (m) | at PoR | (dBA) | (m) | at PoR | (dBA) | (m) | at PoR | (dBA) | (m) | at PoR | (dBA) | (m) | at PoR | (dBA) |
| ASPH comp | Asphalt Plant - Compressor Vent | 838 | 15 | dBA | 808 | 12 | dBA | . 10 |)38 | 3 dBA | 1011 | 3 | dBA | 10 | 072 | 4 | dBA | 1042 | 0 | dBA | 747 | 8 | dBA | 726 | 8 | dBA | 798 | 8 | dBA | 770 | 8 | dBA | 1176 | 16 | dBA | 1152 | 11 | dBA |
| ASPH_DC_m | Asphalt Plant - Dust Collector Blower (motor) | 838 | 23 | dBA | 808 | 20 | dBA | . 10 | 050 | 25 dBA | 1023 | 18 | dB/ | 10 | 086 | 12 | dBA | 1056 | 10 | dBA | 765 | 32 | dBA | 744 | 31 | dBA | 813 | 29 | dBA | 784 | 28 | dBA | 1177 | 23 | dBA | 1153 | 19 | dBA |
| ASPH DC s | Asphalt Plant - Dust Collector Blower (stack) | 838 | 34 | dBA | 808 | 34 | dBA | . 10 | 051 | 33 dBA | 1023 | 32 | dBA | 10 | 088 | 33 | dBA | 1057 | 32 | dBA | 767 | 36 | dBA | 746 | 36 | dBA | 814 | 35 | dBA | 785 | 35 | dBA | 1177 | 32 | dBA | 1153 | 31 | dBA |
| ASPH elev | Asphalt Plant - Elevator Motor | 830 | 22 | dBA | 800 | 19 | dBA | . 10 | 040 | 22 dBA | 1013 | 18 | dB/ | 10 | 077 | 22 | dBA | 1046 | 19 | dBA | 762 | 25 | dBA | 741 | 24 | dBA | 813 | 24 | dBA | 784 | 24 | dBA | 1184 | 20 | dBA | 1160 | 19 | dBA |
| ASPH IDLE TRK1 | Asphalt Plant - Idling Truck | 842 | 13 | dBA | 812 | 9 | dBA | . 10 |)39 | -1 dBA | 1011 | -2 | dB/ | 10 | 072 | 4 | dBA | 1041 | 1 | dBA | 742 | 23 | dBA | 721 | 22 | dBA | 792 | 19 | dBA | 764 | 17 | dBA | 1172 | 13 | dBA | 1148 | 8 | dBA |
| ASPH IDLE TRK2 | Asphalt Plant - Idling Truck | 843 | 13 | dBA | 813 | 9 | dBA | 10 | 039 | -1 dBA | 1012 | -2 | dBA | 10 | 072 | 4 | dBA | 1042 | 2 | dBA | 742 | 23 | dBA | 721 | 22 | dBA | 792 | 19 | dBA | 763 | 17 | dBA | 1171 | 13 | dBA | 1147 | 8 | dBA |
| ASPH_Ldr_Act1 | Asphalt Plant - Loader Activity | 836 | 19 | dBA | 806 | 16 | dBA | . 10 | 039 | 21 dBA | 1012 | 14 | dB/ | 10 | 075 | 23 | dBA | 1044 | 15 | dBA | 753 | 20 | dBA | 732 | 18 | dBA | 803 | 25 | dBA | 774 | 23 | dBA | 1178 | 19 | dBA | 1154 | 15 | dBA |
| ASPH Ldr Act2 | Asphalt Plant - Loader Activity | 838 | 8 | dBA | 808 | 8 | dBA | 10 | 045 | 21 dBA | 1018 | 14 | dBA | 10 | 081 | 23 | dBA | 1050 | 15 | dBA | 758 | 27 | dBA | 737 | 27 | dBA | 806 | 25 | dBA | 778 | 23 | dBA | 1176 | 19 | dBA | 1152 | 15 | dBA |
| ASPH_motor | Asphalt Plant - Conveyor motor, gravel hitting metal plate | 830 | 21 | dBA | 800 | 16 | dBA | . 10 | 044 | 25 dBA | 1017 | 15 | dB/ | 10 | 082 | 27 | dBA | 1051 | 17 | dBA | 769 | 31 | dBA | 748 | 26 | dBA | 818 | 29 | dBA | 790 | 28 | dBA | 1185 | 23 | dBA | 1161 | 17 | dBA |
| ASPH oven | Asphalt Plant - Oven Motor | 833 | 21 | dBA | 803 | 18 | dBA | 10 | 044 | 23 dBA | 1017 | 16 | dB/ | 10 | 081 | 24 | dBA | 1051 | 17 | dBA | 764 | 28 | dBA | 743 | 29 | dBA | 814 | 26 | dBA | 785 | 25 | dBA | 1181 | 21 | dBA | 1158 | 17 | dBA |
| ASPH pugdoor | Asphalt Plant - Pug Mill door (pressure relief noise) | 831 | 26 | dBA | 801 | 22 | dBA | 10 | 040 | 11 dBA | 1012 | 10 | dB/ | 10 | 076 | 11 | dBA | 1046 | 10 | dBA | 760 | 20 | dBA | 739 | 20 | dBA | 811 | 15 | dBA | 782 | 14 | dBA | 1183 | 26 | dBA | 1159 | 22 | dBA |
| ASPH_pugmill | Asphalt Plant - Pug Mill Motor | 830 | 19 | dBA | 800 | 15 | dBA | . 10 |)34 | 21 dBA | 1006 | 13 | dB/ | 10 | 069 | 22 | dBA | 1039 | 15 | dBA | 753 | 27 | dBA | 732 | 25 | dBA | 806 | 25 | dBA | 777 | 23 | dBA | 1184 | 19 | dBA | 1161 | 15 | dBA |
| P4 SE PC CrusherDump | P4 SE, PC loader dumping into crusher | 1117 | 37 | dBA | 1094 | 35 | dBA | . 9 | 30 | 37 dBA | 900 | 29 | dB/ | 84 | 47 | 37 | dBA | 820 | 31 | dBA | 166 | 37 | dBA | 135 | 38 | dBA | 401 | 29 | dBA | 377 | 29 | dBA | 1198 | 24 | dBA | 1183 | 24 | dBA |
| P4 SE PC Ldr | P4 SE, PC Loader | 1119 | 26 | dBA | 1096 | 25 | dBA | . 9 | 32 | 26 dBA | 901 | 19 | dB/ | 84 | 48 | 26 | dBA | 822 | 21 | dBA | 163 | 27 | dBA | 133 | 29 | dBA | 399 | 19 | dBA | 375 | 19 | dBA | 1198 | 14 | dBA | 1182 | 14 | dBA |
| P4 SE PC PrimaryCrush | P4 SE, PC Primary Crusher | 1115 | 40 | dBA | 1092 | 38 | dBA | . 9 | 29 | 40 dBA | 899 | 33 | dBA | 84 | 46 | 40 | dBA | 820 | 35 | dBA | 168 | 41 | dBA | 137 | 42 | dBA | 402 | 33 | dBA | 378 | 33 | dBA | 1199 | 29 | dBA | 1183 | 28 | dBA |
| P4 SE PC PrimaryScreen | P4 SE, PC Primary Screen | 1114 | 35 | dBA | 1090 | 33 | dBA | . 9 | 28 | 36 dBA | 897 | 27 | dB/ | 84 | 45 | 36 | dBA | 819 | 29 | dBA | 169 | 36 | dBA | 139 | 37 | dBA | 403 | 28 | dBA | 380 | 28 | dBA | 1199 | 24 | dBA | 1184 | 23 | dBA |
| P4_SE_PP_Ldr | P4_SE, PP Loader | 855 | 22 | dBA | 828 | 21 | dBA | . 8 | 65 | 24 dBA | 835 | 16 | dB/ | 8 | 57 | 26 | dBA | 826 | 17 | dBA | 500 | 29 | dBA | 473 | 26 | dBA | 632 | 29 | dBA | 603 | 27 | dBA | 1227 | 23 | dBA | 1207 | 20 | dBA |
| P4 SE PP SecondaryCrush1 | P4 SE, PP Secondary Crusher | 859 | 32 | dBA | 832 | 31 | dBA | . 8 | 59 | 34 dBA | 830 | 24 | dB/ | 84 | 48 | 36 | dBA | 818 | 26 | dBA | 488 | 38 | dBA | 462 | 35 | dBA | 626 | 39 | dBA | 596 | 37 | dBA | 1230 | 31 | dBA | 1210 | 30 | dBA |
| P4 SE PP SecondaryCrush2 | P4 SE, PP Secondary Crusher | 860 | 32 | dBA | 833 | 31 | dBA | . 8 | 60 | 34 dBA | 830 | 25 | dB/ | 84 | 49 | 36 | dBA | 818 | 26 | dBA | 488 | 38 | dBA | 461 | 35 | dBA | 625 | 30 | dBA | 595 | 28 | dBA | 1229 | 31 | dBA | 1209 | 30 | dBA |
| P4 SE PP SecondaryTertiaryScreen1 | P4 SE, PP Secondary & Tertiary Screen | 859 | 32 | dBA | 832 | 30 | dBA | . 8 | 60 | 33 dBA | 830 | 24 | dB/ | 84 | 49 | 35 | dBA | 819 | 25 | dBA | 489 | 38 | dBA | 463 | 34 | dBA | 626 | 38 | dBA | 597 | 36 | dBA | 1230 | 31 | dBA | 1209 | 29 | dBA |
| P4 SE PP SecondaryTertiaryScreen2 | P4 SE, PP Secondary & Tertiary Screen | 860 | 32 | dBA | 833 | 30 | dBA | . 8 | 61 | 33 dBA | 831 | 24 | dB/ | 8: | 50 | 35 | dBA | 819 | 25 | dBA | 489 | 38 | dBA | 462 | 34 | dBA | 625 | 38 | dBA | 596 | 36 | dBA | 1229 | 30 | dBA | 1208 | 29 | dBA |
| P4_SE_PP_TertiaryCrush1 | P4_SE, PP Tertiary Crusher | 859 | 18 | dBA | 832 | 17 | dBA | . 8 | 61 | 20 dBA | 831 | 12 | dB/ | 8 | 51 | 22 | dBA | 820 | 13 | dBA | 490 | 24 | dBA | 464 | 21 | dBA | 626 | 24 | dBA | 597 | 23 | dBA | 1229 | 17 | dBA | 1208 | 16 | dBA |
| P4 SE PP TertiaryCrush2 | P4 SE, PP Tertiary Crusher | 860 | 18 | dBA | 833 | 17 | dBA | . 8 | 62 | 20 dBA | 832 | 12 | dBA | 8 | 51 | 22 | dBA | 821 | 13 | dBA | 489 | 24 | dBA | 463 | 21 | dBA | 625 | 24 | dBA | 596 | 23 | dBA | 1228 | 17 | dBA | 1208 | 16 | dBA |
| P4 SE PP Trk1 | P4 SE, PP Idling Truck | 853 | 13 | dBA | 826 | 12 | dBA | . 8 | 70 | 15 dBA | 840 | 7 | dB/ | 80 | 63 | 17 | dBA | 832 | 8 | dBA | 507 | 26 | dBA | 481 | 24 | dBA | 637 | 21 | dBA | 607 | 19 | dBA | 1225 | 15 | dBA | 1204 | 11 | dBA |
| P4 SE PP Trk2 | P4 SE, PP Idling Truck | 850 | 13 | dBA | 823 | 12 | dBA | . 8 | 68 | 15 dBA | 839 | 7 | dBA | 80 | 62 | 17 | dBA | 831 | 8 | dBA | 509 | 26 | dBA | 483 | 24 | dBA | 639 | 21 | dBA | 610 | 19 | dBA | 1226 | 15 | dBA | 1206 | 11 | dBA |
| P4 SE WF Drill | P4_SE, WF Drill | 1159 | 29 | dBA | 1136 | 28 | dBA | . 9 | 55 | 31 dBA | 925 | 30 |) dB/ | 80 | 64 | 31 | dBA | 838 | 31 | dBA | 121 | 40 | dBA | 90 | 42 | dBA | 375 | 30 | dBA | 353 | 30 | dBA | 1193 | 25 | dBA | 1179 | 25 | dBA |
| AP_RD_SHP_AC_RAP_Em | AP, AC and RAP shipped from Offsite, Empty | varies | 23 | dBA | varies | 21 | dBA | va | ries | 20 dBA | varies | 14 | dB/ | va | ries | 19 | dBA | varies | 13 | dBA | varies | 23 | dBA | varies | 20 | dBA | varies | 21 | dBA | varies | 20 | dBA | varies | 18 | dBA | varies | 16 | dBA |
| AP RD SHP AC RAP Fu | AP, AC and RAP shipped from Offsite, Full | varies | 23 | dBA | varies | 20 | dBA | va | ries | 20 dBA | varies | 14 | dB/ | va | ries | 19 | dBA | varies | 13 | dBA | varies | 23 | dBA | varies | 20 | dBA | varies | 21 | dBA | varies | 20 | dBA | varies | 18 | dBA | varies | 16 | dBA |
| AP RD SHP HMA Em | AP, HMA product shipping, Empty | varies | 23 | dBA | varies | 20 | dBA | va | ries | 20 dBA | varies | 14 | dB/ | va | uries | 19 | dBA | varies | 13 | dBA | varies | 23 | dBA | varies | 20 | dBA | varies | 21 | dBA | varies | 20 | dBA | varies | 18 | dBA | varies | 16 | dBA |
| AP RD SHP HMA Fu | AP, HMA product shipping, Full | varies | 23 | dBA | varies | 21 | dBA | va | ries | 20 dBA | varies | 14 | dB/ | va | uries | 19 | dBA | varies | 13 | dBA | varies | 23 | dBA | varies | 20 | dBA | varies | 21 | dBA | varies | 20 | dBA | varies | 18 | dBA | varies | 16 | dBA |
| P4 SE Conveyor | P4 SE, Conveyor | varies | 27 | dBA | varies | 25 | dBA | va | ries | 30 dBA | varies | 21 | dBA | va | uries | 29 | dBA | varies | 20 | dBA | varies | 35 | dBA | varies | 33 | dBA | varies | 28 | dBA | varies | 27 | dBA | varies | 22 | dBA | varies | 20 | dBA |
| P4_SE_RD_Haul_PP_AP_Em | P4 SE, Aggregate Haul road b/w PP and AP, Empty | varies | 14 | dBA | varies | 10 | dBA | va | ries | 16 dBA | varies | 8 | dBA | var | ries | 17 | dBA | varies | 9 | dBA | varies | 23 | dBA | varies | 22 | dBA | varies | 18 | dBA | varies | 16 | dBA | varies | 12 | dBA | varies | 7 | dBA |
| P4 SE RD Haul PP AP Fu | P4 SE, Aggregate Haul road b/w PP and AP, Full | varies | 17 | dBA | varies | 12 | dBA | va | ries | 19 dBA | varies | 10 | dB/ | va | ries | 20 | dBA | varies | 12 | dBA | varies | 26 | dBA | varies | 25 | dBA | varies | 21 | dBA | varies | 19 | dBA | varies | 15 | dBA | varies | 9 | dBA |
| P4_SE_RD_SHP_Aggr_Em | P4_SE, Aggregate Shipping from PP, Empty | varies | 27 | dBA | varies | 24 | dBA | va | ries | 24 dBA | varies | 19 | dBA | var | ries | 24 | dBA | varies | 19 | dBA | varies | 29 | dBA | varies | 27 | dBA | varies | 25 | dBA | varies | 24 | dBA | varies | 21 | dBA | varies | 20 | dBA |
| P4 SE RD SHP Ager Fu | P4 SE Aggregate Shinning from PP Full | varies | 27 | dBA | varies | 24 | dBA | va | ries | dBA | varies | 19 | dB/ | va | ries | 24 | dBA | varies | 19 | dBA | varies | 29 | dBA | varies | 27 | dBA | varies | 25 | dBA | varies | 24 | dBA | varies | 21 | dBA | varies | 20 | dBA |

| oint of Recept | tion ID | | Point of Recepti | on ID | | Point of Recept | ion ID | | | |
|----------------|---------------------|-------------|------------------|-------------------|-----|--|-----------------|---|--|--|
| R50 | _ | | R61 |] | | R00 |] | | | |
| oint of Recept | tion Description | | Point of Recepti | on Description | | Point of Recept | ion Description | | | |
| Outdoor area o | f dwelling (5769 Be | echwood Rd) | Facade of dwell | ing (9944 Lundy's | Ln) | Outdoor area of dwelling (9944 Lundy's Ln) | | | | |
| oint of Recent | tion Coordinates | | Point of Recenti | on Coordinates | | Point of Recent | ion Coordinates | | | |
| X | Y | z | X | Y | Z | x | Y | z | | |
| | | 195.05 | 640084 | 4221622 | | 640050 | | | | |

Table 3a: Acoustic Assessment Summary, Proposed Phase 1A Sinking Cut Upper's Quarry, 1603157

Notes to Table:

- "Table A3" in Appendix A of Basic CCofA Guide.

1. "Continuous" noise sources includes sum of steady, quasi-steady impulsive, tonal, cyclical and buzzing noise sources, with appropriate penalties applied, in accordance with documents NPC-104 and NPC-300. Impulsive and emergency noise sources are assessed separately from continuous noise sources.

2. Daytime occurs from 0700-1900h. Evening occurs from 1900h-2300h. Nighttime occurs from 2300-0700h.

3. Worst-case cumulative sound level from all applicable sources operating.

4. Has an acoustic audit (as defined in Publication NPC-233) been conducted with source in place and operating?

5. Applicable worst-case NPC-300 sound level limit.

6. Performance limit (aka guideline limit) based on following:

- C = Calculated based on road traffic volumes in compliance with NPC-206 requirements.

- M = Measured based on monitoring for a minimum 48 hour period, in accordance with NPC-233 requirements.

- D = Default guideline minima per NPC-300.

| Point of Reception ID | Point of Reception Description | Time Period | Total Sound Level at PoR ^[3] | Verified by Acoustic Audit ^[4] | Performance Limit ^[5] | Peformance Limit Source [6] | Compliance with Performance Limit | UTM Co (Zone | oordinate e 17N) | Height Relative to Local Grade |
|-----------------------------|---------------------------------|-------------|---|---|-------------------------------------|-----------------------------------|--|-----------------|---------------------|--------------------------------------|
| | | | (dBA) | (Yes/No) | (dBA) | (C / M/ D) | (Yes/No) | X (m) | Y (m) | (m) |
| | Econdo of dwalling (10149 | Daytime | 49 | No | 50 | | Yes | | | |
| R1f | Beaverdams Rd) | Evening | 32 | No | 50 | D | Yes | 648766 | 4773660 | 4.5 |
| | | Nighttime | 32 | No | 45 | | Yes | | | |
| R1o | Outdoor area of dwelling (10148 | Daytime | 46 | No | 50 | п | Yes | 648766 | 4773629 | 1.5 |
| RIU | Beaverdams Rd) | Evening | 30 | No | 45 | Ъ | Yes | 048700 | 4//3029 | 1.5 |
| | Facade of dwelling (9722 | Daytime | 47 | No | 50 | | Yes | | | |
| R2f | Beaverdams Rd) | Evening | 31 | No | 50 | D | Yes | 649394 | 4773728 | 4.5 |
| | Beuverdums reaj | Nighttime | 31 | No | 45 | | Yes | | | |
| R20 | Outdoor area of dwelling (9722 | Daytime | 42 | No | 50 | п | Yes | 649391 | 4773698 | 1.5 |
| 1(20 | Beaverdams Rd) | Evening | 26 | No | 45 | Ь | Yes | 047571 | 4775070 | 1.5 |
| | Facade of dwelling (9602 | Daytime | 47 | No | 50 | | Yes | | | |
| R3f | Beaverdams Rd) | Evening | 31 | No | 50 | D | Yes | 649571 | 4773645 | 4.5 |
| | Beaverdams reaj | Nighttime | 31 | No | 45 | | Yes | | | |
| P 30 | Outdoor area of dwelling (9602 | Daytime | 42 | No | 50 | р | Yes | 640553 | 4773620 | 1.5 |
| 1050 | Beaverdams Rd) | Evening | 26 | No | 45 | Ъ | Yes | 047555 | 4773020 | 1.5 |
| | Econdo of dwalling (5594 | Daytime | 50 | No | 50 | | Yes | | | |
| R4f | Beechwood Rd) | Evening | 35 | No | 50 | D | Yes | 649611 | 4772698 | 4.5 |
| | Becchwood Ray | Nighttime | 35 | No | 45 | | Yes | | | |
| R 4o | Outdoor area of dwelling (5584 | Daytime | 45 | No | 50 | П | Yes | 640504 | 1777777 | 1.5 |
| IC+0 | Beechwood Rd) | Evening | 29 | No | 45 | Ъ | Yes | 047374 | 4//2/2/ | 1.5 |
| | Econdo of dwalling (5760 | Daytime | 48 | No | 50 | | Yes | | | |
| R5f | Beechwood Rd) | Evening | 31 | No | 50 | D | Yes | 649553 | 4772408 | 4.5 |
| | Beeenwood Ru) | Nighttime | 31 | No | 45 | | Yes | | | |
| P 50 | Outdoor area of dwelling (5769 | Daytime | 44 | No | 50 | П | Yes | 640532 | 1772120 | 1.5 |
| 100 | Beechwood Rd) | Evening | 29 | No | 45 | Ъ | Yes | 049332 | 4//2429 | 1.5 |
| | Econdo of dwelling (0044 I 1.1. | Daytime | 47 | No | 50 | | Yes | | | |
| R6f | I n) | Evening | 27 | No | 50 | D | Yes | 649084 | 4771672 | 4.5 |
| | Liij | Nighttime | 27 | No | 45 | | Yes | | | |
| D 6a | Outdoor area of dwelling (9944 | Daytime | 41 | No | 50 | D | Yes | 640070 | 4771602 | 1.5 |
| K00 | Lundy's Ln) | Evening | 25 | No | 45 | U U | Ves | 049070 | 4//1093 | 1.5 |

Table 3b: Acoustic Assessment Summary, Proposed Phase 1A South Sinking Cut Upper's Quarry, 1603157

Notes to Table:

- "Table A3" in Appendix A of Basic CCofA Guide.

1. "Continuous" noise sources includes sum of steady, quasi-steady impulsive, tonal, cyclical and buzzing noise sources, with appropriate penalties applied, in accordance with documents NPC-104 and NPC-300. Impulsive and emergency noise sources are assessed separately from continuous noise sources.

2. Daytime occurs from 0700-1900h. Evening occurs from 1900h-2300h. Nighttime occurs from 2300-0700h.

3. Worst-case cumulative sound level from all applicable sources operating.

4. Has an acoustic audit (as defined in Publication NPC-233) been conducted with source in place and operating?

5. Applicable worst-case NPC-300 sound level limit.

6. Performance limit (aka guideline limit) based on following:

- C = Calculated based on road traffic volumes in compliance with NPC-206 requirements.

- M = Measured based on monitoring for a minimum 48 hour period, in accordance with NPC-233 requirements.

- D = Default guideline minima per NPC-300.

| Point of Reception ID | Point of Reception Description | Time Period | Total Sound Level at PoR ^[3] | Verified by Acoustic Audit ^[4] | Performance Limit ^[5] | Peformance Limit Source | Compliance with Performance Limit | UTM Co (Zone | oordinate e 17N) | Height Relative to Local Grade |
|-----------------------------|--|-------------|---|---|-------------------------------------|----------------------------|--|-----------------|---------------------|--------------------------------------|
| | | | (dBA) | (Yes/No) | (dBA) | (C / M/ D) | (Yes/No) | X (m) | Y (m) | (m) |
| | Eccede of dwalling (10148 | Daytime | 44 | No | 50 | | Yes | | | |
| R1f | Beaverdams Rd) | Evening | 30 | No | 50 | D | Yes | 648766 | 4773660 | 4.5 |
| | Beaverdams (cd) | Nighttime | 30 | No | 45 | | Yes | | | |
| P1o | Outdoor area of dwelling (10148 | Daytime | 43 | No | 50 | р | Yes | 648766 | 1773620 | 1.5 |
| KIU | Beaverdams Rd) | Evening | 29 | No | 45 | D | Yes | 048700 | 4773029 | 1.5 |
| | Econds of dwalling (0722 | Daytime | 43 | No | 50 | | Yes | | | |
| R2f | Beaverdams Rd) | Evening | 30 | No | 50 | D | Yes | 649394 | 4773728 | 4.5 |
| | Deaverdanis (Ku) | Nighttime | 30 | No | 45 | | Yes | | | |
| P 20 | Outdoor area of dwelling (9722 | Daytime | 40 | No | 50 | р | Yes | 6/0301 | 1773608 | 1.5 |
| K20 | Beaverdams Rd) | Evening | 25 | No | 45 | D | Yes | 049391 | 4//3098 | 1.5 |
| | Essada of dwalling (0602 | Daytime | 43 | No | 50 | | Yes | | | |
| R3f | Facade of dwelling (9602 Beaverdams Rd) | Evening | 30 | No | 50 | D | Yes | 649571 | 4773645 | 4.5 |
| | Deaverdanis (Ku) | Nighttime | 30 | No | 45 | | Yes | | | |
| P20 | Outdoor area of dwelling (9602 | Daytime | 40 | No | 50 | D | Yes | 640552 | 4772620 | 1.5 |
| K30 | Beaverdams Rd) | Evening | 25 | No | 45 | D | Yes | 049333 | 4773020 | 1.5 |
| | E f. h | Daytime | 49 | No | 50 | | Yes | | | |
| R4f | Facade of dwelling (5584 Beechwood Rd) | Evening | 34 | No | 50 | D | Yes | 649611 | 4772698 | 4.5 |
| | Beeenwood Ruj | Nighttime | 34 | No | 45 | | Yes | | | |
| P 4o | Outdoor area of dwelling (5584 | Daytime | 44 | No | 50 | D | Yes | 640504 | דרדרדג | 1.5 |
| K40 | Beechwood Rd) | Evening | 28 | No | 45 | D | Yes | 049394 | 4//2/2/ | 1.5 |
| | E 1 6 1 11: (5760 | Daytime | 49 | No | 50 | | Yes | | | |
| R5f | Facade of dwelling (5769 Beechwood Rd) | Evening | 29 | No | 50 | D | Yes | 649553 | 4772408 | 4.5 |
| | Beeenwood Ruj | Nighttime | 29 | No | 45 | | Yes | | | |
| P50 | Outdoor area of dwelling (5769 | Daytime | 47 | No | 50 | D | Yes | 640522 | 4772420 | 1.5 |
| K30 | Beechwood Rd) | Evening | 29 | No | 45 | D | Yes | 049332 | 4//2429 | 1.5 |
| | E 1 6 1 11: (0044 E 1 L | Daytime | 47 | No | 50 | | Yes | | | |
| R6f | racade of dwelling (9944 Lundy's | Evening | 31 | No | 50 | D | Yes | 649084 | 4771672 | 4.5 |
| | Liij | Nighttime | 31 | No | 45 | | Yes | | | |
| D4a | Outdoor area of dwelling (9944 | Daytime | 44 | No | 50 | D | Yes | 640070 | 4771602 | 1.5 |
| K00 | Lundy's Ln) | Evening | 26 | No | 45 | D | Ves | 049070 | 4//1093 | 1.5 |

Table 3c: Acoustic Assessment Summary, Proposed Phase 2A Sinking Cut Upper's Quarry, 1603157

Notes to Table:

- "Table A3" in Appendix A of Basic CCofA Guide.

1. "Continuous" noise sources includes sum of steady, quasi-steady impulsive, tonal, cyclical and buzzing noise sources, with appropriate penalties applied, in accordance with documents NPC-104 and NPC-300. Impulsive and emergency noise sources are assessed separately from continuous noise sources.

2. Daytime occurs from 0700-1900h. Evening occurs from 1900h-2300h. Nighttime occurs from 2300-0700h.

3. Worst-case cumulative sound level from all applicable sources operating.

4. Has an acoustic audit (as defined in Publication NPC-233) been conducted with source in place and operating?

5. Applicable worst-case NPC-300 sound level limit.

6. Performance limit (aka guideline limit) based on following:

- C = Calculated based on road traffic volumes in compliance with NPC-206 requirements.

- M = Measured based on monitoring for a minimum 48 hour period, in accordance with NPC-233 requirements.

- D = Default guideline minima per NPC-300.

| Point of Reception ID | Point of Reception Description | Time Period | Total Sound Level at PoR ^[3] | Verified by Acoustic Audit ^[4] | Performance Limit ^[5] | Peformance Limit Source [6] | Compliance with Performance Limit | UTM Co (Zono | oordinate e 17N) | Height Relative to Local Grade |
|-----------------------------|--|-------------|---|---|-------------------------------------|-----------------------------------|--|-----------------|---------------------|--------------------------------------|
| | | | (dBA) | (Yes/No) | (dBA) | (C / M/ D) | (Yes/No) | X (m) | Y (m) | (m) |
| | Econdo of dwalling (10148 | Daytime | 50 | No | 50 | | Yes | | | |
| R1f | Beaverdams Rd) | Evening | 35 | No | 50 | D | Yes | 648766 | 4773660 | 4.5 |
| | | Nighttime | 35 | No | 45 | | Yes | | | |
| R1o | Outdoor area of dwelling (10148 | Daytime | 50 | No | 50 | р | Yes | 648766 | 4773629 | 1.5 |
| RIU | Beaverdams Rd) | Evening | 34 | No | 45 | Ъ | Yes | 048700 | 4773029 | 1.5 |
| | Facada of dwalling (0722 | Daytime | 47 | No | 50 | | Yes | | | |
| R2f | Beaverdams Rd) | Evening | 30 | No | 50 | D | Yes | 649394 | 4773728 | 4.5 |
| | Beaverdams (Ra) | Nighttime | 30 | No | 45 | | Yes | | | |
| P 20 | Outdoor area of dwelling (9722 | Daytime | 43 | No | 50 | р | Yes | 6/0301 | 1773608 | 1.5 |
| 1120 | Beaverdams Rd) | Evening | 28 | No | 45 | Б | Yes | 047371 | 4//3098 | 1.5 |
| | Econdo of dwalling (0602 | Daytime | 48 | No | 50 | | Yes | | | |
| R3f | Beaverdams Rd) | Evening | 32 | No | 50 | D | Yes | 649571 | 4773645 | 4.5 |
| | Beaverdanis (Cu) | Nighttime | 32 | No | 45 | | Yes | | | |
| P20 | Outdoor area of dwelling (9602 | Daytime | 43 | No | 50 | р | Yes | 640552 | 4772620 | 1.5 |
| 1050 | Beaverdams Rd) | Evening | 27 | No | 45 | Б | Yes | 047555 | 4773020 | 1.5 |
| | E 4 f day 11: (5594 | Daytime | 49 | No | 50 | | Yes | | | |
| R4f | Beechwood Rd) | Evening | 32 | No | 50 | D | Yes | 649611 | 4772698 | 4.5 |
| | Decenwood Ruj | Nighttime | 32 | No | 45 | | Yes | | | |
| P 4o | Outdoor area of dwelling (5584 | Daytime | 43 | No | 50 | D | Yes | 640504 | דרדרדה | 1.5 |
| K40 | Beechwood Rd) | Evening | 27 | No | 45 | D | Yes | 049394 | 4//2/2/ | 1.5 |
| | $E_{1} = \frac{1}{2} \int dx $ | Daytime | 45 | No | 50 | | Yes | | | |
| R5f | Beechwood Rd) | Evening | 31 | No | 50 | D | Yes | 649553 | 4772408 | 4.5 |
| | Beeenwood Ruj | Nighttime | 31 | No | 45 | | Yes | | | |
| P 50 | Outdoor area of dwelling (5769 | Daytime | 43 | No | 50 | р | Yes | 640532 | 1772120 | 1.5 |
| 100 | Beechwood Rd) | Evening | 26 | No | 45 | Б | Yes | 049332 | 7//2729 | 1.5 |
| | Erede of the line (0044 Long total | Daytime | 40 | No | 50 | | Yes | | | |
| R6f | Facade of dweining (9944 Lundy's | Evening | 24 | No | 50 | D | Yes | 649084 | 4771672 | 4.5 |
| | Liij | Nighttime | 24 | No | 45 | | Yes | | | |
| D 6a | Outdoor area of dwelling (9944 | Daytime | 39 | No | 50 | D | Yes | 640070 | 4771602 | 1.5 |
| K00 | Lundy's Ln) | Evening | 23 | No | 45 | D | Ves | 049070 | 4//1093 | 1.5 |

Table 3d: Acoustic Assessment Summary, Proposed Phase 3A Upper's Quarry, 1603157

Notes to Table:

- "Table A3" in Appendix A of Basic CCofA Guide.

1. "Continuous" noise sources includes sum of steady, quasi-steady impulsive, tonal, cyclical and buzzing noise sources, with appropriate penalties applied, in accordance with documents NPC-104 and NPC-300. Impulsive and emergency noise sources are assessed separately from continuous noise sources.

2. Daytime occurs from 0700-1900h. Evening occurs from 1900h-2300h. Nighttime occurs from 2300-0700h.

3. Worst-case cumulative sound level from all applicable sources operating.

4. Has an acoustic audit (as defined in Publication NPC-233) been conducted with source in place and operating?

5. Applicable worst-case NPC-300 sound level limit.

6. Performance limit (aka guideline limit) based on following:

- C = Calculated based on road traffic volumes in compliance with NPC-206 requirements.

- M = Measured based on monitoring for a minimum 48 hour period, in accordance with NPC-233 requirements.

- D = Default guideline minima per NPC-300.

| Point of Reception ID | Point of Reception Description | Time Period | Total Sound Level at PoR ^[3] | Verified by Acoustic Audit ^[4] | Performance Limit ^[5] | Peformance Limit Source [6] | Compliance with Performance Limit | UTM Co (Zono | oordinate e 17N) | Height Relative to Local Grade |
|-----------------------------|---------------------------------|-------------|---|---|-------------------------------------|-----------------------------------|--|-----------------|---------------------|--------------------------------------|
| | | | (dBA) | (Yes/No) | (dBA) | (C / M/ D) | (Yes/No) | X (m) | Y (m) | (m) |
| | Econdo of dyvalling (10149 | Daytime | 47 | No | 50 | | Yes | | | |
| R1f | Beaverdams Rd) | Evening | 38 | No | 50 | D | Yes | 648766 | 4773660 | 4.5 |
| | | Nighttime | 38 | No | 45 | | Yes | | | |
| R1o | Outdoor area of dwelling (10148 | Daytime | 47 | No | 50 | п | Yes | 648766 | 4773629 | 1.5 |
| RIU | Beaverdams Rd) | Evening | 36 | No | 45 | D | Yes | 040700 | 4//3027 | 1.5 |
| | Facade of dwelling (9722 | Daytime | 43 | No | 50 | | Yes | | | |
| R2f | Beaverdams Rd) | Evening | 36 | No | 50 | D | Yes | 649394 | 4773728 | 4.5 |
| | | Nighttime | 36 | No | 45 | | Yes | | | |
| R20 | Outdoor area of dwelling (9722 | Daytime | 42 | No | 50 | D | Yes | 649391 | 4773698 | 1.5 |
| 1620 | Beaverdams Rd) | Evening | 33 | No | 45 | D | Yes | 019391 | 1//5050 | 1.5 |
| | Eacade of dwelling (9602 | Daytime | 45 | No | 50 | | Yes | | | |
| R3f | Beaverdams Rd) | Evening | 35 | No | 50 | D | Yes | 649571 | 4773645 | 4.5 |
| | | Nighttime | 35 | No | 45 | | Yes | | | |
| R30 | Outdoor area of dwelling (9602 | Daytime | 44 | No | 50 | п | Yes | 649553 | 4773620 | 1.5 |
| 1050 | Beaverdams Rd) | Evening | 31 | No | 45 | D | Yes | 047555 | 4775020 | 1.5 |
| | Feedda of dwelling (5584 | Daytime | 47 | No | 50 | | Yes | | | |
| R4f | Beechwood Rd) | Evening | 35 | No | 50 | D | Yes | 649611 | 4772698 | 4.5 |
| | Becchwood Rdy | Nighttime | 35 | No | 45 | | Yes | | | |
| R40 | Outdoor area of dwelling (5584 | Daytime | 43 | No | 50 | п | Yes | 649594 | 4772727 | 1.5 |
| 1(40 | Beechwood Rd) | Evening | 33 | No | 45 | D | Yes | 047574 | 4//2/2/ | 1.5 |
| | Feedda of dwelling (5760 | Daytime | 44 | No | 50 | | Yes | | | |
| R5f | Beechwood Rd) | Evening | 35 | No | 50 | D | Yes | 649553 | 4772408 | 4.5 |
| | | Nighttime | 35 | No | 45 | | Yes | | | |
| R50 | Outdoor area of dwelling (5769 | Daytime | 42 | No | 50 | п | Yes | 649532 | 4772429 | 1.5 |
| 100 | Beechwood Rd) | Evening | 34 | No | 45 | D | Yes | 047552 | 4//242) | 1.5 |
| | Facedo of dwalling (0044 Lundwa | Daytime | 40 | No | 50 | | Yes | | | |
| R6f | I n) | Evening | 34 | No | 50 | D | Yes | 649084 | 4771672 | 4.5 |
| | | Nighttime | 34 | No | 45 | | Yes | | | |
| P 60 | Outdoor area of dwelling (9944 | Daytime | 38 | No | 50 | | Yes | 640070 | 4771602 | 1.5 |
| KUU | Lundy's Ln) | Evening | 33 | No | 45 | | Ves | 049070 | 7/1095 | 1.5 |

Table 3e: Acoustic Assessment Summary, Proposed Phase 3B Northeast Upper's Quarry, 1603157

Notes to Table:

- "Table A3" in Appendix A of Basic CCofA Guide.

1. "Continuous" noise sources includes sum of steady, quasi-steady impulsive, tonal, cyclical and buzzing noise sources, with appropriate penalties applied, in accordance with documents NPC-104 and NPC-300. Impulsive and emergency noise sources are assessed separately from continuous noise sources.

2. Daytime occurs from 0700-1900h. Evening occurs from 1900h-2300h. Nighttime occurs from 2300-0700h.

3. Worst-case cumulative sound level from all applicable sources operating.

4. Has an acoustic audit (as defined in Publication NPC-233) been conducted with source in place and operating?

5. Applicable worst-case NPC-300 sound level limit.

6. Performance limit (aka guideline limit) based on following:

- C = Calculated based on road traffic volumes in compliance with NPC-206 requirements.

- M = Measured based on monitoring for a minimum 48 hour period, in accordance with NPC-233 requirements.

- D = Default guideline minima per NPC-300.

| Point of Reception ID | Point of Reception Description | Time Period | Total Sound Level at PoR ^[3] | Verified by Acoustic Audit ^[4] | Performance Limit ^[5] | Peformance Limit Source [6] | Compliance with Performance Limit | UTM Co (Zono | oordinate e 17N) | Height Relative to Local Grade |
|-----------------------------|--|-------------|---|---|-------------------------------------|-----------------------------------|--|-----------------|---------------------|--------------------------------------|
| | | | (dBA) | (Yes/No) | (dBA) | (C / M/ D) | (Yes/No) | X (m) | Y (m) | (m) |
| | Foodo of dwalling (10148 | Daytime | 46 | No | 50 | | Yes | | | |
| R1f | Beaverdams Rd) | Evening | 38 | No | 50 | D | Yes | 648766 | 4773660 | 4.5 |
| | | Nighttime | 38 | No | 45 | | Yes | | | |
| P1o | Outdoor area of dwelling (10148 | Daytime | 44 | No | 50 | р | Yes | 648766 | 1773620 | 1.5 |
| RIU | Beaverdams Rd) | Evening | 37 | No | 45 | Ъ | Yes | 048700 | 4773029 | 1.5 |
| | Econdo of dwalling (0722 | Daytime | 47 | No | 50 | | Yes | | | |
| R2f | Beaverdams Rd) | Evening | 38 | No | 50 | D | Yes | 649394 | 4773728 | 4.5 |
| | Beaverdanis Rdy | Nighttime | 38 | No | 45 | | Yes | | | |
| D 20 | Outdoor area of dwelling (9722 | Daytime | 45 | No | 50 | р | Yes | 640201 | 1772608 | 1.5 |
| K20 | Beaverdams Rd) | Evening | 35 | No | 45 | D | Yes | 049391 | 4//3098 | 1.5 |
| | | Daytime | 48 | No | 50 | | Yes | | | |
| R3f | Facade of dwelling (9602 Beaverdams Rd) | Evening | 38 | No | 50 | D | Yes | 649571 | 4773645 | 4.5 |
| | Beaverdanis Rdy | Nighttime | 38 | No | 45 | | Yes | | | |
| P20 | Outdoor area of dwelling (9602 | Daytime | 47 | No | 50 | D | Yes | 640552 | 4772620 | 1.5 |
| K30 | Beaverdams Rd) | Evening | 35 | No | 45 | D | Yes | 049333 | 4773020 | 1.5 |
| | E | Daytime | 49 | No | 50 | | Yes | | | |
| R4f | Reechwood Rd) | Evening | 41 | No | 50 | D | Yes | 649611 | 4772698 | 4.5 |
| | Beeenwood Ruj | Nighttime | 41 | No | 45 | | Yes | | | |
| P 4o | Outdoor area of dwelling (5584 | Daytime | 45 | No | 50 | D | Yes | 640504 | דרדרדא | 1.5 |
| K40 | Beechwood Rd) | Evening | 39 | No | 45 | D | Yes | 049394 | 4//2/2/ | 1.5 |
| | $\mathbf{E}_{\mathbf{r}} = \mathbf{f}_{\mathbf{r}} + $ | Daytime | 46 | No | 50 | | Yes | | | |
| R5f | Beechwood Rd) | Evening | 39 | No | 50 | D | Yes | 649553 | 4772408 | 4.5 |
| | Becchwood Ruy | Nighttime | 39 | No | 45 | | Yes | | | |
| P50 | Outdoor area of dwelling (5769 | Daytime | 43 | No | 50 | D | Yes | 640522 | 4772420 | 1.5 |
| K30 | Beechwood Rd) | Evening | 38 | No | 45 | D | Yes | 049332 | 4//2429 | 1.5 |
| | | Daytime | 41 | No | 50 | | Yes | | | |
| R6f | racade of dwelling (9944 Lundy's | Evening | 36 | No | 50 | D | Yes | 649084 | 4771672 | 4.5 |
| | Liij | Nighttime | 36 | No | 45 | | Yes | | | |
| D 6a | Outdoor area of dwelling (9944 | Daytime | 39 | No | 50 | D | Yes | 640070 | 4771602 | 1.5 |
| K00 | Lundy's Ln) | Evening | 34 | No | 45 | D | Ves | 049070 | 4//1093 | 1.5 |

Table 3f: Acoustic Assessment Summary, Proposed Phase 4 Southeast Upper's Quarry, 1603157

Notes to Table:

- "Table A3" in Appendix A of Basic CCofA Guide.

1. "Continuous" noise sources includes sum of steady, quasi-steady impulsive, tonal, cyclical and buzzing noise sources, with appropriate penalties applied, in accordance with documents NPC-104 and NPC-300. Impulsive and emergency noise sources are assessed separately from continuous noise sources.

2. Daytime occurs from 0700-1900h. Evening occurs from 1900h-2300h. Nighttime occurs from 2300-0700h.

3. Worst-case cumulative sound level from all applicable sources operating.

4. Has an acoustic audit (as defined in Publication NPC-233) been conducted with source in place and operating?

5. Applicable worst-case NPC-300 sound level limit.

6. Performance limit (aka guideline limit) based on following:

- C = Calculated based on road traffic volumes in compliance with NPC-206 requirements.

- M = Measured based on monitoring for a minimum 48 hour period, in accordance with NPC-233 requirements.

- D = Default guideline minima per NPC-300.

| Point of Reception ID | Point of Reception Description | Time Period | Total Sound Level at PoR ^[3] | Verified by Acoustic Audit ^[4] | Performance Limit ^[5] | Peformance Limit Source [6] | Compliance with Performance Limit | UTM Co (Zone | oordinate e 17N) | Height Relative to Local Grade |
|-----------------------------|--|-------------|---|---|-------------------------------------|-----------------------------------|--|-----------------|---------------------|--------------------------------------|
| | | | (dBA) | (Yes/No) | (dBA) | (C / M/ D) | (Yes/No) | X (m) | Y (m) | (m) |
| | Econdo of dwalling (10148 | Daytime | 45 | No | 50 | | Yes | | | |
| R1f | Beaverdams Rd) | Evening | 38 | No | 50 | D | Yes | 648766 | 4773660 | 4.5 |
| | | Nighttime | 38 | No | 45 | | Yes | | | |
| R1o | Outdoor area of dwelling (10148 | Daytime | 43 | No | 50 | п | Yes | 648766 | 4773629 | 1.5 |
| RIU | Beaverdams Rd) | Evening | 36 | No | 45 | Б | Yes | 040700 | 4775027 | 1.5 |
| | Facade of dwelling (9722 | Daytime | 46 | No | 50 | | Yes | | | |
| R2f | Beaverdams Rd) | Evening | 37 | No | 50 | D | Yes | 649394 | 4773728 | 4.5 |
| | Beuverdams (cd) | Nighttime | 37 | No | 45 | | Yes | | | |
| R20 | Outdoor area of dwelling (9722 | Daytime | 39 | No | 50 | п | Yes | 649391 | 4773698 | 1.5 |
| 1(20 | Beaverdams Rd) | Evening | 33 | No | 45 | Ь | Yes | 047571 | 4//50/0 | 1.5 |
| | Feeda of dwelling (0602 | Daytime | 46 | No | 50 | | Yes | | | |
| R3f | Beaverdams Rd) | Evening | 37 | No | 50 | D | Yes | 649571 | 4773645 | 4.5 |
| | Beaverdanis (Cd) | Nighttime | 37 | No | 45 | | Yes | | | |
| P 30 | Outdoor area of dwelling (9602 | Daytime | 40 | No | 50 | р | Yes | 640553 | 4773620 | 1.5 |
| K30 | Beaverdams Rd) | Evening | 33 | No | 45 | D | Yes | 049333 | 4773020 | 1.5 |
| | E | Daytime | 49 | No | 50 | | Yes | | | |
| R4f | Reechwood Rd) | Evening | 41 | No | 50 | D | Yes | 649611 | 4772698 | 4.5 |
| | Becchwood Ruy | Nighttime | 41 | No | 45 | | Yes | | | |
| P 4o | Outdoor area of dwelling (5584 | Daytime | 48 | No | 50 | П | Yes | 640504 | 1777777 | 1.5 |
| IC+0 | Beechwood Rd) | Evening | 40 | No | 45 | Б | Yes | 047574 | -1/2/2/ | 1.5 |
| | $\mathbf{E}_{\mathbf{r}} = \mathbf{f}_{\mathbf{r}} + $ | Daytime | 46 | No | 50 | | Yes | | | |
| R5f | Beechwood Rd) | Evening | 40 | No | 50 | D | Yes | 649553 | 4772408 | 4.5 |
| | Becchwood Ray | Nighttime | 40 | No | 45 | | Yes | | | |
| P 50 | Outdoor area of dwelling (5769 | Daytime | 44 | No | 50 | D | Yes | 640532 | 1772120 | 1.5 |
| 100 | Beechwood Rd) | Evening | 39 | No | 45 | Ъ | Yes | 047552 | 7//2429 | 1.5 |
| | Econdo of dwalling (0044 Lundrig | Daytime | 40 | No | 50 | | Yes | | | |
| R6f | I n) | Evening | 36 | No | 50 | D | Yes | 649084 | 4771672 | 4.5 |
| | Liij | Nighttime | 36 | No | 45 | | Yes | | | |
| D 6a | Outdoor area of dwelling (9944 | Daytime | 39 | No | 50 | D | Yes | 640070 | 4771602 | 1.5 |
| K00 | Lundy's Ln) | Evening | 34 | No | 45 | | Ves | 049070 | 4//1093 | 1.5 |

Table 3g: Acoustic Assessment Summary, Proposed Phase 5 East Upper's Quarry, 1603157

Notes to Table:

- "Table A3" in Appendix A of Basic CCofA Guide.

1. "Continuous" noise sources includes sum of steady, quasi-steady impulsive, tonal, cyclical and buzzing noise sources, with appropriate penalties applied, in accordance with documents NPC-104 and NPC-300. Impulsive and emergency noise sources are assessed separately from continuous noise sources.

2. Daytime occurs from 0700-1900h. Evening occurs from 1900h-2300h. Nighttime occurs from 2300-0700h.

3. Worst-case cumulative sound level from all applicable sources operating.

4. Has an acoustic audit (as defined in Publication NPC-233) been conducted with source in place and operating?

5. Applicable worst-case NPC-300 sound level limit.

6. Performance limit (aka guideline limit) based on following:

- C = Calculated based on road traffic volumes in compliance with NPC-206 requirements.

- M = Measured based on monitoring for a minimum 48 hour period, in accordance with NPC-233 requirements.

- D = Default guideline minima per NPC-300.

| Point of Reception ID | Point of Reception Description | Time Period | Total Sound Level at PoR ^[3] | Verified by Acoustic Audit ^[4] | Performance Limit ^[5] | Peformance Limit Source [6] | Compliance with Performance Limit | UTM Co (Zone | oordinate e 17N) | Height Relative to Local Grade |
|-----------------------------|---|-------------|---|---|-------------------------------------|-----------------------------------|--|-----------------|---------------------|--------------------------------------|
| | | | (dBA) | (Yes/No) | (dBA) | (C / M/ D) | (Yes/No) | X (m) | Y (m) | (m) |
| | Econdo of dwalling (10149 | Daytime | 41 | No | 50 | | Yes | | | |
| R1f | Beaverdams Rd) | Evening | 38 | No | 50 | D | Yes | 648766 | 4773660 | 4.5 |
| | Beaverdams reaj | Nighttime | 38 | No | 45 | | Yes | | | |
| P1o | Outdoor area of dwelling (10148 | Daytime | 40 | No | 50 | р | Yes | 648766 | 1773620 | 1.5 |
| KIU | Beaverdams Rd) | Evening | 36 | No | 45 | D | Yes | 048700 | 4773029 | 1.5 |
| | Econdo of dwalling (0722 | Daytime | 42 | No | 50 | | Yes | | | |
| R2f | Beaverdams Rd) | Evening | 37 | No | 50 | D | Yes | 649394 | 4773728 | 4.5 |
| | Beaverdains Rdy | Nighttime | 37 | No | 45 | | Yes | | | |
| D2. | Outdoor area of dwelling (9722 | Daytime | 36 | No | 50 | D | Yes | 640201 | 4772608 | 1.5 |
| K20 | Beaverdams Rd) | Evening | 33 | No | 45 | D | Yes | 049391 | 4//3098 | 1.5 |
| | | Daytime | 43 | No | 50 | | Yes | | | |
| R3f | Facade of dwelling (9602 | Evening | 37 | No | 50 | D | Yes | 649571 | 4773645 | 4.5 |
| | Beaveruanis Ru) | Nighttime | 37 | No | 45 | | Yes | | | |
| D2. | Outdoor area of dwelling (9602 | Daytime | 36 | No | 50 | D | Yes | 640552 | 4772620 | 1.5 |
| K30 | Beaverdams Rd) | Evening | 33 | No | 45 | D | Yes | 049555 | 4//3620 | 1.5 |
| | F 1 6 1 11: (5504 | Daytime | 47 | No | 50 | | Yes | | | |
| R4f | Facade of dwelling (5584 | Evening | 41 | No | 50 | D | Yes | 649611 | 4772698 | 4.5 |
| | Beechwood Ru) | Nighttime | 41 | No | 45 | | Yes | | | |
| D.4 | Outdoor area of dwelling (5584 | Daytime | 45 | No | 50 | D | Yes | (40504 | 4770707 | 1.5 |
| K40 | Beechwood Rd) | Evening | 40 | No | 45 | D | Yes | 049394 | 4//2/2/ | 1.5 |
| | E 1 6 1 11: (5560 | Daytime | 43 | No | 50 | | Yes | | | |
| R5f | Facade of dwelling (5/69 Reachwood Pd) | Evening | 40 | No | 50 | D | Yes | 649553 | 4772408 | 4.5 |
| | Beechwood Rd) | Nighttime | 40 | No | 45 | | Yes | | | |
| D.5 - | Outdoor area of dwelling (5769 | Daytime | 42 | No | 50 | D | Yes | (40522 | 4772420 | 1.5 |
| К30 | Beechwood Rd) | Evening | 39 | No | 45 | D | Yes | 049552 | 4//2429 | 1.5 |
| | E 1 61 11: (00441 11 | Daytime | 40 | No | 50 | | Yes | | | |
| R6f | Facade of dwelling (9944 Lundy's | Evening | 36 | No | 50 | D | Yes | 649084 | 4771672 | 4.5 |
| | Lii) | Nighttime | 36 | No | 45 | | Yes | | | |
| D.C. | Outdoor area of dwelling (9944 | Daytime | 38 | No | 50 | P | Yes | (40070 | 4771 (02 | 1.5 |
| K60 | Lundy's Ln) | Evening | 34 | No | 45 | D | Ves | 649070 | 47/1693 | 1.5 |

Table 3h: Acoustic Assessment Summary, Proposed Scenario Impulsive Source Upper's Quarry, 1603157

Notes to Table:

6.

- "Table A3" in Appendix A of Basic CCofA Guide.
- 1. Impulsive noise sources are assessed separately from continuous noise sources.
- 2. Daytime occurs from 0700-1900h. Evening occurs from 1900h-2300h. Nighttime occurs from 2300-0700h.
- 3. Worst-case cumulative sound level from all applicable sources operating.
- 4. Has an acoustic audit (as defined in Publication NPC-233) been conducted with source in place and operating?
- 5. Applicable worst-case NPC-300 sound level limit, based on more than 9 impulses per hour in a Class 2 area.

Performance limit (aka guideline limit) based on following:

- C = Calculated based on road traffic volumes in compliance with NPC-206 requirements.
- M = Measured based on monitoring for a minimum 48 hour period, in accordance with NPC-233 requirements.

- D = Default guideline minima per NPC-300.

| Point of Reception ID | Point of Reception Description | Time Period | Total Sound Level at PoR ^[3] | Verified by Acoustic Audit ^[4] | Performance Limit ^[5] | Peformance Limit Source [6] | Compliance with Performance Limit | UTM Co (Zono | oordinate e 17N) | Height Relative to Local Grade |
|-----------------------------|----------------------------------|-------------|---|---|-------------------------------------|-----------------------------------|--|-----------------|---------------------|--------------------------------------|
| | | | (dBA) | (Yes/No) | (dBA) | (C / M/ D) | (Yes/No) | X (m) | Y (m) | (m) |
| | Econdo of dwelling (10148 | Daytime | 39 | No | 50 | | Yes | | | |
| R1f | Beaverdams Rd) | Evening | 39 | No | 50 | D | Yes | 648766 | 4773660 | 4.5 |
| | Bouveroumbredy | Nighttime | 39 | No | 45 | | Yes | | | |
| R1o | Outdoor area of dwelling (10148 | Daytime | 38 | No | 50 | Б | Yes | 648766 | 4773629 | 1.5 |
| RIU | Beaverdams Rd) | Evening | 38 | No | 45 | D | Yes | 040700 | 4775027 | 1.5 |
| | Econdo of dwalling (0722 | Daytime | 38 | No | 50 | | Yes | | | |
| R2f | Beaverdams Rd) | Evening | 38 | No | 50 | D | Yes | 649394 | 4773728 | 4.5 |
| | Bouveroumbredy | Nighttime | 38 | No | 45 | | Yes | | | |
| P 20 | Outdoor area of dwelling (9722 | Daytime | 36 | No | 50 | D | Yes | 6/0301 | 1773608 | 1.5 |
| 1120 | Beaverdams Rd) | Evening | 36 | No | 45 | D | Yes | 049391 | 4//3098 | 1.5 |
| | Econdo of dwalling (0602 | Daytime | 38 | No | 50 | | Yes | | | |
| R3f | Beaverdams Rd) | Evening | 38 | No | 50 | D | Yes | 649571 | 4773645 | 4.5 |
| | Bouveroumbredy | Nighttime | 38 | No | 45 | | Yes | | | |
| R30 | Outdoor area of dwelling (9602 | Daytime | 36 | No | 50 | р | Yes | 649553 | 4773620 | 1.5 |
| 1050 | Beaverdams Rd) | Evening | 36 | No | 45 | D | Yes | 047555 | 4773020 | 1.5 |
| | Econdo of dwalling (5584 | Daytime | 42 | No | 50 | | Yes | | | |
| R4f | Beechwood Rd) | Evening | 42 | No | 50 | D | Yes | 649611 | 4772698 | 4.5 |
| | Decenwood Ray | Nighttime | 42 | No | 45 | | Yes | | | |
| R40 | Outdoor area of dwelling (5584 | Daytime | 43 | No | 50 | Б | Yes | 649594 | 4772727 | 1.5 |
| 1(+0 | Beechwood Rd) | Evening | 43 | No | 45 | D | Yes | 047574 | 4//2/2/ | 1.5 |
| | Econdo of dwalling (5760 | Daytime | 41 | No | 50 | | Yes | | | |
| R5f | Beechwood Rd) | Evening | 41 | No | 50 | D | Yes | 649553 | 4772408 | 4.5 |
| | Decenwood Ray | Nighttime | 41 | No | 45 | | Yes | | | |
| R50 | Outdoor area of dwelling (5769 | Daytime | 41 | No | 50 | Б | Yes | 649532 | 4772429 | 1.5 |
| 100 | Beechwood Rd) | Evening | 41 | No | 45 | D | Yes | 047552 | 4/7242) | 1.5 |
| | Facada of dwalling (0044 Lundy's | Daytime | 35 | No | 50 | | Yes | | | |
| R6f | Ln) | Evening | 35 | No | 50 | D | Yes | 649084 | 4771672 | 4.5 |
| | | Nighttime | 35 | No | 45 | | Yes | | | |
| R6o | Outdoor area of dwelling (9944 | Daytime | 35 | No | 50 | D | Yes | 649070 | 4771693 | 1.5 |
| KUU | Lundy's Ln) | Evening | 35 | No | 45 | | Yes | 0,04 | 4//10/5 | 1.5 |

Assessment of Impacts for "Impulsive" Noise Sources [1]



FIGURES




















































APPENDIX A











SECTION 3 - ZONES

- 3.1 CLASSIFICATION OF ZONES: For the purpose of this By-law, the following defined areas of the City of Niagara Falls, namely:
 - (a) all of the former Village of Chippawa, and
 - (b) all of the remaining part of the City of Niagara Falls lying north of the middle of the main channel of the Welland River are hereby divided into the following zones, which are hereby established and the lands included in each zone are shown on the Zoning Maps appended hereto as Schedule "A".

| ZONES | SHORT TITLES |
|---|--------------|
| Residential 1A Density Zone | R1A |
| Residential 1B Density Zone | R1B |
| Residential 1C Density Zone | R1C |
| Residential 1D Density Zone | R1D |
| Residential 1E Density Zone | R1E |
| Residential 1F Density Zone | R1F |
| Residential Mobile Home Park Zone | RMP |
| Residential Two Zone | R2 |
| Residential Mixed Zone | R3 |
| Residential Low Density, Group Multiple Dwelling Zone | R4 |
| Residential Apartment 5A Density Zone | R5A |
| Residential Apartment 5B Density Zone | R5B |
| Residential Apartment 5C Density Zone | R5C |
| Residential Apartment 5D Density Zone | R5D |
| Residential Apartment 5E Density Zone | R5E |
| Residential Apartment 5F Density Zone | R5F |

| ZONES | SHORT TITLES |
|--|--------------|
| Transition Residential Multiple Zone | TRM |
| Neighbourhood Commercial Zone | NC |
| General Commercial Zone | GC |
| Deferred Commercial Zone | DC |
| Planned Shopping Centre Commercial Zone | SC |
| Central Business Commercial Zone | СВ |
| Tourist Commercial Zone | ТС |
| Camping Establishment Zone | CE |
| Deferred Tourist Commercial Zone | DTC |
| Automobile Service Station and Gasoline Bar Zone | AS |
| Institutional Zone | 1 |
| Prestige Industrial Zone | PI |
| Light Industrial Zone | LI |
| General Industrial Zone | GI |
| Heavy Industrial Zone | HI |
| Transportation - Distribution Industrial Zone | TDI |
| Extractive Industrial Zone | El |
| Agricultural Zone | A |
| Rural Zone | R |
| Open Space Zone | OS |
| Development Holding Zone | DH |
| Hazard Land Zone | HL |

| ZONES | SHORT TITLES |
|------------------------------------|--------------|
| Parking Zone | Р |
| Parking Holding Zone | PH |
| Environmental Protection Area Zone | EPA |

- 3.2 ZONING MAPS: The Zones aforesaid and the boundaries of such Zones are shown on one or more of the Zoning Maps appended thereto as Schedule "A", referred to in this Bylaw as "Zoning Maps", each of which Zoning Maps and the Key Map contained in the said Schedule "A" and the Setback Plans appended hereto as Schedules "B-1", "B-2", "B-3" and "B-4", Schedule "C" and Schedules "C-A" through to and including "C-F" and Schedules "C-H" through to and including "C-K", and Schedule "D" together with all titles, symbols, notations, references and information shown therein shall form a part of this bylaw to the same extent as if fully described in the text of this By-law." (2004-14, 2012-60)
- 3.3 SHORT TITLES: The short titles of the Zones listed in Section 3.1 may be used to refer to buildings and structures and uses of buildings, structures and land permitted by this Bylaw in such Zones; and whenever in this By-law the word "Zone" is used preceded by any of the said short titles, such references shall mean any area of the City of Niagara Falls delineated and designated on the said Zoning Maps by such short title.
- 3.3.1 "RESIDENTIAL ZONE": The expression "residential zone", whenever used in this By-law, means an area of the City of Niagara Falls delineated on a Zoning Map and designated therein as R1A, R1B, R1C, R1D, R1E, R1F, RMP, R2, R3, R4, R5A, R5B, R5C, R5D, R5E, R5F or TRM.
- 3.3.2 "COMMERCIAL ZONE": The expression "commercial zone" whenever used in this Bylaw, means an area of the City of Niagara Falls delineated on a Zoning Map and designated therein as NC, GC, DC, SC, CB, TC, CE, DTC, AS, P or PH.
- 3.3.3. "INDUSTRIAL ZONE": The expression "industrial zone" whenever used in this By-law means an area of the City of Niagara Falls delineated on a Zoning Map and designated therein as PI, LI, GI, HI, TDI or EI.
- 3.4 ZONE BOUNDARIES: Where any uncertainty exists with respect to the boundary of any zone as shown on the Zoning Maps, the following rules shall apply:
 - (a) a boundary indicated as following a highway, street or lane shall be the centre line of such highway, street or lane;
 - (b) where a street or part of a street referred to in Section 4.27.1 of this By-law as a Type A, Type B, Type C, Type D, Type E or Transitional street.

(i) forms a boundary between zones, it is shown on the Zoning Maps by one or more of the respective symbols set forth in Column 2 of the following Table:

| Column 1 | Column 2 |
|----------------|-----------|
| Type of Street | Symbol |
| Туре А | (Green) |
| Туре В | (Salmon) |
| Туре С | (Magenta) |
| Туре D | (Cyan) |
| Туре Е | (Gold) |
| Transitional | (Red) |

(ii) does not form a boundary between zones, it is shown on the Zoning Maps by one or more of the respective symbols set forth in Column 2 of the following Table:

| Column 1 | Column 2 |
|----------------|-----------|
| Type of Street | Symbol |
| Туре А | (Green) |
| Туре В | (Salmon) |
| Туре С | (Magenta) |
| Туре D | (Cyan) |
| Туре Е | (Gold) |
| Transitional | (Red) |

- (c) generally, boundaries between zones are indicated either by an unbroken heavy line or by one or more of the symbols set forth in subclause I of clause b of this section.
- (d) a boundary indicated as following a watercourse, creek, stream, power canal, or the right-of-way of a railway or of an electrical, gas or oil transmission line shall be







Part 5 | Establishment of Zones

5.1 Establishment of Zones and Zone Symbols

This By-law establishes the following *zones*, and places all lands in the defined area into *zones*, which are defined in Table 5.1.

| Table 5.1: Establishment of Zones | | |
|---|-------------|--|
| Zone Name | Zone Symbol | |
| Residential Zones | | |
| Single Detached A | R1A | |
| Single Detached and Duplex B | R1B | |
| Single Detached and Duplex C | R1C | |
| Single Detached D | R1D | |
| Semi-detached A | R2A | |
| Semi-detached B | R2B | |
| Townhouse A | R3A | |
| Townhouse B | R3B | |
| Triplex and Fourplex | R3C | |
| Private Street Development | R3D | |
| Apartment and Long-term Care Facility A | R4A | |
| Apartment and Long-term Care Facility B | R4B | |
| Commercial Zones | | |
| Downtown Main Street | C1 | |
| Downtown Mixed Use | C2 | |
| General Commercial | C3 | |
| Neighbourhood Commercial | C4 | |
| Highway Commercial | C5 | |
| Mixed Use Commercial | C6 | |
| Employment Zones | | |
| Prestige Employment | M1 | |
| General Industrial | M2 | |
| Employment Mixed Use | M3 | |

| Table 5.1: Establishment of Zones | | |
|-----------------------------------|-------------|--|
| Zone Name | Zone Symbol | |
| Rural Industrial | M4 | |
| Agricultural & Rural Zones | | |
| Agricultural | A | |
| Specialty Crop | AS | |
| Rural | RU | |
| Community Zones | | |
| Major Institutional | l1 | |
| Minor Institutional | 12 | |
| Open Space – Parks and Recreation | OS1 | |
| Open Space - Conservation | OS2 | |
| Environmental Zones | | |
| Environmental Protection 1 | EP1 | |
| Environmental Protection 2 | EP2 | |
| Environmental Protection 3 | EP3 | |
| Other Zones | | |
| Future Development | FD | |
| Utility | U | |



APPENDIX B




B1.8.12 Land Use Compatibility

It is a requirement of this Plan that appropriate measures be undertaken to attenuate the effects of noise, visual intrusion or other undesirable impacts of residential development adjacent to Highways 58 and 20, Thorold Townline Road and other environmentally incompatible land uses.

B1.8.12.1 Residential Development Adjacent to Provincial Highways and Regional Arterial Roads

Where residential development is proposed to be located adjacent to Highway 58 and 20 three alternative design considerations can be utilized to achieve environmental compatibility:

- a) Acoustical barriers such as berms or walls; or
- b) Minimum building setbacks of 65 metres from Highway 20 and 85 metres from Highway 58; or
- c) Single loaded window streets with the dwelling units facing the highway.

For residential development within 250 metres of Highway 58 and 20 and 100 metres of Thorold Townline Road the developer shall be required to prepare a detailed noise study. A noise feasibility study is required within 50 metres of a provincial highway in accordance with Provincial Guideline NPC-300. The noise study shall include recommendations regarding noise attenuation measures which are required in order to satisfy Provincial sound level objectives. Noise attenuation measures may include but shall not be limited to the following:

- a) Sound proofing measures and construction techniques;
- b) Warning clauses; and,
- c) Equipping the dwelling units with air conditioning or special ventilation.

B1.8.12.2 Residential Development Adjacent to Stationary Noise Sources and Industrial Facilities

Located within the Blackhorse Community are a number of existing uses which are stationary noise sources and may therefore impact sensitive receptors. A noise study is required for residential uses and noise sensitive land uses, such as a daycare facility, institutional use, or hotel/motel, if these uses are to be located within:

- a) 300 metres of the commercial vehicle refuelling station; or,
- b) 70 metres of the natural gas metering facility.

The noise study shall include recommendations regarding noise attenuation measures which are required in order to satisfy Provincial sound level objectives.

When residential development is proposed adjacent to the natural gas metering facility a 20 metre separation distance is required measured from lot line to line.

- a) The utilization of window streets abutting the industrial area and the dwelling units having flanking yards;
- b) Sound proofing and construction techniques;
- c) Acoustical barriers such as berms or walls; and
- d) A forced air ventilation system with central air conditioning or some other form of mechanical ventilation.

B1.8.12.3 Aggregate Resource Protection Policies

The Ministry of Natural Resources and Forestry has identified lands east of Thorold Townline Road, north of the Hydro One corridor, as a potential bedrock resource area. Development applications within 500 metres of this potential bedrock resource area shall be reviewed having regard to this identified resource area and the need to demonstrate that future aggregate extraction will not be precluded or hindered and to achieve land use compatibility. Mitigation measures which shall be determined through appropriate studies prepared by the developer may be necessary and include but shall not be limited to the following:

- a) Building orientation;
- b) The utilization of window streets and dwelling units having flanking yards;
- c) Sound proofing and construction techniques;
- d) Increasing building setbacks or possibly the need for additional spatial separation; and

e) Landscape treatments.

In order to determine the necessary mitigation, the developer when proceeding before a quarry application shall be required to prepare the following studies assuming that a proposed quarry will be located on the east side of Thorold Townline Road:

- a) Operational noise;
- b) Blasting;
- c) Traffic; and,
- d) Any other technical report considered appropriate by Council.

The 500 metre study area is identified on Schedule A-3.

It shall also be recognized that Thorold Townline Road is a Regional arterial road and is the likely aggregate haul route required to serve any future aggregate extraction operation to the east. Accordingly, all studies required by any policy of this Plan shall recognize that Thorold Townline Road is a future aggregate haul route. The haul route shall be restricted from the future extraction operation entrance southerly to Highway 20, a major arterial.

Once the proponent has prepared the appropriate studies and the necessary mitigation is incorporated into the proposed development, if necessary, the utilization of such mitigation measures does not relieve the new mineral aggregate operation from providing appropriate setbacks and mitigation measures in order to achieve land use compatibility.

B1.8.12.4 Residential Development Adjacent to Thorold Townline Road

When residential development is proposed to be located adjacent to the Townline Road and the easterly located agricultural lands in the City of Niagara Falls consideration shall be given to utilizing design elements of dwelling orientation, window streets, increased building setbacks, and landscape treatments to achieve land use compatibility.

B1.8.13 Servicing and Transportation

B1.8.13.1 General

- a) All development within the Neighbourhoods of Rolling Meadows shall be developed with full municipal services in accordance with Municipal Policy.
- b) Extension of municipal services into the Neighbourhoods of Rolling will be required to service development.
- c) Easements to accommodate municipal services shall be granted as a condition of development approval.
- d) Easements to accommodate utilities shall be granted as a condition of development approval.
- e) The provision of a water distribution system, wastewater collection system, stormwater management facilities, road network, and other municipal services will be achieved with minimum costs to the City.
- f) In order to achieve the proper co-ordination of services and consistence in development standards, the orderly development of land by way of plan of subdivision and site plan will be required throughout the neighbourhood. Consents to sever land to create development blocks will only be permitted when it is determined to the satisfaction of the City that the severance of land will not prejudice or jeopardize the subsequent development of the balance of the lands.

B1.8.13.2 Infrastructure Improvements

In order to accommodate development within the Neighbourhoods of Rolling Meadows, it will be necessary to address off-site upgrading or expansion of infrastructure such as:

a) The extension of the Allanburg Road trunk sanitary sewer easterly to the



APPENDIX C



Table C.1: Key Parameters Included in the Cadna/A Noise Modelling Upper's Quarry, 1603157

| Parameter | Valua | Pationala |
|---|-------|--|
| 1 al allietei | value | Kauonaie |
| Ground Absorption, within extraction limit | 0.2 | Accounts for hard ground (exposed rock surfaces) within extraction limit |
| Ground Absorption, outside of extraction limit | 0.8 | Accounts for mostly soft ground outside of quarry extraction limit |
| Temperature | 10 °C | Ontario standard conditions |
| Relative Humidity | 70% | Ontario standard conditions |
| Max. Order of Reflection | 1 | 1st order reflection considered |
| Absorption Coefficient Alpha | 0.37 | Cadna/A default value for structured facade |

| Parameter | Unit | Definition |
|-----------|-------|---|
| Nr | | Ray Number |
| Х | (m) | X-axis Cartesian Coordinate |
| Y | (m) | Y-axis Cartesian Coordinate |
| Z | (m) | Z-axis Cartesian Coordinate |
| Refl. | order | Order of Reflection |
| DEN | D/E/N | Time of Day (Day, Evening, or Night) |
| Freq. | (Hz) | 1/1 Octave Band Dominant Frequency or Frequency Type ("A" for A-weighted) |
| Lw | (dBA) | Overall Sound Power Level |
| l/a | dB | Line/Area Source Correction |
| Optime | dB | Operating Time Correction |
| K0 | (dB) | D_omega in ISO 9613-2 (correction for radiation into solid angles less than 4 Pi) |
| Di | (dB) | Directivity Index |
| Adiv | (dB) | Attenuation Due to Divergence |
| Aatm | (dB) | Atmospheric Attenuation |
| Agr | (dB) | Ground Attenuation |
| Afol | (dB) | Attenuation Due to Foliage |
| Ahous | (dB) | Attenuation from Houses |
| Abar | (dB) | Barrier Attenuation |
| Cmet | (dB) | Meteorological Correction |
| RL | (dB) | Reflection Loss |
| Lr | (dBA) | Resulting Noise Impact at Receptor - Leq (1-Hr) |

Cadna/A ISO-9613 Calculation Protocol - Definitions

Sample CadnaA Output - Uppers Quarry - Proposed Phase 1A Sinking Cut

Receiver

Name: Facade of dwelling (5584 Beechwood Rd)

R4f ID:

X: Y: 649610.64 m 4772697.98 m

Z: 190.50 m

| | | Poir | t Source | a ISO | 9613 | Nam | e [.] "P14 | Sink | cut PP | oade | er" IF |) [.] "P1 | A Sink | cut | PP I | dr" | | | | |
|------|--------------|----------------|-----------|--------------------|----------|----------|---------------------|---------|------------|------------|--------------|--------------------|--------|------------|----------------|---------|--------|--------|------------|-------|
| Nr. | Х | Y | Z | Refl. | DEN | Frea. | Lw | | Optime | K0 | Di | Adiv | Aatm | Aar | Afol | Ahous | Abar | Cmet | RL | Lr |
| | (m) | (m) | (m) | | | (Hz) | dB(A) | dB | dB | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | dB(A) |
| 146 | 648801.86 | 4772799.02 | 179.50 | 0 | D | A | 105.6 | 0.0 | 0.0 | 0.0 | 0.0 | 69.2 | 5.1 | -1.7 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 33.0 |
| | | | | - | _ | | | | | | | | | | | | | | | |
| | F | Point Source, | ISO 961 | 3, Nai | me: "F | P1A_S | inkcut, | PC Pr | imary C | rushe | r", ID |): "P1A | _Sink | cut_F | PC_P | rimaryC | rush" | | | |
| Nr. | Х | Y | Z | Refl. | DEN | Freq. | Lw | l/a | Optime | K0 | Di | Adiv | Aatm | Agr | Afol | Ahous | Abar | Cmet | RL | Lr |
| | (m) | (m) | (m) | | | (Hz) | dB(A) | dB | dB | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | dB(A) |
| 147 | 648674.53 | 4772846.65 | 180.00 | 0 | D | A | 117.6 | 0.0 | 0.0 | 0.0 | 0.0 | 70.5 | 3.3 | -1.7 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 45.5 |
| | | | | | | | | | | | | | | | | | | | | |
| | Poi | nt Source, ISC | D 9613, I | Name | : "P1/ | A_Sink | cut, PF | P Seco | ndary C | rushe | r'', ID |): "P1A | Sink | cut_F | PP_S | econdar | yCrus | sh" | | |
| Nr. | X | Y | Z | Refl. | DEN | Freq. | Lw | l/a | Optime | K0 | Di | Adiv | Aatm | Agr | Afol | Ahous | Abar | Cmet | RL | Lr |
| | (m) | (m) | (m) | | _ | (Hz) | dB(A) | dB | dB | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | dB(A) |
| 148 | 648791.38 | 4772792.73 | 180.00 | 0 | D | A | 114.6 | 0.0 | 0.0 | 0.0 | 0.0 | 69.3 | 4.0 | -1.7 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 43.0 |
| | | Point S | | | 13 N | | | linkout | | a Tri | ick" | םיי יחו | 14 01 | nkout | | Trk2" | | | | |
| Nr | X | V | 7 | Refl | | Erea | 1.14_3 | | Ontime | | юк, Пі | Δdiv | ∆_31m | Δar | | | Ahar | Cmet | RI | Ir |
| INI. | (m) | (m) | (m) | rten. | DLIN | (Hz) | | dB | dB | (dB) | | (dB) | (dB) | (dB) | | (dB) | (dB) | (dB) | (dB) | |
| 149 | 648806.63 | 4772810.88 | 180.00 | 0 | П | | 96.3 | 0.0 | 0.0 | | | (GD) 60.2 | 3.8 | -1.8 | | | | | | 25.1 |
| 145 | 040000.00 | 4772010.00 | 100.00 | 0 | 0 | | 00.0 | 0.0 | 0.0 | 0.0 | 0.0 | 05.2 | 0.0 | -1.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 20.1 |
| | | Point S | ource, Is | SO 96 | 13, N | ame: ' | 'P1A S | Sinkcut | , PP Idlii | ng Tru | ıck", | ID: "P | 1A Si | nkcut | t PP | Trk1" | | | | |
| Nr. | Х | Y | Z | Refl. | DEN | Freq. | Lw | l/a | Optime | K0 | Di | Adiv | Aatm | Agr | Afol | Ahous | Abar | Cmet | RL | Lr |
| | (m) | (m) | (m) | | | (Hz) | dB(A) | dB | dB | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | dB(A) |
| 150 | 648804.44 | 4772810.35 | 180.00 | 0 | D | Á | 96.3 | 0.0 | 0.0 | 0.0 | 0.0 | 69.2 | 3.8 | -1.8 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 25.0 |
| | | | | | | | | | | | | 1 | 1 | 1 | 1 | | 1 | 1 | | |
| | Point Source | , ISO 9613, N | lame: "P | 1A_S | inkcut | , PP S | Second | ary & T | Fertiary S | Scree | n", IC |): "P1/ | A_Sink | cut_ | PP_S | econda | ryTert | iarySc | reen" | |
| Nr. | Х | Y | Z | Refl. | DEN | Freq. | Lw | l/a | Optime | K0 | Di | Adiv | Aatm | Agr | Afol | Ahous | Abar | Cmet | RL | Lr |
| | (m) | (m) | (m) | | | (Hz) | dB(A) | dB | dB | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | dB(A) |
| 152 | 648792.65 | 4772791.54 | 180.00 | 0 | D | A | 113.8 | 0.0 | 0.0 | 0.0 | 0.0 | 69.3 | 4.1 | -1.6 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 42.0 |
| | | Delint Course | 00.004 | 0 N | | 14 0 | inter de | | | | | | Cinka | | <u>с р.:</u> : | | | | | |
| Nin | F | Point Source, | 150 961 | 3, Nai | | 1A_5 | INKCUT, | PC Pr | Imary So | creen | , ID: | PIA | _SINKC | ut_P | C_Pri | marySc | reen | Creat | | 1 |
| Nr. | X (m) | Y (mr.) | <u> </u> | Refi. | DEN | Freq. | | i/a | Optime | KU (dD) | | | Aatm | Agr | | Anous | Abar | Cmet | | |
| 450 | (m) | (m) | (m) | 0 | D | (HZ) | | aB | dB | (aB) | | | | (aB) | | | | | | 40 7 |
| 150 | 048075.85 | 4772845.10 | 180.00 | 0 | U | A | 113.8 | 0.0 | 0.0 | 0.0 | 0.0 | 70.5 | 4.5 | -1.9 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 40.7 |
| | Point S | Source ISO 9 | 613 Nai | ne [.] "F | 21A S | Sinkcut | t PC lo | ader d | lumping | into c | rushe | er" ID | · "P1A | Sinl | cut I | PC Cru | sherD | ump" | | |
| Nr. | X | Y | Z | Refl. | DEN | Frea. | Lw | l/a | Optime | K0 | Di | Adiv | Aatm | Aar | Afol | Ahous | Abar | Cmet | RL | Lr |
| | (m) | (m) | (m) | | | (Hz) | dB(A) | dB | dB | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | dB(A) |
| 159 | 648673.29 | 4772848.33 | 180.00 | 0 | D | A | 123.0 | 0.0 | -10.8 | 0.0 | 0.0 | 70.5 | 4.2 | -1.9 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 39.3 |
| | | | | _ | | | | | | | | | | | | | | | | |
| | | Poi | nt Sourc | e, ISC | 9613 | 3, Nam | 1e: "P1 | A_Sinl | kcut, WF | Drill" | , ID: | "P1A_ | Sinkc | ut_W | F_Dr | ill" | | | | |
| Nr. | Х | Y | Z | Refl. | DEN | Freq. | Lw | l/a | Optime | K0 | Di | Adiv | Aatm | Agr | Afol | Ahous | Abar | Cmet | RL | Lr |
| | (m) | (m) | (m) | | | (Hz) | dB(A) | dB | dB | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | dB(A) |
| 160 | 648631.06 | 4772869.76 | 179.50 | 0 | D | A | 110.0 | 0.0 | 0.0 | 0.0 | 0.0 | 71.0 | 6.6 | -2.2 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 34.7 |
| | | | | | | | | | | - | | | | c · | | | | | | |
| | Line Sc | ource, ISO 96 | 13, Nam | e: "P1 | A_Sir | ikcut, i | Aggreg | ate Sh | nipping fr | om P | <u>Ρ, Fι</u> | µוו", ID | : "P1A | _Sinl | kcut_ | RD_SH | P_Age | gr_Fu" | D ' | |
| Nr. | X | Ý | <u> </u> | Retl. | DEN | ⊢req. | | I/a | Optime | K0 | | Adiv | Aatm | Agr | Atol | Anous | Abar | Cmet | KL (JD) | |
| 404 | (m) | (m) | (m) | | DE1. | (Hz) | dB(A) | dB | dB | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | dB(A) |
| 161 | 648/68.21 | 4//28//.52 | 180.57 | 0 | DEN | A | 67.0 | 21.7 | 0.0 | 0.0 | 0.0 | 69.7 | 3.9 | -1.6 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 16.7 |
| 165 | 648622.64 | 47720224.55 | 186.30 | 0 | DEN | A | 67.0 | 22.1 | 0.0 | 0.0 | 0.0 | /1.1 | 4.3 | -1.5 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 15.1 |
| 1/6 | 048527.52 | 4772909.10 | 187.70 | 0 | DEN | A | 07.0 | 15.5 | 0.0 | 0.0 | 0.0 | 71.9 | 4.5 | -1.6 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 1.1 |
| 1/9 | 640706 40 | 4772052.82 | 102.79 | 0 | | A | 67.0 | 13.2 | 0.0 | 0.0 | 0.0 | 70.5 | 4.1 | -1.5 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 1.3 |
| 102 | 040700.19 | 4112902.03 | 100.02 | U | DEN | A | 07.0 | 10.9 | 0.0 | 0.0 | 0.0 | 10.5 | 4.1 | -1.4 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 4.7 |

| | Line Sou | rce, ISO 9613 | 8, Name: | "P1A | _Sink | cut, Ag | ggregat | e Ship | oping from | m PP | , Emp | oty", Il | D: "P1/ | A_Sir | nkcut_ | _RD_SF | IP_Ag | ggr_En | ו" | |
|-----|-----------|---------------|----------|-------|-------|---------|---------|--------|------------|------|-------|----------|---------|-------|--------|--------|-------|--------|------|-------|
| Nr. | Х | Y | Z | Refl. | DEN | Freq. | Lw | l/a | Optime | K0 | Di | Adiv | Aatm | Agr | Afol | Ahous | Abar | Cmet | RL | Lr |
| | (m) | (m) | (m) | | | (Hz) | dB(A) | dB | dB | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | dB(A) |
| 163 | 648765.56 | 4772875.98 | 180.50 | 0 | DEN | A | 67.0 | 21.7 | 0.0 | 0.0 | 0.0 | 69.7 | 3.9 | -1.6 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 16.6 |
| 166 | 648622.41 | 4772930.83 | 186.31 | 0 | DEN | A | 67.0 | 22.1 | 0.0 | 0.0 | 0.0 | 71.1 | 4.3 | -1.5 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 15.1 |
| 174 | 648527.49 | 4772905.03 | 187.73 | 0 | DEN | A | 67.0 | 15.6 | 0.0 | 0.0 | 0.0 | 71.8 | 4.5 | -1.6 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 7.7 |
| 178 | 648717.20 | 4772944.52 | 182.76 | 0 | DEN | A | 67.0 | 13.6 | 0.0 | 0.0 | 0.0 | 70.3 | 4.1 | -1.5 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 7.7 |
| 184 | 648703.40 | 4772950.40 | 185.07 | 0 | DEN | A | 67.0 | 8.8 | 0.0 | 0.0 | 0.0 | 70.5 | 4.1 | -1.4 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 2.6 |
| 186 | 648728.07 | 4772939.89 | 180.50 | 0 | DEN | A | 67.0 | 1.1 | 0.0 | 0.0 | 0.0 | 70.2 | 4.0 | -1.6 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | -4.6 |

| | | Poir | t Source | e, ISO | 9613 | , Name | e: "P1A | _Sink | cut, PC | Loade | er", IC |): "P1/ | A_Sink | cut_F | PC_L | dr" | | | | |
|-----|-----------|------------|----------|--------|------|--------|---------|-------|---------|-------|---------|---------|--------|-------|------|-------|------|------|------|-------|
| Nr. | Х | Y | Z | Refl. | DEN | Freq. | Lw | l/a | Optime | K0 | Di | Adiv | Aatm | Agr | Afol | Ahous | Abar | Cmet | RL | Lr |
| | (m) | (m) | (m) | | | (Hz) | dB(A) | dB | dB | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | dB(A) |
| 169 | 648672.13 | 4772849.77 | 179.50 | 0 | D | A | 105.6 | 0.0 | 0.0 | 0.0 | 0.0 | 70.6 | 5.5 | -1.9 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 31.4 |

| | | Line | Source | , ISO | 9613, | Name | : "P1A | Sinko | cut, Conv | /eyor' | ", ID: | "P1A_ | Sinkcu | ut_Co | nvey | or" | | | | |
|-----|-----------|------------|--------|-------|-------|-------|--------|-------|-----------|--------|--------|-------|--------|-------|------|-------|------|------|------|-------|
| Nr. | Х | Y | Z | Refl. | DEN | Freq. | Lw | l/a | Optime | K0 | Di | Adiv | Aatm | Agr | Afol | Ahous | Abar | Cmet | RL | Lr |
| | (m) | (m) | (m) | | | (Hz) | dB(A) | dB | dB | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | dB(A) |
| 170 | 648733.39 | 4772817.27 | 180.50 | 0 | D | A | 82.7 | 20.8 | 0.0 | 0.0 | 0.0 | 69.9 | 3.8 | -1.9 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 31.7 |

| | | Point Source, | ISO 961 | 13, Na | me: "l | P1A_S | inkcut, | PP T | ertiary C | rushe | r", ID | : "P1A | _Sink | cut_F | Ρ_Τε | ertiaryC | rush" | | | - |
|-----|-----------|---------------|---------|--------|--------|-------|---------|------|-----------|-------|--------|--------|-------|-------|------|----------|-------|------|------|-------|
| Nr. | X | Y | Z | Refl. | DEN | Freq. | Lw | l/a | Optime | K0 | Di | Adiv | Aatm | Agr | Afol | Ahous | Abar | Cmet | RL | Lr |
| | (m) | (m) | (m) | | | (Hz) | dB(A) | dB | dB | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | dB(A) |
| 173 | 648793.79 | 4772790.45 | 180.00 | 0 | D | A | 99.2 | 0.0 | 0.0 | 0.0 | 0.0 | 69.3 | 3.3 | -1.6 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 28.2 |

Receiver

Name: Facade of dwelling (5584 Beechwood Rd)

R4f ID:

649610.64 m 4772697.98 m

X: Y:

Z: 190.50 m

| | | Point Sou | rce, ISO | 9613 | , Nam | ne: "As | phalt F | lant - | Dust Co | llecto | r Blov | ver (st | ack)", | ID: "/ | ASPH | _DC_s | • | | | |
|------|-----------|------------|----------|-------|-------|---------|---------|--------|---------|--------|--------|---------|--------|--------|------|-------|------|------|------|-------|
| Nr. | Х | Y | Z | Refl. | DEN | Freq. | Lw | l/a | Optime | K0 | Di | Adiv | Aatm | Agr | Afol | Ahous | Abar | Cmet | RL | Lr |
| | (m) | (m) | (m) | | | (Hz) | dB(A) | dB | dB | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | dB(A) |
| 1547 | 648854.54 | 4772826.22 | 166.05 | 0 | D | A | 109.5 | 0.0 | 0.0 | 0.0 | 0.0 | 68.7 | 1.8 | -1.3 | 0.0 | 0.0 | 4.6 | 0.0 | 0.0 | 35.7 |

| | | Point So | ource, IS | O 961 | 3, Na | me: "F | 24_SE, | PC PI | rimary C | rushe | r", ID | : "P4_ | SE_P | C_Pri | mary | Crush" | | | | |
|------|--|------------|-----------|-------|-------|--------|--------|-------|----------|-------|--------|--------|------|-------|------|--------|------|------|------|-------|
| Nr. | Nr. X Y Z Refl. DEN Freq. Lw I/a Optime K0 Di Adiv Aatm Agr Afol Ahous Abar Cmet RL Lr | | | | | | | | | | | | | | | | | | | |
| | (m) | (m) | (m) | | | (Hz) | dB(A) | dB | dB | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | dB(A) |
| 1549 | 649480.08 | 4772803.25 | 164.50 | 0 | D | A | 117.6 | 0.0 | 0.0 | 0.0 | 0.0 | 55.6 | 0.9 | -0.8 | 0.0 | 0.0 | 21.2 | 0.0 | 0.0 | 40.7 |

| | | | Point S | Source | e, ISO | 9613, | Name | : "P4_ | SE, PP | Loade | er", ID |): "P4_ | _SE_P | P_Ld | r" | | | | | |
|------|-----------|------------|---------|--------|--------|-------|-------|--------|--------|-------|---------|---------|-------|------|------|-------|------|------|------|-------|
| Nr. | Х | Y | Z | Refl. | DEN | Freq. | Lw | l/a | Optime | K0 | Di | Adiv | Aatm | Agr | Afol | Ahous | Abar | Cmet | RL | Lr |
| | (m) | (m) | (m) | | | (Hz) | dB(A) | dB | dB | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | dB(A) |
| 1551 | 649152.30 | 4772897.23 | 148.50 | 0 | D | A | 105.6 | 0.0 | 0.0 | 0.0 | 0.0 | 65.0 | 4.0 | -2.6 | 0.0 | 0.0 | 10.3 | 0.0 | 0.0 | 28.9 |

| | F | Point Source, | ISO 961 | 3, Na | me: "F | P4_SE | , PC lo | ader c | lumping | into c | rushe | er", ID | :"P4_\$ | SE_P | C_Cr | usherD | ump" | | | |
|------|-----------|---------------|---------|-------|--------|-------|---------|--------|---------|--------|-------|---------|---------|------|------|--------|------|------|------|-------|
| Nr. | Х | Y | Z | Refl. | DEN | Freq. | Lw | l/a | Optime | K0 | Di | Adiv | Aatm | Agr | Afol | Ahous | Abar | Cmet | RL | Lr |
| | (m) | (m) | (m) | | | (Hz) | dB(A) | dB | dB | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | dB(A) |
| 1554 | 649481.42 | 4772802.28 | 164.50 | 0 | D | A | 123.0 | 0.0 | -7.8 | 0.0 | 0.0 | 55.5 | 1.1 | -1.0 | 0.0 | 0.0 | 22.6 | 0.0 | 0.0 | 37.0 |

| | F | Point Source, | ISO 961 | 3, Na | me: "/ | Asphal | t Plant | - Pug | Mill door | r (pres | ssure | relief | noise) | ", ID: | "ASF | PH_pug | door" | | | |
|------|-----------|---------------|---------|-------|--------|--------|---------|-------|-----------|---------|-------|--------|--------|--------|------|--------|-------|------|------|-------|
| Nr. | Х | Y | Z | Refl. | DEN | Freq. | Lw | l/a | Optime | K0 | Di | Adiv | Aatm | Agr | Afol | Ahous | Abar | Cmet | RL | Lr |
| | (m) | (m) | (m) | | | (Hz) | dB(A) | dB | dB | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | dB(A) |
| 1557 | 648862.85 | 4772834.18 | 150.00 | 0 | D | Α | 107.0 | 0.0 | 0.0 | 0.0 | 0.0 | 68.6 | 2.7 | -2.6 | 0.0 | 0.0 | 23.8 | 0.0 | 0.0 | 14.5 |
| 1559 | 648862.85 | 4772834.18 | 150.00 | 1 | D | Α | 107.0 | 0.0 | 0.0 | 0.0 | 0.0 | 68.8 | 2.7 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 19.8 | -86.4 |
| 1562 | 648862.85 | 4772834.18 | 150.00 | 1 | D | Α | 107.0 | 0.0 | 0.0 | 0.0 | 0.0 | 68.8 | 2.7 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 15.3 | 18.0 |

| | Po | int Source, IS | O 9613, | Nam | e: "As | phalt F | Plant - (| Conve | yor moto | or, gra | avel h | itting I | metal p | olate" | , ID: ' | 'ASPH_ | motor | .11 | | |
|------|--|----------------|---------|-----|--------|---------|-----------|-------|----------|---------|--------|----------|---------|--------|---------|--------|-------|------|------|-------|
| Nr. | Ir. X Y Z Refl. DEN Freq. Lw I/a Optime K0 Di Adiv Aatm Agr Afol Ahous Abar Cmet RL Lr | | | | | | | | | | | | | | | | | | | |
| | (m) | (m) | (m) | | | (Hz) | dB(A) | dB | dB | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | dB(A) |
| 1564 | 648854.17 | 4772834.20 | 150.00 | 0 | D | Α | 107.0 | 0.0 | 0.0 | 0.0 | 0.0 | 68.7 | 4.6 | -3.0 | 0.0 | 0.0 | 5.9 | 0.0 | 0.0 | 30.8 |
| 1567 | 648854.17 | 4772834.20 | 150.00 | 1 | D | A | 107.0 | 0.0 | 0.0 | 0.0 | 0.0 | 68.8 | 4.6 | -3.0 | 0.0 | 0.0 | 4.8 | 0.0 | 20.0 | -88.2 |

| | | Point So | urce, IS | O 961 | 3, Na | me: "P | 4_SE, | PC PI | rimary So | creen | ", ID: | "P4_8 | SE_PC | _Prir | naryS | Screen" | | | | |
|------|--|------------|----------|-------|-------|--------|-------|-------|-----------|-------|--------|-------|-------|-------|-------|---------|------|------|------|-------|
| Nr. | Ir. X Y Z Refl. DEN Freq. Lw I/a Optime K0 Di Adiv Aatm Agr Afol Ahous Abar Cmet RL Lr | | | | | | | | | | | | | | | | | | | |
| | (m) | (m) | (m) | | | (Hz) | dB(A) | dB | dB | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | dB(A) |
| 1569 | 649478.69 | 4772804.35 | 164.50 | 0 | D | A | 113.8 | 0.0 | 0.0 | 0.0 | 0.0 | 55.7 | 1.5 | -1.1 | 0.0 | 0.0 | 21.7 | 0.0 | 0.0 | 35.9 |

| | | Po | int Sourc | ce, ISO | O 961 | 3, Nan | ne: "As | phalt l | Plant - P | ug Mi | II Mo | tor", ID |): "ASI | РН_р | ugmil | l'' | | | | |
|------|-----------|------------|-----------|---------|-------|--------|---------|---------|-----------|-------|-------|----------|---------|------|-------|-------|------|------|------|--------|
| Nr. | Х | Y | Z | Refl. | DEN | Freq. | Lw | l/a | Optime | K0 | Di | Adiv | Aatm | Agr | Afol | Ahous | Abar | Cmet | RL | Lr |
| | (m) | (m) | (m) | | | (Hz) | dB(A) | dB | dB | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | dB(A) |
| 1571 | 648870.31 | 4772836.62 | 151.00 | 0 | D | A | 104.8 | 0.0 | 0.0 | 0.0 | 0.0 | 68.6 | 7.2 | -2.4 | 0.0 | 0.0 | 6.5 | 0.0 | 0.0 | 25.1 |
| 1574 | 648870.31 | 4772836.62 | 151.00 | 1 | D | A | 104.8 | 0.0 | 0.0 | 0.0 | 0.0 | 68.9 | 7.3 | -2.4 | 0.0 | 0.0 | 20.6 | 0.0 | 14.2 | -103.7 |
| 1577 | 648870.31 | 4772836.62 | 151.00 | 1 | D | A | 104.8 | 0.0 | 0.0 | 0.0 | 0.0 | 68.6 | 7.2 | -2.4 | 0.0 | 0.0 | 4.7 | 0.0 | 3.4 | 23.2 |

| | | Point Sou | rce, ISO | 9613, | Nam | e: "As | phalt P | ant - I | Dust Col | ector | Blow | /er (m | otor)", | ID: "/ | \SPH | _DC_m | " | | | |
|------|-----------|------------|----------|-------|-----|--------|---------|---------|----------|-------|------|--------|---------|--------|------|-------|------|------|------|-------|
| Nr. | Х | Y | Z | Refl. | DEN | Freq. | Lw | l/a | Optime | K0 | Di | Adiv | Aatm | Agr | Afol | Ahous | Abar | Cmet | RL | Lr |
| | (m) | (m) | (m) | | | (Hz) | dB(A) | dB | dB | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | dB(A) |
| 1579 | 648856.17 | 4772826.28 | 148.00 | 0 | D | A | 104.8 | 0.0 | 0.0 | 0.0 | 0.0 | 68.7 | 2.9 | -2.7 | 0.0 | 0.0 | 4.8 | 0.0 | 0.0 | 31.2 |
| 1582 | 648856.17 | 4772826.28 | 148.00 | 1 | D | A | 104.8 | 0.0 | 0.0 | 0.0 | 0.0 | 68.7 | 2.9 | -2.7 | 0.0 | 0.0 | 4.8 | 0.0 | 8.3 | 22.9 |

| | | | Point | Sourc | e, ISC | D 9613 | , Name | : "P4_ | _SE, WF | Drill' | ', ID: | "P4_S | SE_WF | _Dril | l'' | | | | | |
|------|---|------------|--------|-------|--------|--------|--------|--------|---------|--------|--------|-------|-------|-------|------|------|------|------|------|-------|
| Nr. | r. X Y Z Refl. DEN Freq. Lw I/a Optime K0 Di Adiv Aatm Agr Afol Ahous Abar Cmet RL Lr | | | | | | | | | | | | | | | | | | | |
| | (m) | (m) | (m) | | | (Hz) | dB(A) | dB | dB | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | dB(A) |
| 1584 | 649522.65 | 4772781.71 | 180.50 | 0 | D | Α | 110.0 | 0.0 | 0.0 | 0.0 | 0.0 | 52.7 | 1.6 | -0.7 | 0.0 | 0.0 | 16.4 | 0.0 | 0.0 | 40.0 |

| | | I | Point So | urce, | ISO 9 | 613, N | lame: " | Aspha | alt Plant · | · Ove | n Mot | tor", IE |): "ASI | PH_o | ven" | | | | | |
|------|-----------|------------|----------|-------|-------|--------|---------|-------|-------------|-------|-------|----------|---------|------|------|-------|------|------|------|-------|
| Nr. | Х | Y | Z | Refl. | DEN | Freq. | Lw | l/a | Optime | K0 | Di | Adiv | Aatm | Agr | Afol | Ahous | Abar | Cmet | RL | Lr |
| | (m) | (m) | (m) | | | (Hz) | dB(A) | dB | dB | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | dB(A) |
| 1587 | 648858.27 | 4772831.59 | 151.80 | 0 | D | A | 102.4 | 0.0 | 0.0 | 0.0 | 0.0 | 68.7 | 3.4 | -2.6 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | 28.3 |
| 1590 | 648858.27 | 4772831.59 | 151.80 | 1 | D | A | 102.4 | 0.0 | 0.0 | 0.0 | 0.0 | 68.8 | 3.4 | -2.6 | 0.0 | 0.0 | 4.7 | 0.0 | 46.3 | -18.1 |

| | | Poir | nt Source | e, ISO | 9613 | , Nam | e: "Asp | halt P | lant - Lo | ader / | Activi | ty", ID | : "ASP | H_Lc | lr_Ac | t1" | | | | |
|------|--|------------|-----------|--------|------|-------|---------|--------|-----------|--------|--------|---------|--------|------|-------|------|------|------|------|-------|
| Nr. | Vr. X Y Z Refl. DEN Freq. Lw I/a Optime K0 Di Adiv Aatm Agr Afol Ahous Abar Cmet RL Lr (m) (m) (m) (Hz) dB(A) dB dB (dB) (dB) | | | | | | | | | | | | | | | | | | | |
| | (m) | (m) | (m) | | | (Hz) | dB(A) | dB | dB | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | dB(A) |
| 1597 | 648869.76 | 4772830.27 | 148.50 | 0 | D | A | 101.7 | 0.0 | 0.0 | 0.0 | 0.0 | 68.5 | 3.8 | -2.7 | 0.0 | 0.0 | 12.1 | 0.0 | 0.0 | 20.1 |
| 1600 | 648869.76 | 4772830.27 | 148.50 | 1 | D | A | 101.7 | 0.0 | 0.0 | 0.0 | 0.0 | 68.9 | 3.8 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 20.1 | -93.1 |

| | | Poir | nt Source | e, ISO | 9613 | , Nam | e: "Asp | halt P | lant - Lo | ader / | Activi | ty", ID | : "ASP | H_Lc | lr_Ac | t2" | | | | |
|------|-----------|------------|-----------|--------|------|-------|---------|--------|-----------|--------|--------|---------|--------|------|-------|-------|------|------|------|-------|
| Nr. | Х | Y | Z | Refl. | DEN | Freq. | Lw | l/a | Optime | K0 | Di | Adiv | Aatm | Agr | Afol | Ahous | Abar | Cmet | RL | Lr |
| | (m) | (m) | (m) | | | (Hz) | dB(A) | dB | dB | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | dB(A) |
| 1603 | 648864.03 | 4772827.02 | 148.50 | 0 | D | A | 101.7 | 0.0 | 0.0 | 0.0 | 0.0 | 68.6 | 3.8 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | 27.3 |
| 1607 | 648864.03 | 4772827.02 | 148.50 | 1 | D | A | 101.7 | 0.0 | 0.0 | 0.0 | 0.0 | 68.8 | 3.8 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 44.6 | -17.6 |

| | | Р | oint Sou | rce, IS | SO 96 | 13, Na | ame: "A | sphal | t Plant - | Eleva | itor M | otor", | ID: "A | SPH_ | elev" | | | | | |
|------|-----------|------------|----------|---------|-------|--------|---------|-------|-----------|-------|--------|--------|--------|------|-------|-------|------|------|------|--------|
| Nr. | Х | Y | Z | Refl. | DEN | Freq. | Lw | l/a | Optime | K0 | Di | Adiv | Aatm | Agr | Afol | Ahous | Abar | Cmet | RL | Lr |
| | (m) | (m) | (m) | | | (Hz) | dB(A) | dB | dB | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | dB(A) |
| 1609 | 648861.24 | 4772834.76 | 165.00 | 0 | D | A | 99.8 | 0.0 | 0.0 | 0.0 | 0.0 | 68.6 | 3.1 | -1.5 | 0.0 | 0.0 | 4.8 | 0.0 | 0.0 | 24.9 |
| 1612 | 648861.24 | 4772834.76 | 165.00 | 1 | D | A | 99.8 | 0.0 | 0.0 | 0.0 | 0.0 | 68.8 | 3.1 | -1.6 | 0.0 | 0.0 | 4.8 | 0.0 | 28.5 | -103.8 |

| | | F | oint Sou | irce, l | SO 96 | 613, Na | ame: "F | 4_SE | , PP Idli | ng Tr | uck", | ID: "P | 4_SE_ | PP_ | Trk1" | | | | | |
|------|--|------------|----------|---------|-------|---------|---------|------|-----------|-------|-------|--------|-------|------|-------|------|------|------|------|-------|
| Nr. | Nr. X Y Z Refl. DEN Freq. Lw I/a Optime K0 Di Adiv Aatm Agr Afol Ahous Abar Cmet RL Lr | | | | | | | | | | | | | | | | | | | |
| | (m) | (m) | (m) | | | (Hz) | dB(A) | dB | dB | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | dB(A) |
| 1615 | 649143.29 | 4772895.19 | 149.00 | 0 | D | A | 96.3 | 0.0 | 0.0 | 0.0 | 0.0 | 65.1 | 2.6 | -2.7 | 0.0 | 0.0 | 5.2 | 0.0 | 0.0 | 26.1 |

| | | F | Point Sou | irce, l | SO 96 | 513, Na | ame: "F | 4_SE | , PP Idli | ng Tr | uck", | ID: "P | 4_SE | PP_ | Trk2" | | | | | |
|------|-----------|------------|-----------|---------|-------|---------|---------|------|-----------|-------|-------|--------|------|------|-------|-------|------|------|------|-------|
| Nr. | Х | Y | Z | Refl. | DEN | Freq. | Lw | l/a | Optime | K0 | Di | Adiv | Aatm | Agr | Afol | Ahous | Abar | Cmet | RL | Lr |
| | (m) | (m) | (m) | | | (Hz) | dB(A) | dB | dB | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | dB(A) |
| 1617 | 649141.96 | 4772897.03 | 149.00 | 0 | D | A | 96.3 | 0.0 | 0.0 | 0.0 | 0.0 | 65.2 | 2.6 | -2.7 | 0.0 | 0.0 | 5.2 | 0.0 | 0.0 | 26.0 |

| | | Poir | nt Source | e, ISC | 9613 | , Nam | e: "Asp | halt P | lant - Co | ompre | essor | Vent" | ID: "A | SPH | _com | р" | | | | |
|------|---|------------|-----------|--------|------|-------|---------|--------|-----------|-------|-------|-------|--------|------|------|------|------|------|------|-------|
| Nr. | r. X Y Z Refl. DEN Freq. Lw I/a Optime K0 Di Adiv Aatm Agr Afol Ahous Abar Cmet RL Lr | | | | | | | | | | | | | | | | | | | |
| | (m) | (m) | (m) | | | (Hz) | dB(A) | dB | dB | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | dB(A) |
| 1620 | 648874.75 | 4772829.07 | 146.60 | 0 | D | A | 96.0 | 0.0 | 0.0 | 3.0 | 0.0 | 68.5 | 2.9 | -1.5 | 0.0 | 0.0 | 21.0 | 0.0 | 0.0 | 8.2 |
| 1623 | 648874.75 | 4772829.07 | 146.60 | 1 | D | A | 96.0 | 0.0 | 0.0 | 3.0 | 0.0 | 68.9 | 3.0 | -1.5 | 0.0 | 0.0 | 4.7 | 0.0 | 22.2 | -98.3 |

| | | | Line S | ource | , ISO | 9613, | Name: | "P4_S | SE, Conv | 'eyor' | ', ID: | "P4_S | E_Cor | nveyc | or" | | | | | |
|------|-----------|------------|--------|-------|-------|-------|-------|-------|----------|--------|--------|-------|-------|-------|------|-------|------|------|------|-------|
| Nr. | Х | Y | Z | Refl. | DEN | Freq. | Lw | l/a | Optime | K0 | Di | Adiv | Aatm | Agr | Afol | Ahous | Abar | Cmet | RL | Lr |
| | (m) | (m) | (m) | | | (Hz) | dB(A) | dB | dB | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | dB(A) |
| 1627 | 649434.42 | 4772810.92 | 149.50 | 0 | D | A | 82.7 | 18.8 | 0.0 | 0.0 | 0.0 | 57.6 | 1.2 | -1.4 | 0.0 | 0.0 | 23.8 | 0.0 | 0.0 | 20.4 |
| 1629 | 649359.39 | 4772823.01 | 149.50 | 0 | D | A | 82.7 | 18.8 | 0.0 | 0.0 | 0.0 | 60.1 | 1.5 | -1.8 | 0.0 | 0.0 | 14.9 | 0.0 | 0.0 | 26.9 |
| 1631 | 649246.84 | 4772841.14 | 149.50 | 0 | D | A | 82.7 | 21.8 | 0.0 | 0.0 | 0.0 | 62.9 | 2.0 | -2.3 | 0.0 | 0.0 | 8.5 | 0.0 | 0.0 | 33.5 |
| 1804 | 649473.37 | 4772804.82 | 157.25 | 0 | D | A | 82.7 | 12.0 | 0.0 | 0.0 | 0.0 | 56.0 | 1.0 | -1.1 | 0.0 | 0.0 | 24.8 | 0.0 | 0.0 | 14.1 |
| 1973 | 649171.27 | 4772858.25 | 149.50 | 0 | D | A | 82.7 | 10.0 | 0.0 | 0.0 | 0.0 | 64.4 | 2.3 | -2.6 | 0.0 | 0.0 | 5.8 | 0.0 | 0.0 | 22.8 |
| 1983 | 649168.92 | 4772879.80 | 149.50 | 0 | D | A | 82.7 | 15.2 | 0.0 | 0.0 | 0.0 | 64.6 | 2.3 | -2.6 | 0.0 | 0.0 | 13.6 | 0.0 | 0.0 | 20.0 |
| 2190 | 649475.97 | 4772804.73 | 165.00 | 0 | D | A | 82.7 | 3.7 | 0.0 | 0.0 | 0.0 | 55.8 | 1.0 | -1.1 | 0.0 | 0.0 | 22.3 | 0.0 | 0.0 | 8.4 |

| | Line S | ource, ISO 96 | 613, Nan | 1e: "P | 4 SE, | Aggre | gate H | aul roa | ad b/w P | P and | I AP, | Full", | ID: "P4 | 4_SE | _RD_ | Haul_F | P_AF | _Fu" | | |
|------|-----------|---------------|----------|--------|-------|-------|--------|---------|----------|-------|-------|--------|---------|------|------|--------|------|------|------|--------|
| Nr. | Х | Y | Z | Refl. | DEN | Freq. | Lw | l/a | Optime | K0 | Di | Adiv | Aatm | Agr | Afol | Ahous | Abar | Cmet | RL | Lr |
| | (m) | (m) | (m) | | | (Hz) | dB(A) | dB | dB | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | dB(A) |
| 1633 | 649130.91 | 4772889.48 | 149.50 | 0 | DEN | A | 73.4 | 14.1 | 0.0 | 0.0 | 0.0 | 65.3 | 2.5 | -2.6 | 0.0 | 0.0 | 5.1 | 0.0 | 0.0 | 17.2 |
| 1635 | 649078.32 | 4772852.64 | 149.50 | 0 | DEN | A | 73.4 | 20.1 | 0.0 | 0.0 | 0.0 | 65.9 | 2.6 | -2.6 | 0.0 | 0.0 | 4.9 | 0.0 | 0.0 | 22.7 |
| 1706 | 649017.68 | 4772815.35 | 149.50 | 0 | DEN | A | 73.4 | 16.0 | 0.0 | 0.0 | 0.0 | 66.6 | 2.8 | -2.7 | 0.0 | 0.0 | 4.8 | 0.0 | 0.0 | 17.8 |
| 1709 | 648907.21 | 4772814.73 | 149.50 | 0 | DEN | A | 73.4 | 17.2 | 0.0 | 0.0 | 0.0 | 68.1 | 3.2 | -2.8 | 0.0 | 0.0 | 4.8 | 0.0 | 0.0 | 17.3 |
| 1710 | 648907.21 | 4772814.73 | 149.50 | 1 | DEN | A | 73.4 | 17.2 | 0.0 | 0.0 | 0.0 | 68.6 | 3.4 | -2.8 | 0.0 | 0.0 | 4.8 | 0.0 | 16.5 | 0.2 |
| 1712 | 648907.21 | 4772814.73 | 149.50 | 1 | DEN | A | 73.4 | 17.2 | 0.0 | 0.0 | 0.0 | 68.7 | 3.4 | -2.8 | 0.0 | 0.0 | 4.8 | 0.0 | 51.8 | -35.2 |
| 1714 | 648907.21 | 4772814.73 | 149.50 | 1 | DEN | A | 73.4 | 17.2 | 0.0 | 0.0 | 0.0 | 68.7 | 3.4 | -2.8 | 0.0 | 0.0 | 4.8 | 0.0 | 17.2 | -0.6 |
| 1716 | 648907.21 | 4772814.73 | 149.50 | 1 | DEN | A | 73.4 | 17.2 | 0.0 | 0.0 | 0.0 | 68.7 | 3.4 | -2.8 | 0.0 | 0.0 | 4.8 | 0.0 | 51.3 | -34.7 |
| 1718 | 648953.45 | 4772804.66 | 149.50 | 0 | DEN | A | 73.4 | 16.3 | 0.0 | 0.0 | 0.0 | 67.5 | 3.1 | -2.7 | 0.0 | 0.0 | 4.8 | 0.0 | 0.0 | 17.1 |
| 1720 | 648953.45 | 4772804.66 | 149.50 | 1 | DEN | A | 73.4 | 16.3 | 0.0 | 0.0 | 0.0 | 69.2 | 3.5 | -2.9 | 0.0 | 0.0 | 4.8 | 0.0 | 29.7 | -114.6 |
| 1722 | 648953.45 | 4772804.66 | 149.50 | 1 | DEN | A | 73.4 | 16.3 | 0.0 | 0.0 | 0.0 | 69.1 | 3.5 | -2.9 | 0.0 | 0.0 | 4.8 | 0.0 | 29.2 | -114.1 |
| 1724 | 648986.92 | 4772804.88 | 149.50 | 0 | DEN | A | 73.4 | 14.0 | 0.0 | 0.0 | 0.0 | 67.0 | 2.9 | -2.7 | 0.0 | 0.0 | 4.8 | 0.0 | 0.0 | 15.3 |
| 1726 | 648986.92 | 4772804.88 | 149.50 | 1 | DEN | A | 73.4 | 14.0 | 0.0 | 0.0 | 0.0 | 69.5 | 3.6 | -2.9 | 0.0 | 0.0 | 4.8 | 0.0 | 34.3 | -121.9 |

| | Line S | ource, ISO 96 | 613, Nan | ne: "P | 4 SE, | Aggre | gate H | aul roa | ad b/w P | P and | I AP, | Full", | ID: "P4 | 1_SE | _RD_ | Haul_F | P_AF | '_Fu" | | |
|------|-----------|---------------|-----------|--------|--------------|----------|--------|------------|-----------|-------|--------|----------|----------|------------|------|--------|--------|-------|-------------|--------|
| Nr. | Х | Y | Z | Refl. | DEN | Freq. | Lw | l/a | Optime | K0 | Di | Adiv | Aatm | Agr | Afol | Ahous | Abar | Cmet | RL | Lr |
| | (m) | (m) | (m) | | | (Hz) | dB(A) | dB | dB | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | dB(A) |
| 1728 | 648986.92 | 4772804.88 | 149.50 | 1 | DEN | Á | 73.4 | 14.0 | 0.0 | 0.0 | 0.0 | 69.5 | 3.6 | -2.9 | 0.0 | 0.0 | 4.8 | 0.0 | <u>33.9</u> | -121.5 |
| | | | | | | | | | | | | | | | | | | | | |
| | Line | e Source, ISC |) 9613, I | Name: | "P4 ; | SE, Aç | gregat | e Ship | ping from | n PP, | , Emp | oty", IE |): "P4 | SE | RD S | SHP Ag | ıgr Er | n" | | |
| Nr. | Х | Y | Z | Refl. | DEN | Freq. | Lw | l/a | Optime | K0 | Di | Adiv | Aatm | Agr | Afol | Ahous | Abar | Cmet | RL | Lr |
| | (m) | (m) | (m) | | | (Hz) | dB(A) | dB | dB | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | dB(A) |
| 1639 | 649139.11 | 4772890.32 | 149.50 | 0 | DEN | Â | 71.7 | 10.6 | 0.0 | 0.0 | 0.0 | 65.2 | 2.8 | -2.4 | 0.0 | 0.0 | 5.1 | 0.0 | 0.0 | 11.8 |
| 1641 | 649132.97 | 4772882.08 | 149.50 | 0 | DEN | Α | 71.7 | 9.6 | 0.0 | 0.0 | 0.0 | 65.2 | 2.8 | -2.4 | 0.0 | 0.0 | 5.1 | 0.0 | 0.0 | 10.7 |
| 1644 | 649084 75 | 4772817 35 | 149 50 | 0 | DFN | Α | 717 | 21.8 | 0.0 | 0.0 | 0.0 | 65 7 | 29 | -24 | 0.0 | 0.0 | 5.0 | 0.0 | 0.0 | 22.5 |
| 1680 | 648907 83 | 4772725 25 | 149 50 | 0 | DEN | A | 717 | 21.0 | 0.0 | 0.0 | 0.0 | 68.0 | 3.4 | -2.5 | 0.0 | 0.0 | 4 7 | 0.0 | 0.0 | 19.5 |
| 1695 | 648778 40 | 4772772 26 | 149 50 | 0 | DEN | A | 71 7 | 21.6 | 0.0 | 0.0 | 0.0 | 69.4 | 3.8 | -2.6 | 0.0 | 0.0 | 47 | 0.0 | 0.0 | 18.0 |
| 1698 | 649007 42 | 4772736.56 | 149.50 | 0 | DEN | A | 717 | 18.7 | 0.0 | 0.0 | 0.0 | 66.6 | 3.1 | -2.4 | 0.0 | 0.0 | 4.8 | 0.0 | 0.0 | 18.3 |
| 1731 | 648707.63 | 4772956.98 | 187 10 | 0 | | Δ | 717 | 18.5 | 0.0 | 0.0 | 0.0 | 70.5 | 4 1 | -2.8 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 18.4 |
| 1733 | 648687.35 | 4772847 10 | 149 50 | 0 | DEN | Δ | 717 | 11 1 | 0.0 | 0.0 | 0.0 | 70.4 | 4.1 | -2.7 | 0.0 | 0.0 | 47 | 0.0 | 0.0 | 6.3 |
| 1735 | 648688.95 | 4772854 30 | 1/0 50 | 0 | | A | 71.7 | 25 | 0.0 | 0.0 | 0.0 | 70.4 | // 1 | -2.1 | 0.0 | 0.0 | 6.7 | 0.0 | 0.0 | -4.2 |
| 1737 | 648689.43 | 4772856 50 | 149.50 | 0 | | <u>^</u> | 71.7 | 13 | 0.0 | 0.0 | 0.0 | 70.4 | 4.1 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | -4.2 |
| 1730 | 648680.85 | 4772858 41 | 149.50 | 0 | | ^ | 71.7 | 4.5 | 0.0 | 0.0 | 0.0 | 70.4 | 4.1 | 2.1 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | -0.5 |
| 1739 | 648600 10 | 4772850.04 | 149.50 | 0 | | A | 71.7 | 2.0 | 0.0 | 0.0 | 0.0 | 70.4 | 4.1 | 2.1 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | -4.1 |
| 1741 | 648600.76 | 4772862.48 | 149.50 | 0 | | A | 71.7 | Z.9 5 1 | 0.0 | 0.0 | 0.0 | 70.4 | 4.1 | 2.1 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | -1.9 |
| 1743 | 648601.22 | 4772964 50 | 149.50 | 0 | | A | 71.7 | 0.1 | 0.0 | 0.0 | 0.0 | 70.4 | 4.1 | -2.1 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | 0.3 |
| 1745 | 649601.22 | 4772967.45 | 149.50 | 0 | | A | 71.7 | 0.3 | 0.0 | 0.0 | 0.0 | 70.4 | 4.1 | -2.1 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | -4.5 |
| 1747 | 648691.79 | 4772807.15 | 149.50 | 0 | DEN | <u>A</u> | 71.7 | 0.2 | 0.0 | 0.0 | 0.0 | 70.4 | 4.1 | -2.1 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | 1.4 |
| 1750 | 648692.47 | 4772870.25 | 149.50 | 0 | DEN | <u>A</u> | 71.7 | 3.4 | 0.0 | 0.0 | 0.0 | 70.4 | 4.1 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | -1.4 |
| 1752 | 648693.11 | 4772873.10 | 149.50 | 0 | DEN | <u>A</u> | 71.7 | 5.7 | 0.0 | 0.0 | 0.0 | 70.4 | 4.1 | -2.1 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | 0.9 |
| 1755 | 648693.92 | 4772876.77 | 149.50 | 0 | DEN | <u>A</u> | 71.7 | 5.8 | 0.0 | 0.0 | 0.0 | 70.4 | 4.1 | -2.7 | 0.0 | 0.0 | 5.8 | 0.0 | 0.0 | -0.1 |
| 1757 | 648694.77 | 4772880.62 | 149.50 | 0 | DEN | A | 71.7 | 6.1 | 0.0 | 0.0 | 0.0 | 70.4 | 4.1 | -2.7 | 0.0 | 0.0 | 5.9 | 0.0 | 0.0 | 0.2 |
| 1758 | 648698.25 | 4772896.37 | 149.50 | 0 | DEN | <u> </u> | /1./ | 14.5 | 0.0 | 0.0 | 0.0 | 70.4 | 4.1 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | 9.7 |
| 1763 | 648582.94 | 4772921.88 | 187.43 | 0 | DEN | <u>A</u> | /1./ | 18.6 | 0.0 | 0.0 | 0.0 | /1.4 | 4.4 | -2.8 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 17.2 |
| 1765 | 648547.42 | 4772912.09 | 187.50 | 0 | DEN | <u>A</u> | 71.7 | 1.5 | 0.0 | 0.0 | 0.0 | 71.7 | 4.5 | -2.8 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | -0.2 |
| 1788 | 648645.64 | 4772939.76 | 187.31 | 0 | DEN | <u>A</u> | 71.7 | 17.6 | 0.0 | 0.0 | 0.0 | 71.0 | 4.3 | -2.8 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 16.9 |
| 1791 | 648724.20 | 4772925.31 | 149.50 | 0 | DEN | <u>A</u> | 71.7 | 16.5 | 0.0 | 0.0 | 0.0 | 70.2 | 4.0 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | 11.9 |
| 1794 | 648701.36 | 4772825.84 | 149.50 | 0 | DEN | A | 71.7 | 16.3 | 0.0 | 0.0 | 0.0 | 70.3 | 4.1 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | 11.7 |
| 1863 | 648542.69 | 4772910.77 | 187.55 | 0 | DEN | A | 71.7 | 9.2 | 0.0 | 0.0 | 0.0 | 71.7 | 4.5 | -2.8 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 7.5 |
| 1865 | 648533.50 | 4772908.20 | 187.66 | 0 | DEN | A | 71.7 | 10.3 | 0.0 | 0.0 | 0.0 | 71.8 | 4.5 | -2.8 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 8.5 |
| 1867 | 648523.62 | 4772905.45 | 187.78 | 0 | DEN | A | 71.7 | 9.9 | 0.0 | 0.0 | 0.0 | 71.9 | 4.6 | -2.7 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 8.0 |
| 1868 | 648516.07 | 4772903.34 | 187.87 | 0 | DEN | A | 71.7 | 7.7 | 0.0 | 0.0 | 0.0 | 71.9 | 4.6 | -2.6 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 5.5 |
| 1870 | 648511.97 | 4772902.19 | 187.92 | 0 | DEN | A | 71.7 | 4.3 | 0.0 | 0.0 | 0.0 | 72.0 | 4.6 | -2.6 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 2.1 |
| 2023 | 648751.95 | 4772957.71 | 178.53 | 0 | DEN | A | 71.7 | 11.1 | 0.0 | 0.0 | 0.0 | 70.1 | 4.0 | -2.7 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 11.5 |
| 2032 | 648754.42 | 4772947.09 | 155.33 | 0 | DEN | A | 71.7 | 10.7 | 0.0 | 0.0 | 0.0 | 70.0 | 4.0 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | 6.4 |
| 2109 | 648748.21 | 4772937.54 | 149.50 | 0 | DEN | A | 71.7 | 9.8 | 0.0 | 0.0 | 0.0 | 70.0 | 4.0 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | 5.5 |
| 2186 | 648744.94 | 4772965.81 | 187.11 | 0 | DEN | A | 71.7 | 8.0 | 0.0 | 0.0 | 0.0 | 70.1 | 4.0 | -2.7 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 8.4 |
| 2210 | 648702.72 | 4772912.91 | 149.50 | 0 | DEN | A | 71.7 | 8.0 | 0.0 | 0.0 | 0.0 | 70.4 | 4.1 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | 3.2 |
| 2213 | 648749.67 | 4772963.29 | 187.12 | 0 | DEN | A | 71.7 | 7.6 | 0.0 | 0.0 | 0.0 | 70.1 | 4.0 | -2.7 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 7.9 |
| 2216 | 648753.11 | 4772942.75 | 149.50 | 0 | DEN | A | 71.7 | 7.4 | 0.0 | 0.0 | 0.0 | 70.0 | 4.0 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | 3.2 |
| 2219 | 648753.12 | 4772952.63 | 166.83 | 0 | DEN | A | 71.7 | 7.5 | 0.0 | 0.0 | 0.0 | 70.0 | 4.0 | -2.7 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 7.9 |
| 2325 | 648752.69 | 4772954.51 | 171.01 | 0 | DEN | A | 71.7 | 5.7 | 0.0 | 0.0 | 0.0 | 70.0 | 4.0 | -2.7 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 6.1 |
| 2343 | 648753.47 | 4772951.19 | 162.57 | 0 | DEN | A | 71.7 | 5.4 | 0.0 | 0.0 | 0.0 | 70.0 | 4.0 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | 1.1 |
| 2357 | 648754.15 | 4772948.34 | 159.80 | 0 | DEN | A | 71.7 | 5.2 | 0.0 | 0.0 | 0.0 | 70.0 | 4.0 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | 0.9 |
| 2391 | 648753.76 | 4772949.94 | 159.69 | 0 | DEN | A | 71.7 | 4.6 | 0.0 | 0.0 | 0.0 | 70.0 | 4.0 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | 0.3 |
| 2403 | 648751.31 | 4772960.40 | 185.82 | 0 | DEN | Α | 71.7 | 4.5 | 0.0 | 0.0 | 0.0 | 70.1 | 4.0 | -2.7 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 4.9 |
| 2442 | 648754.26 | 4772946.06 | 149.50 | 0 | DEN | Α | 71.7 | 1.6 | 0.0 | 0.0 | 0.0 | 70.0 | 4.0 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | -2.7 |
| | | | | | | | | | | | | | | | | | | | | , |
| 1 | | | Point 9 | Source | <u>- ISO</u> | 9613 | Name | • "P4 | SF PCI | oade | er" ΙΓ |)· "P4 | SF P | $C \mid c$ | lr" | | | | | |

| | | | Point S | Source | e, ISO | 9613, | Name: | "P4_ | SE, PC | Loade | er", ID |): "P4 _. | _SE_P | C_Lo | lr" | | | | | |
|------|-----------|------------|---------|--------|--------|-------|-------|------|--------|-------|---------|---------------------|-------|------|------|-------|------|------|------|-------|
| Nr. | Х | Y | Z | Refl. | DEN | Freq. | Lw | l/a | Optime | K0 | Di | Adiv | Aatm | Agr | Afol | Ahous | Abar | Cmet | RL | Lr |
| | (m) | (m) | (m) | | | (Hz) | dB(A) | dB | dB | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | dB(A) |
| 1647 | 649483.67 | 4772800.84 | 164.00 | 0 | D | A | 105.6 | 0.0 | 0.0 | 0.0 | 0.0 | 55.4 | 2.2 | -1.1 | 0.0 | 0.0 | 22.0 | 0.0 | 0.0 | 27.1 |

| | Li | ine Source, IS | SO 9613, | Nam | e: "P4 | SE, A | Aggreg | ate Sł | hipping fr | om P | P, Fu | ıll", ID | : "P4_ | SE_F | RD_SI | HP_Agg | gr_Fu'' | | | |
|------|-----------|----------------|----------|-------|--------|-------|--------|--------|------------|------|-------|----------|--------|------|-------|--------|---------|------|------|-------|
| Nr. | Х | Y | Z | Refl. | DEN | Freq. | Lw | l/a | Optime | K0 | Di | Adiv | Aatm | Agr | Afol | Ahous | Abar | Cmet | RL | Lr |
| | (m) | (m) | (m) | | | (Hz) | dB(A) | dB | dB | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | dB(A) |
| 1650 | 649083.00 | 4772818.36 | 149.50 | 0 | DEN | A | 71.7 | 21.8 | 0.0 | 0.0 | 0.0 | 65.7 | 2.9 | -2.4 | 0.0 | 0.0 | 4.9 | 0.0 | 0.0 | 22.4 |
| 1652 | 649129.95 | 4772881.43 | 149.50 | 0 | DEN | A | 71.7 | 7.4 | 0.0 | 0.0 | 0.0 | 65.3 | 2.8 | -2.4 | 0.0 | 0.0 | 5.0 | 0.0 | 0.0 | 8.5 |
| 1653 | 649136.50 | 4772890.23 | 149.50 | 0 | DEN | A | 71.7 | 12.1 | 0.0 | 0.0 | 0.0 | 65.2 | 2.8 | -2.4 | 0.0 | 0.0 | 5.1 | 0.0 | 0.0 | 13.3 |
| 1682 | 648908.30 | 4772726.74 | 149.50 | 0 | DEN | A | 71.7 | 21.3 | 0.0 | 0.0 | 0.0 | 68.0 | 3.4 | -2.5 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | 19.5 |
| 1690 | 648779.52 | 4772773.20 | 149.50 | 0 | DEN | A | 71.7 | 21.6 | 0.0 | 0.0 | 0.0 | 69.4 | 3.8 | -2.6 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | 18.0 |

| Nr. X Y Z Ref. DEN Freq. Lw Math Math Agr Alous Auss Alous Auss Alous Al | | Li | ine Source, IS | SO 9613 | Name | : "P4 | L_SE, / | Aggreg | ate Sl | hipping fi | om P | P, Fi | ıll", ID | : "P4_ | SE_R | D_SH | HP_Agg | r_Fu" | 1 | | |
|--|------|-----------|----------------|---------|---------|-------|---------|--------|--------|------------|------|-------|----------|--------|------|------|--------|-------|------|------|-------|
| (m) (m) (Hz) (| Nr. | Х | Y | Z | Refl. I | DEN | Freq. | Lw | l/a | Optime | K0 | Di | Adiv | Aatm | Agr | Afol | Ahous | Abar | Cmet | RL | Lr |
| 1703 64900.656 477273.79 149.50 0 DEN A 7.7. 18.7 10.0 0.0 0.0 7.1. 2.4. 0.0 | | (m) | (m) | (m) | | | (Hz) | dB(A) | dB | dB | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | dB(A) |
| 1776 648581.82 4772923.96 187.43 0 DEN A 7.7.7 7.8.6 0.0 | 1703 | 649006.55 | 4772737.99 | 149.50 | 0 | DEN | A | 71.7 | 18.7 | 0.0 | 0.0 | 0.0 | 66.7 | 3.1 | -2.4 | 0.0 | 0.0 | 4.8 | 0.0 | 0.0 | 18.2 |
| 1786 648645.08 4772941.51 187.31 0 DEN A 71.7 17.7 10.0 0.0 0.0 17.0 4.3 2.8 0.0 0.0 0.0 17.0 1796 648702.68 4772826.35 149.50 0 DEN A 71.7 16.3 0.0 0.0 0.70.3 4.1 2.7 0.0 0.0 4.7 0.0 0.0 11.7 1796 648753.85 4772957.12 176.06 0 DEN A 71.7 14.5 0.0 0.0 70.0 4.0 2.7 0.0 0.0 4.7 0.0 0.0 0.0 70.4 4.1 2.7 0.0 0.0 4.7 0.0 0.0 0.0 70.4 4.1 2.7 0.0 0.0 4.7 0.0 0.0 0.0 70.4 4.1 2.7 0.0 0.0 0.0 0.0 70.4 4.1 2.7 0.0 0.0 0.0 0.0 70.4 4.1 2.7 0.0 0.0 0.0 0.0 70.4 4.1 2.7 <td< td=""><td>1776</td><td>648581.82</td><td>4772923.96</td><td>187.43</td><td>0</td><td>DEN</td><td>A</td><td>71.7</td><td>18.6</td><td>0.0</td><td>0.0</td><td>0.0</td><td>71.5</td><td>4.4</td><td>-2.8</td><td>0.0</td><td>0.0</td><td>0.0</td><td>0.0</td><td>0.0</td><td>17.3</td></td<> | 1776 | 648581.82 | 4772923.96 | 187.43 | 0 | DEN | A | 71.7 | 18.6 | 0.0 | 0.0 | 0.0 | 71.5 | 4.4 | -2.8 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 17.3 |
| 1790 64872.03 4772924.59 149.50 0 DEN A 71.7 16.5 0.0 0.0 0.0 70.2 4.0 2.7 0.0 0.0 4.7 0.0 0.0 11.9 1796 648703.85 4772967.12 176.06 0 DEN A 71.7 13.8 0.0 0.0 0.0 4.0 2.7 0.0 0.0 4.7 0.0 0.0 14.2 1802 648696.01 4772880.51 149.50 0 DEN A 71.7 14.5 0.0 0.0 0.70 4.1 2.7 0.0 0.0 4.7 0.0 0.0 0.0 0.0 14.1 2.7 0.0 0.0 4.7 0.00 | 1786 | 648645.08 | 4772941.51 | 187.31 | 0 | DEN | A | 71.7 | 17.7 | 0.0 | 0.0 | 0.0 | 71.0 | 4.3 | -2.8 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 17.0 |
| 1796 648702.68 4772867.32 149.50 0 DEN A 71.7 16.3 0.0 0.0 70.3 4.1 -2.7 0.0 0.0 4.7 0.0 0.0 14.2 1799 648753.85 4772957.12 176.06 0 DEN A 71.7 13.8 0.0 0.0 0.0 70.0 4.0 -2.7 0.0 0.0 4.7 0.0 0.0 0.0 14.2 1830 648699.37 4772896.12 149.50 0 DEN A 71.7 15.8 0.0 0.0 70.4 4.1 -2.7 0.0 0.0 6.0 0.0 0.0 0.2 14.1 -2.7 0.0 0.0 6.0 0.0 | 1790 | 648725.03 | 4772924.59 | 149.50 | 0 | DEN | A | 71.7 | 16.5 | 0.0 | 0.0 | 0.0 | 70.2 | 4.0 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | 11.9 |
| 1799 648753.85 4772957.74 176.06 0 DEN A 71.7 13.8 0.0 0.0 70.0 4.0 -2.7 0.0 | 1796 | 648702.68 | 4772826.35 | 149.50 | 0 | DEN | A | 71.7 | 16.3 | 0.0 | 0.0 | 0.0 | 70.3 | 4.1 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | 11.7 |
| 1802 648755.28 4772949.98 157.24 0 DEN A 71.7 12.2 0.0 0.0 0.0 0.0 2.7 0.0 0.0 4.7 0.0 0.0 0.0 1.7 1833 648699.37 4772896.12 149.50 0 DEN A 71.7 5.8 0.0 0.0 0.7 4.4 1.2.7 0.0 0.0 4.7 0.0 0.0 0.0 1.0 1.0 0.0 0.0 1.0 0.0 0.0 1.0 0.0 0.0 4.1 2.7 0.0 0.0 4.7 0.0 0.0 0.0 1.4 1.1 2.7 0.0 0.0 0.0 0.0 1.2 1.8 1.4 1.2 0.0 0.0 0.0 0.0 1.1 2.7 0.0 0.0 0.0 0.0 1.2 1.1 1.1 1.1 0.0 0.0 0.0 1.1 2.7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 | 1799 | 648753.85 | 4772957.12 | 176.06 | 0 | DEN | A | 71.7 | 13.8 | 0.0 | 0.0 | 0.0 | 70.0 | 4.0 | -2.7 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 14.2 |
| 1830 648699.37 4772866.12 149.50 0 DEN A 71.7 14.5 0.0 0.0 0.70.4 4.1 2.7 0.0 0.0 4.7 0.0 0.0 0.0 0.0 0.0 0.0 4.1 2.7 0.0 0. | 1802 | 648755.28 | 4772949.98 | 157.24 | 0 | DEN | A | 71.7 | 12.2 | 0.0 | 0.0 | 0.0 | 70.0 | 4.0 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | 8.0 |
| 1833 648696.01 4772805.61 149.50 0 DEN A 71.7 5.8 0.0 0.0 0.7 4 1-2.7 0.0 0.0 6.0 0.0 0.0 0.2 1835 648695.18 4772873.82 149.50 0 DEN A 71.7 1.4 0.0 0.0 0.70 4.1 2.7 0.0 | 1830 | 648699.37 | 4772896.12 | 149.50 | 0 | DEN | A | 71.7 | 14.5 | 0.0 | 0.0 | 0.0 | 70.4 | 4.1 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | 9.7 |
| 1835 648695.18 477287.66 149.50 0 DEN A 71.7 6.1 0.0 0.0 70.4 4.1 2.7 0.0 0.0 0.0 0.0 70.4 4.1 2.7 0.0 </td <td>1833</td> <td>648696.01</td> <td>4772880.51</td> <td>149.50</td> <td>0</td> <td>DEN</td> <td>A</td> <td>71.7</td> <td>5.8</td> <td>0.0</td> <td>0.0</td> <td>0.0</td> <td>70.4</td> <td>4.1</td> <td>-2.7</td> <td>0.0</td> <td>0.0</td> <td>6.0</td> <td>0.0</td> <td>0.0</td> <td>-0.2</td> | 1833 | 648696.01 | 4772880.51 | 149.50 | 0 | DEN | A | 71.7 | 5.8 | 0.0 | 0.0 | 0.0 | 70.4 | 4.1 | -2.7 | 0.0 | 0.0 | 6.0 | 0.0 | 0.0 | -0.2 |
| 1837 648694.57 4772873.82 149.50 0 DEN A 71.7 2.4 0.0 0.0 70.3 4.1 2.7 0.0 0.0 0.0 0.0 70.3 4.1 2.7 0.0< | 1835 | 648695.18 | 4772876.66 | 149.50 | 0 | DEN | A | 71.7 | 6.1 | 0.0 | 0.0 | 0.0 | 70.4 | 4.1 | -2.7 | 0.0 | 0.0 | 5.9 | 0.0 | 0.0 | 0.2 |
| 1861 648727.75 4772964.09 187.15 0 DEN A 71.7 14.4 0.0 0.0 0.0 70.3 4.1 -2.7 0.0 | 1837 | 648694.57 | 4772873.82 | 149.50 | 0 | DEN | A | 71.7 | 2.4 | 0.0 | 0.0 | 0.0 | 70.4 | 4.1 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | -2.4 |
| 1888 648703.57 4772957.74 187.20 0 DEN A 71.7 13.5 0.0 0.0 70.5 4.1 2.8 0.0< | 1861 | 648727.75 | 4772964.09 | 187.15 | 0 | DEN | A | 71.7 | 14.4 | 0.0 | 0.0 | 0.0 | 70.3 | 4.1 | -2.7 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 14.5 |
| 1892 648520.98 4772907.90 187.83 0 DEN A 71.7 1.2 0.0 0.0 71.9 4.6 -2.8 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 71.9 4.5 -2.8 0.0 0. | 1888 | 648703.57 | 4772957.74 | 187.20 | 0 | DEN | A | 71.7 | 13.5 | 0.0 | 0.0 | 0.0 | 70.5 | 4.1 | -2.8 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 13.4 |
| 1893 648526.62 4772909.39 187.76 0 DEN A 71.7 10.1 0.0 0.0 71.9 4.5 -2.8 0.0 | 1892 | 648520.98 | 4772907.90 | 187.83 | 0 | DEN | A | 71.7 | 1.2 | 0.0 | 0.0 | 0.0 | 71.9 | 4.6 | -2.8 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | -0.8 |
| 1896 648536.87 4772912.10 187.63 0 DEN A 71.7 10.4 0.0 0.0 71.8 4.5 2.8 0.0< | 1893 | 648526.62 | 4772909.39 | 187.76 | 0 | DEN | A | 71.7 | 10.1 | 0.0 | 0.0 | 0.0 | 71.9 | 4.5 | -2.8 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 8.3 |
| 1898 648544.39 4772914.08 187.53 0 DEN A 71.7 6.7 0.0 0.0 71.7 4.5 -2.8 0.0< | 1896 | 648536.87 | 4772912.10 | 187.63 | 0 | DEN | A | 71.7 | 10.4 | 0.0 | 0.0 | 0.0 | 71.8 | 4.5 | -2.8 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 8.6 |
| 1902 648682.94 4772952.40 187.24 0 DEN A 71.7 13.1 0.0 0.0 70.7 4.2 2.8 0.0 0.0 0.0 0.0 0.0 12.7 1932 648691.53 4772858.14 149.50 0 DEN A 71.7 0.9 0.0 0.0 70.4 4.1 2.7 0.0 0.0 4.7 0.0 0.0 -3.9 1935 648691.07 4772854.03 149.50 0 DEN A 71.7 2.5 0.0 0.0 70.4 4.1 -2.7 0.0 0.0 4.8 0.0 0.0 4.4 2.7 0.0 0.0 4.4 0.0 0.0 0.0 70.4 4.1 -2.7 0.0 0.0 4.7 0.0 0.0 4.4 2.7 0.0 0.0 4.7 0.0 0.0 4.4 1.2.7 0.0 0.0 4.1 2.7 0.0 0.0 4.1 2.7 0.0 0.0 4.1 2.7 0.0 0.0 4.1 2.7 0.0 0.0 </td <td>1898</td> <td>648544.39</td> <td>4772914.08</td> <td>187.53</td> <td>0</td> <td>DEN</td> <td>A</td> <td>71.7</td> <td>6.7</td> <td>0.0</td> <td>0.0</td> <td>0.0</td> <td>71.7</td> <td>4.5</td> <td>-2.8</td> <td>0.0</td> <td>0.0</td> <td>0.0</td> <td>0.0</td> <td>0.0</td> <td>5.0</td> | 1898 | 648544.39 | 4772914.08 | 187.53 | 0 | DEN | A | 71.7 | 6.7 | 0.0 | 0.0 | 0.0 | 71.7 | 4.5 | -2.8 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 5.0 |
| 1932 648691.53 4772858.14 149.50 0 DEN A 71.7 0.9 0.0 0.0 70.4 4.1 -2.7 0.0 0.0 4.7 0.0 0.0 -3.9 1935 648691.07 4772856.22 149.50 0 DEN A 71.7 2.5 0.0 0.0 70.4 4.1 -2.7 0.0 0.0 4.7 0.0 0.0 -4.3 1943 648689.420 4772872.02 149.50 0 DEN A 71.7 2.9 0.0 0.0 70.4 4.1 -2.7 0.0 0.0 4.7 0.0 0.0 -1.9 2006 648694.20 4772872.02 149.50 0 DEN A 71.7 2.9 0.0 0.0 70.4 4.1 -2.7 0.0 0.0 4.7 0.0 0.0 -1.4 2011 648693.23 4772864.36 149.50 0 DEN A 71.7 6.1 0.0 0.0 70.4 4.1 -2.7 0.0 0.0 4.7 0.0 | 1902 | 648682.94 | 4772952.40 | 187.24 | 0 | DEN | A | 71.7 | 13.1 | 0.0 | 0.0 | 0.0 | 70.7 | 4.2 | -2.8 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 12.7 |
| 1935 648691.07 4772856.22 149.50 0 DEN A 71.7 4.3 0.0 0.0 70.4 4.1 -2.7 0.0 0.0 4.7 0.0 0.0 -4.4 1940 648690.55 4772854.03 149.50 0 DEN A 71.7 2.5 0.0 0.0 70.4 4.1 -2.7 0.0 0.0 6.8 0.0 0.0 -4.3 1943 648689.42 4772847.25 149.50 0 DEN A 71.7 2.9 0.0 0.0 70.4 4.1 -2.7 0.0 0.0 4.7 0.0 0.0 -1.9 2006 648693.23 4772869.99 149.50 0 DEN A 71.7 3.4 0.0 0.0 70.4 4.1 -2.7 0.0 0.0 4.7 0.0 0.0 -1.4 2011 648693.23 4772864.36 149.50 0 DEN A 71.7 6.1 0.0 0.0 70.4 4.1 -2.7 0.0 0.0 4.7 0.0 | 1932 | 648691.53 | 4772858.14 | 149.50 | 0 | DEN | A | 71.7 | 0.9 | 0.0 | 0.0 | 0.0 | 70.4 | 4.1 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | -3.9 |
| 1940 648690.55 4772854.03 149.50 0 DEN A 71.7 2.5 0.0 0.0 70.4 4.1 -2.7 0.0 0.0 6.8 0.0 0.0 -4.3 1943 648688.94 4772847.25 149.50 0 DEN A 71.7 10.8 0.0 0.0 70.4 4.1 -2.7 0.0 0.0 4.7 0.0 0.0 6.6 2006 648694.20 4772872.02 149.50 0 DEN A 71.7 2.9 0.0 0.0 70.4 4.1 -2.7 0.0 0.0 4.7 0.0 0.0 -1.9 2008 648693.82 4772860.93 149.50 0 DEN A 71.7 6.1 0.0 0.0 70.4 4.1 -2.7 0.0 0.0 4.7 0.0 0.0 -1.4 2011 648692.74 4772864.36 149.50 0 DEN A 71.7 0.7 0.0 0.0 70.4 4.1 -2.7 0.0 0.0 4.7 0.0 | 1935 | 648691.07 | 4772856.22 | 149.50 | 0 | DEN | A | 71.7 | 4.3 | 0.0 | 0.0 | 0.0 | 70.4 | 4.1 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | -0.4 |
| 1943 648688.94 4772847.25 149.50 0 DEN A 71.7 10.8 0.0 0.0 70.4 4.1 -2.7 0.0 0.0 4.7 0.0 0.0 6.1 2006 648694.20 4772872.02 149.50 0 DEN A 71.7 2.9 0.0 0.0 70.4 4.1 -2.7 0.0 0.0 4.7 0.0 0.0 -1.9 2008 648693.82 4772869.99 149.50 0 DEN A 71.7 3.4 0.0 0.0 70.4 4.1 -2.7 0.0 0.0 4.7 0.0 0.0 -1.4 2011 648693.23 4772864.36 149.50 0 DEN A 71.7 6.1 0.0 0.0 70.4 4.1 -2.7 0.0 0.0 4.7 0.0 0.0 -4.1 2011 648692.34 4772864.36 149.50 0 DEN A 71.7 4.9 0.0 0.0 70.4 4.1 -2.7 0.0 0.0 4.7 0.0 | 1940 | 648690.55 | 4772854.03 | 149.50 | 0 | DEN | A | 71.7 | 2.5 | 0.0 | 0.0 | 0.0 | 70.4 | 4.1 | -2.7 | 0.0 | 0.0 | 6.8 | 0.0 | 0.0 | -4.3 |
| 2006 648694.20 4772872.02 149.50 0 DEN A 71.7 2.9 0.0 0.0 70.4 4.1 -2.7 0.0 0.0 4.7 0.0 0.0 -1.9 2008 648693.82 4772869.99 149.50 0 DEN A 71.7 3.4 0.0 0.0 70.4 4.1 -2.7 0.0 0.0 4.7 0.0 0.0 -1.4 2011 648693.23 4772866.93 149.50 0 DEN A 71.7 6.1 0.0 0.0 70.4 4.1 -2.7 0.0 0.0 4.7 0.0 0.0 -1.4 2014 648692.74 4772864.36 149.50 0 DEN A 71.7 0.7 0.0 0.0 70.4 4.1 -2.7 0.0 0.0 4.7 0.0 0.0 -4.1 2017 648692.34 4772859.75 149.50 0 DEN A 71.7 3.2 0.0 0.0 70.4 4.1 -2.7 0.0 0.0 4.7 0.0 | 1943 | 648688.94 | 4772847.25 | 149.50 | 0 | DEN | A | 71.7 | 10.8 | 0.0 | 0.0 | 0.0 | 70.4 | 4.1 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | 6.1 |
| 2008 648693.82 4772869.99 149.50 0 DEN A 71.7 3.4 0.0 0.0 70.4 4.1 -2.7 0.0 0.0 4.7 0.0 0.0 -1.4 2011 648693.23 4772866.93 149.50 0 DEN A 71.7 6.1 0.0 0.0 70.4 4.1 -2.7 0.0 0.0 4.7 0.0 0.0 1.3 2014 648692.74 4772864.36 149.50 0 DEN A 71.7 0.7 0.0 0.0 70.4 4.1 -2.7 0.0 0.0 4.7 0.0 0.0 -4.1 2017 648692.34 4772852.75 149.50 0 DEN A 71.7 3.2 0.0 0.0 70.4 4.1 -2.7 0.0 0.0 4.7 0.0 0.0 -1.4 2019 648691.86 4772859.75 149.50 0 DEN A 71.7 3.2 0.0 0.0 70.0 4.0 -2.7 0.0 0.0 4.7 0.0 | 2006 | 648694.20 | 4772872.02 | 149.50 | 0 | DEN | A | 71.7 | 2.9 | 0.0 | 0.0 | 0.0 | 70.4 | 4.1 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | -1.9 |
| 2011 648693.23 4772866.93 149.50 0 DEN A 71.7 6.1 0.0 0.0 70.4 4.1 -2.7 0.0 0.0 4.7 0.0 0.0 1.3 2014 648692.74 4772864.36 149.50 0 DEN A 71.7 0.7 0.0 0.0 70.4 4.1 -2.7 0.0 0.0 4.7 0.0 0.0 -4.1 2017 648692.34 4772862.28 149.50 0 DEN A 71.7 4.9 0.0 0.0 70.4 4.1 -2.7 0.0 0.0 4.7 0.0 0.0 -4.1 2019 648691.86 4772859.75 149.50 0 DEN A 71.7 3.2 0.0 0.0 70.4 4.1 -2.7 0.0 0.0 4.7 0.0 0.0 -1.6 2095 648749.24 4772936.89 149.50 0 DEN A 71.7 9.2 0.0 0.0 70.1 4.0 -2.7 0.0 0.0 4.6 2.7 | 2008 | 648693.82 | 4772869.99 | 149.50 | 0 | DEN | A | 71.7 | 3.4 | 0.0 | 0.0 | 0.0 | 70.4 | 4.1 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | -1.4 |
| 2014 648692.74 4772864.36 149.50 0 DEN A 71.7 0.7 0.0 0.0 70.4 4.1 -2.7 0.0 0.0 4.7 0.0 0.0 -4.1 2017 648692.34 4772862.28 149.50 0 DEN A 71.7 4.9 0.0 0.0 70.4 4.1 -2.7 0.0 0.0 4.7 0.0 0.0 0.1 2019 648691.86 4772859.75 149.50 0 DEN A 71.7 3.2 0.0 0.0 70.4 4.1 -2.7 0.0 0.0 4.7 0.0 0.0 -1.6 2095 648749.24 4772936.89 149.50 0 DEN A 71.7 9.2 0.0 0.0 70.0 4.0 -2.7 0.0 0.0 4.7 0.0 0.0 9.5 2120 648745.26 4772967.67 187.11 0 DEN A 71.7 8.9 0.0 0.0 70.0 4.0 -2.7 0.0 0.0 4.6 2.12 | 2011 | 648693.23 | 4772866.93 | 149.50 | 0 | DEN | A | 71.7 | 6.1 | 0.0 | 0.0 | 0.0 | 70.4 | 4.1 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | 1.3 |
| 2017 648692.34 4772862.28 149.50 0 DEN A 71.7 4.9 0.0 0.0 70.4 4.1 -2.7 0.0 0.0 4.7 0.0 0.0 0.1 2019 648691.86 4772859.75 149.50 0 DEN A 71.7 3.2 0.0 0.0 70.4 4.1 -2.7 0.0 0.0 4.7 0.0 0.0 -1.6 2095 648749.24 4772936.89 149.50 0 DEN A 71.7 9.2 0.0 0.0 70.0 4.0 -2.7 0.0 0.0 4.7 0.0 0.0 5.7 2120 648745.26 4772967.67 187.11 0 DEN A 71.7 9.2 0.0 0.0 70.0 4.0 -2.7 0.0 0.0 0.0 9.5 2131 648754.61 4772943.40 149.50 0 DEN A 71.7 8.9 0.0 0.0 70.1 4.0 -2.7 0.0 0.0 4.6 2.12 648751.23 4772964. | 2014 | 648692.74 | 4772864.36 | 149.50 | 0 | DEN | A | 71.7 | 0.7 | 0.0 | 0.0 | 0.0 | 70.4 | 4.1 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | -4.1 |
| 2019 648691.86 4772859.75 149.50 0 DEN A 71.7 3.2 0.0 0.0 70.4 4.1 -2.7 0.0 0.0 4.7 0.0 0.0 -1.6 2095 648749.24 4772936.89 149.50 0 DEN A 71.7 10.0 0.0 0.0 70.0 4.0 -2.7 0.0 0.0 4.7 0.0 0.0 5.7 2120 648745.26 4772967.67 187.11 0 DEN A 71.7 9.2 0.0 0.0 70.0 4.0 -2.7 0.0 0.0 0.0 9.5 2131 648754.61 4772943.40 149.50 0 DEN A 71.7 8.9 0.0 0.0 70.0 4.0 -2.7 0.0 0.0 4.6 2142 648751.23 4772964.48 187.11 0 DEN A 71.7 8.6 0.0 0.0 70.0 4.0 -2.7 0.0 0.0 0.0 4.6 2142 648751.23 4772905.30 187.89 0 <td< td=""><td>2017</td><td>648692.34</td><td>4772862.28</td><td>149.50</td><td>0</td><td>DEN</td><td>A</td><td>71.7</td><td>4.9</td><td>0.0</td><td>0.0</td><td>0.0</td><td>70.4</td><td>4.1</td><td>-2.7</td><td>0.0</td><td>0.0</td><td>4.7</td><td>0.0</td><td>0.0</td><td>0.1</td></td<> | 2017 | 648692.34 | 4772862.28 | 149.50 | 0 | DEN | A | 71.7 | 4.9 | 0.0 | 0.0 | 0.0 | 70.4 | 4.1 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | 0.1 |
| 2095 648749.24 4772936.89 149.50 0 DEN A 71.7 10.0 0.0 0.0 70.0 4.0 -2.7 0.0 0.0 4.7 0.0 0.0 5.7 2120 648745.26 4772967.67 187.11 0 DEN A 71.7 9.2 0.0 0.0 70.0 4.0 -2.7 0.0 0.0 0.0 9.5 2131 648754.61 4772943.40 149.50 0 DEN A 71.7 8.9 0.0 0.0 70.0 4.0 -2.7 0.0 0.0 4.0 0.0 0.0 4.6 2.7 0.0 0.0 4.0 -2.7 0.0 0.0 0.0 9.5 2131 648754.61 4772943.40 149.50 0 DEN A 71.7 8.9 0.0 0.0 70.0 4.0 -2.7 0.0 0.0 4.0 -2.7 0.0 0.0 0.0 9.0 2142 648511.34 4772905.30 187.89 0 DEN A 71.7 0.5 | 2019 | 648691.86 | 4772859.75 | 149.50 | 0 | DEN | A | 71.7 | 3.2 | 0.0 | 0.0 | 0.0 | 70.4 | 4.1 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | -1.6 |
| 2120 648745.26 4772967.67 187.11 0 DEN A 71.7 9.2 0.0 0.0 70.1 4.0 -2.7 0.0 0.0 0.0 0.0 9.5 2131 648754.61 4772943.40 149.50 0 DEN A 71.7 8.9 0.0 0.0 70.0 4.0 -2.7 0.0 0.0 4.7 0.0 0.0 4.6 2142 648751.23 4772964.48 187.11 0 DEN A 71.7 8.6 0.0 0.0 70.1 4.0 -2.7 0.0 0.0 0.0 4.6 2142 64851.23 4772965.30 187.89 0 DEN A 71.7 0.5 0.0 0.0 70.1 4.0 -2.7 0.0 0.0 0.0 0.0 9.0 2162 648516.12 4772905.30 187.86 0 DEN A 71.7 9.4 0.0 0.0 71.9 4.6 -2.7 0.0 0.0 0.0 0.0 7.4 2163 648516.12 | 2095 | 648749.24 | 4772936.89 | 149.50 | 0 | DEN | A | 71.7 | 10.0 | 0.0 | 0.0 | 0.0 | 70.0 | 4.0 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | 5.7 |
| 2131 648754.61 4772943.40 149.50 0 DEN A 71.7 8.9 0.0 0.0 70.0 4.0 -2.7 0.0 0.0 4.7 0.0 0.0 4.6 2142 648751.23 4772964.48 187.11 0 DEN A 71.7 8.6 0.0 0.0 70.1 4.0 -2.7 0.0 0.0 0.0 9.0 2162 648511.34 4772905.30 187.89 0 DEN A 71.7 9.6 0.0 0.0 70.0 4.0 -2.7 0.0 0.0 0.0 9.0 2162 648516.12 4772905.30 187.89 0 DEN A 71.7 9.4 0.0 0.0 71.9 4.6 -2.7 0.0 0.0 0.0 0.0 -1.7 2163 648516.12 4772906.59 187.86 0 DEN A 71.7 9.4 0.0 0.0 71.9 4.6 -2.7 0.0 0.0 0.0 0.0 7.4 2225 648703.63 4772912. | 2120 | 648745.26 | 4772967.67 | 187.11 | 0 | DEN | A | 71.7 | 9.2 | 0.0 | 0.0 | 0.0 | 70.1 | 4.0 | -2.7 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 9.5 |
| 2142 648751.23 4772964.48 187.11 0 DEN A 71.7 8.6 0.0 0.0 70.1 4.0 -2.7 0.0 0.0 0.0 0.0 9.0 2162 648511.34 4772905.30 187.89 0 DEN A 71.7 0.5 0.0 0.0 72.0 4.6 -2.7 0.0 0.0 0.0 0.0 -1.7 2163 648516.12 4772906.59 187.86 0 DEN A 71.7 9.4 0.0 0.0 71.9 4.6 -2.7 0.0 0.0 0.0 0.0 7.4 2225 648703.63 4772912.51 149.50 0 DEN A 71.7 7.7 0.0 0.0 70.4 4.1 -2.7 0.0 0.0 0.0 7.4 2225 648703.63 4772912.51 149.50 0 DEN A 71.7 7.7 0.0 0.0 70.4 4.1 -2.7 0.0 0.0 4.0 0.0 0.0 3.0 3.0 3.0 3.0 </td <td>2131</td> <td>648754.61</td> <td>4772943.40</td> <td>149.50</td> <td>0</td> <td>DEN</td> <td>A</td> <td>71.7</td> <td>8.9</td> <td>0.0</td> <td>0.0</td> <td>0.0</td> <td>70.0</td> <td>4.0</td> <td>-2.7</td> <td>0.0</td> <td>0.0</td> <td>4.7</td> <td>0.0</td> <td>0.0</td> <td>4.6</td> | 2131 | 648754.61 | 4772943.40 | 149.50 | 0 | DEN | A | 71.7 | 8.9 | 0.0 | 0.0 | 0.0 | 70.0 | 4.0 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | 4.6 |
| 2162 648511.34 4772905.30 187.89 0 DEN A 71.7 0.5 0.0 0.0 72.0 4.6 -2.7 0.0 0.0 0.0 -1.7 2163 648516.12 4772906.59 187.86 0 DEN A 71.7 9.4 0.0 0.0 71.9 4.6 -2.7 0.0 0.0 0.0 0.0 7.4 2225 648703.63 4772912.51 149.50 0 DEN A 71.7 7.7 0.0 0.0 70.4 4.1 -2.7 0.0 0.0 0.0 0.0 3.0 | 2142 | 648751.23 | 4772964.48 | 187.11 | 0 | DEN | A | 71.7 | 8.6 | 0.0 | 0.0 | 0.0 | 70.1 | 4.0 | -2.7 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 9.0 |
| 2163 648516.12 4772906.59 187.86 0 DEN A 71.7 9.4 0.0 0.0 71.9 4.6 -2.7 0.0 0.0 0.0 7.4 2225 648703.63 4772912.51 149.50 0 DEN A 71.7 7.7 0.0 0.0 70.4 4.1 -2.7 0.0 0.0 0.0 3.0 | 2162 | 648511.34 | 4772905.30 | 187.89 | 0 | DEN | A | 71.7 | 0.5 | 0.0 | 0.0 | 0.0 | 72.0 | 4.6 | -2.7 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | -1.7 |
| 2225 648703.63 4772912.51 149.50 0 DEN A 71.7 7.7 0.0 0.0 70.4 4.1 -2.7 0.0 0.0 4.7 0.0 0.0 3.0 | 2163 | 648516.12 | 4772906.59 | 187.86 | 0 | DEN | A | 71.7 | 9.4 | 0.0 | 0.0 | 0.0 | 71.9 | 4.6 | -2.7 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 7.4 |
| | 2225 | 648703.63 | 4772912.51 | 149.50 | 0 | DEN | A | 71.7 | 7.7 | 0.0 | 0.0 | 0.0 | 70.4 | 4.1 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | 3.0 |

| | | Point Sourc | e, ISO 9 | 613, N | lame: | "P4_\$ | SE, PP | Seco | ndary Cr | usher | ", ID: | "P4_ | SE_PF | _Sec | conda | ryCrush | 2" | | | |
|------|-----------|-------------|----------|--------|-------|--------|--------|------|----------|-------|--------|------|-------|------|-------|---------|------|------|------|-------|
| Nr. | Х | Y | Z | Refl. | DEN | Freq. | Lw | l/a | Optime | K0 | Di | Adiv | Aatm | Agr | Afol | Ahous | Abar | Cmet | RL | Lr |
| | (m) | (m) | (m) | | | (Hz) | dB(A) | dB | dB | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | dB(A) |
| 1654 | 649166.16 | 4772898.39 | 149.00 | 0 | D | Α | 114.6 | 0.0 | 0.0 | 0.0 | 0.0 | 64.8 | 2.8 | -2.6 | 0.0 | 0.0 | 11.8 | 0.0 | 0.0 | 37.9 |

| | | Point Sourc | e, ISO 9 | 613, I | lame: | "P4_\$ | SE, PP | Seco | ndary Cr | usher | ", ID: | "P4_ | SE_PF | _Sec | onda | ryCrusł | 11" | | | |
|------|-----------|-------------|----------|---------------|-------|--------|--------|------|----------|-------|--------|------|-------|------|------|---------|------|------|------|-------|
| Nr. | Х | Y | Z | Refl. | DEN | Freq. | Lw | l/a | Optime | K0 | Di | Adiv | Aatm | Agr | Afol | Ahous | Abar | Cmet | RL | Lr |
| | (m) | (m) | (m) | | | (Hz) | dB(A) | dB | dB | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | dB(A) |
| 1655 | 649165.78 | 4772899.34 | 149.00 | 0 | D | A | 114.6 | 0.0 | 0.0 | 0.0 | 0.0 | 64.8 | 2.8 | -2.6 | 0.0 | 0.0 | 11.6 | 0.0 | 0.0 | 38.0 |

| | | Poir | nt Source | e, ISO | 9613 | , Nam | e: "Asp | halt P | lant - Idli | ng Tr | uck", | ID: "/ | ASPH_ | IDLE | _TRK | (2" | | | | |
|------|-----------|------------|-----------|--------|------|-------|---------|--------|-------------|-------|-------|--------|-------|------|------|-------|------|------|------|--------|
| Nr. | Х | Y | Z | Refl. | DEN | Freq. | Lw | l/a | Optime | K0 | Di | Adiv | Aatm | Agr | Afol | Ahous | Abar | Cmet | RL | Lr |
| | (m) | (m) | (m) | | | (Hz) | dB(A) | dB | dB | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | dB(A) |
| 1657 | 648879.73 | 4772824.63 | 149.50 | 0 | D | A | 96.3 | 0.0 | 0.0 | 0.0 | 0.0 | 68.4 | 3.5 | -2.9 | 0.0 | 0.0 | 4.8 | 0.0 | 0.0 | 22.5 |
| 1660 | 648879.73 | 4772824.63 | 149.50 | 1 | D | A | 96.3 | 0.0 | 0.0 | 0.0 | 0.0 | 68.5 | 3.6 | -2.9 | 0.0 | 0.0 | 14.7 | 0.0 | 59.5 | -47.0 |
| 1662 | 648879.73 | 4772824.63 | 149.50 | 1 | D | A | 96.3 | 0.0 | 0.0 | 0.0 | 0.0 | 69.0 | 3.7 | -3.0 | 0.0 | 0.0 | 4.8 | 0.0 | 32.2 | -110.5 |

| | | Poir | nt Source | e, ISC | 9613 | , Nam | e: "Asp | halt P | lant - Idli | ng Tr | uck", | ID: "A | SPH_ | IDLE | _TRK | (1" | | | | |
|------|-----------|------------|-----------|--------|------|-------|---------|--------|-------------|-------|-------|--------|------|------|------|-------|------|------|------|--------|
| Nr. | Х | Y | Z | Refl. | DEN | Freq. | Lw | l/a | Optime | K0 | Di | Adiv | Aatm | Agr | Afol | Ahous | Abar | Cmet | RL | Lr |
| | (m) | (m) | (m) | | | (Hz) | dB(A) | dB | dB | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | dB(A) |
| 1666 | 648879.52 | 4772825.56 | 149.50 | 0 | D | A | 96.3 | 0.0 | 0.0 | 0.0 | 0.0 | 68.4 | 3.5 | -2.9 | 0.0 | 0.0 | 4.8 | 0.0 | 0.0 | 22.5 |
| 1670 | 648879.52 | 4772825.56 | 149.50 | 1 | D | A | 96.3 | 0.0 | 0.0 | 0.0 | 0.0 | 68.5 | 3.6 | -2.9 | 0.0 | 0.0 | 15.3 | 0.0 | 59.6 | -47.8 |
| 1672 | 648879.52 | 4772825.56 | 149.50 | 1 | D | A | 96.3 | 0.0 | 0.0 | 0.0 | 0.0 | 69.0 | 3.7 | -3.0 | 0.0 | 0.0 | 4.8 | 0.0 | 32.2 | -110.4 |

| | Point S | ource, ISO 96 | 613, Nan | 1e: "Р | 4_SE, | , PP S | econda | ry & 1 | ertiary S | creer | n", ID | : "P4_ | SE_PF | P_Se | conda | aryTertia | arySci | reen2" | | |
|------|-----------|---------------|----------|--------|-------|--------|--------|--------|-----------|-------|--------|--------|-------|------|-------|-----------|--------|--------|------|-------|
| Nr. | Х | Y | Z | Refl. | DEN | Freq. | Lw | l/a | Optime | K0 | Di | Adiv | Aatm | Agr | Afol | Ahous | Abar | Cmet | RL | Lr |
| | (m) | (m) | (m) | | | (Hz) | dB(A) | dB | dB | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | dB(A) |
| 1674 | 649164.92 | 4772897.98 | 149.00 | 0 | D | A | 113.8 | 0.0 | 0.0 | 0.0 | 0.0 | 64.8 | 3.0 | -2.6 | 0.0 | 0.0 | 11.0 | 0.0 | 0.0 | 37.5 |

| | Point S | ource, ISO 96 | 613, Nan | ie: "P | 4_SE, | PP S | econda | ry & T | ertiary S | creer | ו", ID | : "P4_ | SE_PF | _Se | conda | aryTertia | arySci | reen1" | | |
|------|-----------|---------------|----------|--------|-------|-------|--------|--------|-----------|-------|--------|--------|-------|------|-------|-----------|--------|--------|------|-------|
| Nr. | Х | Y | Z | Refl. | DEN | Freq. | Lw | l/a | Optime | K0 | Di | Adiv | Aatm | Agr | Afol | Ahous | Abar | Cmet | RL | Lr |
| | (m) | (m) | (m) | | | (Hz) | dB(A) | dB | dB | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | dB(A) |
| 1677 | 649164.51 | 4772898.84 | 149.00 | 0 | D | A | 113.8 | 0.0 | 0.0 | 0.0 | 0.0 | 64.8 | 3.0 | -2.6 | 0.0 | 0.0 | 10.9 | 0.0 | 0.0 | 37.6 |

| | Line Sou | urce, ISO 961 | 3, Name | : "P4 | SE, A | ggreg | ate Hau | ul road | b/w PP | and A | \ Ρ, Ε | mpty" | , ID: "F | P4_SI | E_RD | _Haul_ | PP_A | P_Em' | | |
|------|-----------|---------------|---------|-------|-------|-------|---------|---------|--------|-------|---------------|-------|----------|-------|------|--------|------|-------|------|--------|
| Nr. | Х | Y | Z | Refl. | DEN | Freq. | Lw | l/a | Optime | K0 | Di | Adiv | Aatm | Agr | Afol | Ahous | Abar | Cmet | RL | Lr |
| | (m) | (m) | (m) | | | (Hz) | dB(A) | dB | dB | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | dB(A) |
| 1686 | 649132.52 | 4772888.09 | 149.50 | 0 | DEN | A | 69.7 | 13.8 | 0.0 | 0.0 | 0.0 | 65.3 | 2.4 | -2.5 | 0.0 | 0.0 | 5.1 | 0.0 | 0.0 | 13.3 |
| 1688 | 649079.54 | 4772851.39 | 149.50 | 0 | DEN | A | 69.7 | 20.2 | 0.0 | 0.0 | 0.0 | 65.9 | 2.5 | -2.6 | 0.0 | 0.0 | 4.9 | 0.0 | 0.0 | 19.2 |
| 1762 | 649018.07 | 4772813.70 | 149.50 | 0 | DEN | A | 69.7 | 16.0 | 0.0 | 0.0 | 0.0 | 66.6 | 2.7 | -2.6 | 0.0 | 0.0 | 4.8 | 0.0 | 0.0 | 14.2 |
| 1767 | 648907.31 | 4772812.89 | 149.50 | 0 | DEN | A | 69.7 | 17.3 | 0.0 | 0.0 | 0.0 | 68.1 | 3.0 | -2.7 | 0.0 | 0.0 | 4.8 | 0.0 | 0.0 | 13.8 |
| 1769 | 648907.31 | 4772812.89 | 149.50 | 1 | DEN | A | 69.7 | 17.3 | 0.0 | 0.0 | 0.0 | 68.6 | 3.2 | -2.8 | 0.0 | 0.0 | 4.8 | 0.0 | 18.0 | -4.9 |
| 1770 | 648907.31 | 4772812.89 | 149.50 | 1 | DEN | A | 69.7 | 17.3 | 0.0 | 0.0 | 0.0 | 68.7 | 3.2 | -2.8 | 0.0 | 0.0 | 4.8 | 0.0 | 54.4 | -41.3 |
| 1772 | 648907.31 | 4772812.89 | 149.50 | 1 | DEN | A | 69.7 | 17.3 | 0.0 | 0.0 | 0.0 | 68.7 | 3.2 | -2.8 | 0.0 | 0.0 | 4.8 | 0.0 | 18.7 | -5.6 |
| 1774 | 648907.31 | 4772812.89 | 149.50 | 1 | DEN | A | 69.7 | 17.3 | 0.0 | 0.0 | 0.0 | 68.7 | 3.2 | -2.8 | 0.0 | 0.0 | 4.8 | 0.0 | 53.9 | -40.8 |
| 1779 | 648954.09 | 4772802.59 | 149.50 | 0 | DEN | A | 69.7 | 16.3 | 0.0 | 0.0 | 0.0 | 67.5 | 2.9 | -2.7 | 0.0 | 0.0 | 4.8 | 0.0 | 0.0 | 13.5 |
| 1781 | 648954.09 | 4772802.59 | 149.50 | 1 | DEN | A | 69.7 | 16.3 | 0.0 | 0.0 | 0.0 | 69.2 | 3.4 | -2.8 | 0.0 | 0.0 | 4.8 | 0.0 | 31.8 | -120.3 |
| 1783 | 648954.09 | 4772802.59 | 149.50 | 1 | DEN | A | 69.7 | 16.3 | 0.0 | 0.0 | 0.0 | 69.2 | 3.3 | -2.8 | 0.0 | 0.0 | 4.8 | 0.0 | 31.3 | -119.8 |
| 1843 | 648987.53 | 4772802.96 | 149.50 | 0 | DEN | A | 69.7 | 14.0 | 0.0 | 0.0 | 0.0 | 67.0 | 2.8 | -2.6 | 0.0 | 0.0 | 4.8 | 0.0 | 0.0 | 11.7 |
| 1845 | 648987.53 | 4772802.96 | 149.50 | 1 | DEN | A | 69.7 | 14.0 | 0.0 | 0.0 | 0.0 | 69.5 | 3.4 | -2.8 | 0.0 | 0.0 | 4.8 | 0.0 | 36.3 | -127.5 |
| 1847 | 648987.53 | 4772802.96 | 149.50 | 1 | DEN | A | 69.7 | 14.0 | 0.0 | 0.0 | 0.0 | 69.5 | 3.4 | -2.8 | 0.0 | 0.0 | 4.8 | 0.0 | 35.9 | -127.1 |

| | Line | e Source, ISO | 9613, N | ame: | "AP, / | AC and | RAP | shippe | d from C | Offsite | , Em | pty", I | D: "AP | _RD | SHP | _AC_R | AP_E | m'' | | |
|------|-----------|---------------|---------|-------|--------|--------|-------|--------|----------|---------|------|---------|--------|------|------|-------|------|------|------|-------|
| Nr. | Х | Y | Z | Refl. | DEN | Freq. | Lw | l/a | Optime | K0 | Di | Adiv | Aatm | Agr | Afol | Ahous | Abar | Cmet | RL | Lr |
| | (m) | (m) | (m) | | | (Hz) | dB(A) | dB | dB | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | dB(A) |
| 1805 | 648854.10 | 4772824.67 | 149.50 | 0 | DEN | Α | 68.7 | 17.0 | 0.0 | 0.0 | 0.0 | 68.7 | 3.6 | -2.6 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | 11.3 |
| 1807 | 648854.10 | 4772824.67 | 149.50 | 1 | DEN | Α | 68.7 | 17.0 | 0.0 | 0.0 | 0.0 | 68.7 | 3.6 | -2.6 | 0.0 | 0.0 | 4.7 | 0.0 | 19.9 | -8.6 |
| 1852 | 648748.87 | 4772829.28 | 149.50 | 0 | DEN | Α | 68.7 | 17.4 | 0.0 | 0.0 | 0.0 | 69.8 | 3.9 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | 10.3 |
| 1857 | 648582.08 | 4772924.01 | 187.43 | 0 | DEN | A | 68.7 | 18.4 | 0.0 | 0.0 | 0.0 | 71.4 | 4.4 | -2.8 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 14.1 |
| 1874 | 648716.72 | 4772961.26 | 187.17 | 0 | DEN | A | 68.7 | 17.0 | 0.0 | 0.0 | 0.0 | 70.4 | 4.1 | -2.8 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 14.0 |
| 1886 | 648724.77 | 4772924.42 | 149.50 | 0 | DEN | A | 68.7 | 16.4 | 0.0 | 0.0 | 0.0 | 70.2 | 4.0 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | 8.9 |
| 1890 | 648639.14 | 4772939.74 | 187.32 | 0 | DEN | A | 68.7 | 16.9 | 0.0 | 0.0 | 0.0 | 71.0 | 4.3 | -2.8 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 13.1 |
| 1956 | 648697.76 | 4772852.98 | 149.50 | 0 | DEN | A | 68.7 | 6.6 | 0.0 | 0.0 | 0.0 | 70.3 | 4.1 | -2.7 | 0.0 | 0.0 | 7.2 | 0.0 | 0.0 | -3.6 |
| 1958 | 648710.76 | 4772843.05 | 149.50 | 0 | DEN | A | 68.7 | 14.5 | 0.0 | 0.0 | 0.0 | 70.2 | 4.0 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | 7.0 |
| 1967 | 648816.82 | 4772822.79 | 149.50 | 0 | DEN | A | 68.7 | 13.9 | 0.0 | 0.0 | 0.0 | 69.1 | 3.7 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | 7.7 |
| 1985 | 648699.40 | 4772895.90 | 149.50 | 0 | DEN | Α | 68.7 | 14.4 | 0.0 | 0.0 | 0.0 | 70.4 | 4.1 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | 6.7 |
| 1987 | 648696.05 | 4772880.50 | 149.50 | 0 | DEN | A | 68.7 | 5.8 | 0.0 | 0.0 | 0.0 | 70.4 | 4.1 | -2.7 | 0.0 | 0.0 | 6.0 | 0.0 | 0.0 | -3.2 |
| 1989 | 648695.53 | 4772878.14 | 149.50 | 0 | DEN | A | 68.7 | 0.1 | 0.0 | 0.0 | 0.0 | 70.4 | 4.1 | -2.7 | 0.0 | 0.0 | 5.9 | 0.0 | 0.0 | -8.8 |
| 2035 | 648754.54 | 4772953.97 | 168.09 | 0 | DEN | A | 68.7 | 8.2 | 0.0 | 0.0 | 0.0 | 70.0 | 4.0 | -2.7 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 5.7 |
| 2037 | 648755.32 | 4772950.00 | 157.25 | 0 | DEN | A | 68.7 | 12.2 | 0.0 | 0.0 | 0.0 | 70.0 | 4.0 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | 4.9 |
| 2097 | 648784.26 | 4772822.42 | 149.50 | 0 | DEN | A | 68.7 | 12.4 | 0.0 | 0.0 | 0.0 | 69.5 | 3.8 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | 5.8 |
| 2112 | 648753.70 | 4772958.16 | 178.99 | 0 | DEN | A | 68.7 | 12.3 | 0.0 | 0.0 | 0.0 | 70.0 | 4.0 | -2.7 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 9.7 |
| 2148 | 648798.64 | 4772821.27 | 149.50 | 0 | DEN | A | 68.7 | 10.7 | 0.0 | 0.0 | 0.0 | 69.3 | 3.8 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | 4.3 |
| 2167 | 648695.49 | 4772876.08 | 149.50 | 0 | DEN | A | 68.7 | 5.0 | 0.0 | 0.0 | 0.0 | 70.4 | 4.1 | -2.7 | 0.0 | 0.0 | 5.9 | 0.0 | 0.0 | -4.0 |
| 2169 | 648695.63 | 4772872.62 | 149.50 | 0 | DEN | Α | 68.7 | 5.8 | 0.0 | 0.0 | 0.0 | 70.4 | 4.1 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | -2.0 |
| 2172 | 648695.75 | 4772869.63 | 149.50 | 0 | DEN | A | 68.7 | 3.5 | 0.0 | 0.0 | 0.0 | 70.4 | 4.1 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | -4.3 |
| 2174 | 648695.88 | 4772866.44 | 149.50 | 0 | DEN | Α | 68.7 | 6.2 | 0.0 | 0.0 | 0.0 | 70.4 | 4.1 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | -1.6 |
| 2177 | 648695.98 | 4772864.08 | 149.50 | 0 | DEN | A | 68.7 | -2.5 | 0.0 | 0.0 | 0.0 | 70.4 | 4.1 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | -10.2 |
| 2200 | 648526.89 | 4772909.46 | 187.86 | 0 | DEN | Α | 68.7 | 9.9 | 0.0 | 0.0 | 0.0 | 71.9 | 4.5 | -2.8 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 5.0 |
| 2203 | 648535.60 | 4772911.74 | 187.89 | 0 | DEN | A | 68.7 | 9.1 | 0.0 | 0.0 | 0.0 | 71.8 | 4.5 | -2.8 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 4.3 |
| 2231 | 648749.03 | 4772936.75 | 149.50 | 0 | DEN | Α | 68.7 | 10.3 | 0.0 | 0.0 | 0.0 | 70.0 | 4.0 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | 3.0 |
| 2261 | 648667.84 | 4772948.21 | 187.27 | 0 | DEN | Α | 68.7 | 10.5 | 0.0 | 0.0 | 0.0 | 70.8 | 4.2 | -2.8 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 7.0 |
| 2274 | 648695.99 | 4772861.94 | 149.50 | 0 | DEN | A | 68.7 | 5.7 | 0.0 | 0.0 | 0.0 | 70.4 | 4.1 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | -2.0 |
| 2277 | 648695.98 | 4772859.00 | 149.50 | 0 | DEN | Α | 68.7 | 3.3 | 0.0 | 0.0 | 0.0 | 70.4 | 4.1 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | -4.4 |
| 2280 | 648695.97 | 4772857.34 | 149.50 | 0 | DEN | Α | 68.7 | 0.8 | 0.0 | 0.0 | 0.0 | 70.4 | 4.1 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | -7.0 |
| 2282 | 648695.97 | 4772855.55 | 149.50 | 0 | DEN | A | 68.7 | 3.8 | 0.0 | 0.0 | 0.0 | 70.4 | 4.1 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | -3.9 |
| 2287 | 648745.25 | 4772967.66 | 187.11 | 0 | DEN | A | 68.7 | 9.3 | 0.0 | 0.0 | 0.0 | 70.1 | 4.0 | -2.7 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 6.6 |
| 2305 | 648754.63 | 4772943.48 | 149.50 | 0 | DEN | A | 68.7 | 8.9 | 0.0 | 0.0 | 0.0 | 70.0 | 4.0 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | 1.7 |
| 2308 | 648511.35 | 4772905.30 | 187.89 | 0 | DEN | A | 68.7 | 0.5 | 0.0 | 0.0 | 0.0 | 72.0 | 4.6 | -2.7 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | -4.6 |
| 2310 | 648516.74 | 4772906.76 | 187.87 | 0 | DEN | A | 68.7 | 10.0 | 0.0 | 0.0 | 0.0 | 71.9 | 4.6 | -2.7 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 5.0 |

| | Line | e Source, ISO | 9613, N | lame: | "AP, / | AC and | d RAP | shippe | ed from C | Offsite | e, Em | pty", I | D: "AP | _RD | _SHP | _AC_R | AP_E | m" | | |
|------|------------|---------------|---------|-------|--------|----------|--------|------------|-----------|---------|---------------------|---------|--------|------|------|-------|------|------------|------|-------|
| Nr. | Х | Y | Z | Refl. | DEN | Freq. | Lw | l/a | Optime | K0 | Di | Adiv | Aatm | Agr | Afol | Ahous | Abar | Cmet | RL | Lr |
| | (m) | (m) | (m) | | | (Hz) | dB(A) | dB | dB | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | dB(A) |
| 2312 | 648521.86 | 4772908 15 | 187.85 | 0 | DEN | Δ | 68.7 | -24 | 0.0 | 0.0 | 0.0 | 71 9 | 46 | -2.8 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | -7.3 |
| 2012 | 640751.00 | 4772064.42 | 106.05 | 0 | DEN | | 60.7 | 07 | 0.0 | 0.0 | 0.0 | 70.1 | 4.0 | 2.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 6.0 |
| 2001 | 040731.20 | 4772904.42 | 100.95 | 0 | DEN | | 00.7 | 0.7 | 0.0 | 0.0 | 0.0 | 70.1 | 4.0 | -2.1 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 2345 | 048088.03 | 4772953.85 | 187.23 | 0 | DEN | A | 68.7 | 8.9 | 0.0 | 0.0 | 0.0 | 70.6 | 4.2 | -2.8 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 5.7 |
| 2395 | 648703.62 | 4772912.28 | 149.50 | 0 | DEN | A | 68.7 | 7.9 | 0.0 | 0.0 | 0.0 | 70.4 | 4.1 | -2.7 | 0.0 | 0.0 | 4./ | 0.0 | 0.0 | 0.2 |
| 2417 | 648675.54 | 4772950.43 | 187.25 | 0 | DEN | A | 68.7 | 6.8 | 0.0 | 0.0 | 0.0 | 70.7 | 4.2 | -2.8 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 3.4 |
| 2426 | 648679.94 | 4772951.59 | 187.24 | 0 | DEN | A | 68.7 | 6.3 | 0.0 | 0.0 | 0.0 | 70.7 | 4.2 | -2.8 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 2.9 |
| 2445 | 648683.41 | 4772952.51 | 187.24 | 0 | DEN | A | 68.7 | 4.7 | 0.0 | 0.0 | 0.0 | 70.7 | 4.2 | -2.8 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 1.3 |
| 2447 | 648546.64 | 4772914.67 | 187.56 | 0 | DEN | A | 68.7 | 5.5 | 0.0 | 0.0 | 0.0 | 71.7 | 4.5 | -2.8 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.8 |
| 2450 | 648543 26 | 4772913 80 | 187 73 | 0 | DFN | A | 68 7 | 54 | 0.0 | 0.0 | 0.0 | 717 | 45 | -28 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 07 |
| 2470 | 648540 12 | 4772012 04 | 187.89 | 0 | DEN | Δ | 68.7 | 0.6 | 0.0 | 0.0 | 0.0 | 71.8 | 4.5 | -2.8 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | -4.2 |
| 2470 | 640541.22 | 4772012.04 | 107.05 | 0 | | | 60.7 | 2.0 | 0.0 | 0.0 | 0.0 | 71.0 | 4.5 | 2.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 7.7 |
| 2409 | 040541.55 | 4772913.29 | 107.03 | 0 | DEN | A . | 00.7 | -2.9 | 0.0 | 0.0 | 0.0 | 71.0 | 4.5 | -2.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | -1.1 |
| 2493 | 040040.00 | 4//2913.15 | 107.07 | 0 | DEIN | A | 00.7 | -3.0 | 0.0 | 0.0 | 0.0 | /1.0 | 4.5 | -2.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | -0.4 |
| | | Line Ce | | 0.004 | 0 N | | | ام میں م | | | - | | | 0115 | | A [| | | | |
| | | Line So | | 0 961 | 3, Na | me: A | P, HM/ | A proa | uct snip | bing, | Full [™] , | | P_RD | _SHF | | A_Fu | | a (| - | |
| Nr. | X | Y | Z | Refl. | DEN | Freq. | Lw | l/a | Optime | K0 | Di | Adiv | Aatm | Agr | Atol | Ahous | Abar | Cmet | RL | Lr |
| | (m) | (m) | (m) | | | (Hz) | dB(A) | dB | dB | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | dB(A) |
| 1811 | 648854.16 | 4772824.66 | 149.50 | 0 | DEN | A | 68.7 | 17.0 | 0.0 | 0.0 | 0.0 | 68.7 | 3.6 | -2.6 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | 11.3 |
| 1813 | 648854.16 | 4772824.66 | 149.50 | 1 | DEN | A | 68.7 | 17.0 | 0.0 | 0.0 | 0.0 | 68.7 | 3.6 | -2.6 | 0.0 | 0.0 | 4.7 | 0.0 | 19.7 | -8.4 |
| 1849 | 648748.85 | 4772829.22 | 149.50 | 0 | DEN | A | 68.7 | 17.4 | 0.0 | 0.0 | 0.0 | 69.8 | 3.9 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | 10.3 |
| 1859 | 648582.97 | 4772924.27 | 187.43 | 0 | DEN | A | 68.7 | 18.4 | 0.0 | 0.0 | 0.0 | 71.4 | 4.4 | -2.8 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 14.1 |
| 1881 | 648725.03 | 4772924 56 | 149 50 | 0 | DFN | Δ | 68 7 | 16 5 | 0.0 | 0.0 | 0.0 | 70.2 | 4 0 | -27 | 0.0 | 0.0 | 47 | 0.0 | 0.0 | 8.9 |
| 1801 | 648630 68 | 4772030 07 | 187 32 | n | DEN | | 68.7 | 16.8 | 0.0 | 0.0 | 0.0 | 71 0 | 4.3 | -2.8 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 13.0 |
| 1001 | 6/8722 52 | 1772062 02 | 187.02 | | DEN | | 69.7 | 15.6 | 0.0 | 0.0 | 0.0 | 70.2 | 7.3 | -2.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 10.0 |
| 1904 | 649607.90 | 4772903.03 | 140 50 | 0 | | | 60.7 | 6.7 | 0.0 | 0.0 | 0.0 | 70.3 | 4.1 | -2.0 | 0.0 | 0.0 | 7.0 | 0.0 | 0.0 | 12.7 |
| 1940 | 040097.02 | 4772053.01 | 149.50 | 0 | DEN | A | 00.7 | 0.7 | 0.0 | 0.0 | 0.0 | 70.3 | 4.1 | -2.1 | 0.0 | 0.0 | 1.2 | 0.0 | 0.0 | -3.5 |
| 1951 | 648710.78 | 4772843.00 | 149.50 | 0 | DEN | A | 68.7 | 14.5 | 0.0 | 0.0 | 0.0 | 70.2 | 4.0 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | 7.0 |
| 1962 | 648816.88 | 4772822.78 | 149.50 | 0 | DEN | A | 68.7 | 13.9 | 0.0 | 0.0 | 0.0 | 69.1 | 3.7 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | 7.7 |
| 2026 | 648754.48 | 4772954.33 | 168.51 | 0 | DEN | A | 68.7 | 8.8 | 0.0 | 0.0 | 0.0 | 70.0 | 4.0 | -2.7 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 6.2 |
| 2029 | 648755.32 | 4772950.08 | 157.24 | 0 | DEN | A | 68.7 | 12.2 | 0.0 | 0.0 | 0.0 | 70.0 | 4.0 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | 4.9 |
| 2091 | 648699.84 | 4772898.02 | 149.50 | 0 | DEN | A | 68.7 | 13.8 | 0.0 | 0.0 | 0.0 | 70.4 | 4.1 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | 6.0 |
| 2100 | 648784.26 | 4772822.41 | 149.50 | 0 | DEN | A | 68.7 | 12.4 | 0.0 | 0.0 | 0.0 | 69.5 | 3.8 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | 5.8 |
| 2124 | 648697.27 | 4772956.05 | 187.21 | 0 | DEN | A | 68.7 | 12.6 | 0.0 | 0.0 | 0.0 | 70.5 | 4.1 | -2.8 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 9.4 |
| 2127 | 648753 63 | 4772958 48 | 179.54 | 0 | DEN | A | 68.7 | 12.1 | 0.0 | 0.0 | 0.0 | 70.0 | 4.0 | -27 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 9.5 |
| 21/5 | 648708.63 | 4772821 27 | 1/0.04 | 0 | | | 68.7 | 10.7 | 0.0 | 0.0 | 0.0 | 60.3 | 3.8 | -2.7 | 0.0 | 0.0 | 47 | 0.0 | 0.0 | 13 |
| 2140 | 6407 30.03 | 4772005 25 | 197.00 | | | | 60.7 | 0.7 | 0.0 | 0.0 | 0.0 | 72.0 | 1.6 | -2.1 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | 4.5 |
| 2232 | 046511.15 | 4772905.35 | 107.90 | 0 | | A | 00.7 | 0.3 | 0.0 | 0.0 | 0.0 | 74.0 | 4.0 | -2.1 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | -4.0 |
| 2237 | 048510.59 | 4772906.79 | 187.89 | 0 | DEN | A | 68.7 | 10.1 | 0.0 | 0.0 | 0.0 | 71.9 | 4.0 | -2.1 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 5.0 |
| 2239 | 648523.89 | 4772908.71 | 187.88 | 0 | DEN | A | 68.7 | 6.9 | 0.0 | 0.0 | 0.0 | /1.9 | 4.6 | -2.8 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 2.0 |
| 2242 | 648695.69 | 4772872.15 | 149.50 | 0 | DEN | A | 68.7 | 4.5 | 0.0 | 0.0 | 0.0 | 70.4 | 4.1 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | -3.2 |
| 2244 | 648695.78 | 4772869.63 | 149.50 | 0 | DEN | A | 68.7 | 3.4 | 0.0 | 0.0 | 0.0 | 70.4 | 4.1 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | -4.3 |
| 2246 | 648695.88 | 4772866.44 | 149.50 | 0 | DEN | A | 68.7 | 6.2 | 0.0 | 0.0 | 0.0 | 70.4 | 4.1 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | -1.6 |
| 2249 | 648695.97 | 4772863.86 | 149.50 | 0 | DEN | A | 68.7 | 0.1 | 0.0 | 0.0 | 0.0 | 70.4 | 4.1 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | -7.7 |
| 2251 | 648696.01 | 4772862.88 | 149.50 | 0 | DEN | A | 68.7 | -0.3 | 0.0 | 0.0 | 0.0 | 70.4 | 4.1 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | -8.1 |
| 2253 | 648749.20 | 4772936.85 | 149.50 | 0 | DEN | A | 68.7 | 10.1 | 0.0 | 0.0 | 0.0 | 70.0 | 4.0 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | 2.8 |
| 2266 | 648528 91 | 4772910 03 | 187 88 | 0 | DEN | A | 68 7 | 74 | 0.0 | 0.0 | 0.0 | 718 | 45 | -28 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 25 |
| 2267 | 648535 71 | 4772911 80 | 187 90 | 0 | | | 68.7 | 03 | 0.0 | 0.0 | 0.0 | 71.8 | 4.5 | -2.8 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 4.5 |
| 2270 | 648667 02 | 4772048 31 | 187.00 | | | | 68 7 | 10 / | 0.0 | 0.0 | 0.0 | 70.9 | 4.0 | _2.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 6.0 |
| 2270 | 040007.90 | 4772940.31 | 107.27 | 0 | | | 00.7 | 10.4 | 0.0 | 0.0 | 0.0 | 70.0 | 4.2 | -2.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.9 |
| 2290 | 040/45.20 | 4770004.00 | 140.50 | | | A | 00.7 | 9.3 | 0.0 | 0.0 | 0.0 | 70.1 | 4.0 | -2.1 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 2294 | 048096.86 | 4112884.38 | 149.50 | | DEN | A | 08.7 | 0.2 | 0.0 | 0.0 | 0.0 | 10.4 | 4.1 | -2.1 | 0.0 | 0.0 | 4.1 | 0.0 | 0.0 | -1.6 |
| 2297 | 648696.03 | 4772880.50 | 149.50 | 0 | DEN | A | 68.7 | 5.8 | 0.0 | 0.0 | 0.0 | 70.4 | 4.1 | -2.7 | 0.0 | 0.0 | 6.0 | 0.0 | 0.0 | -3.2 |
| 2300 | 648695.52 | 4772878.16 | 149.50 | 0 | DEN | A | 68.7 | -0.0 | 0.0 | 0.0 | 0.0 | 70.4 | 4.1 | -2.7 | 0.0 | 0.0 | 5.9 | 0.0 | 0.0 | -8.9 |
| 2302 | 648754.63 | 4772943.46 | 149.50 | 0 | DEN | A | 68.7 | 8.9 | 0.0 | 0.0 | 0.0 | 70.0 | 4.0 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | 1.7 |
| 2315 | 648696.01 | 4772861.24 | 149.50 | 0 | DEN | A | 68.7 | 3.7 | 0.0 | 0.0 | 0.0 | 70.4 | 4.1 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | -4.0 |
| 2318 | 648696.00 | 4772859.00 | 149.50 | 0 | DEN | A | 68.7 | 3.3 | 0.0 | 0.0 | 0.0 | 70.4 | 4.1 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | -4.4 |
| 2321 | 648695.99 | 4772857.34 | 149.50 | 0 | DEN | A | 68.7 | 0.8 | 0.0 | 0.0 | 0.0 | 70.4 | 4.1 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | -7.0 |
| 2323 | 648695 98 | 4772855 59 | 149 50 | n | | Δ | 68.7 | 3.6 | 0.0 | 0.0 | 0.0 | 70 4 | 4 1 | -27 | 0.0 | 0.0 | 47 | 0.0 | 0.0 | -4 1 |
| 2335 | 648751 26 | 4772064 46 | 187.07 | | | | 68 7 | 8.0 8.8 | 0.0 | 0.0 | 0.0 | 70 1 | 4.1 | _2.7 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 6.0 |
| 2000 | 642625 27 | 4772052 02 | 187.07 | | DEN | | 69.7 | 0.0 | 0.0 | 0.0 | 0.0 | 70.0 | 4.0 | -2.1 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 5.0 |
| 2301 | 040000.27 | 4770040 40 | 101.23 | | | A | | 0.3 | 0.0 | 0.0 | 0.0 | 70.0 | 4.2 | -2.ŏ | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 5.0 |
| 2400 | 048/03./0 | 4772912.42 | 149.50 | | DEN | A | 08.7 | 1.9 | 0.0 | 0.0 | 0.0 | 10.4 | 4.1 | -2.1 | 0.0 | 0.0 | 4.1 | 0.0 | 0.0 | 0.1 |
| 2409 | 648545.86 | 4//2914.49 | 187.64 | 0 | DEN | <u> </u> | 68.7 | 8.6 | 0.0 | 0.0 | 0.0 | /1.7 | 4.5 | -2.8 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 3.9 |
| 2414 | 648675.67 | 4772950.45 | 187.25 | 0 | DEN | A | 68.7 | 7.1 | 0.0 | 0.0 | 0.0 | 70.7 | 4.2 | -2.8 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 3.7 |
| 2420 | 648695.50 | 4772876.09 | 149.50 | 0 | DEN | A | 68.7 | 5.0 | 0.0 | 0.0 | 0.0 | 70.4 | 4.1 | -2.7 | 0.0 | 0.0 | 5.9 | 0.0 | 0.0 | -3.9 |
| 2423 | 648695.62 | 4772874.04 | 149.50 | 0 | DEN | A | 68.7 | -0.3 | 0.0 | 0.0 | 0.0 | 70.4 | 4.1 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | -8.0 |
| 2434 | 648680.08 | 4772951.59 | 187.24 | 0 | DEN | A | 68.7 | 6.0 | 0.0 | 0.0 | 0.0 | 70.7 | 4.2 | -2.8 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 2.6 |
| 2459 | 648541.57 | 4772913 36 | 187.83 | 0 | DEN | A | 68.7 | 0.1 | 0.0 | 0.0 | 0.0 | 71.8 | 4.5 | -2.8 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | -4.6 |

| | | Line So | urce, IS | O 961 | 3, Nar | ne: "A | P, HMA | ۹ prod | luct ship | oing, | Full", | ID: "A | P_RD | _SHF | P_HM | A_Fu" | | | | |
|------|---|------------|----------|-------|--------|--------|--------|--------|-----------|-------|--------|--------|------|------|------|-------|------|------|------|-------|
| Nr. | Nr. X Y Z Refl. DEN Freq. Lw I/a Optime K0 Di Adiv Aatm Agr Afol Ahous Abar Cmet RL L (m) (m) (m) (m) (H2) dB(A) dB (dB) (dB) | | | | | | | | | | | | | | | Lr | | | | |
| | (m) | (m) | (m) | | | (Hz) | dB(A) | dB | dB | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | dB(A) |
| 2462 | 648542.23 | 4772913.53 | 187.80 | 0 | DEN | A | 68.7 | -4.8 | 0.0 | 0.0 | 0.0 | 71.7 | 4.5 | -2.8 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | -9.6 |
| 2468 | 648540.46 | 4772913.06 | 187.88 | 0 | DEN | A | 68.7 | 1.0 | 0.0 | 0.0 | 0.0 | 71.8 | 4.5 | -2.8 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | -3.8 |

| | LII | ne Source, IS | O 9613, | Name | : "AP | , AC a | nd RAF | ^o ship | oed from | Offsi | te, Fi | ull", ID | : "AP_ | RD_ | SHP_ | AC_RA | P_Fu | " | | |
|------|-----------|---------------|---------|-------|-------|--------|--------|-------------------|----------|-------|--------|----------|--------|--------------|------|-------|------|------|------|------------|
| Nr. | Х | Y | Z | Refl. | DEN | Freq. | Lw | l/a | Optime | K0 | Di | Adiv | Aatm | Agr | Afol | Ahous | Abar | Cmet | RL | Lr |
| | (m) | (m) | (m) | | | (Hz) | dB(A) | dB | dB | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | dB(A) |
| 1817 | 648855.31 | 4772823.42 | 149.50 | 0 | DEN | A | 68.7 | 16.8 | 0.0 | 0.0 | 0.0 | 68.7 | 3.6 | -2.6 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | 11.1 |
| 1820 | 648855.31 | 4772823.42 | 149.50 | 1 | DEN | A | 68.7 | 16.8 | 0.0 | 0.0 | 0.0 | 68.7 | 3.6 | -2.6 | 0.0 | 0.0 | 4.7 | 0.0 | 20.8 | -9.7 |
| 1854 | 648547.38 | 4772912.13 | 187.50 | 0 | DEN | A | 68.7 | 1.1 | 0.0 | 0.0 | 0.0 | 71.7 | 4.5 | -2.8 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | -3.6 |
| 1855 | 648582.70 | 4772921.85 | 187.43 | 0 | DEN | A | 68.7 | 18.6 | 0.0 | 0.0 | 0.0 | 71.4 | 4.4 | -2.8 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 14.2 |
| 1872 | 648645.49 | 4772939.72 | 187.31 | 0 | DEN | A | 68.7 | 17.7 | 0.0 | 0.0 | 0.0 | 71.0 | 4.3 | -2.8 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 13.9 |
| 1884 | 648724.08 | 4772925.26 | 149.50 | 0 | DEN | A | 68.7 | 16.5 | 0.0 | 0.0 | 0.0 | 70.2 | 4.0 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | 8.9 |
| 1906 | 648761.28 | 4772825.07 | 149.50 | 0 | DEN | A | 68.7 | 14.9 | 0.0 | 0.0 | 0.0 | 69.7 | 3.9 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | 8.0 |
| 1914 | 648695.81 | 4772853.02 | 149.50 | 0 | DEN | A | 68.7 | 5.0 | 0.0 | 0.0 | 0.0 | 70.4 | 4.1 | -2.7 | 0.0 | 0.0 | 7.1 | 0.0 | 0.0 | -5.1 |
| 1916 | 648709.29 | 4772842.40 | 149.50 | 0 | DEN | A | 68.7 | 14.9 | 0.0 | 0.0 | 0.0 | 70.2 | 4.0 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | 1.4 |
| 1924 | 648818.15 | 4772821.17 | 149.50 | 0 | DEN | A | 68.7 | 14.2 | 0.0 | 0.0 | 0.0 | 69.1 | 3.7 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | 8.0 |
| 1929 | 648724.87 | 4772961.47 | 187.15 | 0 | DEN | A | 68.7 | 15.4 | 0.0 | 0.0 | 0.0 | 70.3 | 4.1 | -2.7 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 12.5 |
| 1992 | 648698.23 | 4772896.28 | 149.50 | 0 | | A | 60.7 | 14.5 | 0.0 | 0.0 | 0.0 | 70.4 | 4.1 | -2.1 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | 0.7 |
| 1993 | 640094.04 | 4772020.25 | 149.50 | 0 | | A | 60.7 | 0.C | 0.0 | 0.0 | 0.0 | 70.4 | 4.1 | -2.1 | 0.0 | 0.0 | 5.9 | 0.0 | 0.0 | -3.3 |
| 2020 | 649604 46 | 4772030.33 | 149.50 | 0 | | A | 60.7 | 6.2 | 0.0 | 0.0 | 0.0 | 70.0 | 4.0 | -2.1 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | 0.0 |
| 2003 | 648694.40 | 4772872.84 | 149.50 | 0 | | Λ | 68.7 | 5.7 | 0.0 | 0.0 | 0.0 | 70.4 | 4.1 | -2.1 | 0.0 | 0.0 | 17 | 0.0 | 0.0 | -2.0 |
| 2007 | 648694.40 | 4772869.87 | 149.50 | 0 | | Δ | 68.7 | 3.4 | 0.0 | 0.0 | 0.0 | 70.4 | 4.1 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | -2.0 |
| 2003 | 648694.50 | 4772866 70 | 149.50 | 0 | | Λ Δ | 68.7 | 6.2 | 0.0 | 0.0 | 0.0 | 70.4 | 4.1 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | -4.5 |
| 2073 | 648694 51 | 4772864 12 | 149.50 | 0 | DEN | Δ | 68.7 | 0.2 | 0.0 | 0.0 | 0.0 | 70.4 | 4.1 | -27 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | -7.7 |
| 2076 | 648694.52 | 4772861.97 | 149.50 | 0 | DEN | A | 68.7 | 5.2 | 0.0 | 0.0 | 0.0 | 70.4 | 4 1 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | -2.6 |
| 2079 | 648694 53 | 4772859 26 | 149.50 | 0 | DEN | A | 68.7 | 3.3 | 0.0 | 0.0 | 0.0 | 70.4 | 4 1 | -27 | 0.0 | 0.0 | 47 | 0.0 | 0.0 | -4.4 |
| 2081 | 648694.54 | 4772857.59 | 149.50 | 0 | DEN | A | 68.7 | 0.8 | 0.0 | 0.0 | 0.0 | 70.4 | 4.1 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | -7.0 |
| 2084 | 648694.54 | 4772855.62 | 149.50 | 0 | DEN | A | 68.7 | 4.4 | 0.0 | 0.0 | 0.0 | 70.4 | 4.1 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | -3.4 |
| 2088 | 648694.55 | 4772854.13 | 149.50 | 0 | DEN | A | 68.7 | -6.0 | 0.0 | 0.0 | 0.0 | 70.4 | 4.1 | -2.7 | 0.0 | 0.0 | 7.0 | 0.0 | 0.0 | -16.0 |
| 2106 | 648784.43 | 4772820.67 | 149.50 | 0 | DEN | A | 68.7 | 12.2 | 0.0 | 0.0 | 0.0 | 69.4 | 3.8 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | 5.6 |
| 2118 | 648699.22 | 4772954.75 | 187.20 | 0 | DEN | Α | 68.7 | 12.6 | 0.0 | 0.0 | 0.0 | 70.5 | 4.1 | -2.8 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 9.4 |
| 2134 | 648798.77 | 4772819.63 | 149.50 | 0 | DEN | Α | 68.7 | 11.0 | 0.0 | 0.0 | 0.0 | 69.3 | 3.8 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | 4.6 |
| 2157 | 648753.09 | 4772952.75 | 168.18 | 0 | DEN | Α | 68.7 | 8.8 | 0.0 | 0.0 | 0.0 | 70.0 | 4.0 | -2.7 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 6.2 |
| 2160 | 648753.88 | 4772949.36 | 162.69 | 0 | DEN | Α | 68.7 | 7.4 | 0.0 | 0.0 | 0.0 | 70.0 | 4.0 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | 0.1 |
| 2179 | 648524.67 | 4772905.74 | 187.85 | 0 | DEN | Α | 68.7 | 8.8 | 0.0 | 0.0 | 0.0 | 71.9 | 4.6 | -2.7 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 3.9 |
| 2181 | 648533.20 | 4772908.10 | 187.89 | 0 | DEN | Α | 68.7 | 10.0 | 0.0 | 0.0 | 0.0 | 71.8 | 4.5 | -2.8 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 5.2 |
| 2183 | 648538.71 | 4772909.63 | 187.91 | 0 | DEN | Α | 68.7 | 1.5 | 0.0 | 0.0 | 0.0 | 71.8 | 4.5 | -2.8 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | -3.3 |
| 2222 | 648754.34 | 4772947.36 | 154.95 | 0 | DEN | Α | 68.7 | 10.4 | 0.0 | 0.0 | 0.0 | 70.0 | 4.0 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | 3.1 |
| 2227 | 648752.15 | 4772956.76 | 176.35 | 0 | DEN | A | 68.7 | 10.3 | 0.0 | 0.0 | 0.0 | 70.1 | 4.0 | -2.7 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 7.8 |
| 2256 | 648748.13 | 4772937.49 | 149.50 | 0 | DEN | A | 68.7 | 9.9 | 0.0 | 0.0 | 0.0 | 70.0 | 4.0 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | 2.6 |
| 2337 | 648686.51 | 4772951.37 | 187.23 | 0 | DEN | A | 68.7 | 9.1 | 0.0 | 0.0 | 0.0 | 70.6 | 4.2 | -2.8 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 5.8 |
| 2341 | 648753.34 | 4772943.47 | 149.50 | 0 | DEN | A | 68.7 | 8.5 | 0.0 | 0.0 | 0.0 | 70.0 | 4.0 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | 1.2 |
| 2348 | 648512.04 | 4772902.19 | 187.92 | 0 | DEN | A | 68.7 | 4.2 | 0.0 | 0.0 | 0.0 | 72.0 | 4.6 | -2.6 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | -1.1 |
| 2351 | 648516.09 | 4772903.34 | 187.88 | 0 | DEN | A | 68.7 | 7.6 | 0.0 | 0.0 | 0.0 | /1.9 | 4.6 | -2.6 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 2.5 |
| 2353 | 648519.94 | 4772904.42 | 187.85 | 0 | DEN | A | 68.7 | 3.4 | 0.0 | 0.0 | 0.0 | /1.9 | 4.6 | -2.7 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | -1./ |
| 2372 | 648744.93 | 4772965.78 | 187.11 | 0 | DEN | A | 68.7 | 8.1 | 0.0 | 0.0 | 0.0 | 70.1 | 4.0 | -2.7 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 5.4 |
| 23/8 | 648751.44 | 4772959.80 | 184.18 | 0 | | A | 00.7 | 1.0 | 0.0 | 0.0 | 0.0 | 70.1 | 4.0 | -2.1 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 5.2 |
| 2304 | 640702.00 | 4772062.22 | 149.50 | 0 | | A | 00.7 | 0.1 | 0.0 | 0.0 | 0.0 | 70.4 | 4.1 | -2.1 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | 0.3 |
| 2397 | 649676 12 | 4772903.23 | 107.00 | 0 | | A | 60.7 | 7.0 | 0.0 | 0.0 | 0.0 | 70.1 | 4.0 | -2.1 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.U 2 0 |
| 2412 | 648680.63 | 4772040.82 | 107.20 | 0 | | A | 68.7 | 6.1 | 0.0 | 0.0 | 0.0 | 70.7 | 4.2 | -2.0 2.9 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 3.0 2.7 |
| 2429 | 648545 12 | 4772949.02 | 187.61 | 0 | | Λ | 68.7 | 53 | 0.0 | 0.0 | 0.0 | 70.7 | 4.2 | -2.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 2.7 |
| 2452 | 648540 25 | 4772010 12 | 187 00 | 0 | | ۸ ۸ | 68.7 | _1 1 | 0.0 | 0.0 | 0.0 | 71 P | 4.5 | -2.0 _2.9 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | -5.0 |
| 2478 | 648541.87 | 4772910.13 | 187.80 | 0 | DEN | Δ | 68.7 | -1.1 | 0.0 | 0.0 | 0.0 | 71.0 | 4.5 | -2.0 -2.8 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | -5.9 |
| 2484 | 648543 10 | 4772010.07 | 187 73 | 0 | DEN | Δ | 68.7 | -20 | 0.0 | 0.0 | 0.0 | 717 | 4.5 | -2.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | -6.7 |
| 2486 | 648539.68 | 4772909 92 | 187.91 | 0 | DEN | Δ | 68.7 | -2.0 | 0.0 | 0.0 | 0.0 | 71.8 | 4.5 | -2.8 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | -6.8 |
| 2491 | 648542 42 | 4772910 73 | 187 78 | 0 | DEN | Δ | 68.7 | -34 | 0.0 | 0.0 | 0.0 | 71 7 | 4.5 | -2.8 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | -8.1 |
| 2494 | 648540 93 | 4772910 29 | 187.88 | 0 | DEN | A | 68 7 | -3.6 | 0.0 | 0.0 | 0.0 | 718 | 4.5 | -2.8 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | -8.4 |
| 2496 | 648541.34 | 4772910.41 | 187.85 | 0 | DEN | A | 68.7 | -3.7 | 0.0 | 0.0 | 0.0 | 71.8 | 4.5 | -2.8 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | -8.4 |
| 2498 | 648542.76 | 4772910.82 | 187.76 | 0 | DEN | A | 68.7 | -5.9 | 0.0 | 0.0 | 0.0 | 71.7 | 4.5 | -2.8 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | -10.7 |

| | | Line Sour | ce, ISO | 9613, | Name | e: "AP | , HMA | produc | ct shippir | ng, Er | npty'' | , ID: " | AP_R | D_SH | P_HN | /IA_Em | | | | |
|------|-----------|------------|---------|-------|------|--------|-------|--------|------------|--------|--------|---------|------|------|------|--------|------|------|------|-------|
| Nr. | Х | Y | Z | Refl. | DEN | Freq. | Lw | l/a | Optime | K0 | Di | Adiv | Aatm | Agr | Afol | Ahous | Abar | Cmet | RL | Lr |
| | (m) | (m) | (m) | | | (Hz) | dB(A) | dB | dB | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | dB(A) |
| 1824 | 648855.34 | 4772823.41 | 149.50 | 0 | DEN | A | 68.7 | 16.8 | 0.0 | 0.0 | 0.0 | 68.7 | 3.6 | -2.6 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | 11.1 |
| 1826 | 648855.34 | 4772823.41 | 149.50 | 1 | DEN | A | 68.7 | 16.8 | 0.0 | 0.0 | 0.0 | 68.7 | 3.6 | -2.6 | 0.0 | 0.0 | 4.7 | 0.0 | 20.8 | -9.7 |
| 1839 | 648547.50 | 4772912.12 | 187.50 | 0 | DEN | A | 68.7 | 0.8 | 0.0 | 0.0 | 0.0 | 71.7 | 4.5 | -2.8 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | -3.9 |
| 1840 | 648589.87 | 4772923.90 | 187.42 | 0 | DEN | A | 68.7 | 19.4 | 0.0 | 0.0 | 0.0 | 71.4 | 4.4 | -2.8 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 15.1 |
| 1876 | 648718.93 | 4772959.74 | 187.17 | 0 | DEN | A | 68.7 | 16.7 | 0.0 | 0.0 | 0.0 | 70.4 | 4.1 | -2.8 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 13.8 |
| 1879 | 648724.21 | 4772925.31 | 149.50 | 0 | DEN | A | 68.7 | 16.5 | 0.0 | 0.0 | 0.0 | 70.2 | 4.0 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | 8.9 |
| 1900 | 648738.26 | 4772829.50 | 149.50 | 0 | DEN | A | 68.7 | 15.3 | 0.0 | 0.0 | 0.0 | 69.9 | 4.0 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | 8.1 |
| 1909 | 648695.80 | 4772853.04 | 149.50 | 0 | DEN | A | 68.7 | 5.2 | 0.0 | 0.0 | 0.0 | 70.4 | 4.1 | -2.7 | 0.0 | 0.0 | 7.1 | 0.0 | 0.0 | -4.9 |
| 1911 | 648709.32 | 4772842.40 | 149.50 | 0 | DEN | A | 68.7 | 14.9 | 0.0 | 0.0 | 0.0 | 70.2 | 4.0 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | 7.4 |
| 1920 | 648818.18 | 4772821.15 | 149.50 | 0 | DEN | A | 68.7 | 14.2 | 0.0 | 0.0 | 0.0 | 69.1 | 3.7 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | 8.1 |
| 1996 | 648647.85 | 4772940.38 | 187.31 | 0 | DEN | A | 68.7 | 15.3 | 0.0 | 0.0 | 0.0 | 70.9 | 4.3 | -2.8 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 11.6 |
| 2025 | 648765.65 | 4772824.22 | 149.50 | 0 | DEN | A | 68.7 | 13.4 | 0.0 | 0.0 | 0.0 | 69.6 | 3.9 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | 6.5 |
| 2040 | 648694.50 | 4772876.91 | 149.50 | 0 | DEN | A | 68.7 | 6.4 | 0.0 | 0.0 | 0.0 | 70.4 | 4.1 | -2.7 | 0.0 | 0.0 | 5.9 | 0.0 | 0.0 | -2.5 |
| 2041 | 648694.50 | 4772872.84 | 149.50 | 0 | DEN | A | 68.7 | 5.7 | 0.0 | 0.0 | 0.0 | 70.4 | 4.1 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | -2.0 |
| 2043 | 648694.50 | 4772869.87 | 149.50 | 0 | DEN | A | 68.7 | 3.4 | 0.0 | 0.0 | 0.0 | 70.4 | 4.1 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | -4.3 |
| 2045 | 648694.50 | 4772866.70 | 149.50 | 0 | DEN | A | 68.7 | 6.2 | 0.0 | 0.0 | 0.0 | 70.4 | 4.1 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | -1.6 |
| 2047 | 648694.50 | 4772864.12 | 149.50 | 0 | DEN | A | 68.7 | 0.1 | 0.0 | 0.0 | 0.0 | 70.4 | 4.1 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | -7.7 |
| 2050 | 648694.50 | 4772861.98 | 149.50 | 0 | DEN | A | 68.7 | 5.2 | 0.0 | 0.0 | 0.0 | 70.4 | 4.1 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | -2.6 |
| 2053 | 648694 51 | 4772859 26 | 149 50 | 0 | DFN | A | 68.7 | 3.3 | 0.0 | 0.0 | 0.0 | 70.4 | 41 | -27 | 0.0 | 0.0 | 47 | 0.0 | 0.0 | -4 4 |
| 2056 | 648694 51 | 4772857 60 | 149 50 | 0 | DEN | A | 68.7 | 0.8 | 0.0 | 0.0 | 0.0 | 70.4 | 4 1 | -27 | 0.0 | 0.0 | 47 | 0.0 | 0.0 | -7.0 |
| 2057 | 648694 51 | 4772855.63 | 149 50 | 0 | DEN | A | 68.7 | 44 | 0.0 | 0.0 | 0.0 | 70.4 | 4 1 | -27 | 0.0 | 0.0 | 47 | 0.0 | 0.0 | -34 |
| 2062 | 648694 51 | 4772854 16 | 149 50 | 0 | DEN | A | 68.7 | -6.8 | 0.0 | 0.0 | 0.0 | 70.4 | 4 1 | -27 | 0.0 | 0.0 | 7.0 | 0.0 | 0.0 | -16.8 |
| 2102 | 648784 46 | 4772820 67 | 149 50 | 0 | DEN | A | 68.7 | 12.2 | 0.0 | 0.0 | 0.0 | 69.4 | 3.8 | -27 | 0.0 | 0.0 | 47 | 0.0 | 0.0 | 5.6 |
| 2115 | 648699.26 | 4772900 94 | 149 50 | 0 | DEN | A | 68.7 | 12.6 | 0.0 | 0.0 | 0.0 | 70.4 | 4 1 | -27 | 0.0 | 0.0 | 47 | 0.0 | 0.0 | 4.8 |
| 2123 | 648751 95 | 4772957 69 | 178 99 | 0 | DEN | A | 68 7 | 12.2 | 0.0 | 0.0 | 0.0 | 70.1 | 4.0 | -27 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 9.6 |
| 2138 | 648798 80 | 4772819 62 | 149 50 | 0 | DEN | A | 68.7 | 11 0 | 0.0 | 0.0 | 0.0 | 69.3 | 3.8 | -27 | 0.0 | 0.0 | 4 7 | 0.0 | 0.0 | 4.5 |
| 2150 | 648524.34 | 4772905 67 | 187 85 | 0 | DEN | A | 68.7 | 92 | 0.0 | 0.0 | 0.0 | 71.9 | 4.6 | -27 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 4 2 |
| 2153 | 648533 15 | 4772908 11 | 187.89 | 0 | DEN | A | 68.7 | 10.0 | 0.0 | 0.0 | 0.0 | 71.8 | 4.5 | -2.8 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 5.2 |
| 2155 | 648538 89 | 4772909 71 | 187 91 | 0 | DFN | A | 68.7 | 2.8 | 0.0 | 0.0 | 0.0 | 71.8 | 4.5 | -2.8 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | -2.0 |
| 2194 | 648696 29 | 4772887 30 | 149 50 | 0 | DEN | A | 68.7 | 9.8 | 0.0 | 0.0 | 0.0 | 70.4 | 4 1 | -27 | 0.0 | 0.0 | 4 7 | 0.0 | 0.0 | 21 |
| 2197 | 648694 88 | 4772880 85 | 149 50 | 0 | DFN | A | 68.7 | 5.5 | 0.0 | 0.0 | 0.0 | 70.4 | 4 1 | -27 | 0.0 | 0.0 | 5.9 | 0.0 | 0.0 | -34 |
| 2206 | 648754.46 | 4772947.08 | 155.39 | 0 | DEN | A | 68.7 | 10.7 | 0.0 | 0.0 | 0.0 | 70.0 | 4.0 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | 3.5 |
| 2259 | 648748.22 | 4772937.51 | 149.50 | 0 | DEN | A | 68.7 | 9.8 | 0.0 | 0.0 | 0.0 | 70.0 | 4.0 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | 2.5 |
| 2285 | 648668.80 | 4772946.67 | 187.26 | 0 | DEN | A | 68.7 | 10.0 | 0.0 | 0.0 | 0.0 | 70.8 | 4.2 | -2.8 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 6.5 |
| 2328 | 648692.16 | 4772952.73 | 187.22 | 0 | DEN | A | 68.7 | 9.2 | 0.0 | 0.0 | 0.0 | 70.6 | 4.1 | -2.8 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 5.9 |
| 2333 | 648753.60 | 4772950.64 | 161.75 | 0 | DEN | A | 68.7 | 8.6 | 0.0 | 0.0 | 0.0 | 70.0 | 4.0 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | 1.3 |
| 2355 | 648752.97 | 4772953.37 | 168.21 | 0 | DEN | A | 68.7 | 8.4 | 0.0 | 0.0 | 0.0 | 70.0 | 4.0 | -2.7 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 5.8 |
| 2360 | 648753.26 | 4772943.23 | 149.50 | 0 | DEN | A | 68.7 | 8.2 | 0.0 | 0.0 | 0.0 | 70.0 | 4.0 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | 0.9 |
| 2363 | 648511.95 | 4772902.22 | 187.92 | 0 | DEN | A | 68.7 | 4.1 | 0.0 | 0.0 | 0.0 | 72.0 | 4.6 | -2.6 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | -1.1 |
| 2365 | 648516.01 | 4772903.35 | 187.88 | 0 | DEN | A | 68.7 | 7.7 | 0.0 | 0.0 | 0.0 | 71.9 | 4.6 | -2.6 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 2.5 |
| 2368 | 648519.59 | 4772904.35 | 187.84 | 0 | DEN | A | 68.7 | 2.0 | 0.0 | 0.0 | 0.0 | 71.9 | 4.6 | -2.7 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | -3.1 |
| 2371 | 648744.87 | 4772965.78 | 187.11 | 0 | DEN | A | 68.7 | 8.1 | 0.0 | 0.0 | 0.0 | 70.1 | 4.0 | -2.7 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 5.4 |
| 2375 | 648702.67 | 4772912.81 | 149.50 | 0 | DEN | A | 68.7 | 8.2 | 0.0 | 0.0 | 0.0 | 70.4 | 4.1 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | 0.4 |
| 2381 | 648749.68 | 4772963.17 | 186.87 | 0 | DEN | A | 68.7 | 7.7 | 0.0 | 0.0 | 0.0 | 70.1 | 4.0 | -2.7 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 5.1 |
| 2406 | 648685.26 | 4772951.12 | 187.23 | 0 | DEN | A | 68.7 | 7.7 | 0.0 | 0.0 | 0.0 | 70.6 | 4.2 | -2.8 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 4.4 |
| 2432 | 648754.16 | 4772948.31 | 159.86 | 0 | DEN | A | 68.7 | 5.4 | 0.0 | 0.0 | 0.0 | 70.0 | 4.0 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | -1.9 |
| 2436 | 648680.53 | 4772949.89 | 187.24 | 0 | DEN | A | 68.7 | 5.9 | 0.0 | 0.0 | 0.0 | 70.7 | 4.2 | -2.8 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 2.5 |
| 2439 | 648675.46 | 4772948.58 | 187.25 | 0 | DEN | A | 68.7 | 5.9 | 0.0 | 0.0 | 0.0 | 70.7 | 4.2 | -2.8 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 2.5 |
| 2455 | 648545.41 | 4772911.54 | 187.59 | 0 | DEN | A | 68.7 | 5.0 | 0.0 | 0.0 | 0.0 | 71.7 | 4.5 | -2.8 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.3 |
| 2457 | 648678.00 | 4772949.23 | 187.25 | 0 | DEN | A | 68.7 | 1.2 | 0.0 | 0.0 | 0.0 | 70.7 | 4.2 | -2.8 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | -2.2 |
| 2465 | 648543.27 | 4772910.96 | 187.73 | 0 | DEN | A | 68.7 | 1.1 | 0.0 | 0.0 | 0.0 | 71.7 | 4.5 | -2.8 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | -3.6 |
| 2474 | 648754.44 | 4772946.55 | 149.50 | 0 | DEN | A | 68.7 | -2.9 | 0.0 | 0.0 | 0.0 | 70.0 | 4.0 | -2.7 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | -10.1 |
| 2476 | 648542.28 | 4772910.69 | 187.79 | 0 | DEN | A | 68.7 | -1.2 | 0.0 | 0.0 | 0.0 | 71.7 | 4.5 | -2.8 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | -5.9 |
| 2480 | 648540.13 | 4772910.06 | 187.91 | 0 | DEN | A | 68.7 | -1.8 | 0.0 | 0.0 | 0.0 | 71.8 | 4.5 | -2.8 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | -6.5 |
| 2482 | 648541.60 | 4772910.48 | 187.84 | 0 | DEN | A | 68.7 | -1.8 | 0.0 | 0.0 | 0.0 | 71.7 | 4.5 | -2.8 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | -6.6 |
| 2488 | 648540.71 | 4772910.22 | 187.89 | 0 | DEN | A | 68.7 | -2.6 | 0.0 | 0.0 | 0.0 | 71.8 | 4.5 | -2.8 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | -7.3 |
| 2499 | 648541.06 | 4772910.32 | 187.87 | 0 | DEN | A | 68.7 | -7.6 | 0.0 | 0.0 | 0.0 | 71.8 | 4.5 | -2.8 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | -12.3 |
| 2501 | 648541 22 | 4772910 37 | 187.86 | 0 | DEN | A | 68 7 | -84 | 0.0 | 0.0 | 0.0 | 71.8 | 4 5 | -2.8 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | -13 2 |
| | | , | | | | | | | | | | | | | | | | | | |

| | | Point So | urce, IS | D 961 | 3, Nar | ne: "P | 4_SE, | ΡΡ Τε | ertiary Cr | usher | ", ID: | "P4_ | SE_PF | _Ter | tiaryC | rush2" | | | | |
|------|---|------------|----------|-------|--------|--------|-------|-------|------------|-------|--------|------|-------|------|--------|--------|------|------|------|-------|
| Nr. | r. X Y Z Refl. DEN Freq. Lw I/a Optime K0 Di Adiv Aatm Agr Afol Ahous Abar Cmet RL Lr | | | | | | | | | | | | | | | | | | | |
| | (m) | (m) | (m) | | | (Hz) | dB(A) | dB | dB | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | dB(A) |
| 1999 | 649163.60 | 4772897.34 | 149.00 | 0 | D | A | 99.2 | 0.0 | 0.0 | 0.0 | 0.0 | 64.8 | 2.3 | -2.4 | 0.0 | 0.0 | 10.3 | 0.0 | 0.0 | 24.2 |

| | | Point So | urce, IS | D 961 | 3, Nai | me: "P | 4_SE, | ΡΡ Τε | ertiary Cr | ushe | r", ID: | "P4_ | SE_PF | P_Ter | tiaryC | Crush1" | | | | |
|------|--|------------|----------|-------|--------|--------|-------|-------|------------|------|---------|------|-------|-------|--------|---------|------|------|------|-------|
| Nr. | Nr. X Y Z Refl. DEN Freq. Lw I/a Optime K0 Di Adiv Aatm Agr Afol Ahous Abar Cmet RL Lr | | | | | | | | | | | | | | | | | | | |
| | (m) | (m) | (m) | | | (Hz) | dB(A) | dB | dB | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | (dB) | dB(A) |
| 2002 | 649163.10 | 4772898.30 | 149.00 | 0 | D | A | 99.2 | 0.0 | 0.0 | 0.0 | 0.0 | 64.8 | 2.3 | -2.4 | 0.0 | 0.0 | 10.2 | 0.0 | 0.0 | 24.2 |



APPENDIX D



SY

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APPENDIX D: ALTERNATE EXTRACTION SCENARIO

Alternate Extraction Scenario Description

Subject to agreement from the City of Niagara Falls, Walker proposes an alternative extraction scenario in which these road allowances can also be extracted:

- i. Upper's Lane, between the North Extraction Area and the Mid Extraction Area; and
- ii. The unopened road allowance between Lots 120 and 136, between the Mid Extraction Area and the South Extraction Area.

The layout of the site and phases for the Alternate Extraction Scenario can be found in **Figure D.1**.

Walker owns all of the lands north and south of Upper's Lane and the unopened road allowance between Thorold Townline Road and Beechwood Road, with exception of the Bible Baptist Church property which has secured access from Beechwood Road. Subject to an agreement with the City, Walker proposes to extract this portion of Upper's Lane and the unopened road allowance to maximize access to the aggregate resource and to create a more integrated operation and rehabilitation plan.

Should Agreement with the City be reached, extraction at the site can be simplified greatly. A single sinking cut would then be required, as opposed to multiple sinking cuts in the Proposed Extraction Scenario. Initial operations will be similar to the Proposed Extraction Scenario, with a portable plant operating at the top of rock until sufficient area has been opened to move the plant to the first bench and then the final quarry floor. Once on the quarry floor, the plant can be expanded.

In addition to aggregate extraction and processing, the site will also include a hot mix asphalt (HMA) batch plant, capable of producing 4,900 tonnes per day of HMA. Operations include the receipt and drying of washed aggregate, receipt and storage of asphalt cement, mixing and storage of HMA, and loading highway trucks for shipment to the job site.

The initial sinking cut is performed in the southern region of Phase 1A. The sinking cut will consist of only drilling, extraction, aggregate processing, and aggregate shipping. Once sufficient area has been extracted in Phase 1A, the asphalt plant will be constructed on the Quarry floor south of Upper's Lane.

Phases 1A, 2, and 3 will be extracted in two benches down to the Quarry floor. Phases 1B and 1C will be extracted in one bench to approximately 155 masl. After extraction, Phase 1B will be backfilled to a final elevation of approximately 175 masl to accommodate the realignment of Upper's Creek. The mobile crusher plant will be close to the surface during the sinking cut and descend in elevation as material is extracted. The crusher plant will remain on the Quarry floor once it reaches there. The exception is Phase 1B, where the crusher plant may be relocated to a higher elevation of 155 masl to accommodate Phase 1B's higher final depth. For all of the phases, the crusher plant will follow the working face as closely as possible to reduce hauling distance.

In addition to aggregate extraction and processing, the site will also include the hot mix asphalt (HMA) batch plant, described under the proposed extraction scenario, to be located in Phase 1A.

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The hours of operation at the Quarry for the Alternative Extraction Scenario are the same as those for the Proposed Extraction Scenarios as described in **Section 2** of the report.

The modelled phases for the Alternate Extraction Scenario are:

- Alternate Phase 1B North (AP1B_N*):
 - Extraction in northern portion of Alternate Phase 1B, with AP operational
- Alternate Phase 2 Northeast (AP2_NE*):
 - Extraction in the northeastern corner of Alternate Phase 2, with AP operational
- Alternate Phase 3 Southeast (AP3_SE*);
 - Extraction in the southeastern corner of Alternate Phase 3, with AP operational

The operation overviews of the modelled scenarios are shown in Figures D.2a through D.2c.

Noise Sources

The sources modelled for the Alternate Extraction Scenarios are the same as those for the Proposed Extraction Scenarios as described in **Section 3** of the report.

A summary of significant sound sources is provided in **Table D.1**, including sound power levels, location, sound characteristics, operating duration, and vehicle route assumptions. Sound power levels for the proposed sources are based on historical measurement data on file at RWDI. The overview of the locations of the modelled sources are shown in **Figures D.2a** through **D.2c**.

Noise Control Recommendations

The following recommendations are provided in order to meet the applicable criteria described in **Section 5** of the report:

- Minimum 3 m tall perimeter berms should be constructed around the Quarry as shown in Figure D.1 The perimeter berms should be constructed as soon as possible during site preparation prior to extraction.
- 2. The primary crusher should stay within 30 m of the working face to maximize shielding effect of the Quarry terrain.
- 3. For alternate phase 3, WAI should maintain an 8m tall barrier at a radius of 40 m to the southeast of the processing plant secondary crushers as shown in **Figure D.2c**. The barrier can be material stockpiles, noise walls, or a combination of both. The barrier should extend long enough to shield R4 and R5 from the secondary crushers.

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Impact Assssessment

The same assessment methodology as described in **Section 7** of the report was used for the Alternate Extraction Scenarios.

The predicted sound levels at PORs were assessed using applicable sound level limits, as shown in **Tables D.2a** to **D.2c** for continuous sources, and **Table D.2d** for impulsive sources. The predicted sound levels at each POR complies with the applicable NPC-300 Class 2 exclusion limits for all scenarios with the implementation of the mitigation measures described above.

Predicted sound level contours (isopleths of equal sound level) for continuous sources were generated for the modelled phases of the alternate extraction scenarios. The sound level contours are shown in **Figures D.3a** through **D.3f**.

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Table D.1: Noise Source Summary - Alternate Extraction Scenario Upper's Quarry, 1603157

| Upper's Quarry, 1603157 | | | | | | Upper's Quarry, 1603157 | 7 | | | | | | | | | | | |
|------------------------------------|--|---|----------------------------------|-----------------------------------|-------------------------|-------------------------|--|---|----------------------------------|---------------|-------------------------|--------|--------|----------------|-------|--------------|---|------------------------|
| Notes to Table: | | | | | | | | | | | | | | 1 | | | | |
| 1. | Wherever possible, the Source ID matches the identifiers used in | the ESDM report. | | | | 6. | Source type indicates Cadna/A modelling | g methodology. For I | Point, Line, and Area source | es, PWLs repi | resent | | | | | | | |
| 2. | Sound Power Level of Source, in dBA, not including sound chara NPC-104. | acteristic adjustme | ents per | | | | the overall level for the entire source. W point source, and PWL is calculated from | here source type is N n a single-vehicle pas | Nobile Equipment, the sourcesby. | e is modelled | as a moving | | | | | | | |
| 3. | Source Location: $O = Outside$ of building, including the roof, $I = I$ | Inside of building | | | | 7. | Sound Power Level Data Source: - Man = Manufacturer's Data | | - EC = Engineering Calc b | ased on speci | fications | | | | | | | |
| 4. | Sound Characteristic, per NPC-104: - S = Steady | - I = Impuls | ive | - T = Tonal | | | - Mea = Measured Directly - Hist = Historical Data on File at RWD | ſ | - Same ### = same type as | source no. # | ## | | | | | | | |
| | - Q = Quasi-Steady Impulsive | - B = Buzzi | ng | - C = Cyclic | | 8 | For loader dumping into primary crusher | , it is assumed each o | lump takes approximately 1 | 0s | | | | | | | | |
| 5. | Noise control measures currently in place or specified in construc - S = Silencer/Muffler - A = Acoustic lining, plenum - B = Barrier/Berm | ction drawings: - L = Laggin - E = Acous | ng stic enclosure | - O = Other - U = Uncontrolled | | | | | | | | | | | | | | |
| | Where noise control measures are specified in construction drawi octave band sound power levels include the effects of the noise or recommended in the mitigation section of this report are not inclu | ings or were found ontrol measures. I uded in this table. | d on existing e Noise control | quipment, neasures | | | | | | | | | | | | | | |
| Saurae ID ^[1] | Source Description | Sound | Source | Sound | Noise Control | 1/1 Octav | /e Band Sound Power Level Data if available | Source Tune [6] | BWL Data Source ^[7] | Height | Local Roof Height Ab | Height | s | ource Co-ordin | ates | Operating Ti | ne during Wors Point Sources, [†] OR | st-case hour for 8] |
| Source in | | Level ^[2] | Location ^[3] | Characteristics ^[4] | Measures ^[5] | | (dB) | Source Type | I WE Data Source | Roof | Grade | Grade | | (m) | | Vehicle Pass | by per Hour & Sources | Speed for Line |
| | | (dBA) | (I or O) | (S,Q,I,B,T,C) | (S,A,B,L,E,O,U) | 31.5 63 125 | 250 500 1000 2000 4000 8000 | | | (m) | (m) | (m) | X | Y | Z | Daytime | Evening | Nighttime |
| | | | | | | | Point Sources | | | | | | | | | | | |
| AP1B_N_PC_CrusherDump | Alternate P1B North, PC loader dumping into crusher | 123 | 0 | S | U | 115.4 120.3 122.2 | 120.0 118.3 118.5 116.6 111.1 102.3 | Point | Hist | - | - | 3.0 | 648792 | 4773389 | 168.7 | 60 dumps/hr | - | - |
| AP1B_N_PC_Ldr | Alternate P1B North, PC loader | 106 | 0 | S | U | 102.4 111.2 104.7 | 101.4 99.9 99.2 97.5 97.7 98.5 | Point | Hist | - | - | 2.5 | 648793 | 4773390 | 168.2 | 60 min | - | - |
| AP1B_N_PC_PrimaryCrush | Alternate P1B North, PC Primary Crusher | 118 | 0 | S | U | 108.9 119.8 115.0 | 118.7 114.6 112.2 109.6 104.4 99.6 | Point | Hist | - | - | 3.0 | 648791 | 4773388 | 168.7 | 60 min | - | - |
| AP1B_N_PC_PrimaryScreen | Alternate P1B North, PC Primary Screen | 114 | 0 | S | U | 111.4 113.6 111.5 | 111.1 110.9 106.9 106.5 105.2 101.7 | Point | Hist | - | - | 3.0 | 648791 | 4773387 | 168.7 | 60 min | - | - |
| AP1B_N_PP_Ldr | Alternate P1B North, PP loader | 106 | 0 | S | U | 102.4 111.2 104.7 | 101.4 99.9 99.2 97.5 97.7 98.5 | Point | Hist | - | - | 2.5 | 648709 | 4773141 | 145.5 | 60 min | 60 min | 60 min |
| AP1B_N_PP_SecondaryCrush1 | Alternate P1B North, PP Secondary Crusher | 115 | 0 | S | U | 102.3 108.9 111.7 | 110.8 109.6 110.5 107.4 104.6 99.0 | Point | Hist | - | - | 3.0 | 648709 | 4773154 | 146.0 | 60 min | - | - |
| AP1B_N_PP_SecondaryCrush2 | Alternate P1B North, PP Secondary Crusher | 115 | 0 | S | U | 102.3 108.9 111.7 | 110.8 109.6 110.5 107.4 104.6 99.0 | Point | Hist | - | - | 3.0 | 648710 | 4773154 | 146.0 | 60 min | - | - |
| AP1B_N_PP_SecondaryTertiaryScreen1 | Alternate P1B North, PP Secondary & Tertiary Screen | 114 | 0 | S | U | 111.4 113.6 111.5 | 111.1 110.9 106.9 106.5 105.2 101.7 | Point | Hist | - | - | 3.0 | 648709 | 4773152 | 146.0 | 60 min | - | - |
| AP1B_N_PP_SecondaryTertiaryScreen2 | Alternate P1B North, PP Secondary & Tertiary Screen | 114 | 0 | S | U | 111.4 113.6 111.5 | 111.1 110.9 106.9 106.5 105.2 101.7 | Point | Hist | - | - | 3.0 | 648710 | 4773152 | 146.0 | 60 min | - | - |
| AP1B_N_PP_TertiaryCrush1 | Alternate P1B North, PP Tertiary Crusher | 99 | 0 | S | U | 103.4 106.7 97.1 | 99.9 96.0 92.8 91.3 88.6 83.9 | Point | Hist | - | - | 3.0 | 648709 | 4773150 | 146.0 | 60 min | - | - |
| AP1B_N_PP_TertiaryCrush2 | Alternate P1B North, PP Tertiary Crusher | 99 | 0 | S | U | 103.4 106.7 97.1 | 99.9 96.0 92.8 91.3 88.6 83.9 | Point | Hist | - | - | 3.0 | 648710 | 4773150 | 146.0 | 60 min | - | - |
| AP1B_N_PP_Trk1 | Alternate P1B North, PP Idling Truck | 96 | 0 | S | U | 101.7 98.9 94.6 | 90.2 90.5 92.8 90.1 81.6 73.8 | Point | Hist | - | - | 3.0 | 648707 | 4773129 | 146.0 | 60 min | 60 min | 60 min |
| AP1B_N_PP_Trk2 | Alternate P1B North, PP Idling Truck | 96 | 0 | S | U | 101.7 98.9 94.6 | 90.2 90.5 92.8 90.1 81.6 73.8 | Point | Hist | - | - | 3.0 | 648709 | 4773129 | 146.0 | 60 min | 60 min | 60 min |
| AP1B_N_WF_Drill | Alternate P1B North, WF Drill | 110 | 0 | S | U | 96.8 101.2 99.3 | 96.9 102.5 104.3 104.4 102.0 99.5 | Point | Hist | - | - | 2.5 | 648805 | 4773411 | 175.5 | 60 min | - | - |
| AP2_NE_PC_CrusherDump | Alternate P2 NE, PC loader dumping into crusher | 123 | 0 | S | U | 115.4 120.3 122.2 | 120.0 118.3 118.5 116.6 111.1 102.3 | Point | Hist | - | - | 3.0 | 649438 | 4773415 | 165.0 | 60 dumps/hr | - | - |
| AP2_NE_PC_Ldr | Alternate P2 NE, PC loader | 106 | 0 | S | U | 102.4 111.2 104.7 | 101.4 99.9 99.2 97.5 97.7 98.5 | Point | Hist | - | - | 2.5 | 649441 | 4773417 | 164.5 | 60 min | - | - |
| AP2_NE_PC_PrimaryCrush | Alternate P2 NE, PC Primary Crusher | 118 | 0 | S | U | 108.9 119.8 115.0 | 118.7 114.6 112.2 109.6 104.4 99.6 | Point | Hist | - | - | 3.0 | 649436 | 4773413 | 165.0 | 60 min | - | - |
| AP2_NE_PC_PrimaryScreen | Alternate P2 NE, PC Primary Screen | 114 | 0 | S | U | 111.4 113.6 111.5 | 111.1 110.9 106.9 106.5 105.2 101.7 | Point | Hist | - | - | 3.0 | 649435 | 4773411 | 165.0 | 60 min | - | - |
| AP2_NE_PP_Ldr | Alternate P2 NE, PP loader | 106 | 0 | S | U | 102.4 111.2 104.7 | 101.4 99.9 99.2 97.5 97.7 98.5 | Point | Hist | - | - | 2.5 | 648892 | 4773262 | 150.5 | 60 min | 60 min | 60 min |
| AP2_NE_PP_SecondaryCrush1 | Alternate P2 NE, PP Secondary Crusher | 115 | 0 | S ~ | U | 102.3 108.9 111.7 | 110.8 109.6 110.5 107.4 104.6 99.0 | Point | Hist | - | - | 3.0 | 648906 | 4773263 | 151.0 | 60 min | - | - |
| AP2_NE_PP_SecondaryCrush2 | Alternate P2 NE, PP Secondary Crusher | 115 | 0 | s | U | 102.3 108.9 111.7 | 110.8 109.6 110.5 107.4 104.6 99.0 | Point | Hist | - | - | 3.0 | 648907 | 47/3262 | 151.0 | 60 min | - | - |
| AP2_NE_PP_SecondaryTertiaryScreen1 | Alternate P2 NE, PP Secondary & Tertiary Screen | 114 | 0 | s | U | 111.4 113.6 111.5 | 111.1 110.9 106.9 106.5 105.2 101.7 | Point | Hist | - | - | 3.0 | 648905 | 4//3263 | 151.0 | 60 min | - | - |
| AP2_NE_PP_SecondaryTertiaryScreen2 | Alternate P2 NE, PP Secondary & Tertiary Screen | 114 | | S | U | 111.4 113.6 111.5 | 111.1 110.9 106.9 106.5 105.2 101.7 | Point | Hist | - | - | 3.0 | 648905 | 4773262 | 151.0 | 60 min | - | - |
| AF2_NE_FF_IeruaryCrush1 | Alternate P2 NE, PP Tertiary Crusher | 99 | | 5 c | U | 103.4 106.7 97.1 | <u>99.9</u> 90.0 92.8 91.3 88.6 83.9 | Point | Hist | - | - | 3.0 | 648903 | 4//3203 | 151.0 | 60 min | - | |
| AF2_NE_FF_I eruaryCrush2 | Alternate P2 NE, PP Teruary Crusher | 99 | | 5 | U | 105.4 106./ 9/.1 | <u>99.9</u> 90.0 92.8 91.3 88.6 83.9 | Point | HIST | - | - | 3.0 | 648902 | 4//3202 | 151.0 | 60 min | | |
| AFZ_NE_FF_ITKI | Alternate P2 NE, PP Idling Truck | 96 | | S | U | 101.7 98.9 94.6 | <u>90.2</u> <u>90.5</u> <u>92.8</u> <u>90.1</u> <u>81.6</u> <u>73.8</u> | Point | Hist | | - | 3.0 | 648884 | 4//3204 | 151.0 | 60 min | 60 min | 60 min |
| AP2 NE WE Drill | Alternate P2 NE WE Drill | 110 | | s | U | 96.8 101.2 00.2 | 96.9 102.5 104.3 104.4 102.0 90.5 | Point | Hiet | | | 2.5 | 649461 | 4773447 | 177.5 | 60 min | - | 00 11111 |
| AP3 SE PC CrusherDump | Alternate P3 SF_PC loader dumping into crucher | 173 | | <u> </u> | п | 115.4 120.3 122.2 | 120.0 118.3 118.5 116.6 111.1 102.2 | Point | Hiet | | - | 3.0 | 640482 | 4772801 | 164.0 | 60 dume/hr | - | - |
| AP3 SE PC Ldr | Alternate P3 SE, PC Loader | 125 | | 5 | U U | 102.4 111.2 104.7 | 101 4 99 9 99 2 97 5 97 7 98 5 | Point | Hist | - | - | 2.5 | 649483 | 4772801 | 163.5 | 60 min | - | - |
| AP3 SE PC PrimaryCrush | Alternate P3 SE, PC Primary Crusher | 118 | | s | U | 108.9 119.8 115.0 | 118.7 114.6 112.2 109.6 104.4 99.6 | Point | Hist | - | - | 3.0 | 649481 | 4772802 | 164.0 | 60 min | - | |
| AP3 SE PC PrimaryScreen | Alternate P3 SE, PC Primary Screen | 114 | 0 | s | U | 111.4 113.6 111.5 | 111.1 110.9 106.9 106.5 105.2 101.7 | Point | Hist | - | - | 3.0 | 649480 | 4772803 | 164.0 | 60 min | - | - |

Table 1: Additional Data

Table D.1: Noise Source Summary - Alternate Extraction Scenario Upper's Quarry, 1603157

| Notes to Table: | | |
|-----------------|--|--|
| 1. | Wherever possible, the Source ID matches the identifiers used in the ESDM report. | |
| 2. | Sound Power Level of Source, in dBA, not including sound characteristic adjustments per NPC-104. | |
| 3. | Source Location: O = Outside of building, including the roof, I = Inside of building. | |
| 4. | Sound Characteristic, per NPC-104:- S = Steady- I = Impulsive- Q = Quasi-Steady Impulsive- B = Buzzing | - T = Tonal - C = Cyclic |
| 5. | Noise control measures currently in place or specified in construction drawings: - S = Silencer/Muffler - L = Lagging - A = Acoustic lining, plenum - E = Acoustic enclo - B = Barrier/Berm - B = Barrier/Berm | - O = Other osure - U = Uncontrolled ting equipment, ntrol measures |

Table 1: Additional Data

7.

8

- Upper's Quarry, 1603157
 - Source type indicates Cadna/A modelling methodology. For Point, Line, and Area sources, PWLs represent the overall level for the entire source. Where source type is Mobile Equipment, the source is modelled as a moving point source, and PWL is calculated from a single-vehicle passby. 6.
 - Sound Power Level Data Source: Man = Manufacturer's Data Mea = Measured Directly Hist = Historical Data on File at RWDI

EC = Engineering Calc based on specifications
 Same ### = same type as source no. ###

For loader dumping into primary crusher, it is assumed each dump takes approximately 10s

| Source ID ^[1] | Source Description | Sound Power Level ^[2] | Source Location ^[3] | Sound Characteristics ^[4] | Noise Control Measures ^[5] | | 1/1 Octave Band Sound Power Level Data if available (dB) | Source Type ^[6] | PWL Data Source ^[7] | Height Above Roof | Local Roof Height Ab. Grade | Height Above Grade | s | ource Co-ordin for point sour (m) | nates ces | Operating Tim P Vehicle Passby | e during Wors oint Sources, OR y per Hour & Sources | st-case hour for ^[8] Speed for Line |
|------------------------------------|---|--|-----------------------------------|---|--|----|---|----------------------------|--------------------------------|-------------------------|-----------------------------------|--------------------------|--------|---|--------------|--------------------------------------|---|--|
| | | (dBA) | (I or O) | (S,Q,I,B,T,C) | (S,A,B,L,E,O,U) | 31 | <u>31.5 63 125 250 500 1000 2000 4000 8000</u> | | | (m) | (m) | (m) | X | Y | Z | Daytime | Evening | Nighttime |
| AP3_SE_PP_Ldr | Alternate P3 SE, PP Loader | 106 | 0 | S | U | 10 | 102.4 111.2 104.7 101.4 99.9 99.2 97.5 97.7 98.5 | Point | Hist | - | - | 2.5 | 649152 | 4772897 | 147.5 | 60 min | 60 min | 60 min |
| AP3_SE_PP_SecondaryCrush1 | Alternate P3 SE, PP Secondary Crusher | 115 | 0 | S | U | 10 | 102.3 108.9 111.7 110.8 109.6 110.5 107.4 104.6 99.0 | Point | Hist | - | - | 3.0 | 649166 | 4772899 | 148.0 | 60 min | - | - |
| AP3_SE_PP_SecondaryCrush2 | Alternate P3 SE, PP Secondary Crusher | 115 | 0 | S | U | 10 | 102.3 108.9 111.7 110.8 109.6 110.5 107.4 104.6 99.0 | Point | Hist | - | - | 3.0 | 649166 | 4772898 | 148.0 | 60 min | - | |
| AP3_SE_PP_SecondaryTertiaryScreen1 | Alternate P3 SE, PP Secondary & Tertiary Screen | 114 | 0 | S | U | 11 | 111.4 113.6 111.5 111.1 110.9 106.9 106.5 105.2 101.7 | Point | Hist | - | - | 3.0 | 649165 | 4772899 | 148.0 | 60 min | - | |
| AP3_SE_PP_SecondaryTertiaryScreen2 | Alternate P3 SE, PP Secondary & Tertiary Screen | 114 | 0 | S | U | 11 | 111.4 113.6 111.5 111.1 110.9 106.9 106.5 105.2 101.7 | Point | Hist | - | - | 3.0 | 649165 | 4772898 | 148.0 | 60 min | - | |
| AP3_SE_PP_TertiaryCrush1 | Alternate P3 SE, PP Tertiary Crusher | 99 | 0 | Š | U | 10 | 103.4 106.7 97.1 99.9 96.0 92.8 91.3 88.6 83.9 | Point | Hist | - | - | 3.0 | 649163 | 4772898 | 148.0 | 60 min | - | |
| AP3_SE_PP_TertiaryCrush2 | Alternate P3 SE, PP Tertiary Crusher | 99 | 0 | S ~ | U | 10 | 103.4 106.7 97.1 99.9 96.0 92.8 91.3 88.6 83.9 | Point | Hist | - | - | 3.0 | 649163 | 4772897 | 148.0 | 60 min | - | - |
| AP3_SE_PP_Trk1 | Alternate P3 SE, PP Idling Truck | 96 | 0 | ŝ | U | 10 | 101.7 98.9 94.6 90.2 90.5 92.8 90.1 81.6 73.8 | Point | Hist | - | - | 3.0 | 649143 | 4772895 | 148.0 | 60 min | 60 min | 60 min |
| AP3_SE_PP_Trk2 | Alternate P3 SE, PP Idling Truck | 96 | 0 | ŝ | U | 10 | 101.7 98.9 94.6 90.2 90.5 92.8 90.1 81.6 73.8 | Point | Hist | - | - | 3.0 | 649142 | 4772897 | 148.0 | 60 min | 60 min | 60 min |
| AP3_SE_WF_Drill | Alternate P3 SE, WF Drill | 110 | 0 | s | U | 96 | 96.8 101.2 99.3 96.9 102.5 104.3 104.4 102.0 99.5 | Point | Hist | - | - | 2.5 | 649512 | 4//2/88 | 180.5 | 60 min | - | - |
| ASPH_comp | Asphalt Plant - Compressor Vent | 96 | 0 | S | U | 91 | 91.4 88.5 99.4 96.2 93.0 90.2 87.4 84.9 81.3 | Point | Hist | - | - | 0.6 | 648875 | 4//2829 | 143.6 | 60 min | 60 min | 60 min |
| ASPH_DC_m | Asphalt Plant - Dust Collector Blower (motor) | 105 | 0 | S | U | 11 | 110.8 113.6 105.4 104.1 102.2 99.8 94.9 93.4 91.5 | Point | Hist | - | - | 2.0 | 648856 | 4//2826 | 145.0 | 60 min | 60 min | 60 min |
| ASPH_DC_S | Asphalt Plant - Dust Collector Blower (stack) | 110 | 0 | 5 | U | 12 | 125.3 126.2 117.0 110.0 105.8 105.3 98.5 95.6 86.1 | Point | Hist | 0.1 | 20.0 | 20.1 | 048833 | 4//2820 | 163.1 | 60 min | 60 min | 60 min |
| ASPH_elev | Asphalt Plant - Elevator Motor | 100 | 0 | S | U | 95 | 95.7 97.7 95.1 95.2 97.8 95.5 91.5 87.3 77.2 | Point | Hist | - | - | 19.0 | 648861 | 4//2835 | 162.0 | 60 min | 60 min | 60 min |
| ASPH_IDLE_TRK1 | Asphalt Plant - Idling Truck | 90 | 0 | 5 | U | 10 | 101.7 98.9 94.0 90.2 90.3 92.8 90.1 81.0 73.8 101.7 08.9 04.6 00.2 00.5 02.8 00.1 81.6 73.8 | Point | Hist | | - | 3.5 | 648880 | 4772825 | 146.5 | 60 min | 60 min | 60 min |
| ASTIL_IDEE_TKK2 | Asphalt Plant Sile Impulsive | 127 | 0 | З | U | 10 | 101.7 98.9 94.0 90.2 90.5 92.8 90.1 81.0 75.8 122.0 127.0 114.5 107.6 106.6 108.5 117.0 122.2 122.2 | Doint | Hist | 1.0 | 21.0 | 22.0 | 640000 | 4772842 | 140.5 | 60 min | 60 min | 60 min |
| ASPH_Imp_sho | Asphalt Plant - Sho - Impulsive | 102 | 0 | I S | U | 12 | 102.6 100.2 104.1 00.2 07.2 05.8 04.2 02.1 88.0 | Point | Hist | 1.0 | 21.0 | 22.0 | 648870 | 4772830 | 145.5 | 60 min | 60 min | 60 min |
| ASPH Ldr Act? | Asphalt Plant - Loader Activity | 102 | 0 | S | U | 10 | 103.6 109.2 104.1 99.2 97.3 95.8 94.2 93.1 88.0 | Point | Hist | - | - | 2.5 | 648864 | 4772827 | 145.5 | 60 min | 60 min | 60 min |
| ASPU motor | Asphalt Plant Conveyor motor graval hitting metal plate | 102 | 0 | s | U | 10 | 100.5 102.5 04.2 05.5 08.0 102.0 05.1 01.4 | Point | List | _ | - | 4.0 | 648854 | 4772824 | 147.0 | 60 min | 60 min | 60 min |
| ASPH oven | Asphalt Plant - Oven Motor | 107 | 0 | S | U | 11 | 100.5 102.5 94.2 95.5 98.9 105.0 102.0 95.1 91.4 111.4 110.7 104.0 100.1 98.3 07.8 93.9 91.9 89.0 | Point | Hist | - | - | 5.8 | 648858 | 4772834 | 148.8 | 60 min | 60 min | 60 min |
| ASPH pugdoor | Asphalt Plant - Pug Mill door (pressure relief noise) | 102 | 0 | S | U | | 114 6 112 8 109 9 106 3 105 2 101 2 96 8 94 9 93 4 | Point | Hist | - | - | 4.0 | 648863 | 4772834 | 147.0 | 60 min | 60 min | 60 min |
| ASPH nugmill | Asphalt Plant - Pug Mill Motor | 105 | 0 | s | U | | 0.0 105.0 104.6 100.8 94.8 94.7 96.6 99.5 99.3 | Point | Hist | <u> </u> | | 5.0 | 648870 | 4772837 | 148.0 | 60 min | 60 min | 60 min |
| //or ri_pugimii | Asphalt Funt Fug Min Motor | 105 | 0 | 5 | 0 | | 0.0 100.0 101.0 100.0 71.0 71.7 70.0 77.5 77.5 | Tomt | mst | | | 5.0 | 010070 | 1772037 | 110.0 | 00 1111 | 00 11111 | 00 1111 |
| | | | | | | | Line Sources | | | | | | | | | | | |
| AP1B N Conveyor | Alternate P1B North, Conveyor | 83 | 0 | S | U | 74 | 74.5 75.5 79.0 77.3 78.8 79.2 75.6 69.1 58.5 | Line | Hist | - | - | 3.5 | - | - | - | 60 min | - | - |
| AP1B N RD Haul PP AP Em | Alternate P1B North, Aggregate Haul road b/w PP and AP, Empty | 108 | 0 | S | U | 11 | 110.2 113.9 109.7 105.1 104.6 102.7 101.6 92.5 89.4 | Line | Hist | - | - | 3.5 | - | - | - | 3/hr, 20kph | 3/hr, 20kph | 3/hr, 20kph |
| AP1B N RD Haul PP AP Fu | Alternate P1B North, Aggregate Haul road b/w PP and AP, Full | 112 | 0 | S | U | 10 | 108.8 108.3 109.9 109.0 106.2 108.2 104.3 98.4 94.8 | Line | Hist | - | - | 3.5 | - | - | - | 3/hr, 20kph | 3/hr, 20kph | 3/hr, 20kph |
| AP1B N RD SHP Aggr Em | Alternate P1B North, Aggregate Shipping from PP, Empty | 104 | 0 | S | U | 10 | 107.7 110.2 108.3 99.9 99.4 98.6 96.7 93.6 91.6 | Line | Hist | - | - | 3.5 | - | - | - | 12/hr, 20kph | 12/hr, 20kph | 12/hr, 20kph |
| AP1B N RD SHP Aggr Fu | Alternate P1B North, Aggregate Shipping from PP, Full | 104 | 0 | S | U | 10 | 107.7 110.2 108.3 99.9 99.4 98.6 96.7 93.6 91.6 | Line | Hist | - | - | 3.5 | - | - | - | 12/hr, 20kph | 12/hr, 20kph | 12/hr, 20kph |
| AP2_NE_Conveyor | Alternate P2 NE, Conveyor | 83 | 0 | S | U | 74 | 74.5 75.5 79.0 77.3 78.8 79.2 75.6 69.1 58.5 | Line | Hist | - | - | 3.5 | - | - | - | 60 min | - | - |
| AP2_NE_RD_Haul_PP_AP_Em | Alternate P2 NE, Aggregate Haul road b/w PP and AP, Empty | 108 | 0 | S | U | 11 | 110.2 113.9 109.7 105.1 104.6 102.7 101.6 92.5 89.4 | Line | Hist | - | - | 3.5 | - | - | - | 3/hr, 20kph | 3/hr, 20kph | 3/hr, 20kph |
| AP2_NE_RD_Haul_PP_AP_Fu | Alternate P2 NE, Aggregate Haul road b/w PP and AP, Full | 112 | 0 | S | U | 10 | 108.8 108.3 109.9 109.0 106.2 108.2 104.3 98.4 94.8 | Line | Hist | - | - | 3.5 | - | - | - | 3/hr, 20kph | 3/hr, 20kph | 3/hr, 20kph |
| AP2_NE_RD_SHP_Aggr_Em | Alternate P2 NE, Aggregate Shipping from PP, Empty | 104 | 0 | S | U | 10 | 107.7 110.2 108.3 99.9 99.4 98.6 96.7 93.6 91.6 | Line | Hist | - | - | 3.5 | - | - | - | 12/hr, 20kph | 12/hr, 20kph | 12/hr, 20kph |
| AP2_NE_RD_SHP_Aggr_Fu | Alternate P2 NE, Aggregate Shipping from PP, Full | 104 | 0 | S | U | 10 | 107.7 110.2 108.3 99.9 99.4 98.6 96.7 93.6 91.6 | Line | Hist | - | - | 3.5 | - | - | - | 12/hr, 20kph | 12/hr, 20kph | 12/hr, 20kph |
| AP3_SE_Conveyor | Alternate P3 SE, Conveyor | 83 | 0 | S | U | 74 | 74.5 75.5 79.0 77.3 78.8 79.2 75.6 69.1 58.5 | Line | Hist | - | - | 3.5 | - | - | - | 60 min | - | - |
| AP3_SE_RD_Haul_PP_AP_Em | Alternate P3 SE, Aggregate Haul road b/w PP and AP, Empty | 108 | 0 | S | U | 11 | 110.2 113.9 109.7 105.1 104.6 102.7 101.6 92.5 89.4 | Line | Hist | - | - | 3.5 | - | - | - | 3/hr, 20kph | 3/hr, 20kph | 3/hr, 20kph |
| AP3_SE_RD_Haul_PP_AP_Fu | Alternate P3 SE, Aggregate Haul road b/w PP and AP, Full | 112 | 0 | S | U | 10 | 108.8 108.3 109.9 109.0 106.2 108.2 104.3 98.4 94.8 | Line | Hist | - | - | 3.5 | - | - | - | 3/hr, 20kph | 3/hr, 20kph | 3/hr, 20kph |
| AP3_SE_RD_SHP_Aggr_Em | Alternate P3 SE, Aggregate Shipping from PP, Empty | 104 | 0 | S | U | 10 | 107.7 110.2 108.3 99.9 99.4 98.6 96.7 93.6 91.6 | Line | Hist | - | - | 3.5 | - | - | - | 12/hr, 20kph | 12/hr, 20kph | 12/hr, 20kph |
| AP3_SE_RD_SHP_Aggr_Fu | Alternate P3 SE, Aggregate Shipping from PP, Full | 104 | 0 | S | U | 10 | 107.7 110.2 108.3 99.9 99.4 98.6 96.7 93.6 91.6 | Line | Hist | - | - | 3.5 | - | - | - | 12/hr, 20kph | 12/hr, 20kph | 12/hr, 20kph |
| AP_RD_SHP_AC_RAP_Em | AP, AC and RAP shipped from Offsite, Empty | 104 | 0 | S | U | 10 | 107.7 110.2 108.3 99.9 99.4 98.6 96.7 93.6 91.6 | Line | Hist | - | - | 3.5 | - | - | - | 6/hr, 20kph | 6/hr, 20kph | 6/hr, 20kph |
| AP_RD_SHP_AC_RAP_Fu | AP, AC and RAP shipped from Offsite, Full | 104 | 0 | S | U | 10 | 107.7 110.2 108.3 99.9 99.4 98.6 96.7 93.6 91.6 | Line | Hist | - | - | 3.5 | - | - | - | 6/hr, 20kph | 6/hr, 20kph | 6/hr, 20kph |
| AP_RD_SHP_HMA_Em | AP, HMA product shipping, Empty | 104 | 0 | S | U | 10 | 107.7 110.2 108.3 99.9 99.4 98.6 96.7 93.6 91.6 | Line | Hist | - | - | 3.5 | - | - | - | 6/hr, 20kph | 6/hr, 20kph | 6/hr, 20kph |
| AP_RD_SHP_HMA_Fu | AP, HMA product shipping, Full | 104 | 0 | S | U | 10 | 107.7 110.2 108.3 99.9 99.4 98.6 96.7 93.6 91.6 | Line | Hist | - | - | 3.5 | - | - | - | 6/hr, 20kph | 6/hr, 20kph | 6/hr, 20kph |

Table D.2a: Acoustic Assessment Summary, Alternate Phase 1B North Upper's Quarry, 1603157

Notes to Table:

- "Table A3" in Appendix A of Basic CCofA Guide.

1. "Continuous" noise sources includes sum of steady, quasi-steady impulsive, tonal, cyclical and buzzing noise sources, with appropriate penalties applied, in accordance with documents NPC-104 and NPC-300. Impulsive and emergency noise sources are assessed separately from continuous noise sources.

2. Daytime occurs from 0700-1900h. Evening occurs from 1900h-2300h. Nighttime occurs from 2300-0700h.

3. Worst-case cumulative sound level from all applicable sources operating.

4. Has an acoustic audit (as defined in Publication NPC-233) been conducted with source in place and operating?

5. Applicable worst-case NPC-300 sound level limit.

6. Performance limit (aka guideline limit) based on following:

- C = Calculated based on road traffic volumes in compliance with NPC-206 requirements.

- M = Measured based on monitoring for a minimum 48 hour period, in accordance with NPC-233 requirements.

- D = Default guideline minima per NPC-300.

| Point of Reception ID | Point of Reception Description | Time Period | Total Sound Level at PoR ^[3] | Verified by Acoustic Audit ^[4] | Performance Limit ^[5] | Peformance Limit Source | Compliance with Performance Limit | UTM Co (Zone | oordinate e 17N) | Height Relative to Local Grade |
|-----------------------------|---|-------------|---|---|-------------------------------------|----------------------------|--|-----------------|---------------------|--------------------------------------|
| | | | (dBA) | (Yes/No) | (dBA) | (C / M/ D) | (Yes/No) | X (m) | Y (m) | (m) |
| | Econdo of dwalling (10149 | Daytime | 47 | No | 50 | | Yes | | | |
| R1f | Beaverdams Rd) | Evening | 39 | No | 50 | D | Yes | 648766 | 4773660 | 4.5 |
| | Beuverdums reaj | Nighttime | 39 | No | 45 | | Yes | | | |
| P1o | Outdoor area of dwelling (10148 | Daytime | 46 | No | 50 | р | Yes | 648766 | 4772620 | 1.5 |
| KIU | Beaverdams Rd) | Evening | 37 | No | 45 | D | Yes | 048700 | 4773029 | 1.5 |
| | Econdo of dwalling (0722 | Daytime | 40 | No | 50 | | Yes | | | |
| R2f | Beaverdams Rd) | Evening | 33 | No | 50 | D | Yes | 649394 | 4773728 | 4.5 |
| | Beaverdanis (Cu) | Nighttime | 33 | No | 45 | | Yes | | | |
| D 20 | Outdoor area of dwelling (9722 | Daytime | 38 | No | 50 | р | Yes | 640201 | 1772608 | 1.5 |
| K20 | Beaverdams Rd) | Evening | 28 | No | 45 | D | Yes | 049391 | 4//3098 | 1.5 |
| | Econdo of dwalling (0602 | Daytime | 37 | No | 50 | | Yes | | | |
| R3f | Beaverdams Rd) | Evening | 32 | No | 50 | D | Yes | 649571 | 4773645 | 4.5 |
| | Beaverdains Rd) | Nighttime | 32 | No | 45 | | Yes | | | |
| P20 | Outdoor area of dwelling (9602 | Daytime | 35 | No | 50 | D | Yes | 640552 | 4772620 | 1.5 |
| K30 | Beaverdams Rd) | Evening | 27 | No | 45 | D | Yes | 049333 | 4773020 | 1.5 |
| | Errola of travilling (5594 | Daytime | 37 | No | 50 | | Yes | | | |
| R4f | Facade of dwelling (5584 Beechwood Rd) | Evening | 33 | No | 50 | D | Yes | 649611 | 4772698 | 4.5 |
| | Beeenwood Ru) | Nighttime | 33 | No | 45 | | Yes | | | |
| P 4o | Outdoor area of dwelling (5584 | Daytime | 30 | No | 50 | D | Yes | 640504 | דרדרדה | 1.5 |
| K40 | Beechwood Rd) | Evening | 27 | No | 45 | D | Yes | 049394 | 4//2/2/ | 1.5 |
| | Erector of travilling (57(0 | Daytime | 38 | No | 50 | | Yes | | | |
| R5f | Beechwood Rd) | Evening | 30 | No | 50 | D | Yes | 649553 | 4772408 | 4.5 |
| | Becchwood Ray | Nighttime | 30 | No | 45 | | Yes | | | |
| P 50 | Outdoor area of dwelling (5769 | Daytime | 32 | No | 50 | D | Yes | 640532 | 1772120 | 1.5 |
| 100 | Beechwood Rd) | Evening | 29 | No | 45 | Ъ | Yes | 047552 | 7//2429 | 1.5 |
| | Essade of dwalling (0044 Lundrig | Daytime | 38 | No | 50 | | Yes | | | |
| R6f | I n) | Evening | 30 | No | 50 | D | Yes | 649084 | 4771672 | 4.5 |
| | | Nighttime | 30 | No | 45 | | Yes | | | |
| P 60 | Outdoor area of dwelling (9944 | Daytime | 37 | No | 50 | D | Yes | 640070 | 4771602 | 1.5 |
| KOO | Lundy's Ln) | Evening | 30 | No | 45 | U | Ves | 049070 | +//1093 | 1.5 |

Assessment of Impacts for "Continuous" Noise Sources ^[1]

Table D.2b: Acoustic Assessment Summary, Alternate Phase 2 Northeast Upper's Quarry, 1603157

Notes to Table:

- "Table A3" in Appendix A of Basic CCofA Guide.

1. "Continuous" noise sources includes sum of steady, quasi-steady impulsive, tonal, cyclical and buzzing noise sources, with appropriate penalties applied, in accordance with documents NPC-104 and NPC-300. Impulsive and emergency noise sources are assessed separately from continuous noise sources.

2. Daytime occurs from 0700-1900h. Evening occurs from 1900h-2300h. Nighttime occurs from 2300-0700h.

3. Worst-case cumulative sound level from all applicable sources operating.

4. Has an acoustic audit (as defined in Publication NPC-233) been conducted with source in place and operating?

5. Applicable worst-case NPC-300 sound level limit.

6. Performance limit (aka guideline limit) based on following:

- C = Calculated based on road traffic volumes in compliance with NPC-206 requirements.

- M = Measured based on monitoring for a minimum 48 hour period, in accordance with NPC-233 requirements.

- D = Default guideline minima per NPC-300.

| Point of Reception ID | Point of Reception Description | Time Period | Total Sound Level at PoR ^[3] | Verified by Acoustic Audit ^[4] | Performance Limit ^[5] | Peformance Limit Source [6] | Compliance with Performance Limit | UTM Coordinate (Zone 17N) | | Height Relative to Local Grade |
|-----------------------------|--|-------------|---|---|-------------------------------------|-----------------------------------|--|------------------------------|-----------|--------------------------------------|
| | | | (dBA) | (Yes/No) | (dBA) | (C / M/ D) | (Yes/No) | X (m) | Y (m) | (m) |
| R1f | Econdo of dwalling (10149 | Daytime | 46 | No | 50 | | Yes | | | |
| | Beaverdams Rd) | Evening | 41 | No | 50 | D | Yes | 648766 | 4773660 | 4.5 |
| | | Nighttime | 41 | No | 45 | | Yes | | | |
| R1o | Outdoor area of dwelling (10148 | Daytime | 45 | No | 50 | D | Yes | 648766 | 4773629 | 1.5 |
| | Beaverdams Rd) | Evening | 40 | No | 45 | | Yes | 048700 | | |
| | Facade of dwelling (9722 | Daytime | 47 | No | 50 | | Yes | 649394 | 4773728 | 4.5 |
| R2f | Beaverdams Rd) | Evening | 35 | No | 50 | D | Yes | | | |
| | Beuverdums reaj | Nighttime | 35 | No | 45 | | Yes | | | |
| R2o | Outdoor area of dwelling (9722 Beaverdams Rd) | Daytime | 45 | No | 50 | р | Yes | 649391 | 4773698 | 1.5 |
| | | Evening | 34 | No | 45 | D | Yes | 047571 | | |
| R3f | Facade of dwelling (9602 Beaverdams Rd) | Daytime | 48 | No | 50 | D | Yes | 649571 | 4773645 | 4.5 |
| | | Evening | 36 | No | 50 | | Yes | | | |
| | | Nighttime | 36 | No | 45 | | Yes | | | |
| P 30 | Outdoor area of dwelling (9602 Beaverdams Rd) | Daytime | 48 | No | 50 | D | Yes | 649553 | 4773620 | 1.5 |
| 1050 | | Evening | 33 | No | 45 | Б | Yes | | | |
| | Facade of dwelling (5584 Beechwood Rd) | Daytime | 48 | No | 50 | D | Yes | 649611 | 4772698 | 4.5 |
| R4f | | Evening | 36 | No | 50 | | Yes | | | |
| | | Nighttime | 36 | No | 45 | | Yes | | | |
| R 4o | Outdoor area of dwelling (5584 Beechwood Rd) | Daytime | 44 | No | 50 | D | Yes | 649594 | 4772727 | 1.5 |
| IC+0 | | Evening | 30 | No | 45 | | Yes | | | |
| | Facade of dwelling (5769 Beechwood Rd) | Daytime | 45 | No | 50 | D | Yes | 649553 | 4772408 | 4.5 |
| R5f | | Evening | 32 | No | 50 | | Yes | | | |
| | | Nighttime | 32 | No | 45 | | Yes | | | |
| P 50 | Outdoor area of dwelling (5769 Beechwood Rd) | Daytime | 43 | No | 50 | D Yes Yes | Yes | 649532 | 4772420 | 1.5 |
| K30 | | Evening | 31 | No | 45 | | 047552 | 4//2429 | 1.5 | |
| | Facade of dwelling (9944 Lundy's Ln) | Daytime | 40 | No | 50 | D | Yes | 649084 | | |
| R6f | | Evening | 31 | No | 50 | | Yes | | 4771672 | 4.5 |
| | | Nighttime | 31 | No | 45 | | Yes | | | |
| P60 | Outdoor area of dwelling (9944 | Daytime | 39 | No | 50 | D — | Yes | 640070 | 0 4771693 | 1.5 |
| R60 | Lundy's Ln) | Evening | 31 | No | 45 | | Vec | 049070 | | 1.5 |

Assessment of Impacts for "Continuous" Noise Sources [1]

Table D.2c: Acoustic Assessment Summary, Alternate Phase 3 Southeast Upper's Quarry, 1603157

Notes to Table:

- "Table A3" in Appendix A of Basic CCofA Guide.

1. "Continuous" noise sources includes sum of steady, quasi-steady impulsive, tonal, cyclical and buzzing noise sources, with appropriate penalties applied, in accordance with documents NPC-104 and NPC-300. Impulsive and emergency noise sources are assessed separately from continuous noise sources.

2. Daytime occurs from 0700-1900h. Evening occurs from 1900h-2300h. Nighttime occurs from 2300-0700h.

3. Worst-case cumulative sound level from all applicable sources operating.

4. Has an acoustic audit (as defined in Publication NPC-233) been conducted with source in place and operating?

5. Applicable worst-case NPC-300 sound level limit.

6. Performance limit (aka guideline limit) based on following:

- C = Calculated based on road traffic volumes in compliance with NPC-206 requirements.

- M = Measured based on monitoring for a minimum 48 hour period, in accordance with NPC-233 requirements.

- D = Default guideline minima per NPC-300.

| Point of Reception ID | Point of Reception Description | Time Period | Total Sound Level at PoR ^[3] | Verified by Acoustic Audit ^[4] | Performance Limit ^[5] | Peformance Limit Source [6] | Compliance with Performance Limit | UTM Coordinate (Zone 17N) | | Height Relative to Local Grade |
|-----------------------------|--|-------------|---|---|-------------------------------------|-----------------------------------|--|------------------------------|-----------|--------------------------------------|
| | | | (dBA) | (Yes/No) | (dBA) | (C / M/ D) | (Yes/No) | X (m) | Y (m) | (m) |
| R1f | Econdo of dyvalling (10149 | Daytime | 48 | No | 50 | | Yes | | 4773660 | |
| | Beaverdams Rd) | Evening | 41 | No | 50 | D | Yes | 648766 | | 4.5 |
| | | Nighttime | 41 | No | 45 | | Yes | | | |
| D1a | Outdoor area of dwelling (10148 | Daytime | 47 | No | 50 | D | Yes | 648766 | 4773629 | 1.5 |
| KIU | Beaverdams Rd) | Evening | 40 | No | 45 | | Yes | 048700 | | |
| | Econdo of dwalling (0722 | Daytime | 47 | No | 50 | | Yes | 649394 | 4773728 | 4.5 |
| R2f | Facade of dwelling (9/22 Beauerdama Bd) | Evening | 38 | No | 50 | D | Yes | | | |
| | Beaverdains Rdy | Nighttime | 38 | No | 45 | | Yes | | | |
| D 20 | Outdoor area of dwelling (9722 Beaverdams Rd) | Daytime | 45 | No | 50 | р | Yes | 640201 | 1772608 | 1.5 |
| K20 | | Evening | 37 | No | 45 | | Yes | 049391 | H//30/0 | |
| | Facade of dwelling (9602 Beaverdams Rd) | Daytime | 47 | No | 50 | D | Yes | 649571 | 4773645 | 4.5 |
| R3f | | Evening | 38 | No | 50 | | Yes | | | |
| | | Nighttime | 38 | No | 45 | | Yes | | | |
| P20 | Outdoor area of dwelling (9602 Beaverdams Rd) | Daytime | 46 | No | 50 | л | Yes | 649553 | 4773620 | 1.5 |
| K30 | | Evening | 37 | No | 45 | D | Yes | | | |
| | Facade of dwelling (5584 Beechwood Rd) | Daytime | 49 | No | 50 | D | Yes | 649611 | | |
| R4f | | Evening | 41 | No | 50 | | Yes | | 4772698 | 4.5 |
| | | Nighttime | 41 | No | 45 | | Yes | | | |
| P 4o | Outdoor area of dwelling (5584 Beechwood Rd) | Daytime | 48 | No | 50 | D | Yes | 649594 | 4772727 | 1.5 |
| K40 | | Evening | 40 | No | 45 | | Yes | | | |
| | Facade of dwelling (5769 Beechwood Rd) | Daytime | 43 | No | 50 | D | Yes | 649553 | | |
| R5f | | Evening | 40 | No | 50 | | Yes | | 4772408 | 4.5 |
| | | Nighttime | 40 | No | 45 | | Yes | | | |
| P 50 | Outdoor area of dwelling (5769 Beechwood Rd) | Daytime | 42 | No | 50 | р | Yes | 649532 | 4772420 | 1.5 |
| KJU | | Evening | 39 | No | 45 | Ъ | Yes | 047552 | 4//2429 | 1.5 |
| R6f | Facade of dwelling (9944 Lundy's Ln) | Daytime | 42 | No | 50 | D | Yes | 649084 | | |
| | | Evening | 37 | No | 50 | | Yes | | 4771672 | 4.5 |
| | | Nighttime | 37 | No | 45 | | Yes | | | |
| P60 | Outdoor area of dwelling (9944 | Daytime | 41 | No | 50 | D Yes | Yes | (10070 | 0 4771602 | 1.5 |
| K60 | Lundy's Ln) | Evening | 36 | No | 45 | | Ves | 049070 | +//1093 | 1.5 |

Assessment of Impacts for "Continuous" Noise Sources ^[1]

Table D.2d: Acoustic Assessment Summary, Alternate Scenario Impulsive Source Upper's Quarry, 1603157

Notes to Table:

6.

- "Table A3" in Appendix A of Basic CCofA Guide.
- 1. Impulsive noise sources are assessed separately from continuous noise sources.
- 2. Daytime occurs from 0700-1900h. Evening occurs from 1900h-2300h. Nighttime occurs from 2300-0700h.
- 3. Worst-case cumulative sound level from all applicable sources operating.
- 4. Has an acoustic audit (as defined in Publication NPC-233) been conducted with source in place and operating?
- 5. Applicable worst-case NPC-300 sound level limit, based on more than 9 impulses per hour in a Class 2 area.

Performance limit (aka guideline limit) based on following:

- C = Calculated based on road traffic volumes in compliance with NPC-206 requirements.
- M = Measured based on monitoring for a minimum 48 hour period, in accordance with NPC-233 requirements.

- D = Default guideline minima per NPC-300.

| Point of Reception ID | Point of Reception Description | Time Period | Total Sound Level at PoR ^[3] | Verified by Acoustic Audit ^[4] | Performance Limit ^[5] | Peformance Limit Source | Compliance with Performance Limit | UTM Coordinate (Zone 17N) | | Height Relative to Local Grade |
|-----------------------------|--|-------------|---|---|-------------------------------------|----------------------------|--|------------------------------|-----------|--------------------------------------|
| | | | (dBA) | (Yes/No) | (dBA) | (C / M/ D) | (Yes/No) | X (m) | Y (m) | (m) |
| | Facade of dwelling (10148 Beaverdams Rd) | Daytime | 41 | No | 50 | | Yes | | 4773660 | |
| R1f | | Evening | 41 | No | 50 | D | Yes | 648766 | | 4.5 |
| | | Nighttime | 41 | No | 45 | | Yes | | | |
| D1a | Outdoor area of dwelling (10148 | Daytime | 41 | No | 50 | D | Yes | 648766 | 4773629 | 1.5 |
| KIU | Beaverdams Rd) | Evening | 41 | No | 45 | Ъ | Yes | 048700 | | |
| | Econdo of dwalling (0722 | Daytime | 38 | No | 50 | | Yes | 649394 | 4773728 | 4.5 |
| R2f | Beaverdams Rd) | Evening | 38 | No | 50 | D | Yes | | | |
| | Deavertains (Cd) | Nighttime | 38 | No | 45 | | Yes | | | |
| P20 | Outdoor area of dwelling (9722 Beaverdams Rd) | Daytime | 38 | No | 50 | D | Yes | 649391 | 4773698 | 1.5 |
| R20 | | Evening | 38 | No | 45 | | Yes | | | |
| R3f | Facade of dwelling (9602 Beaverdams Rd) | Daytime | 38 | No | 50 | D | Yes | 649571 | 4773645 | |
| | | Evening | 38 | No | 50 | | Yes | | | 4.5 |
| | | Nighttime | 38 | No | 45 | | Yes | | | |
| D2- | Outdoor area of dwelling (9602 Beaverdams Rd) | Daytime | 38 | No | 50 | П | Yes | 640553 | 4773620 | 1.5 |
| K30 | | Evening | 38 | No | 45 | D | Yes | 049333 | | |
| | Facade of dwelling (5584 Beechwood Rd) | Daytime | 42 | No | 50 | D | Yes | 649611 | 4772698 | 4.5 |
| R4f | | Evening | 42 | No | 50 | | Yes | | | |
| | | Nighttime | 42 | No | 45 | | Yes | | | |
| P4o | Outdoor area of dwelling (5584 Beechwood Rd) | Daytime | 43 | No | 50 | D — | Yes | 649594 | 4772727 | 1.5 |
| K40 | | Evening | 43 | No | 45 | | Yes | | | |
| | Facade of dwelling (5769 Beechwood Rd) | Daytime | 41 | No | 50 | D | Yes | 649553 | 4772408 | 4.5 |
| R5f | | Evening | 41 | No | 50 | | Yes | | | |
| | | Nighttime | 41 | No | 45 | | Yes | | | |
| R5o | Outdoor area of dwelling (5769 Beechwood Rd) | Daytime | 42 | No | 50 | D | Yes | 649532 | 4772429 | 1.5 |
| | | Evening | 42 | No | 45 | | Yes | | | |
| R6f | Facade of dwelling (9944 Lundy's Ln) | Daytime | 35 | No | 50 | D | Yes | 649084 | 4 4771672 | 4.5 |
| | | Evening | 35 | No | 50 | | Yes | | | |
| | | Nighttime | 35 | No | 45 | | Yes | | | |
| R6o | Outdoor area of dwelling (9944 | Daytime | 36 | No | 50 | D Yes Yes | Yes | 640070 | 4771602 | 1.5 |
| KOO | Lundy's Ln) | Evening | 36 | No | 45 | | 049070 | +//1095 | 1.5 | |

Assessment of Impacts for "Impulsive" Noise Sources [1]






















APPENDIX E



SLAVI GROZEV, P.ENG., B.A.SC. SENIOR ENGINEER T: 647-475-1048 X 2609 | Slavi.Grozev@rwdi.com

Slavi is an acoustics specialist who supports our clients with a range of noise-related processes, including permitting, compliance, modeling and complaint investigation. His project experience spans a range of industries, including manufacturing, utilities and distribution, food and beverage, quarries and pits, wastewater treatment, waste disposal and land development. Our clients benefit in particular from the depth of Slavi's experience with transportation-related noise. In a previous role with the Ontario Ministry of Transportation, he carried out noise impact assessments of highway and transit corridors and interchange reconfigurations, and also supported roadway noise abatement strategies and transportation policy development. Slavi is RAQS-certified and is experienced in a variety of road traffic models including TNM 2.5.

Technical Expertise

- Compliance and permitting
- Environmental Noise
- Government Reporting
- Industrial Noise
- Noise Impact Assessments
- Noise Modeling
- Transportation Noise

Project Experience

- Lafarge Woodstock Quarry, Woodstock, ON
- McCreedy Mine, Sudbury, ON
- IKO Crusher Plant, Ingersoll, ON
- Tri City Spencer Pit, Guelph, ON
- Tri City Kitchener Pit, Kitchener, ON
- KPM Reid Pit, Brantford, ON

Employment History

2019-Present Senior Engineer, RWDI

2017-2019 Senior Environmental Engineer (Acoustics), Arcadis Canada Inc.

2015-2017

Senior Policy Analyst, Acoustics, Air Quality and Climate Change, Ontario Ministry of Transportation

2010-2015 Project Manager/Engineer, Air and Noise Quality Group, GHD Limited

Education

Bachelor of Science (Chemical Engineering) (Hons.), University of Waterloo, Waterloo, ON, 2010

Affiliations

Member, Professional Engineers of Ontario, 2015 – Present

ΧŅ

Member, Air & Waste Management Association, 2018 - Present

RAY LI, M.SC., P.ENG. NOISE AND VIBRATION ENGINEER

T: 403-232-6771 X 6283 | Ray.Li@rwdi.com

Ray joined RWDI in 2018 and has become an integral part of the noise, acoustics, and vibration team. He has conducted noise and vibration studies in multiple jurisdictions across Canada and for a wide range of clients. His expertise is with energy production, industrial facilities, and mining operations.

Ray is also well versed in construction vibration and has helped clients manage construction vibration levels in dense urban areas.

Project Experience

Energy & Power

- Prairie Lights Power Plant AB
- Hidden Lake Compressor Station AB
- Buffalo Creek Compressor Station AB
- Hidden Lake Compressor Station AB
- Kaybob Gas Plant AB
- ALC Scotford Generator Addition AB
- Fox Creek Wells AB
- Enbridge Valve Stations Blowdown BC
- Claresholm Solar Farm AB
- Greengate Solar Farm AB

Ontario Regulatory Applications

- ECA/EASR noise assessment for industrial facilities
- Land use planning for developments

Construction Vibration

- Calgary Cancer Centre Calgary, AB
- Trans Mountain Pipeline Edmonton, AB

Mining and Quarry

- Upper's Quarry Niagara Falls, ON
- Melbourne Road Quarry Thunder Bay, ON
- North Coal Sparwood, BC
- Portable Crusher Plants ON

Employment History

2018-Present Noise and Vibration Engineer, RWDI

2016-2018 **Research Assistant**, **University of Alberta**

2015 Engineer-in-Training, **TransCanada Pipelines**

2013-2014 **Engineering Intern, TransCanada Pipelines**

Education

Master of Science (Materials Engineering), University of Alberta, Canada

Bachelor of Science (Mech. Engineering), University of Calgary, Canada

Affiliation

Association of Professional Engineers and Geoscientists of Alberta (APEGA)



