## UPPER'S QUARRY

FINAL : OCTOBER 2021

## REPORT PREPARED FOR

WALKER AGGREGATES INC.
1206 ROSEWARNE DRIVE THOROLD, ON L2V 3Y8

REPORT PREPARED BY
THE MUNICIPAL
this report has been formatted for double-sided printing

## EXECUTIVE SUMMARY

The Municipal Infrastructure Group Ltd. (TMIG) was retained by Walker Aggregates Inc., to prepare a Traffic Impact Study (TIS) for the proposed Upper's Quarry. The proposed Upper's Quarry is located generally on lands situated south of Beaverdams Road, north of Lundy's Lane, west of Beechwood Road, and east of Thorold Townline Road, in the City of Niagara Falls, Region of Niagara, adjacent to City of Thorold.

The proposed Upper's Quarry has an approximate area of 106.3 hectares (262.7 acres) and an extraction area of 96.8 hectares ( 239.2 acres). The quarry is anticipated to have an annual extraction limit of 1.8 million tonnes of aggregate and a maximum annual production of 400,000 tonnes of asphalt from a portable asphalt plant to be located on-site.

The proposed Upper's Quarry access is proposed to be located at the Upper's Lane and Thorold Townline Road intersection. This proposed access is not dependent upon the sale of the Upper's Lane road allowance, as quarry traffic will either enter the site directly from this location on Thorold Townline Road, or travel to the same location via Upper's Lane. The proposed haul route will not make use of Beechwood Road to the east of Upper's Lane.

Two possible routes have been considered as appropriate 'haul routes' for material that will be shipped from the proposed Upper's Quarry to serve local and broader markets.

## Haul Route Option 1

The first option of a haul route for trucks to / from Upper's Quarry would utilize Thorold Townline Road to the north of the site, as it is a regional road and provides the most direct route to / from the quarry. The haul route includes the following roads:

- Thorold Townline Road north of the site access to Thorold Stone Road
- Highway 406 via Thorold Stone Road westbound
- Queen Elizabeth Way (QEW) via Taylor Rd northbound
- Queen Elizabeth Way (QEW) via Thorold Stone Road eastbound


## Haul Route Option 2

Davis Road is designated as a provincial highway and is a major boundary road in close proximity to the site. Accordingly, it can also be considered an appropriate roadway to accommodate truck traffic to / from the quarry. The use of Davis Road as a second option for a haul route would result in a more circuitous haul route, as access to Davis Road would require quarry trucks to first travel south on Thorold Townline Road to Lundy's Lane, and then proceed west to Davis Road. The second haul route option includes the following roadways:

- Thorold Townline Road south of the site access to Lundy's Lane
- Lundy's Lane west to Davis Road
- Davis Road north to Thorold Stone Road
- Highway 406 via Thorold Stone Road westbound
- Queen Elizabeth Way (QEW) via Thorold Stone Road (eastbound) and Taylor Road northbound
- Queen Elizabeth Way (QEW) via Thorold Stone Road eastbound

Based on analysis results for both haul routes and the future transportation network, TMIG recommends that Haul Route Option 1 be chosen as the preferred Haul Route, subject to approval by the Town and an appraisal of the cost of any road improvements potentially required to accommodate truck traffic.
Haul Route Option 1 will also be seen as a preferable route by current and future residents within the vicinity of the proposed Upper's Quarry, as the Rolling Meadows Secondary Plan area represents a large amount of future residential traffic that will travel along Davis Road and Lundy's Lane. As such, it would be ideal to have truck traffic travel north directly on Thorold Townline Road (Haul Route Option 1), compared to the more circuitous route around the boundary of the future Rolling Meadows area (Haul Route Option 2).

The traffic analysis considers traffic conditions at planning horizon years of 2025 and 2035. It is assumed that the proposed Upper's Quarry will be fully operational by the 2025 study horizon year. There are no planned changes to the existing local road network in the immediate vicinity of the proposed Upper's Quarry.

Two background developments were identified that are expected to be built-out by the 2035 planning horizon, and have been included in traffic analysis efforts. Approximately 100 acres of employment lands are owned by Walker on the west side of Thorold Townline Road, opposite Upper's Lane. These employment lands fall within The Neighbourhoods of Rolling Meadows Secondary Plan area.

The Rolling Meadows Development will consist of a mix of residential and employment land uses, is proposed to be built in five phases, and is planned to be fully built-out by 2030. Combined, the Thorold Townline Road Employment Lands and the Rolling Meadows Development are expected to generate a total of 2,254 trips during the a.m. peak hour, and 2,880 trips during the p.m. peak hour. Due to the significant amount of growth represented by the background developments (the equivalent of an annual growth rate of $5.14 \%$ in the a.m. peak hour and $4.51 \%$ in the p.m. peak), no additional background growth has been applied to the study area road network to avoid an over conservative analysis of future traffic conditions.

Based on the proposed annual extraction limit of aggregate and operation hours, hourly truck traffic of up to 47 inbound and 31 outbound trucks during the a.m. peak hour and 31 inbound and 31 outbound trucks during the p.m. peak hour were predicted. It was assumed that 7 aggregate-related employees would travel inbound and outbound during each peak hour.

Based on the proposed annual production limit of asphalt and operation hours, hourly truck traffic of up to 11 inbound and 7 outbound trucks during the a.m. peak hour and 7 inbound and 7 outbound trucks during the p.m. peak hour was predicted. It was assumed that 4 asphalt-related employees would travel inbound and outbound during each peak hour.

Walker Aggregates Inc. supplied TMIG with historical shipping data upon which to base the distribution of truck traffic to the broader transportation network outside of the proposed Upper's Quarry study area.

Overall, the study area intersections operate well or at acceptable levels under all planning horizons. Some individual movements are approaching capacity, particularly under 2035 conditions, but still operate with acceptable delays of 80 seconds or less, indicating a Level of Service (LOS) 'E' or better. Some geometric changes and modifications to signal timing plans are recommended in order to address any capacity or queuing issues in order to allow for efficient movement of traffic through the study area.

Haul Route Option 1 via Thorold Townline to the north was identified as the preferred haul route, and accordingly future total traffic operations were analyzed for Haul Route Option 1 only. A summary of recommendations and timing of the improvements are provided below.

## Background Conditions (2025 \& 2035)

- With adjustments to existing signal timing plans, all study intersections operate at acceptable levels under 2025 and 2035 background conditions. Some individual movements are approaching capacity but operate at acceptable levels of service.
- A signal warrant was conducted for the intersection of Thorold Townline Road and Beaverdams Road under 2025 Background conditions to confirm if the combined existing and 2025 background traffic would justify the installation of a traffic signal. Based on Justification 7 of Book 12 of the Ontario Traffic Manual (OTM), the estimated 2025 background traffic volumes fulfill Justification 1A and 1B at $97 \%$ and $100 \%$ respectively. Although not warranted under 2025 Background conditions, based on the $120 \%$ threshold applied to Justification 7 and the near 100\% justification fulfillment it is TMIG's opinion signals should be considered at this intersection under 2025 Background conditions.
- Construction of an auxiliary southbound right turn lane at the intersection of Thorold Townline Road and Lundy's Lane by the 2035 background planning horizon was found to provide better overall operations at the intersection. Interim adjustments to signal timings and introduction of protected phases could potentially negate the need for a southbound right turn lane, however, high volumes of southbound rightturning vehicles are predicted in 2035 that would benefit from a dedicated lane compared to the existing shared through/right turn lane. Given that the proposed Upper's Quarry is assumed to be active by 2025,
quarry related traffic is not the primary cause of the high volume of right-turning vehicles predicted in 2035, particularly based on preferred Haul Route Option 1 (via Thorold Townline Road), as minimal staff site traffic travels through the intersection, and heavy vehicle site traffic will not travel through the Thorold Townline Road and Lundy's Lane intersection. The operational impact of Haul Route Option 1 site-related traffic at this intersection is negligible and will not trigger the aforementioned road improvements.
- There is opportunity to widen the existing 24 metre ROW at the Thorold Townline Road and Lundy's Lane intersection to the designated 26.2 metre road allowance to accommodate a southbound right turn lane. Furthermore, the Region may require road widening dedications in addition to the designated road allowances without the need for amendments to the Official Plan for purposes such as turning lanes at intersections.
- It is recommended the Thorold Townline Road and Lundy's Lane intersection be monitored in the future to determine whether constructing the dedicated southbound right turn lane would be the most appropriate solution to accommodate background development traffic volumes within the vicinity of the intersection.


## Total Conditions (2025 \& 2035)

- With adjustments to existing signal timing plans, all study intersections operate acceptably under 2025 and 2035 total conditions. Some intersections/movements are approaching, or are at capacity, but operate at acceptable levels of service.
- The proposed access design will be constructed in 2025 prior to the quarry becoming active. The proposed access design provides deceleration and accelerations lanes northbound at the site access (via Upper's Lane). A slip around lane is provided southbound, thus accommodating left-turning vehicles into the site and preventing blockage of through traffic at the site access.
- The southbound queue at Thorold Stone Road and Thorold Townline Road should be monitored in 2035 to determine if any upgrades to the intersection are needed to address the potential for long queues to build up (southbound left experiences a queue up to 160 m according to simulations). The long southbound left queue buildup does not occur under 2025 total conditions when Upper's Quarry is active, as such, quarry related traffic is not the cause of the long queues predicted in 2035.
- In general, it is suggested that the Thorold Townline Road and Beaverdams Road intersection be monitored for signalization in 2025, and that signals be installed prior to the 2035 planning horizon (i.e. prior to the combined full build-out of the Rolling Meadows development, Thorold Townline Road Employment Lands, and the proposed Upper's Lane Quarry).


## Preferred Haul Route

TMIG recommends that Haul Route Option 1 be chosen as the preferred Haul Route, subject to approval by the Town and an appraisal of the cost of any road improvements required to accommodate truck traffic.

Haul Route Option 1 will also be seen as a preferable route by current and future residents within the vicinity of Upper's Quarry, as the Rolling Meadows Secondary Plan area represents a large amount of future residential traffic that will travel along Davis Road and Lundy's Lane. As such, it would be ideal to have truck traffic travel north directly on Thorold Townline Road (Haul Route Option 1), compared to the more circuitous route around the boundary of the future Rolling Meadows area (Haul Route Option 2).

Of note, Haul Route Option 1 will direct trucks northbound on Thorold Townline Road through a non-residential area, however, a causeway has been constructed along Thorold Townline Road to cross a waterway immediately south of Beaverdams Road. Depending on the structural properties of the causeway, improvements may need to be made in order to sustain the regular truck traffic associated with the proposed Upper's Quarry. Before the choice of haul route is finalized, it is recommended that Walker Aggregates Inc. and the Town perform a review of the existing load capacity of Thorold Townline Road in order to determine if any upgrades are required, and if so, what cost would be associated with the upgrades. If it is found that upgrades are required, it should be determined if the upgrades would be needed to service the future Rolling Meadows development regardless of any Upper's Quarry operations. The cost of the roadway upgrades should be assigned proportionately to the parties that will derive direct benefits from the upgrades.

Additionally, the City of Thorold Official Plan (Section B1.8.12.3) Aggregate Resource Protection Policy states the following:
"It shall also be recognized that Thorold Townline Road is a Regional arterial road and is the likely aggregate haul route required to serve any future aggregate extraction operation to the east. Accordingly, all studies required by any policy of this Plan shall recognize that Thorold Townline Road is a future aggregate haul route. The haul route shall be restricted from the future extraction operation entrance southerly to Highway 20, a major arterial."

Based on our interpretation of the policy above the City prefers the proposed Haul Route Option 1.

THE MUNICIPAL INFRASTRUCTURE GROUP LTD.

## A T.Y. LIN INTERNATIONAL COMPANY



Kyla Zijlstra, B.A.Sc., E.I.T.
Technical Lead | kzijlstra@tmig.ca


Michael Dowdall, C.E.T., MITE
Project Manager, Traffic Director \| mdowdall@tmig.ca

## CONTENTS

1 INTRODUCTION ..... 1
1.1 Retainer and Objective .....  1
2 BASELINE TRAFFIC CONDITIONS ..... 3
2.1 Site Environs ..... 3
2.2 Phasing Plan ..... 5
2.3 Existing Road Network ..... 6
2.4 Thorold Townline Road Right-of-Way ..... 6
2.5 Proposed Haul Routes .....  .7
2.6 Study Area Intersections ..... 9
2.7 Baseline Traffic Volumes ..... 11
2.8 Upper's Lane Quarry Access Considerations ..... 11
2.9 Existing Quarry Operations ..... 11
3 FUTURE BACKGROUND CONDITIONS ..... 13
3.1 Study Horizon Years ..... 13
3.2 Study Area Road Network Improvements ..... 13
3.3 Future Background Developments ..... 13
3.3.1 Rolling Meadows Development ..... 13
3.3.2 Thorold Townline Road Employment Lands. ..... 18
3.4 Future Background Growth ..... 21
3.5 Background Traffic Volumes ..... 21
4 SITE GENERATED TRAFFIC ..... 24
4.1 Site Trip Generation ..... 24
4.2 Traffic Distribution and Assignment ..... 26
5 FUTURE TOTAL TRAFFIC ..... 31
6 CAPACITY ANALYSIS ..... 34
6.1 Davis Road at Thorold Stone Road ..... 35
6.2 Davis Road at Niagara Falls Road/Beaverdams Road ..... 37
6.3 Davis Road at Lundy's Lane ..... 39
6.4 Thorold Townline Road at Thorold Stone Road ..... 41
6.5 Thorold Townline Road at Lundy's Lane. ..... 43
6.6 Thorold Townline Road at Beaverdams Road ..... 45
6.7 Thorold Townline Road at Proposed Upper's Quarry Access ..... 47
7 QUEUEING ANALYSIS ..... 48
8 QUARRY ACCESS ..... 52
8.1 Location ..... 52
8.2 Access Design ..... 52
8.3 Site Access Operation ..... 52
8.4 Sightline Assessment ..... 52
9 CONCLUSION ..... 54
9.1 Haul Route Options ..... 54
9.2 Preferred Haul Route ..... 54
9.3 Capacity Analysis Results and Recommendations ..... 55
9.4 Conceptual Site Access Design ..... 56
APPENDICES
APPENDIX A PREMINARY SITE PLAN
APPENDIX B TRAFFIC DATA
APPENDIX C CAPACITY ANALYSIS
APPENDIX D QUEUEING ANALYSIS
APPENDIX E CONCEPTUAL SITE ACCESS DESIGN AND OPERATIONS
APPENDIX F SIGHTLINE ASSESSMENT
FIGURES
Figure 1-1 Upper's Quarry Location Map ..... 2
Figure 2-1 Surrounding Land Uses ..... 4
Figure 2-2 Simplified Operation Schematics ..... 5
Figure 2-3 Proposed Haul Route Options ..... 8
Figure 2-4 Study Area Existing Lane Configurations ..... 10
Figure 2-5 Existing Traffic Volumes ..... 12
Figure 3-1 Rolling Meadows Secondary Plan Land Uses ..... 15
Figure 3-2 2025 Background Traffic Volumes - Rolling Meadows ..... 16
Figure 3-3 2035 Background Traffic Volumes - Rolling Meadows ..... 17
Figure 3-4 2025 Background Traffic Volumes - Thorold Townline Road Employment Lands. ..... 19
Figure 3-5 2035 Background Traffic Volumes - Thorold Townline Road Employment Lands ..... 20
Figure 3-6 2025 Background Total Traffic Volumes ..... 22
Figure 3-7 2035 Background Total Traffic Volumes ..... 23
Figure 4-1 Upper's Quarry Site Traffic Volumes - Haul Route Option 1 Truck Trips ..... 28
Figure 4-2 Upper's Quarry Site Traffic Volumes - Employee Automobile Trips ..... 29
Figure 4-3 Upper's Quarry Site Traffic Volumes - Haul Route Option 1 Total Trips ..... 30
Figure 5-1 2025 Total Traffic Volumes - Haul Route Option 1 ..... 32
Figure 5-2 2035 Total Traffic Volumes - Haul Route Option 1 ..... 33

## TABLES

Table 3-1 Future Thorold Townline Road Employment Lands Site Trip Generation ..... 18
Table 4-1 Monthly Material Shipping Estimates ..... 25
Table 4-2 Directional Distribution of Upper's Quarry Truck Trips ..... 26
Table 6-1 Study Area Peak Hour Factors ..... 34
Table 6-2 Capacity Analysis of Davis Road at Thorold Stone Road. ..... 35
Table 6-3 Capacity Analysis of Davis Road at Niagara Falls Road/Beaverdams Road ..... 37
Table 6-4 Capacity Analysis of Davis Road at Lundy's Lane ..... 39
Table 6-5 Capacity Analysis of Thorold Townline Road and Thorold Stone Road. ..... 41
Table 6-6 Capacity Analysis of Thorold Townline Road at Lundy's Lane ..... 43
Table 6-7 Capacity Analysis of Thorold Townline Road at Beaverdams Road ..... 46
Table 6-8 Capacity Analysis of Thorold Townline Road at Proposed Upper's Quarry Access ..... 47
Table 7-1 Existing (2018) and Future Total Background (2025 \& 2035) Queuing Analysis ..... 48
Table 7-2 Future Total (2025 \& 2035) Haul Route Option 1 Queuing Analysis ..... 50

## 1 INTRODUCTION

The Municipal Infrastructure Group Ltd. (TMIG), a T.Y. Lin International Company, was retained by Walker Aggregates Inc., to prepare a Traffic Impact Study (TIS) for the proposed Upper's Quarry. The proposed Upper's Quarry is located generally on lands situated south of Beaverdams Road, north of Lundy's Lane, west of Beechwood Road, and east of Thorold Townline Road, in the City of Niagara Falls, Region of Niagara, adjacent to City of Thorold.

This TIS has been prepared in support of a Class A Licence (Quarry Below Groundwater) under the Aggregate Resources Act (ARA) application, Regional Official Plan Amendment (ROPA), City Official Plan Amendment (OPA), and City Zoning By-Law Amendment (ZBA). The proposed Upper's Quarry has an approximate licence area of 106.3 hectares ( 262.7 acres) and an extraction area of 96.8 hectares ( 239.2 acres). The site will incorporate setbacks of 15 m along the north and south boundaries. Setbacks of 30 m will be provided along the western boundary, and setbacks of 15 m and 30 m will be provided along the east boundary. A preliminary Existing Features and Cross Sections Plan is provided in Appendix A.

The proposed Upper's Quarry access is proposed to be located at the Upper's Lane and Thorold Townline Road intersection. This proposed access is not dependent upon the sale of the Upper's Lane road allowance, as quarry traffic will either enter the site directly from this location on Thorold Townline Road, or travel to the same location via Upper's Lane. The proposed haul route will not make use of Beechwood Road to the east of Upper's Lane.

The quarry is anticipated to have an annual extraction limit of 1.8 million tonnes of aggregate and a maximum annual production of 400,000 tonnes of asphalt from a portable asphalt plant to be located on-site. As per the proposed Upper's Quarry Operational Plan, the proposed quarry will have the following hours of operation:

- Drilling, extraction: Monday to Saturday 7:00 am-7:00 pm
- Processing: Monday to Saturday 7:00 am - 7:00 pm
- Blasting: Monday to Friday 8:00 am - 6:00 pm
- Shipping: 24 hours (7 days/week)

It is noted that a response to emergencies is not limited by the hours of operation. A preliminary Operational Plan is provided in Appendix A.

### 1.1 Retainer and Objective

The Traffic Impact Study will assess the extent of traffic-related impacts on the abutting roadway system generated by the proposed quarry. The objectives of this study are to:

- Establish baseline traffic conditions for the study area and update the existing traffic conditions,
- Derive the future background operating conditions for the study intersections at a future 2025 and 2035 planning horizon,
- Analyze future operating conditions for the study intersections at a future 2025 and 2035 planning horizon,
- Determine what, if any, traffic impacts there are on the study area haul route from the proposed quarry,
- Recommend road network improvements to address any future traffic impacts within the study area.

The proposed Upper's Quarry location is illustrated in Figure 1-1.


Figure 1-1
Location Map

## LEGEND

|  | Proposed Upper's Quarry Site ( $\pm 106.3$ ha) |  | Existing Walker Brothers Quarry |
| :---: | :---: | :---: | :---: |
|  | Other Lands Owner by Walker Aggregates ( $\pm 31.6$ ha) |  | Property Line |
| (--- | Municipal Boundary |  |  |



## 2 BASELINE TRAFFIC CONDITIONS

This section summarizes the surrounding road network, the data collection program, presents the existing traffic volume conditions on the proximate study area roadways and assesses the current operating conditions at the intersections examined in this study. These 'baseline conditions' form the foundation for future background traffic projections and the incremental site-impact analyses investigated later herein.

### 2.1 Site Environs

The proposed quarry is generally located on the east side of Thorold Townline Road, west of Beechwood Road, south of Beaverdams Road, and north of Lundy's Lane. A solitary quarry access is proposed via the Upper's Lane and Thorold Townline Road intersection.

The site is located on lands designated as "Good General Agriculture Area" by the Region's and City's Official Plans, as are the surrounding lands to the north, south and east of the site, whilst lands to the west are designated as an urban area. The lands immediately west of Thorold Townline Road have been identified in the Rolling Meadows Secondary Plan as a future employment area, and the lands further west are designated as a residential area.

The site and surrounding lands are largely undeveloped with a few residential farms which will be demolished. An existing church is situated immediately east of the proposed quarry and has direct access to Beechwood Road. The existing Fernwood subdivision is located southeast of the proposed quarry, to the east of Beechwood Road.

The existing watercourse which currently runs through the site is to be realigned and enhanced as part of the future quarry operations. Upon completion, the realigned watercourse will be referred to as Upper's Creek and run along the east side of Thorold Townline Road. The proposed quarry and adjacent land uses are illustrated in Figure 2-1.


Figure 2-1

## Surrounding Land <br> Use

## LEGEND

Data Source: First Base Solutions Aerial Flown 2017

| $\square$ | Proposed Upper's Quarry Site |
| :--- | :--- |
| Adjacent Lands Owned By |  |
| Walker Aggregates |  |


| Rolling Meadows Secondary Plan Area |  | TransCanada Pipeline |
| :--- | :--- | :--- |
| Existing (Residential) Dwelling within |  | Fernwood Subdivision |
| 500 m Radius (Outside Urban Area) |  |  |$\quad-\quad$ CN Railway

## Upper's Quarry, <br> City of Niagara Falls, <br> Region of Niagara, Ontario

City of Thorold Urban Area
DATE: April 8, $2020 \quad$ Urban Area
SCALE 1:15000

### 2.2 Phasing Plan

The phasing plan for the proposed quarry has been designed to identify the sequence of operation throughout the life of the quarry and maximize progressive rehabilitation of the site. Overall, the proposed quarry includes three (3) phases which have been illustrated in Figure 2-2.

Figure 2-2 Simplified Operation Schematics


### 2.3 Existing Road Network

Based on road network connectivity and proposed access to the quarry, the abutting Thorold Townline Road will be an integral part of the quarry's haul route. Boundary roadways that make up the haul route(s) to the quarry include:

- Thorold Townline Road/Taylor Road (Regional Road 70) is a two-lane regional road generally oriented in a north-south direction, with a posted speed limit of $80 \mathrm{~km} / \mathrm{h}$ in the study area and is under the jurisdiction of Niagara Region. Thorold Townline Road provides a connection to Thorold Stone Road Road to north and Lundy's Lane to the south.
- Thorold Stone Road (Regional Road 57 / Highway 58) is generally oriented in an east-west direction and has a four-lane cross section with a posted speed limit of $80 \mathrm{~km} / \mathrm{h}$ in the study area. It is under the jurisdiction of Niagara Region east of Davis Road. Thorold Stone Road provides a connection to Highway 406 to the west via the Thorold Tunnel, and a connection to the Queen Elizabeth Way (QEW) to the east. Within the study area, Thorold Stone Road is under the jurisdiction of the Ministry of Transportation (MTO) west of Davis Road, and is known as Highway 58.
- Davis Road (Highway 58) is a north-south highway under the jurisdiction of the MTO, and has a posted speed limit of $80 \mathrm{~km} / \mathrm{h}$. Davis Road provides a connection between Lundy's Lane to the south and Thorold Stone Road to the north. Davis Road has a 2-lane cross-section between Lundy's Lane and a point approximately 300 metres south of Beaverdams Road where it transitions to a 4-lane cross-section northward to Thorold Stone Road.
- Lundy's Lane (Regional Road 20 / Highway 20) is generally oriented in an east-west direction within the study area and has a two-lane cross section with a posted speed limit of $80 \mathrm{~km} / \mathrm{h}$. Lundy's Lane is under the jurisdiction of Niagara Region, with the exception of the portion between Davis Road and Thorold Townline Road, which is under the jurisdiction of the MTO. Lundy's Lane provides a connection to Highway 406 in the west, and Highway 420 and the QEW in the east.


### 2.4 Thorold Townline Road Right-of-Way

Thorold Townline Road currently provides a right-of-way (ROW) width of 20 metres, within proximity of the proposed site access, between Thorold Stone Road and a distance approximately 320 metres north of Lundy's Lane at which point the ROW width increases to approximately 24 metres.

Niagara Region OP Chapter 9 - Transportation (adopted as Amendment 13 to the OP) has policies set in place to ensure the Region will:

- Ensure that corridors are identified and protected to meet current and projected needs for various modes of travel including active transportation.
- Support opportunities for multi-modal use where feasible, in particular prioritizing transit and goods movement needs over those of single occupant automobiles.
- For goods movement corridors, provide for linkages to planned or existing intermodal opportunities where feasible.

Moreover, the Region's OP (Policy 9.C.7) states:
'The widths for Regional Road allowances are designated in the Table titled "Road Allowance Widths". Each Regional Road allowance which is not presently at its designated width is a highway to be widened.'

Region OP Table 9-1 (Road Allowance Widths) identifies a designated 26.2 metre road Thorold Townline Road allowance width between Thorold Stone Road and Chippawa Creek Road, inclusive of the proposed site access (via Upper's Lane) and its intersection with Lundy's Lane. Road widening requirements will be confirmed with the Region as part of the application review process, and, as necessary, the Site Plans will be modified to reflect those requirements at that time.

Region OP Policy 9.C. 12 states:
'Land for Regional Road widening normally will be required equally from both sides of the centreline of the designated Regional Road unless existing land uses, topographic features or other physical or environmental constraints necessitate taking greater widening on one side than the other'

Additionally, Region OP Policy 9.C. 13 states:
'The Region may require road widening dedications in addition to the designated road allowances indicated in the Table titled "Road Allowance Widths" without the need for amendments to this Plan for purposes such as turning lanes at intersections or to provide suitable access to major traffic generator developments.'

Therefore, as discussed in Section 6.5, there is opportunity to widen the existing 24 metre ROW at the Thorold Townline Road and Lundy's Lane intersection to the designated 26.2 metre road allowance and/or provide a road widening dedications in addition to the designated road allowance to accommodate a southbound right turn lane.

### 2.5 Proposed Haul Routes

Two possible routes have been considered as appropriate 'haul routes' for material that will be shipped from the proposed Upper's Quarry to serve local and broader markets. Haul Route Option 1 and Option 2 are illustrated in Figure 2-3.

## Haul Route Option 1

The first option of a haul route for trucks to / from the proposed Upper's Quarry would utilize Thorold Townline Road to the north of the site, as it is a regional road and provides the most direct route to / from the quarry. The haul route includes the following roads:

- Thorold Townline Road north of the site access to Thorold Stone Road
- Highway 406 via Thorold Stone Road westbound
- Queen Elizabeth Way (QEW) via Taylor Rd northbound
- Queen Elizabeth Way (QEW) via Thorold Stone Road eastbound


## Haul Route Option 2

Davis Road is designated as a provincial highway and is a major boundary road in close proximity to the site. Accordingly, it can also be considered an appropriate roadway to accommodate truck traffic to / from the quarry. The use of Davis Road as a second option for a haul route would result in a more circuitous haul route, as access to Davis Road would require quarry trucks to first travel south on Thorold Townline Road to Lundy's Lane, and then proceed west to Davis Road. The second haul route option includes the following roadways:

- Thorold Townline Road south of the site access to Lundy's Lane
- Lundy's Lane west to Davis Road
- Davis Road north to Thorold Stone Road
- Highway 406 via Thorold Stone Road westbound
- Queen Elizabeth Way (QEW) via Thorold Stone Road (eastbound) and Taylor Road northbound
- Queen Elizabeth Way (QEW) via Thorold Stone Road eastbound


TMIG recommends that Haul Route Option 1 be chosen as the preferred Haul Route, subject to approval by the Town and an appraisal of the cost of any road improvements potentially required to accommodate truck traffic.

Haul Route Option 1 will also be seen as a preferable route by current and future residents within the vicinity of the proposed Upper's Quarry, as the Rolling Meadows Secondary Plan area represents a large amount of future residential traffic that will travel along Davis Road and Lundy's Lane. As such, it would be ideal to have truck traffic travel north directly on Thorold Townline Road (Haul Route Option 1), compared to the more circuitous route around the boundary of the future Rolling Meadows area (Haul Route Option 2).

Additionally, the City of Thorold Official Plan (Section B1.8.12.3) Aggregate Resource Protection Policy states the following:
> "It shall also be recognized that Thorold Townline Road is a Regional arterial road and is the likely aggregate haul route required to serve any future aggregate extraction operation to the east. Accordingly, all studies required by any policy of this Plan shall recognize that Thorold Townline Road is a future aggregate haul route. The haul route shall be restricted from the future extraction operation entrance southerly to Highway 20, a major arterial."

Based on our interpretation of the policy above, the City prefers the proposed Haul Route Option 1.
Of note, Haul Route Option 1 will direct trucks northbound on Thorold Townline Road through a non-residential area, however, a causeway has been constructed along Thorold Townline Road to cross a waterway immediately south of Beaverdams Road. Depending on the structural properties of the causeway, improvements may need to be made in order to sustain the regular truck traffic associated with the proposed Upper's Quarry. Before the choice of haul route is finalized, it is recommended that Walker Aggregates Inc. and the Town perform a review of the existing load capacity of Thorold Townline Road in order to determine if any upgrades are required, and if so, what cost would be associated with the upgrades. If it is found that upgrades are required, it should be determined if the upgrades would be needed to service the future Rolling Meadows development regardless of any Upper's Quarry operations. The cost of the roadway upgrades should be assigned proportionately to the parties that will derive direct benefits from the upgrades.

As Haul Route Option 1 via Thorold Townline to the north has been identified as the preferred haul route, future total traffic operations were analyzed for Haul Route Option 1 only.

### 2.6 Study Area Intersections

The following study area intersections were analyzed:

- Thorold Townline Road at Thorold Stone Road
- Thorold Townline Road at Beaverdams Road
- Thorold Townline Road at Upper's Lane (proposed Upper's Quarry access via Upper's Lane)
- Thorold Townline Road at Lundy's Lane
- Davis Road at Thorold Stone Road
- Davis Road at Beaverdams Road
- Davis Road at Lundy's Lane

The existing lane configurations at each study area intersection and the extent of the study area can be seen in Figure 2-4.

Stop Control
Signal Control
Rolling Meadows Secondary Plan Area
Provincial Road
Regional Road Local Road

### 2.7 Baseline Traffic Volumes

Turning movement counts were commissioned by TMIG for study intersections identified in Section 2.6. Weekday a.m. and p.m. peak period counts were collected twice for each study location over two days. Count data was collected on June 14 and June 19, 2018. Traffic volumes from the two surveys were then averaged to establish baseline volumes for existing conditions. Count data collected at study intersections over the two day period is provided in Appendix B.

Baseline existing weekday a.m. and p.m. peak hour volumes are shown in Figure 2-5.

### 2.8 Upper's Lane Quarry Access Considerations

Upper's Lane is a rural public road that operates in a general east-west direction and provides access between Thorold Townline Road and Beechwood Road. Upper's Lane bisects the land owned by Walker Aggregates Inc. that will form the proposed Upper's Quarry.

Although the road is open to the public, negligible existing traffic utilizes the road, as evidenced by the volumes recorded at the intersection of Thorold Townline and Upper's Lane. The a.m. peak hour records a total of 1 inbound and 1 outbound vehicle, and the p.m. peak hour records a total of 2 inbound and 1 outbound vehicles (refer to Figure 2-5). It is noted that these traffic counts were taken when Bible Baptist Church was still being accessed from Upper's Lane. The access to Bible Baptist Church was re-located and only has access points to Beechwood Road, resulting in minimal traffic expected to access the church property via Upper's Lane given the surrounding land uses and alternative routes to the church from populated areas.

Figure 2-5 identifies the intersection of Upper's Lane and Thorold Townline Road as the location of the "Proposed Upper's Quarry Access", as although Upper's Lane is a public road and is not considered to be the Quarry's physical entrance, this intersection represents the primary point at which the proposed quarry traffic will enter and exit the broader study area road network and interact with non-quarry traffic sources. In other words, regardless as to where the access to the proposed quarry is physically located along Upper's Lane, all property (and access points) along the Upper's Lane corridor is now owned by the applicant and minimal public traffic is expected to interact with proposed quarry traffic along Upper's Lane.

### 2.9 Existing Quarry Operations

Traffic generated by Walker Brothers Quarry (WBQ) located at 2800 Thorold Townline Road, north of Thorold Stone Road, was captured by the weekday a.m. and p.m. peak period turning movement counts collected at the study area intersections.
It is expected the WBQ will be depleted in +/-10 years. Ideally Walker Aggregates would prefer to have +/-5 years to transition between the WBQ and Uppers Quarry so production at Uppers Quarry can begin lower than maximum permitted (when operations are at the surface) and scale up when operations are deeper into the quarry.
As result, the forecasted total truck volumes on the road network contained herein provides a more conservative analysis and is expected to have less of an impact on the operations of the study intersections than reported.

## 3 FUTURE BACKGROUND CONDITIONS

### 3.1 Study Horizon Years

The analysis considers future background traffic conditions at planning horizon years of 2025 and 2035. For analysis purposes, it is assumed that the proposed Upper's Quarry will be fully operational by the 2025 study horizon year.

### 3.2 Study Area Road Network Improvements

There are no planned changes to the existing local road network in the immediate vicinity of the proposed Upper's Quarry.

Niagara Region's 2017 Transportation Master Plan (TMP) identified capacity improvements to Highway 20 (Lundy's Lane) on the capital works list, however, these improvements to Highway 20 have not yet been placed in the capital budget. The type of capacity improvements were not detailed in the TMP, as the improvements are not planned until sometime between the years of 2032 and 2041. The improvements will occur between Kottmeier Rd (west of the Welland Canal) and Davis Road. Given that the improvements fall outside of the immediate study area and could potentially be completed beyond the 2035 study horizon year, no capacity improvements to Highway 20 were assumed as a conservative measure.

### 3.3 Future Background Developments

### 3.3.1 Rolling Meadows Development

The Neighbourhoods of Rolling Meadows Secondary Plan was first approved in 2000, was updated in 2007 to conform to the Provincial Growth Plan, and was later integrated into the City of Thorold's OP in 2015. The Rolling Meadows Secondary Plan Area is generally bounded by Thorold Townline Road to the east, Davis Road to the west, Lundy's Lane to the south, and a hydro corridor to the north (south of Beaverdams Road). Schedule A-3 of the City's OP outlines the planned Land Uses of the Rolling Meadows Secondary Plan area, and is provided in Figure 3-1.

According to the Rolling Meadows Development Traffic Impact Study dated October 31 ${ }^{\text {st }}$, 2018, the Rolling Meadows development covers approximately 160 hectares of land within the City of Thorold and is,
"... a proposed multi-phase development consisting of primarily residential land uses, including singlefamily homes, townhouses, medium density units and high density units. A total of approximately 2,099 residential units are currently proposed. Commercial/Retail areas totaling a gross floor area (GFA) of approximately $240,800 \mathrm{ft}^{2}$ are proposed with the majority situated along the Highway 20 frontage with some located centrally within the neighbourhood. Two institutional blocks are also proposed; assumed to be Elementary Schools accommodating up to 300 students each."

Given the wide range of uses within the proposed Rolling Meadows development, TMIG did not generate the background traffic of the development from first principles in favour of adopting the site traffic volumes detailed in the 2018 Rolling Meadows traffic study to remain consistent with traffic modeling efforts that have already been undertaken.

The site traffic assignment developed for the Rolling Meadows traffic report was generally maintained, however, the intersections of Davis Road and Thorold Townline at Thorold Stone Road were not included within the Rolling Meadows study area. A significant percentage of Rolling Meadows site traffic, 49\%, was assigned to/from the north via Davis Road, however, the distribution of the site traffic at the intersection of Davis Road and Thorold Stone Road is unknown. Due to the high delays observed under future background traffic conditions at the Davis Road and Thorold Townline at Thorold Stone Road intersection, TMIG reassigned some of this northbound traffic ( $14 \%$ of total traffic) to an alternate routing via Lundy's Lane to the
west, assuming that a large portion of the 49\% of Rolling Meadows traffic that travels north on Davis Road is ultimately bound for Highway 406, which is also accessible via Lundy's Lane.

The Rolling Meadows development is proposed to be constructed in five phases. Phases 1 through 5 are proposed to be completed in 2019, 2021, 2023, 2028, and 2030, respectively. Accordingly, site traffic generated by Phases 1 through 3 was included as background traffic for the 2025 planning horizon, and the total site traffic generated by Phases 1 through 5 was included as background traffic for the 2035 planning horizon.

Figures 3-2 and 3-3 provide the weekday a.m. and p.m. peak hour site traffic volumes produced by the Rolling Meadows development by 2025 and 2035, respectively.

Figure 3-1 Rolling Meadows Secondary Plan Land Uses


## LEGEND

|  | Upper's Quarry Boundary |
| :--- | :--- |
| XX | AM Peak Hour Volumes |
| (XX) | PM Peak Hour Volumes |

- Stop Control
Signal Control

Rolling Meadows Secondary Plan Area

Provincial Road Regional Road Local Road

|  | Upper's Quarry Boundary |
| :--- | :--- |
| XX | AM Peak Hour Volumes |
| (XX) | PM Peak Hour Volumes |
| $\ddots \quad$ | Stop Control <br> Rolling Meadows Secondary <br> Plan Area |
|  | Provincial Road <br> Regional Road <br> Local Road |

### 3.3.2 Thorold Townline Road Employment Lands

Approximately 100 acres of future employment lands are located west of Thorold Townline Road (within the Rolling Meadows Secondary Plan area) to the north and south of Upper's Lane. Walker Aggregates Inc. currently owns the majority of these employment lands in addition to the proposed Upper's Quarry.
The City of Thorold's OP (2015) has designated the Thorold Townline Road Employment Lands as a mix of Light Industrial and "Prestige Industrial" land uses. Descriptions of the types of permitted uses allowed on these lands are located in Section B1.8.8 of the Official Plan.

At the time of this report, a specific development timeline for the Thorold Townline Road Employment Lands was not available. For analysis purposes, it was assumed that half of the employment lands would be constructed by the 2025 study horizon year, and that full build-out would occur before the 2035 study horizon year.
Site traffic generated by the future employment lands during the weekday a.m. and p.m. peak hours was estimated by applying the fitted curve equations for Land Use Code (LUC) 130 Industrial Park and LUC 150 Warehousing in Trip Generation, $10^{\text {th }}$ Edition, published by the Institute of Transportation Engineers (ITE). No reductions for transit or active transportation were applied to the base trips generated by the ITE fitted curve equations. Table 3-1 summarizes the estimated trips generated by the future employment lands.

Table 3-1 Future Thorold Townline Road Employment Lands Site Trip Generation

| Parameters | Peak Hour Trip Generation |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Weekday AM |  |  | Weekday PM |  |  |
|  | In | Out | Total | In | Out | Total |
|  | ITE LUC 130 - Industrial Park (50 acres) |  |  |  |  |  |
| ITE Equation | $\operatorname{Ln}(\mathrm{T})=0.78 \operatorname{Ln}(\mathrm{X})+2.82$ |  |  | $\ln (\mathrm{T})=0.72 \operatorname{Ln}(\mathrm{X})+3.06$ |  |  |
| Gross Trip Rate | 5.90 | 1.20 | 7.10 | 1.50 | 5.64 | 7.14 |
| Trip Ratio | 83\% | 17\% | - | 21\% | 79\% | - |
| Gross Trips | 295 | 60 | 355 | 75 | 282 | 357 |
|  | ITE LUC 150 - Warehousing ( 50 acres) |  |  |  |  |  |
| ITE Equation | $\mathrm{T}=7.55(\mathrm{X})+49.85$ |  |  | $\mathrm{T}=6.74(\mathrm{X})+49.08$ |  |  |
| Gross Trip Rate | 6.14 | 2.40 | 8.54 | 2.70 | 5.02 | 7.72 |
| Trip Ratio | 72\% | 28\% | - | 35\% | 65\% | - |
| Gross Trips | 307 | 120 | 427 | 135 | 251 | 386 |
| Total (2035) | 602 | 180 | 782 | 210 | 533 | 743 |

The estimated 2025 and 2035 weekday a.m. and p.m. peak hour trips generated by the Thorold Townline Road Employment Lands were assigned to the study road network as shown in Figure 3-4 and Figure 3-5.

## LEGEND

|  | Upper's Quarry Boundary |
| :--- | :--- |
| XX | AM Peak Hour Volumes |
| $(X X)$ | PM Peak Hour Volumes |

$\begin{array}{ll}- & \text { Stop Control } \\ \text { Signal Control }\end{array}$
Rolling Meadows Secondary Plan Area

Provincial Road
Regional Road
Local Road


### 3.4 Future Background Growth

A significant amount of growth is expected to occur within the study area due largely to the implementation of the Rolling Meadows Secondary Plan. By 2035, the Rolling Meadows residential and employment uses (including the Thorold Townline Road Employment Lands) are projected to generate a combined total of 2,254 trips during the weekday a.m. peak hour, and 2,880 trips during the weekday p.m. peak hour. This represents a substantial amount of growth that will occur across the study area road network.

For example, under existing conditions the northbound through movement at the intersection of Davis Road and Beaverdams Road is recorded to have a volume of 267 and 275 vehicles during the existing weekday a.m. and p.m. peak hour, respectively. By 2035, volumes of 626 and 582 vehicles during the weekday a.m. and p.m. peak hours are predicted under future background traffic conditions. This represents an increase of 359 and 307 vehicles from existing traffic conditions. This increase in traffic is equivalent to an annual growth rate of $5.14 \%$ in the weekday a.m. peak hour and $4.51 \%$ in the weekday p.m. peak hour, calculated based on growth over 17 years (from 2018 to 2035). Similar increases in traffic can be seen throughout the study area road network.

As the Rolling Meadows residential and employment uses (including the Thorold Townline Road Employment Lands) are the only projected developments within the area, and create a substantial growth on the road network (approximately $5 \%$ annual growth rate) it was deemed that no further growth on the road network should be applied. As the Rolling Meadows Secondary Plan area provides a large volume of residential and employment traffic, applying additional annual growth on the major roads would over-estimate the future traffic analysis. To ensure an accurate estimation of the future traffic volumes, the annual growth rate applied on the roadways only included the growth due to the substantial, confirmed background traffic.

### 3.5 Background Traffic Volumes

The 2018 baseline traffic and the background development site traffic were combined to produce the 2025 and 2035 background total weekday a.m. and p.m. peak hour traffic volumes.

The background total (2025 and 2035) traffic volumes are presented in Figures 3-6 and 3-7.

|  | Upper's Quarry Boundary |
| :--- | :--- |
| XX | AM Peak Hour Volumes |
| (XX) | PM Peak Hour Volumes |
| $\cdots$ | Stop Control |
| $\cdots$ | Signal Control <br> Rolling Meadows Secondary <br> Plan Area |
|  | Provincial Road <br> Regional Road <br> Local Road |


|  | Upper's Quarry Boundary |
| :--- | :--- |
| XX | AM Peak Hour Volumes |
| $(X X)$ | PM Peak Hour Volumes |
| $\ddots \quad$ | Stop Control <br> Rolling Meadows Secondary <br> Plan Area |
|  | Srovincial Road <br> Regional Road <br> Local Road |

## 4 SITE GENERATED TRAFFIC

For analysis purposes, it is assumed that the proposed Upper's Quarry will be fully operational by the 2025 study horizon year (i.e. ship maximum annual amount of material allowed to be extracted). However, this is understood to be a conservative assumption, and operations will begin lower than the maximum annual limit when quarry operations start at the surface. Over time, once operations are deeper into the quarry, annual extraction levels will increase and approach the maximum annual extraction limit. Accordingly, truck traffic from the quarry will increase over time to eventually meet the maximum operations outlined in this report. In this sense, the 2025 analysis results in particular can be considered conservative in terms of the assumed volume of trucks assigned to the study area road network.

### 4.1 Site Trip Generation

In order to generate the estimated truck traffic associated with the proposed Upper's Quarry, the following assumptions and base data have been adopted:

- Aggregate Maximum Annual Shipping Limit (License application) $=1,800,000$ tonnes
- Asphalt Maximum Annual Shipping Limit (License application) $=400,000$ tonnes
- Quarry operations proposed as follows:
- Shipping hours of 7:00 am to 7:00 pm (12.0 hours) from Monday to Saturday
- Total of 72 shipping hours a week or an average of 312 hours a month
- Average truck capacity of 35 tonnes

The quarry is proposed to operate year-round from January to December with variable amounts of material extraction and shipping depending on the month. Based on historical shipping data records archived by TMIG, peak shipping generally occurs during the 'construction season' between the months of May and October. Table 4-1 summarizes the average monthly breakdown of material extraction based on archived historical data from existing quarry operations in the area. The estimated percentage of total annual material shipped per month was applied to the 1,800,000-tonne annual shipping limit.

Table 4-1 Monthly Material Shipping Estimates

| Month | Material Volume <br> Per Month <br> (Percent of Total) |
| :---: | :---: |
| January | $3 \%$ |
| February | $4 \%$ |
| March | $5 \%$ |
| April | $7 \%$ |
| May | $12 \%$ |
| June | $13 \%$ |
| July | $11 \%$ |
| August | $10 \%$ |
| September | $10 \%$ |
| October | $7 \%$ |
| November | $6 \%$ |
| December | $100 \%$ |
| Total |  |

To account for the occasional periods of higher-volume trucking that is likely to occur during high-construction activity (typically between May and October), the trip generation used in the analysis of quarry-generated traffic impacts is based on the peak level of shipping / trucking activity during these busy summertime periods. Based on Table 4-1, June represents the peak month during the peak construction season, with approximately $13 \%$ of the total annual material shipped during that month. As a conservative measure, an additional $5 \%$ was added onto the peak month percentage to account for potential fluctuations in monthly material shipped due to variations in market demand from year to year. Approximately $18 \%$ was applied to the annual Upper's Quarry extraction limit, resulting in 330,000 tonnes of the annual aggregate material estimated to be extracted during the peak summer month. This equates to 1,058 tonnes of material per hour based on an average of 312 shipping hours per month. With a capacity of approximately 35 tonnes per truck, 1,058 tonnes of material extraction generate approximately 31 outbound loaded aggregate truck trips per hour (plus the same number of returning trucks).

31 aggregate trucks trips per hour is considered to be a highly conservative estimate of the number of trucks that will be able to leave the quarry each hour, given there is only one weighing scale planned to service all outbound loaded trucks. The quarry is capable of shipping outside of the peak demand period (7:00 a.m. to 7:00 p.m.), which will likely be required during the peak construction season to fulfill all aggregate orders.

During the peak month of demand, approximately 73,333 tonnes of the annual asphalt limit is estimated to be produced by the on-site portable asphalt plant. This equates to 235 tonnes of asphalt per hour based on an average of 312 shipping hours per month. With a capacity of approximately 35 tonnes per truck, 235 tonnes of asphalt generate approximately 7 outbound loaded truck trips per hour (plus the same number of returning trucks).

It has been TMIG's experience that additional peaking occurs during early morning shipping activity, to provide material to construction sites in the morning. As a result, additional outbound loaded trucks could occasionally occur, creating a short-lived 'peak within a peak' condition (generally occurring prior to the adjacent street peak).

To account for this peaking, the a.m. peak hour outbound truck volume was increased by an additional 50\%, equating to 47 aggregate and 11 asphalt loaded truck trips per hour. We have adopted this peak trip
generation as the design-hour vehicle volume for our site-impact analysis that follows. As alluded to above, these 'peak within a peak' activities are predicted to occur largely outside of the adjacent street peak hours, so in this respect we are predicting an unlikely (and conservative) scenario of the quarry and adjacent street peaks coinciding.

Aggregate recycling will be part of the tonnage limit under the new Aggregate Resources Act. These loads are already accounted for in the analysis. Extracted aggregate and recycled aggregate will be limited to 1,800,000 tonnes per year.

With adoption of the various peaking factors described above and employed in the regular aggregate shipping activity estimates, we have portrayed a conservative (high) trucking activity level of site-related traffic flows, and therefore impacts on the abutting street system.

It is assumed that approximately 7 aggregate-related and 4 asphalt-related employees will be working at the quarry per shift. Therefore, as a conservative measure, a total of 11 inbound and outbound employee trips were generated during both the a.m. and p.m. peak hours (assuming a shift change occurs within the peak hour of the surrounding road network).

### 4.2 Traffic Distribution and Assignment

Walker Aggregates Inc. supplied TMIG with two years of historical shipping data from an existing quarry in Niagara Region which is similar in size to the proposed Upper's Quarry. The historical shipping data was used to base the distribution of truck traffic to the broader transportation network outside of the Upper's Quarry study area. The total tonnage shipped each year was separated into the geographical location of the customers, averaged, and the percent of the total aggregate shipped to each location was determined. A summary of the directional distribution of truck traffic for the proposed Upper's Quarry is provided in Table 4-2.

Of note, approximately $5 \%$ of all truck trips are expected to make use of either Highway 406 or the Queen Elizabeth Way (QEW) to travel south to make local deliveries. A load limit on Lundy's Lane was identified at the Allanburg Bridge that crosses the Welland Canal, and as such, no southbound truck traffic was assigned via Lundy's Lane/R.R. 20 to the west of the subject site.

Table 4-2 Directional Distribution of Upper's Quarry Truck Trips

| Direction To / From | \% Distribution |
| :---: | :---: |
| North <br> via Taylor Road and QEW | $30 \%$ |
| East <br> via Thorold Stone Road and QEW | $30 \%$ |
| West <br> via Thorold Stone Road and Hwy 406 | $40 \%$ |
| Total | $\mathbf{1 0 0 \%}$ |

As discussed in Section 2.5, two possible haul routes were identified, however, only the preferred haul route was used for analysis purposes. The preferred haul route (Haul Route Option 1 via Thorold Townline Road) is the most direct and would primarily make use of Thorold Townline Road to access the broader transportation network. The preferred haul route option is described in greater detail below (the inbound trucks will follow the reverse of the outbound route described).

## Haul Route Option 1

Outbound aggregate and asphalt trucks were assigned to the road network as follows:

- Right turn out of quarry access to travel north on Thorold Townline Road to Thorold Stone Road
- Trucks traveling west to Highway 406 turn left onto Thorold Stone Road
- Trucks traveling north to the QEW via Taylor Road continue northbound at Thorold Stone Road
- Trucks traveling east to the QEW turn right onto Thorold Stone Road

All of the above-mentioned roadways are either regional or provincial roads, and as such, have been assumed to be designed to road standards acceptable and appropriate for use as aggregate haul routes.

The trip distribution summarized in Table 4-2 has been applied to the calculated estimates of the peak hourly truck trips as described in Section 4.1, and the resultant truck traffic volume assignments are shown in Figure 4-1 for Haul Route Option 1.

Given the lack of current employment uses in direct vicinity of the subject site, it was determined that Transportation Tomorrow Survey (TTS) Data would not provide a correct representation of traffic patterns for employment trip assignment purposes. The distribution of quarry employee traffic was based on logical routing between the quarry and surrounding major towns and cities that are likely to house quarry employees. The estimated employee site trips in each of the study peak hours are shown in Figure 4-2.

The estimated truck and employee site trips were combined to produce the total site-related trips presented in Figure 4-3.

## LEGEND

|  | Upper's Quarry Boundary |
| :--- | :--- |
| XX | AM Peak Hour Volumes |
| (XX) | PM Peak Hour Volumes |

$\begin{array}{ll}- & \text { Stop Control } \\ \text { Signal Control }\end{array}$
$\square$ Rolling Meadows Secondary Plan Area

Provincial Road
Regional Road
Local Road

## LEGEND

|  | Upper's Quarry Boundary |
| :--- | :--- |
| XX | AM Peak Hour Volumes |
| (XX) | PM Peak Hour Volumes |

$\begin{array}{ll}- & \text { Stop Control } \\ \text { Signal Control }\end{array}$
Rolling Meadows Secondary Plan Area

Provincial Road Regional Road Local Road

## LEGEND

|  | Upper's Quarry Boundary |
| :--- | :--- |
| XX | AM Peak Hour Volumes |
| (XX) | PM Peak Hour Volumes |

$\begin{array}{ll}- & \text { Stop Control } \\ \text { Signal Control }\end{array}$
$\square$ Rolling Meadows Secondary Plan Area

Provincial Road
Regional Road
Local Road

## 5

FUTURE TOTAL TRAFFIC

The future total traffic conditions for the peak study hours in the 2025 and 2035 planning horizons were derived by combining the projected future background traffic with the corresponding estimate of the total site generated traffic (quarry trucks and employees).

Figure 5-1 summarizes the future total traffic volumes for Haul Route Option 1 for the 2025 planning horizon during the weekday a.m. and p.m. peak hours. Figure 5-2 summarizes the future total traffic volumes for Haul Route Option 1 for the 2035 planning horizon during the weekday a.m. and p.m. peak hours.

## LEGEND

|  | Upper's Quarry Boundary |
| :--- | :--- |
| XX | AM Peak Hour Volumes |
| (XX) | PM Peak Hour Volumes |
| $\cdots$ | Stop Control |
| $\cdots$ | Signal Control <br> Rolling Meadows Secondary <br> Plan Area |
|  | Provincial Road <br> Regional Road <br> Local Road |


|  | Upper's Quarry Boundary |
| :--- | :--- |
| XX | AM Peak Hour Volumes |
| (XX) | PM Peak Hour Volumes |
| $\cdots$ | Stop Control |
| $\cdots$ | Signal Control <br> Rolling Meadows Secondary <br> Plan Area |
|  | Provincial Road <br> Regional Road <br> Local Road |

## 6 CAPACITY ANALYSIS

The capacity analysis identifies how well the intersections and driveways are operating under existing conditions and how they are expected to operate in the future. The analysis contained within this report utilized the Highway Capacity Manual (HCM) 2000 techniques within the Synchro Version 10 Software package. The reported intersection volume-to-capacity ratios (v/c) are a measure of the volume versus the capacity of each turning movement, while the levels-of-service (LOS) are a measure of the average delay for each turning movement. Queuing characteristics are reported as the predicted 95th percentile queue for each turning movement.

## Synchro Calibration Volume and Lane Settings:

The ideal saturated flow (flow rate) used in the analysis follows the Synchro 10 recommended default of 1,900 vphpl.

The peak hour factor (PHF) of the flow rate has been calculated to provide the most accurate representation of the peak 15 -minutes for the study times. The specific calculated peak hour factors used are provided in Table 6-1.

Table 6-1 Study Area Peak Hour Factors

| Intersection Name | AM PHF | PM PHF |
| :---: | :---: | :---: |
| Davis Road \& Thorold Stone Road | 0.96 | 0.95 |
| Davis Rd \& Niagara Falls Road /Beaverdams Road | 0.95 | 0.95 |
| Davis Road \& Lundy's Lane | 0.94 | 0.93 |
| Thorold Townline Road /Taylor Road \& Thorold Stone Road | 0.96 | 0.96 |
| Thorold Townline Road \& Lundy's Lane | 0.93 | 0.91 |
| Thorold Townline Road \& Beaverdams Road | 0.92 | 0.93 |
| Thorold Townline Road \& Upper's Lane | 0.93 | 0.91 |

For the purpose of the future site impact analyses, the heavy vehicle percentages calculated from the existing turning movement counts and applied to the Synchro analysis were updated for the 2025 and 2035 future total scenarios. The heavy vehicle percentages were increased for movements throughout the study area network to which proposed Upper's Quarry aggregate and asphalt traffic will be added to, as per the preferred haul route. The increased percentages were calculated by estimating the volume of heavy vehicles performing a given movement under 2025 or 2035 future background conditions (existing heavy vehicle percentage assumed), adding the estimated volume of heavy vehicle site traffic, and finally dividing the 2025 or 2035 future total heavy vehicle volumes by the total mixed-traffic volume for each movement.

The analysis includes identification of all intersections and for all movements; v/c ratios, LOS indicators and 95th percentile queue lengths. Critical intersections and movements shall be highlighted (in bold). 'Critical' intersections and movements include:

- through, shared through, or right-turn movements with a v/c ratio greater than 0.85 at signalized intersections
- exclusive turning movements with a v/c ratio greater than 0.90 at signalized intersections
- queue length of an individual movement is projected to exceed available turning lane storage at $95^{\text {th }}$ percentile volumes at signalized intersections
- movements at unsignalized intersections that are expected to operate at LOS 'D' or worse, and/or the estimated $95^{\text {th }}$ percentile queue length exceeds the available storage space

The following tables summarize the Synchro/HCM capacity results for the study intersections during the weekday a.m. and p.m. peak hours under existing, future background, and future total traffic conditions (for both haul route options). Detailed Synchro intersection capacity sheets are provided in Appendix C.

### 6.1 Davis Road at Thorold Stone Road

Signalized capacity analyses during the weekday a.m. and p.m. peak hours are summarized in Table 6-2 for the intersection of Davis Road at Thorold Stone Road.

Table 6-2 Capacity Analysis of Davis Road at Thorold Stone Road

| Condition | Movement | AM Peak Hour |  |  | PM Peak Hour |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | v/c | $\begin{gathered} \text { Delay } \\ (\mathrm{s}) \end{gathered}$ | LOS | v/c | $\begin{gathered} \text { Delay } \\ (\mathbf{s}) \end{gathered}$ | LOS |
| Existing | Overall | 0.59 | 22 | C | 0.62 | 23 | C |
|  | EBL | 0.13 | 13 | B | 0.19 | 16 | B |
|  | EBT | 0.49 | 16 | B | 0.67 | 20 | C |
|  | EBR | 0.20 | 13 | B | 0.40 | 16 | B |
|  | WBL | 0.31 | 17 | B | 0.66 | 42 | D |
|  | WBTR | 0.60 | 18 | B | 0.62 | 19 | B |
|  | NBL | 0.66 | 45 | D | 0.66 | 45 | D |
|  | NBLT | 0.66 | 45 | D | 0.65 | 45 | D |
|  | NBR | 0.11 | 34 | C | 0.06 | 35 | C |
|  | SBL | 0.02 | 50 | D | 0.04 | 48 | D |
|  | SBT | 0.03 | 50 | D | 0.06 | 48 | D |
|  | SBR | 0.01 | 50 | D | 0.02 | 48 | D |
| Future Background (2025) | Overall | 0.66 | 35 | D | 0.72 | 33 | C |
|  | EBL | 0.13 | 21 | C | 0.18 | 23 | C |
|  | EBT | 0.64 | 28 | C | 0.76 | 32 | C |
|  | EBR | 0.29 | 22 | C | 0.62 | 30 | C |
|  | WBL | 0.36 | 32 | C | 0.69 | 31 | C |
|  | WBTR | 0.60 | 34 | C | 0.59 | 19 | B |
|  | NBL | 0.80 | 56 | E | 0.77 | 64 | E |
|  | NBLT | 0.81 | 58 | E | 0.79 | 65 | E |
|  | NBR | 0.15 | 37 | D | 0.09 | 45 | D |
|  | SBL | 0.02 | 56 | E | 0.05 | 65 | E |
|  | SBT | 0.04 | 57 | E | 0.08 | 65 | E |
|  | SBR | 0.01 | 56 | E | 0.02 | 64 | E |


| Condition | Movement | AM Peak Hour |  |  | PM Peak Hour |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | v/c | Delay (s) | LOS | v/c | Delay <br> (s) | LOS |
| Future Total (2025) <br> Haul Route Option 1 (Thorold Townline Road) | Overall | 0.66 | 29 | C | 0.77 | 34 | C |
|  | EBL | 0.14 | 15 | B | 0.20 | 23 | C |
|  | EBT | 0.54 | 19 | B | 0.82 | 33 | C |
|  | EBR | 0.24 | 15 | B | 0.62 | 28 | C |
|  | WBL | 0.47 | 28 | C | 0.77 | 51 | D |
|  | WBTR | 0.63 | 25 | C | 0.63 | 24 | C |
|  | NBL | 0.78 | 55 | D | 0.80 | 60 | E |
|  | NBLT | 0.80 | 56 | E | 0.82 | 62 | E |
|  | NBR | 0.15 | 37 | D | 0.09 | 40 | D |
|  | SBL | 0.02 | 56 | E | 0.04 | 55 | D |
|  | SBT | 0.04 | 57 | E | 0.07 | 55 | D |
|  | SBR | 0.01 | 56 | E | 0.02 | 54 | D |
| Future Background (2035) | Overall | 0.74 | 41 | D | 0.86 | 46 | D |
|  | EBL | 0.15 | 24 | C | 0.23 | 28 | C |
|  | EBT | 0.72 | 32 | C | 0.91 | 44 | D |
|  | EBR | 0.38 | 26 | C | 0.84 | 44 | D |
|  | WBL | 0.52 | 43 | D | 0.88 | 67 | E |
|  | WBTR | 0.64 | 41 | D | 0.66 | 29 | C |
|  | NBL | 0.88 | 64 | E | 0.92 | 76 | E |
|  | NBLT | 0.89 | 65 | E | 0.94 | 78 | E |
|  | NBR | 0.18 | 36 | D | 0.13 | 39 | D |
|  | SBL | 0.02 | 56 | E | 0.04 | 55 | D |
|  | SBT | 0.04 | 57 | E | 0.07 | 55 | D |
|  | SBR | 0.01 | 56 | E | 0.02 | 54 | D |
| Future Total (2035) <br> Haul Route Option 1 (Thorold Townline Road) | Overall | 0.75 | 33 | C | 0.87 | 46 | D |
|  | EBL | 0.16 | 17 | B | 0.24 | 29 | C |
|  | EBT | 0.59 | 21 | C | 0.94 | 47 | D |
|  | EBR | 0.31 | 17 | B | 0.84 | 45 | D |
|  | WBL | 0.73 | 47 | D | 0.88 | 65 | E |
|  | WBTR | 0.67 | 29 | C | 0.68 | 30 | C |
|  | NBL | 0.87 | 61 | E | 0.92 | 76 | E |
|  | NBLT | 0.87 | 63 | E | 0.94 | 78 | E |
|  | NBR | 0.18 | 35 | D | 0.13 | 39 | D |
|  | SBL | 0.02 | 56 | E | 0.04 | 55 | D |
|  | SBT | 0.04 | 57 | E | 0.07 | 55 | D |
|  | SBR | 0.01 | 56 | E | 0.02 | 54 | D |

Under existing conditions, the intersection operates well during the a.m. and p.m. peak hours with overall LOS ' C ' and $\mathrm{v} / \mathrm{c}$ ratios of 0.59 and 0.62 during the a.m. and p.m. peak hours, respectively, indicating reserve capacity. Individual movements operate with $\mathrm{v} / \mathrm{c}$ ratios of 0.67 or less and LOS 'D' or better.

Under 2025 background conditions, the intersection is expected to continue operating at acceptable levels with overall $\mathrm{v} / \mathrm{c}$ ratios of 0.66 and 0.72 with LOS ' $D$ ' and ' $C$ ' during the a.m. and p.m. peak hours, respectively. However, some individual movements are predicted to experience longer delays (LOS 'E'), during the a.m. and p.m. peak hours compared to existing conditions. Individual movements are predicted to operate with v/c ratios of 0.80 or less, indicating reserve capacity remains.

Based on 2025 future total traffic conditions for Haul Route Option 1, the intersection is expected to continue operating at acceptable levels with an overall LOS ' $C$ ' and $\mathrm{v} / \mathrm{c}$ ratios of 0.66 and 0.77 during the a.m. and p.m. peak hours, respectively. Individual movements are predicted to experience LOS ' $E$ ' or better and $v / \mathrm{c}$ ratios of 0.82 or less.

The intersection is expected to operate at acceptable levels under 2035 background conditions with overall LOS ' $D$ ' and $v / c$ ratios of 0.74 and 0.86 during the $a . m$. and p.m. peak hours, respectively. During the p.m. peak hour, the northbound left and shared left/through movements are approaching capacity (v/c of 0.92 and 0.94 ), however, both movements still operate with acceptable delays and LOS ' $E$ '. The eastbound through movement is also approaching capacity during the p.m. peak hour, predicted to operate with a v/c ratio of 0.91 , however, it is expected to operate with acceptable delay and LOS ' $D$ '.

Under 2035 future total traffic conditions for Haul Route Option 1, the intersection is expected to operate at acceptable levels with overall LOS ' $C$ ' and ' $D$ ' and $v / \mathrm{c}$ ratios of 0.75 and 0.87 during the a.m. and p.m. peak hours, respectively. During the p.m. peak hour, the northbound left and shared left/through movements are approaching capacity ( $\mathrm{v} / \mathrm{c}$ of 0.92 and 0.94 ), however, both movements still operate with acceptable delays and LOS ' $E$ '. The eastbound through movement continues to approach capacity during the p.m. peak hour, predicted to operate with a v/c ratio of 0.94 , however, it is expected to continue operating with acceptable delay and LOS 'D'.

Overall, this intersection is expected to have acceptable future operations despite some movements approaching capacity in 2035, and there are no required geometric improvements to the intersection.

### 6.2 Davis Road at Niagara Falls Road/Beaverdams Road

Signalized capacity analyses during the weekday a.m. and p.m. peak hours are summarized in Table 6-3 for the intersection of Davis Road at Niagara Falls Road/Beaverdams Road.

Table 6-3 Capacity Analysis of Davis Road at Niagara Falls Road/Beaverdams Road

| Condition | Movement | AM Peak Hour |  |  | PM Peak Hour |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | v/c | $\begin{gathered} \text { Delay } \\ \text { (s) } \end{gathered}$ | LOS | v/c | $\begin{gathered} \text { Delay } \\ \text { (s) } \end{gathered}$ | LOS |
| Existing | Overall | 0.28 | 22 | C | 0.35 | 23 | C |
|  | EBLTR | 0.24 | 11 | B | 0.20 | 12 | B |
|  | WBLTR | 0.16 | 10 | A | 0.23 | 12 | B |
|  | NBL | 0.02 | 26 | C | 0.02 | 24 | C |
|  | NBTR | 0.37 | 29 | C | 0.32 | 26 | C |
|  | SBL | 0.31 | 30 | C | 0.58 | 33 | C |
|  | SBT | 0.23 | 28 | C | 0.26 | 26 | C |
|  | SBR | 0.03 | 26 | C | 0.07 | 24 | C |
| Future Background (2025) | Overall | 0.37 | 26 | C | 0.47 | 25 | C |
|  | EBLTR | 0.24 | 11 | B | 0.23 | 14 | B |
|  | WBLTR | 0.17 | 11 | B | 0.32 | 15 | B |
|  | NBL | 0.07 | 27 | C | 0.05 | 23 | C |
|  | NBTR | 0.64 | 34 | C | 0.44 | 27 | C |
|  | SBL | 0.51 | 36 | D | 0.72 | 41 | D |
|  | SBT | 0.31 | 29 | C | 0.46 | 28 | C |
|  | SBR | 0.03 | 27 | C | 0.07 | 24 | C |


| Condition | Movement | AM Peak Hour |  |  | PM Peak Hour |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | v/c | Delay (s) | LOS | v/c | $\begin{gathered} \text { Delay } \\ (\mathrm{s}) \end{gathered}$ | LOS |
| Future Total (2025) <br> Haul Route Option 1 (Thorold Townline Road) | Overall | 0.37 | 26 | C | 0.47 | 25 | C |
|  | EBLTR | 0.24 | 11 | B | 0.23 | 14 | B |
|  | WBLTR | 0.17 | 11 | B | 0.32 | 15 | B |
|  | NBL | 0.07 | 27 | C | 0.05 | 23 | C |
|  | NBTR | 0.64 | 34 | C | 0.44 | 27 | C |
|  | SBL | 0.51 | 36 | D | 0.72 | 41 | D |
|  | SBT | 0.31 | 29 | C | 0.46 | 28 | C |
|  | SBR | 0.03 | 27 | C | 0.07 | 24 | C |
| Future Background (2035) | Overall | 0.43 | 26 | C | 0.53 | 25 | C |
|  | EBLTR | 0.27 | 14 | B | 0.27 | 17 | B |
|  | WBLTR | 0.17 | 13 | B | 0.32 | 18 | B |
|  | NBL | 0.10 | 24 | C | 0.13 | 21 | C |
|  | NBTR | 0.70 | 32 | C | 0.51 | 25 | C |
|  | SBL | 0.56 | 35 | D | 0.79 | 46 | D |
|  | SBT | 0.36 | 27 | C | 0.57 | 26 | C |
|  | SBR | 0.03 | 23 | C | 0.07 | 20 | B |
| Future Total (2035) <br> Haul Route Option 1 (Thorold Townline Road) | Overall | 0.43 | 27 | C | 0.53 | 25 | C |
|  | EBLTR | 0.27 | 14 | B | 0.27 | 17 | B |
|  | WBLTR | 0.19 | 13 | B | 0.32 | 18 | B |
|  | NBL | 0.11 | 25 | C | 0.13 | 21 | C |
|  | NBTR | 0.71 | 33 | C | 0.51 | 25 | C |
|  | SBL | 0.57 | 36 | D | 0.79 | 46 | D |
|  | SBT | 0.36 | 27 | C | 0.57 | 26 | C |
|  | SBR | 0.03 | 24 | C | 0.07 | 20 | B |

Under existing conditions, the intersection operates very well during the a.m. and p.m. peak hours with overall LOS ' $C$ ' and $\mathrm{v} / \mathrm{c}$ ratios of 0.28 and 0.35 during the a.m. and p.m. peak hours, respectively, indicating significant reserve capacity.

Under 2025 background conditions, the intersection is expected to continue operating at acceptable levels, maintaining an overall LOS ' C ' during peak hours with predicted overall $\mathrm{v} / \mathrm{c}$ ratios of 0.37 and 0.47 during the a.m. and p.m. peak hours, respectively. Individual movements are predicted to operate with $\mathrm{v} / \mathrm{c}$ ratios of 0.72 or less and experience LOS 'D' or better during both peak hours.

Based on 2025 future total traffic conditions for Haul Route Option 1, the intersection is expected to continue operating at acceptable levels with an overall LOS ' $C$ ' and $\mathrm{v} / \mathrm{c}$ ratios of 0.37 and 0.47 during the a.m. and p.m. peak hours, respectively. Individual movements are predicted to continue experiencing LOS 'D' or better and operate with $\mathrm{v} / \mathrm{c}$ ratios of 0.72 or less.

The intersection is expected to operate at acceptable levels under 2035 background conditions with overall LOS ' C ' and $\mathrm{v} / \mathrm{c}$ ratios of 0.43 and 0.53 during the a.m. and p.m. peak hours, respectively, indicating reserve capacity remains. Individual movements are predicted to experience LOS 'D' or better and v/c ratios of 0.79 or less.

Under 2035 future total traffic conditions for Haul Route Option 1, the intersection is expected to operate at acceptable levels with overall LOS ' C ' and $\mathrm{v} / \mathrm{c}$ ratios of 0.43 and 0.53 during the a.m. and p.m. peak hours, respectively. Similar to 2035 background conditions, reserve capacity remains, and individual movements are predicted to experience LOS ' $D$ ' or better and operate with $\mathrm{v} / \mathrm{c}$ ratios of 0.79 or less.

Overall, this intersection is expected to have acceptable future operations and there are no required geometric improvements to the intersection.

### 6.3 Davis Road at Lundy's Lane

Signalized capacity analyses during the weekday a.m. and p.m. peak hours are summarized in Table 6-4 for the intersection of Davis Road at Lundy's Lane.

Table 6-4 Capacity Analysis of Davis Road at Lundy's Lane

| Condition | Movement | AM Peak Hour |  |  | PM Peak Hour |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | v/c | Delay (s) | LOS | v/c | Delay (s) | LOS |
| Existing | Overall | 0.43 | 15 | B | 0.46 | 20 | C |
|  | EBL | 0.19 | 6 | A | 0.36 | 19 | B |
|  | EBTR | 0.39 | 8 | A | 0.61 | 21 | C |
|  | WBL | 0.07 | 5 | A | 0.10 | 14 | B |
|  | WBT | 0.28 | 7 | A | 0.55 | 20 | B |
|  | WBR | 0.03 | 5 | A | 0.04 | 13 | B |
|  | NBL | 0.12 | 33 | C | 0.11 | 20 | B |
|  | NBTR | 0.60 | 38 | D | 0.27 | 22 | C |
|  | SBL | 0.36 | 35 | C | 0.19 | 21 | C |
|  | SBT | 0.35 | 34 | C | 0.20 | 21 | C |
|  | SBR | 0.06 | 32 | C | 0.08 | 19 | B |
| Future Background (2025) | Overall | 0.59 | 18 | B | 0.78 | 36 | D |
|  | EBL | 0.30 | 10 | B | 0.77 | 37 | D |
|  | EBTR | 0.52 | 12 | B | 0.72 | 29 | C |
|  | WBL | 0.11 | 9 | A | 0.15 | 28 | C |
|  | WBT | 0.40 | 11 | B | 0.82 | 44 | D |
|  | WBR | 0.17 | 9 | A | 0.20 | 45 | D |
|  | NBL | 0.09 | 26 | C | 0.18 | 40 | D |
|  | NBTR | 0.44 | 29 | C | 0.51 | 46 | D |
|  | SBL | 0.76 | 42 | D | 0.70 | 32 | C |
|  | SBT | 0.27 | 28 | C | 0.20 | 25 | C |
|  | SBR | 0.11 | 26 | C | 0.11 | 24 | C |
| Future Total (2025) <br> Haul Route Option 1 (Thorold Townline Road) | Overall | 0.59 | 18 | B | 0.79 | 36 | D |
|  | EBL | 0.30 | 10 | B | 0.69 | 28 | C |
|  | EBTR | 0.52 | 12 | B | 0.68 | 26 | C |
|  | WBL | 0.11 | 8 | A | 0.14 | 26 | C |
|  | WBT | 0.40 | 11 | B | 0.78 | 41 | D |
|  | WBR | 0.17 | 8 | A | 0.19 | 52 | D |
|  | NBL | 0.09 | 27 | C | 0.19 | 41 | D |
|  | NBTR | 0.45 | 29 | C | 0.53 | 48 | D |
|  | SBL | 0.78 | 45 | D | 0.77 | 39 | D |
|  | SBT | 0.27 | 28 | C | 0.21 | 27 | C |
|  | SBR | 0.11 | 27 | C | 0.11 | 26 | C |
| Future Background (2035) | Overall | 0.62 | 17 | B | 0.94 | 39 | D |
|  | EBL | 0.36 | 10 | A | 0.89 | 58 | E |
|  | EBTR | 0.59 | 12 | B | 0.74 | 23 | C |


|  | WBL | 0.16 | 8 | A | 0.23 | 22 | C |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | WBT | 0.48 | 10 | A | 0.87 | 42 | D |
|  | WBR | 0.10 | 7 | A | 0.19 | 34 | C |
|  | NBL | 0.11 | 29 | C | 0.19 | 41 | D |
|  | NBTR | 0.54 | 33 | C | 0.57 | 49 | D |
|  | SBL | 0.71 | 43 | D | 0.91 | 71 | E |
|  | SBT | 0.32 | 31 | C | 0.26 | 34 | C |
|  | SBR | 0.12 | 29 | C | 0.13 | 32 | C |
|  | Overall | 0.62 | 17 | B | 0.95 | 39 | D |
|  | EBL | 0.36 | 10 | A | 0.90 | 59 | E |
|  | EBTR | 0.59 | 12 | B | 0.75 | 23 | C |
|  | WBL | 0.16 | 8 | A | 0.23 | 22 | C |
| Future Total (2035) | WBT | 0.48 | 10 | A | 0.88 | 43 | D |
|  | WBR | 0.10 | 7 | A | 0.19 | 33 | C |
| Haul Route Option 1 | NBL | 0.11 | 29 | C | 0.19 | 41 | D |
|  | NBTR | 0.55 | 33 | C | 0.57 | 49 | D |
|  | SBL | 0.72 | 43 | D | 0.91 | 71 | E |
|  | SBT | 0.32 | 31 | C | 0.26 | 34 | C |
|  | SBR | 0.12 | 29 | C | 0.13 | 32 | C |

Under existing conditions, the intersection operates well during the a.m. and p.m. peak hours with overall LOS ' B ' and ' C ' and $\mathrm{v} / \mathrm{c}$ ratios of 0.43 and 0.46 during the a.m. and p.m. peak hours, respectively, indicating significant reserve capacity. Individual movements operate with a $\mathrm{v} / \mathrm{c}$ of 0.61 or less and LOS ' D ' or better.

Under 2025 background conditions, the intersection is expected to continue operating at acceptable levels with overall LOS ' $B$ ' and ' $D$ ' and $\mathrm{v} / \mathrm{c}$ ratios of 0.59 and 0.78 during the a.m. and p.m. peak hours, respectively. Individual movements are predicted to experience LOS ' D ' or better and $\mathrm{v} / \mathrm{c}$ ratios of 0.82 .

Based on 2025 future total traffic conditions for Haul Route Option 1, the intersection is expected to continue operating at acceptable levels with overall LOS ' B ' and ' D ' and $\mathrm{v} / \mathrm{c}$ ratios of 0.59 and 0.79 during the a.m. and p.m. peak hours, respectively. Individual movements are predicted to experience LOS ' $D$ ' or better and $\mathrm{v} / \mathrm{c}$ ratios of 0.78 or less.

The intersection is expected to operate at acceptable levels under 2035 background conditions with overall LOS ' $B$ ' and ' $D$ ' and $\mathrm{v} / \mathrm{c}$ ratios of 0.62 and 0.94 during the a.m. and p.m. peak hours, respectively. During the p.m. peak hour, the southbound left movement is approaching capacity (v/c of 0.91), however, the movement operates with acceptable delay and LOS ' $E$ '. All other movements at the intersection experience LOS ' $E$ ' or better and $\mathrm{v} / \mathrm{c}$ ratios of 0.89 or less during both peak hours.

Under 2035 future total traffic conditions for Haul Route Option 1, the intersection is expected to operate at acceptable levels with overall LOS 'B' and 'D' and $\mathrm{v} / \mathrm{c}$ ratios of 0.62 and 0.95 during the a.m. and p.m. peak hours, respectively. During the p.m. peak hour, the eastbound left and southbound left movements are approaching capacity ( $\mathrm{v} / \mathrm{c}$ ratios of 0.90 and 0.91 , respectively), however, the movements operate with acceptable delays and LOS ' $E$ ' or better. All other movements at the intersection experience LOS ' $E$ ' or better and $\mathrm{v} / \mathrm{c}$ ratios of 0.88 or less during both peak hours.

Overall, this intersection is expected to have acceptable future operations despite some movements approaching capacity in 2035, and there are no required geometric improvements to the intersection.

### 6.4 Thorold Townline Road at Thorold Stone Road

Signalized capacity analyses during the weekday a.m. and p.m. peak hours are summarized in Table 6-5 for the intersection of Thorold Townline Road at Thorold Stone Road.

Table 6-5 Capacity Analysis of Thorold Townline Road and Thorold Stone Road

| Condition | Movement | AM Peak Hour |  |  | PM Peak Hour |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | v/c | Delay <br> (s) | LOS | v/c | Delay (s) | LOS |
| Existing | Overall | 0.78 | 24 | C | 0.73 | 26 | C |
|  | EBL | 0.69 | 12 | B | 0.59 | 13 | B |
|  | EBT | 0.28 | 6 | A | 0.47 | 11 | B |
|  | EBR | $\begin{gathered} 0.03 \\ (0.04) \\ \hline \end{gathered}$ | $\begin{gathered} 5 \\ \text { (3) } \\ \hline \end{gathered}$ | $\begin{gathered} \text { A } \\ \text { (A) } \\ \hline \end{gathered}$ | $\begin{gathered} 0.02 \\ (0.03) \\ \hline \end{gathered}$ | $\begin{aligned} & \hline 8 \\ & (4) \\ & \hline \end{aligned}$ | $\begin{gathered} \text { A } \\ \text { (A) } \end{gathered}$ |
|  | WBL | 0.06 | 12 | B | 0.13 | 16 | B |
|  | WBT | 0.43 | 16 | B | 0.48 | 19 | B |
|  | WBR | 0.05 | 12 | B | 0.02 | 14 | B |
|  | NBL | 1.03 | 168 | F | 1.04 | 164 | F |
|  | NBTR | 0.47 | 43 | D | 0.24 | 34 | C |
|  | SBL | 0.29 | 41 | D | 0.17 | 34 | C |
|  | SBTR | 0.79 | 59 | E | 0.88 | 59 | E |
| Future Background (2025) | Overall | 0.83 | 40 | D | 0.79 | 35 | C |
|  | EBL | 0.80 | 52 | D | 0.74 | 28 | C |
|  | EBT | 0.42 | 34 | C | 0.67 | 29 | C |
|  | EBR | $\begin{gathered} 0.08 \\ (0.14) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 68 \\ (22) \\ \hline \end{gathered}$ | $\begin{gathered} \mathrm{E} \\ \text { (C) } \end{gathered}$ | $\begin{gathered} 0.04 \\ (0.07) \\ \hline \end{gathered}$ | $\begin{aligned} & \hline 19 \\ & \text { (2) } \end{aligned}$ | $\begin{gathered} \hline B \\ (A) \\ \hline \end{gathered}$ |
|  | WBL | 0.34 | 20 | B | 0.34 | 23 | C |
|  | WBT | 0.65 | 34 | C | 0.65 | 34 | C |
|  | WBR | 0.05 | 24 | C | 0.02 | 24 | C |
|  | NBL | 0.50 | 33 | C | 0.59 | 32 | C |
|  | NBTR | 0.35 | 31 | C | 0.46 | 34 | C |
|  | SBL | 0.20 | 36 | D | 0.15 | 30 | C |
|  | SBTR | 0.88 | 65 | E | 0.89 | 62 | E |
| Future Total (2025) <br> Haul Route Option 1 (Thorold Townline Road) | Overall | 0.87 | 45 | D | 0.82 | 47 | D |
|  | EBL | 0.88 | 68 | E | 0.76 | 53 | D |
|  | EBT | 0.48 | 39 | D | 0.69 | 50 | D |
|  | EBR | $\begin{gathered} 0.11 \\ (0.21) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 68 \\ (24) \end{gathered}$ | $\begin{gathered} \hline \mathrm{E} \\ (C) \\ \hline \end{gathered}$ | $\begin{gathered} 0.06 \\ (0.12) \\ \hline \end{gathered}$ | $\begin{aligned} & \hline 122 \\ & (25) \end{aligned}$ | $\begin{gathered} \hline F \\ (C) \\ \hline \end{gathered}$ |
|  | WBL | 0.42 | 23 | C | 0.48 | 26 | C |
|  | WBT | 0.74 | 40 | D | 0.68 | 36 | D |
|  | WBR | 0.05 | 28 | C | 0.02 | 25 | C |
|  | NBL | 0.56 | 31 | C | 0.73 | 41 | D |
|  | NBTR | 0.42 | 29 | C | 0.54 | 34 | C |
|  | SBL | 0.20 | 35 | D | 0.15 | 28 | C |
|  | SBTR | 0.88 | 64 | E | 0.91 | 63 | E |
| Future Background (2035) | Overall | 0.93 | 50 | D | 0.91 | 57 | E |
|  | EBL | 0.93 | 79 | E | 0.87 | 66 | E |
|  | EBT | 0.60 | 43 | D | 0.79 | 59 | E |
|  | EBR | $\begin{gathered} 0.16 \\ (0.27) \\ \hline \end{gathered}$ | $\begin{gathered} 76 \\ (24) \\ \hline \end{gathered}$ | $\begin{gathered} \hline \mathrm{E} \\ \text { (C) } \end{gathered}$ | $\begin{gathered} 0.05 \\ (0.11) \\ \hline \end{gathered}$ | $\begin{aligned} & 245 \\ & (20) \\ & \hline \end{aligned}$ | $\begin{gathered} \hline \mathrm{F} \\ (B) \\ \hline \end{gathered}$ |


|  | WBL | 0.74 | 33 | C | 0.63 | 34 | C |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | WBT | 0.82 | 45 | D | 0.83 | 43 | D |
|  | WBR | 0.05 | 29 | C | 0.02 | 26 | C |
|  | NBL | 0.58 | 31 | C | 0.88 | 60 | E |
|  | NBTR | 0.40 | 28 | C | 0.72 | 39 | D |
|  | SBL | 0.18 | 32 | C | 0.20 | 29 | C |
|  | SBTR | 0.94 | 70 | E | 0.93 | 67 | E |
| Future Total (2035) <br> Haul Route Option 1 (Thorold Townline Road) | Overall | 0.95 | 52 | D | 0.93 | 61 | E |
|  | EBL | 0.94 | 79 | E | 0.90 | 76 | E |
|  | EBT | 0.65 | 47 | D | 0.89 | 68 | E |
|  | EBR | $\begin{gathered} 0.21 \\ (0.34) \end{gathered}$ | $\begin{gathered} 74 \\ (26) \end{gathered}$ | $\begin{aligned} & \mathrm{E} \\ & \text { (C) } \end{aligned}$ | $\begin{gathered} 0.07 \\ (0.17) \end{gathered}$ | $\begin{aligned} & 157 \\ & \text { (25) } \end{aligned}$ | $\begin{gathered} \hline \mathrm{F} \\ \text { (C) } \end{gathered}$ |
|  | WBL | 0.80 | 39 | D | 0.79 | 55 | D |
|  | WBT | 0.86 | 49 | D | 0.92 | 55 | D |
|  | WBR | 0.05 | 31 | C | 0.02 | 29 | C |
|  | NBL | 0.78 | 48 | D | 0.83 | 46 | D |
|  | NBTR | 0.50 | 28 | C | 0.71 | 35 | D |
|  | SBL | 0.18 | 31 | C | 0.18 | 27 | C |
|  | SBTR | 0.94 | 69 | E | 0.94 | 68 | E |

Note: Italicized rows indicate values where the Highway Capacity Manual (HCM) 2000 result differed significantly from the Intersection Capacity Utilization (ICU) results, which have been provided in brackets. Based on the capacity and demand at these locations, the level of delay is not reasonable according to HCM.

Under existing conditions, the intersection operates at acceptable levels during the a.m. and p.m. peak hours with overall LOS ' $C$ ' and $\mathrm{v} / \mathrm{c}$ ratios of 0.78 and 0.73 during the a.m. and p.m. peak hours, respectively. The northbound left movement is currently operating at capacity with LOS ' $F$ ' and $v / c$ ratios of 1.03 and 1.04 during the a.m. and p.m. peak hours, respectively. Capacity issues at this intersection are addressed in future background and total conditions through adjustments to the existing signal timing plan.

Under 2025 background conditions, the intersection is expected to continue operating at acceptable levels with overall LOS 'D' and 'C' and v/c ratios of 0.87 and 0.82 during the a.m. and p.m. peak hours, respectively. Individual movements are predicted to experience LOS ' $E$ ' or better.

Based on 2025 future total traffic conditions for Haul Route Option 1, the intersection is expected to continue operating at acceptable levels with overall LOS 'D' and v/c ratios of 0.87 and 0.82 during the a.m. and p.m. peak hours, respectively. The southbound shared through/right movement is approaching capacity with v/c ratios of 0.88 and 0.91 during the a.m. and p.m. peak hours, respectively, however, the movement is still experiencing acceptable delays. The eastbound right movement is expected to operate with relatively high delay during both peak hours, however, given the relatively low turning volumes and the queueing results, it was determined that the HCM delay calculation for the movement was not reasonable and that lower delays would be experienced (closer to those predicted in the ICU results for the intersection).

The intersection is expected to operate at acceptable levels under 2035 background conditions with overall LOS 'D' and ' $E$ ' and $\mathrm{v} / \mathrm{c}$ ratios of 0.93 and 0.91 during the a.m. and p.m. peak hours, respectively. The southbound shared through/right movement continues to approach capacity with v/c ratios of 0.94 and 0.93 during the a.m. and p.m. peak hours, respectively, and experiences acceptable delays of 70 seconds or less. The eastbound left movement is approaching capacity with a v/c ratio of 0.93 during the a.m. peak hour and continues to experience acceptable delay (LOS 'E'). As mentioned previously, while the eastbound right movement is predicted to experience high delays, this is likely due to an error in Synchro's HCM 2000 capacity analysis methodology. Based on ICU results, the movement is expected to operate with acceptable levels of delay.

Under 2035 future total traffic conditions for Haul Route Option 1, the intersection is predicted to approach capacity with overall LOS 'D' and 'E' and v/c ratios of 0.95 and 0.93 during the a.m. and p.m. peak hours, respectively. The southbound shared through/right movement continues to approach capacity with v/c ratios
of 0.94 during both the a.m. and p.m. peak hours. Overall, all movements at the intersection experience acceptable levels of delay (LOS 'E' or better) despite several movements approaching capacity. Based on ICU results, the eastbound right movement is expected to operate with acceptable levels of delay compared to the HCM results.

Overall, this intersection is expected to have acceptable future operations despite some movements approaching capacity in 2025 and 2035. There are no required geometric improvements to the intersection, however, the intersection could benefit from monitoring to determine if constructing a dedicated southbound right turn lane will improve overall operations of the intersection and address any potential queueing problems for the southbound left turn lane identified in Section 7 of this report.

### 6.5 Thorold Townline Road at Lundy's Lane

In order to address significant delays and capacity issues experienced by the northbound left movement under 2035 future total conditions, a variety of signal timing plans were tested to determine if all intersection movements could operate under capacity with acceptable delays. It was found that the addition of a dedicated southbound right turn lane aided in improving not only southbound operations, but the northbound left operations as well.

This is due in part to the high volume of southbound right vehicles being blocked by southbound through movements in the existing shared lane that are stopped by a red light. By constructing a southbound right turn lane, more southbound right turning vehicles are able to move through the intersection on a red light, providing more gaps for northbound left turning traffic during the green phase.

The southbound right turn lane was applied to all 2025 and 2035 analysis scenarios to provide consistent signal timing plans and the associated benefits of the dedicated lane on the overall traffic operations at the intersection. It is suggested that the intersection be monitored in the future to determine whether constructing the dedicated right turn lane in 2025 or making adjustments to the signal timings in the interim condition, including the addition of protected phases, would be the most economical solution.

As discussed in Section 2.4, there is opportunity to widen the existing 24 metre ROW at the Thorold Townline Road and Lundy's Lane intersection to the designated 26.2 metre road allowance to accommodate a southbound right turn lane. Furthermore, the Region may require road widening dedications in addition to the designated road allowances without the need for amendments to the Official Plan for purposes such as turning lanes at intersections.

Signalized capacity analyses during the weekday a.m. and p.m. peak hours are summarized in Table 6-6 for the intersection of Thorold Townline Road at Lundy's Lane.

Table 6-6 Capacity Analysis of Thorold Townline Road at Lundy's Lane

| Condition | Movement | AM Peak Hour |  |  | PM Peak Hour |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | v/c | Delay (s) | LOS | v/c | Delay (s) | LOS |
| Existing | Overall | 0.39 | 17 | B | 0.43 | 18 | B |
|  | EBL | 0.10 | 6 | A | 0.07 | 5 | A |
|  | EBT | 0.33 | 7 | A | 0.37 | 7 | A |
|  | EBR | 0.07 | 5 | A | 0.08 | 5 | A |
|  | WBL | 0.06 | 5 | A | 0.08 | 5 | A |
|  | WBTR | 0.27 | 7 | A | 0.36 | 7 | A |
|  | NBL | 0.34 | 39 | D | 0.65 | 51 | D |
|  | NBTR | 0.62 | 44 | D | 0.59 | 44 | D |
|  | SBL | 0.09 | 36 | D | 0.18 | 37 | D |
|  | SBTR | 0.38 | 39 | D | 0.52 | 42 | D |
| Future Background | Overall | 0.48 | 16 | B | 0.52 | 21 | C |


| Condition | Movement | AM Peak Hour |  |  | PM Peak Hour |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | v/c | Delay (s) | LOS | v/c | Delay (s) | LOS |
| (2025) | EBL | 0.29 | 7 | A | 0.20 | 7 | A |
|  | EBT | 0.45 | 8 | A | 0.44 | 10 | A |
|  | EBR | 0.09 | 5 | A | 0.09 | 6 | A |
|  | WBL | 0.08 | 5 | A | 0.09 | 5 | A |
|  | WBTR | 0.34 | 7 | A | 0.49 | 9 | A |
|  | NBL | 0.35 | 38 | D | 0.67 | 58 | E |
|  | NBTR | 0.62 | 43 | D | 0.63 | 52 | D |
|  | SBL | 0.15 | 35 | D | 0.43 | 49 | D |
|  | SBT | 0.31 | 37 | D | 0.43 | 47 | D |
|  | SBR | 0.05 | 34 | C | 0.09 | 42 | D |
| Future Total (2025) <br> Haul Route Option 1 (Thorold Townline Road) | Overall | 0.48 | 16 | B | 0.52 | 21 | C |
|  | EBL | 0.30 | 8 | A | 0.20 | 6 | A |
|  | EBT | 0.45 | 8 | A | 0.44 | 8 | A |
|  | EBR | 0.09 | 5 | A | 0.09 | 4 | A |
|  | WBL | 0.08 | 5 | A | 0.09 | 5 | A |
|  | WBTR | 0.34 | 7 | A | 0.49 | 8 | A |
|  | NBL | 0.35 | 38 | D | 0.67 | 59 | E |
|  | NBTR | 0.62 | 43 | D | 0.63 | 52 | D |
|  | SBL | 0.15 | 35 | D | 0.44 | 49 | D |
|  | SBT | 0.31 | 37 | D | 0.43 | 47 | D |
|  | SBR | 0.05 | 34 | C | 0.10 | 42 | D |
| Future Background (2035) | Overall | 0.54 | 16 | B | 0.68 | 23 | C |
|  | EBL | 0.45 | 10 | B | 0.41 | 11 | B |
|  | EBT | 0.52 | 9 | A | 0.57 | 12 | B |
|  | EBR | 0.10 | 5 | A | 0.10 | 6 | A |
|  | WBL | 0.09 | 6 | A | 0.12 | 6 | A |
|  | WBTR | 0.44 | 8 | A | 0.65 | 12 | B |
|  | NBL | 0.39 | 38 | D | 0.66 | 57 | E |
|  | NBTR | 0.62 | 43 | D | 0.64 | 52 | D |
|  | SBL | 0.29 | 37 | D | 0.77 | 74 | E |
|  | SBT | 0.31 | 37 | D | 0.41 | 46 | D |
|  | SBR | 0.07 | 34 | C | 0.13 | 42 | D |
| Future Total (2035) <br> Haul Route Option 1 (Thorold Townline Road) | Overall | 0.54 | 16 | B | 0.68 | 23 | C |
|  | EBL | 0.46 | 10 | B | 0.42 | 11 | B |
|  | EBT | 0.52 | 9 | A | 0.57 | 12 | B |
|  | EBR | 0.10 | 5 | A | 0.10 | 6 | A |
|  | WBL | 0.09 | 6 | A | 0.12 | 6 | A |
|  | WBTR | 0.44 | 8 | A | 0.65 | 12 | B |
|  | NBL | 0.39 | 38 | D | 0.66 | 56 | E |
|  | NBTR | 0.62 | 43 | D | 0.64 | 52 | D |
|  | SBL | 0.30 | 38 | D | 0.77 | 74 | E |
|  | SBT | 0.31 | 37 | D | 0.41 | 46 | D |
|  | SBR | 0.07 | 34 | C | 0.13 | 42 | D |

Under existing conditions, the intersection operates very well during the a.m. and p.m. peak hours with overall LOS ' $B$ ' and $\mathrm{v} / \mathrm{c}$ ratios of 0.39 and 0.43 during the a.m. and p.m. peak hours, respectively, indicating reserve capacity. Individual movements experience LOS 'D' or better.

Under 2025 background conditions, the intersection is expected to continue operating at acceptable levels with overall LOS ' $B$ ' and ' $C$ ' and $\mathrm{v} / \mathrm{c}$ ratios of 0.48 and 0.52 during the a.m. and p.m. peak hours, respectively. Individual movements are predicted to experience LOS 'D' or better with the exception of the northbound left movement that is predicted to experience LOS 'E' during the p.m. peak hour.

Based on 2025 future total traffic conditions for Haul Route Option 1, the intersection is expected to continue operating at acceptable levels with an overall LOS 'B' and 'C' and v/c ratios of 0.48 and 0.52 during the a.m. and p.m. peak hours, respectively. With the exception of the northbound left movement that is predicted to experience LOS 'E' during the p.m. peak hour, all other individual movements are predicted to experience LOS 'D' or better.

The intersection is expected to operate at acceptable levels under 2035 background conditions with overall LOS ' $B$ ' and ' $C$ ' and $v / c$ ratios of 0.54 and 0.68 during the a.m. and p.m. peak hours, respectively, indicating reserve capacity remains. With the exception of the northbound left and southbound left movements that are predicted to experience LOS 'E' during the p.m. peak hour, all other individual movements are predicted to experience LOS 'D' or better.

Under 2035 future total traffic conditions for Haul Route Option 1, the intersection is expected to operate with overall LOS ' $B$ ' and ' $C$ ' and $\mathrm{v} / \mathrm{c}$ ratios of 0.54 and 0.68 during the a.m. and p.m. peak hours, respectively. With the exception of the northbound left and southbound left movements that are predicted to experience LOS 'E' during the p.m. peak hour, all other individual movements are predicted to experience LOS 'D' or better during both peak hours.

Overall, this intersection is expected to have acceptable future operations upon the construction of a dedicated southbound right turn lane. It is suggested that the southbound right turn lane be constructed prior to the 2035 planning horizon to facilitate efficient movement of traffic at the intersection. It should be noted that under the preferred Haul Route Option 1 traffic scenario, the site attributes a nominal volume of traffic to the southbound right turn movement (4 two-way trips) during the peak hour, as result the impact of site-related traffic on the intersection is negligible. Therefore, as previously mentioned, it is suggested that the intersection be monitored in the future to determine whether constructing the dedicated southbound right turn lane or making adjustments to the signal timings in the interim condition, including the addition of protected phases, would be the most appropriate solution to accommodate background traffic volumes.

### 6.6 Thorold Townline Road at Beaverdams Road

A signal warrant was conducted for the intersection of Thorold Townline Road and Beaverdams Road under 2025 Background conditions to confirm if the combined existing and 2025 background traffic would justify the installation of a traffic signal. Based on Justification 7 of Book 12 of the Ontario Traffic Manual (OTM), the estimated 2025 background traffic volumes fulfill Justification 1A and 1B at $97 \%$ and $100 \%$ respectively. Although not warranted under 2025 Background conditions, based on the $120 \%$ threshold applied to Justification 7 and the near 100\% justification fulfillment it is TMIG's opinion signals should be considered at this intersection under 2025 Background conditions.

In general, it is suggested that the intersection be monitored for signalization in 2025, and that signals be installed prior to the 2035 planning horizon (i.e. prior to the combined full build-out of the Rolling Meadows development, Thorold Townline Road Employment Lands, and the proposed Upper's Lane Quarry).

Unsignalized and Signalized capacity analyses during the weekday a.m. and p.m. peak hours are summarized in Table 6-7 for the intersection of Thorold Townline Road at Beaverdams Road.

Table 6-7 Capacity Analysis of Thorold Townline Road at Beaverdams Road

| Condition | Movement | AM Peak Hour |  |  | PM Peak Hour |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | v/c | Delay (s) | LOS | v/c | Delay (s) | LOS |
| Existing | EBLTR | 0.23 | 10 | A | 0.39 | 12 | B |
|  | WBLTR | 0.31 | 10 | B | 0.33 | 11 | B |
|  | NBLTR | 0.33 | 11 | B | 0.32 | 12 | B |
|  | SBLTR | 0.22 | 10 | B | 0.34 | 12 | B |
| Future Background (2025) | EBLTR | 0.36 | 14 | B | 0.57 | 20 | C |
|  | WBLTR | 0.43 | 15 | B | 0.57 | 20 | C |
|  | NBLTR | 0.58 | 18 | C | 0.83 | 36 | E |
|  | SBLTR | 0.67 | 22 | C | 0.63 | 22 | C |
| Future Total (2025) | Overall | 0.48 | 18 | B | 0.54 | 23 | C |
|  | EBLTR | 0.39 | 29 | C | 0.34 | 17 | B |
| Haul Route Option 1 (Thorold Townline Road) | WBLTR | 0.46 | 30 | C | 0.35 | 17 | B |
|  | NBLTR | 0.48 | 13 | B | 0.76 | 30 | C |
|  | SBLTR | 0.50 | 13 | B | 0.58 | 23 | C |
| Future Background (2035) | Overall | 0.64 | 20 | B | 0.79 | 27 | C |
|  | EBLTR | 0.36 | 28 | C | 0.40 | 22 | C |
|  | WBLTR | 0.57 | 33 | C | 0.68 | 31 | C |
|  | NBLTR | 0.49 | 13 | B | 0.87 | 32 | C |
|  | SBLTR | 0.67 | 17 | B | 0.49 | 17 | B |
| Future Total (2035) | Overall | 0.70 | 21 | C | 0.86 | 29 | C |
|  | EBLTR | 0.36 | 28 | C | 0.45 | 26 | C |
| Haul Route Option 1 (Thorold Townline Road) | WBLTR | 0.57 | 33 | C | 0.79 | 41 | D |
|  | NBLTR | 0.62 | 15 | B | 0.90 | 32 | C |
|  | SBLTR | 0.76 | 20 | B | 0.55 | 15 | B |

Under existing conditions, the unsignalized intersection operates with excellent operational characteristics during the a.m. and p.m. peak hours with delays of 12 seconds or less.

Under 2025 background conditions, the unsignalized intersection is expected to continue operating at acceptable levels, however, northbound traffic is expected to experience LOS ' $E$ ', and a delay of 36 seconds during the p.m. peak hour.

Under 2025 future total traffic conditions for Haul Route Option 1, the signalized intersection is expected to operate well with LOS ' $C$ ' or better, and reserve capacity during both the weekday a.m. and p.m. peak hours.

The signalized intersection is expected to operate well under 2035 background conditions with LOS ' C ' or better, and delays of 33 seconds or less during the a.m. and p.m. peak hours. In general, all movements have considerable reserve capacity with the exception of the shared northbound movement during the p.m. peak hour that experiences a v/c ratio of 0.87 . The northbound shared left/through/right lane is approaching capacity, but still operates with acceptable levels of delay.

Under 2035 future total traffic conditions for Haul Route Option 1, the intersection continues to operate well with individual movements at LOS ' $C$ ' or better and delays of 33 seconds or less during the a.m. peak hour. During the p.m. peak hour, movements operate at LOS 'D' or better and delays of 41 seconds or less. The northbound shared left/through/right movement is approaching capacity with a v/c ratio of 0.90 , but still operates with acceptable levels of delay. During the p.m. peak hour, the intersection is expected to operate with an overall $\mathrm{v} / \mathrm{c}$ ratio of 0.86 , however, it operates with an acceptable overall LOS ' C '.

Overall, this intersection should be monitored for signalization under 2025 background and total conditions, and is expected to have acceptable future operations upon signalization prior to 2035.

### 6.7 Thorold Townline Road at Proposed Upper's Quarry Access

It is proposed that the access to Upper's Quarry be located at the Upper's Lane intersection with Thorold Townline Road as, regardless of ownership of the road, Upper's Lane will primarily serve Quarry traffic, not public traffic.

Unsignalized capacity analyses during the weekday a.m. and p.m. peak hours are summarized in Table 6-8 for the intersection of Thorold Townline Road at Upper's Lane.

Table 6-8 Capacity Analysis of Thorold Townline Road at Proposed Upper's Quarry Access

| Condition | Movement | AM Peak Hour |  |  | PM Peak Hour |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Delay <br> (s) | LOS | v/c | Delay <br> (s) | LOS |  |
| Future Total <br> (2025) | WBLR | 0.14 | 13 | B | 0.10 | 13 | B |
| Haul Route Option 1 <br> (Thorold Townline Road) | SBL | 0.06 | 9 | A | 0.06 | 9 | A |
| Future Total <br> (2035) | WBLR | 0.18 | 15 | C | 0.14 | 16 | C |
| Haul Route Option 1 | SBL | 0.06 | 10 | B | 0.07 | 11 | B |

Under 2025 future total traffic conditions, the quarry access via Thorold Townline Road is expected to operate with excellent operational characteristics and substantial reserve capacity during both the weekday a.m. and p.m. peak hours. The delay to the westbound vehicles exiting the quarry is minimal, a mere 13 seconds during both the peak hours.

Under 2035 future total traffic conditions, Haul Route Option 1 (via Thorold Townline Road), continues to operate well with acceptable delay to westbound vehicles exiting the quarry.

Overall, the proposed Upper's Quarry access via Thorold Townline Road is expected to have acceptable future operations and there are no required improvements other than the conceptual access design discussed in Section 8 of this report.

## 7 QUEUEING ANALYSIS

Queuing analysis of the study intersections and the proposed Upper's Quarry site access was undertaken, and detailed reports are provided in Appendix D. A summary of the predicted 95th percentile queues for the weekday a.m. and p.m. peak hours under existing, background, and future total traffic is provided in Table 71 and Table 7-2. The queuing reports were prepared using SimTraffic microsimulation software using the following methodology: 30 minutes seeding time, one-hour recording, and 5 simulation runs.

Table 7-1 Existing (2018) and Future Total Background (2025 \& 2035) Queuing Analysis

| Intersection | Movement | Available Storage (m) | $95^{\text {th }}$ Percentile Queue Length ( m ) |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | 2018 Existing |  | 2025 Total <br> Background |  | 2035 Total <br> Background |  |
|  |  |  | AM | PM | AM | PM | AM | PM |
| Davis Road at Thorold Stone Road | EBL | 105 | 12 | 16 | 11 | 15 | 13 | 15 |
|  | WBL | 70 | 30 | 46 | 41 | 42 | 104 | 62 |
|  | NBL | 275 | 55 | 54 | 86 | 72 | 96 | 142 |
|  | SBL | 30 | - | 1 veh | 1 veh | 1 veh | 1 veh | 1 veh |
| Davis Road at Niagara Falls Road/ <br> Beaverdams Road | NBL | 80 | 1 veh | 1 veh | 14 | 9 | 21 | 15 |
|  | SBL | 140 | 27 | 47 | 32 | 48 | 31 | 53 |
| Davis Road at Lundy's Lane | EBL | 85 | 27 | 34 | 46 | 57 | 42 | 72 |
|  | WBL | 65 | 17 | 17 | 22 | 17 | 26 | 52 |
|  | WBR | 80 | 11 | 14 | 29 | 43 | 21 | 90 |
|  | NBL | 55 | 19 | 20 | 18 | 23 | 18 | 23 |
|  | SBL | 90 | 33 | 23 | 95 | 104 | 70 | 191 |
|  | SBR | 100 | 21 | 19 | 29 | 34 | 41 | 61 |
| Thorold Townline Road at Thorold Stone Road | EBL | 100 | 82 | 67 | 102 | 79 | 117 | 83 |
|  | EBR | 50 | 12 | 8 | 32 | 24 | 54 | 72 |
|  | WBL | 85 | 15 | 15 | 51 | 31 | 104 | 60 |
|  | WBR | 90 | 18 | 11 | 20 | 14 | 18 | 14 |
|  | NBL | 80 | 34 | 27 | 50 | 57 | 66 | 62 |
|  | SBL | 75 | 26 | 25 | 27 | 33 | 123 | 183 |
| Thorold Townline Road at Lundy's Lane | EBL | 90 | 19 | 20 | 41 | 33 | 61 | 76 |
|  | EBR | 20 | 18 | 23 | 16 | 26 | 34 | 27 |
|  | WBL | 55 | 12 | 16 | 14 | 16 | 16 | 17 |
|  | NBL | 25 | 30 | 42 | 34 | 44 | 34 | 55 |
|  | SBL | 25 | 12 | 14 | 20 | 31 | 22 | 48 |
|  | SBR | 30 | - | - | 20 | 30 | 27 | 52 |
| Thorold Townline Road at <br> Beaverdams Road | EBLTR | - | 21 | 35 | 46 | 58 | 44 | 65 |
|  | WBLTR | - | 16 | 19 | 45 | 49 | 58 | 98 |
|  | NBLTR | - | 36 | 32 | 74 | 113 | 148 | 254 |
|  | SBLTR | - | 25 | 26 | 68 | 91 | 122 | 216 |
| Thorold Townline Road at Upper's Lane | WBLR | - | 1 veh | 1 veh | 29 | 23 | 25 | 26 |

## Existing Conditions

Under existing conditions, the $95^{\text {th }}$ percentile queue lengths of dedicated movements at study intersections are not predicted to exceed the available storage, with the exception of the intersection of Thorold Townline Road and Lundy's Lane. The northbound left turn queue exceeds its storage by 5 metres during the a.m. peak hour, and by 17 metres during the p.m. peak hour. The 5 and 17 metres that the queue exceeds the existing storage for these two movements is representative of approximately one and two vehicles, respectively, and is considered to be an acceptable level of queueing although the extra vehicles may not fully fit in the allotted storage area.

## 2025 Background Conditions

Under 2025 background conditions, the $95^{\text {th }}$ percentile queue lengths at study intersections are generally not predicted to exceed the available storage. The northbound left queue at Thorold Townline Road and Lundy's Lane continues to exceed available storage during both peak hours by up to 19 metres.

## 2035 Background Conditions

Overall, the study intersections experience minimal $95^{\text {th }}$ percentile queuing problems under 2035 background traffic conditions.

Under 2035 background conditions, the intersection of Davis Road and Lundy's Lane becomes congested with background traffic and it is predicted that several dedicated turn movements may have $95^{\text {th }}$ percentile queues that will extend beyond existing storage (eastbound left, westbound left, westbound right, and southbound left). In particular, the southbound left turn at Davis Road and Lundy's Lane during the p.m. peak hour experiences a large increase in the $95^{\text {th }}$ percentile queue length between 2025 and 2035 background conditions. The queue length is predicted to be 211 metres long, exceeding the 90 metres of available storage.

As seen in Table 7-2, this queue continues to exceed the available storage under 2025 and 2035 future total conditions. It is recommended the intersection be monitored as the Rolling Meadows development phases are constructed to determine if any adjustments to signal timings and/or physical improvements to the roadway, such as extending the storage, is required. A minimal amount of non-aggregate site traffic is expected to travel through this intersection and will not create any measurable impacts to operations.

The $95^{\text {th }}$ percentile queue of eastbound left turn and westbound left turn movements at the intersection of Thorold Townline Road and Thorold Stone Road are predicted to exceed storage during the a.m. peak hour under 2035 background conditions. The eastbound left is predicted to exceed storage by 17 metres, equivalent to approximately two cars. The westbound left is predicted to exceed storage by 21 metres, which is equivalent to approximately three cars. During the p.m. peak hour, the $95^{\text {th }}$ percentile queue of the southbound left movement is expected to exceed available storage by 61 metres.

As discussed in Section 6.4, the intersection could benefit from monitoring in the future to determine if further signal timing modification or geometric improvements (such as a dedicated southbound right turn lane) would improve overall operations of the intersection and aid in moving the southbound traffic through the intersection more efficiently. A dedicated right-turn lane could potentially assist in reducing the queue spillback of the southbound through and right-turn traffic that may block the southbound left-turn lane at times.

Under 2035 background traffic conditions, the northbound left and southbound left queues at Thorold Townline Road and Lundy's Lane continue to meet or exceed available storage during the a.m. and p.m. peak hours. It should be noted that a railway crossing is located approximately 80 metres south of the intersection and extending the northbound left turn lane will not be a viable option. It is recommended that queue lengths be monitored at this intersection, and that the adjustment of the signal timings and phases should be reviewed to address the $95^{\text {th }}$ percentile queues given the geometric constraints.

As discussed in Section 6.5, the dedicated southbound right lane at Thorold Townline Road and Lundy's Lane is suggested to be constructed prior to 2035 to aid in the overall operation of the intersection and to reduce delays. It should be noted under the preferred Haul Route Option 1 traffic scenario, the site attributes a nominal volume of traffic to the southbound right turn movement (4 two-way trips) during the peak hour. As a result, the operational impact of site-related traffic at this intersection is negligible and will not trigger the aforementioned road improvements. As such, it is suggested that the intersection be monitored in the future
to determine whether constructing the dedicated southbound right turn lane would be the most appropriate solution to accommodate background development traffic volumes within the vicinity of the intersection.

Table 7-2 Future Total (2025 \& 2035) Haul Route Option 1 Queuing Analysis

| Intersection | Movement | Available Storage (m) | $95^{\text {th }}$ Percentile Queue Length (m) |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | 2025 Total Haul Route Option 1 (Thorold Townline Rd) |  | 2035 Total Haul Route Option 1 (Thorold Townline Rd) |  |
|  |  |  | AM | PM | AM | PM |
| Davis Road at Thorold Stone Road | EBL | 105 | 11 | 16 | 12 | 16 |
|  | WBL | 70 | 56 | 42 | 79 | 61 |
|  | NBL | 275 | 88 | 75 | 101 | 112 |
|  | SBL | 30 | 1 veh | 1 veh | 1 veh | 1 veh |
| Davis Road at Niagara Falls Road/ <br> Beaverdams Road | NBL | 80 | 16 | 8 | 18 | 15 |
|  | SBL | 140 | 29 | 47 | 28 | 48 |
| Davis Road at Lundy's Lane | EBL | 85 | 45 | 58 | 43 | 81 |
|  | WBL | 65 | 23 | 18 | 23 | 24 |
|  | WBR | 80 | 30 | 45 | 23 | 54 |
|  | NBL | 55 | 21 | 22 | 20 | 24 |
|  | SBL | 90 | 76 | 112 | 54 | 162 |
|  | SBR | 100 | 31 | 30 | 38 | 48 |
| Thorold Townline Road at Thorold Stone Road | EBL | 100 | 103 | 76 | 115 | 98 |
|  | EBR | 50 | 34 | 35 | 46 | 96 |
|  | WBL | 85 | 42 | 31 | 94 | 82 |
|  | WBR | 90 | 34 | 13 | 21 | 39 |
|  | NBL | 80 | 52 | 50 | 65 | 85 |
|  | SBL | 75 | 40 | 33 | 67 | 159 |
| Thorold Townline Road at Lundy's Lane | EBL | 90 | 41 | 30 | 68 | 60 |
|  | EBR | 20 | 21 | 20 | 27 | 27 |
|  | WBL | 55 | 12 | 18 | 15 | 19 |
|  | NBL | 25 | 35 | 42 | 32 | 58 |
|  | SBL | 25 | 17 | 29 | 22 | 50 |
|  | SBR | 30 | 22 | 31 | 24 | 53 |
| Thorold Townline Road at Beaverdams Road | EBLTR | - | 45 | 54 | 45 | 59 |
|  | WBLTR | - | 47 | 46 | 55 | 102 |
|  | NBLTR | - | 63 | 113 | 112 | 540 |
|  | SBLTR | - | 69 | 81 | 109 | 225 |
| Thorold Townline Road at Upper's Lane | WBLR | - | 24 | 26 | 29 | 27 |
|  | SBL | 15 | 19 | 16 | 21 | 19 |

## 2025 Total Conditions

Under 2025 total traffic (Haul Route Option \#1) conditions, study intersections experience minimal queueing problems with the exception of the following movements that experience $95^{\text {th }}$ percentile queues that exceed the available storage length by 5 metres or more:

- Southbound Left at Davis Road and Lundy's Lane (p.m. peak hour)
- Northbound Left at Thorold Townline Road and Lundy's Lane (a.m. and p.m. peak hours)

The 95th percentile queue for the southbound left movement at the intersection of Thorold Townline Road and the proposed Upper's Quarry access is predicted to be 19 and 16 metres during the weekday a.m. and p.m. peak hours, respectively. Given the minor predicted exceedance, the southbound left turn storage of 30 metres, as proposed in the conceptual site access design, can adequately accommodate the predicted $95^{\text {th }}$ percentile queues under 2025 total conditions. The westbound queues at the site access will be accommodated by internal site roadways.

## 2035 Total Conditions

Under 2035 total traffic (Haul Route Option \#1) conditions, study intersections experience longer queues than under 2025 total conditions, however, only the following movements experience $95^{\text {th }}$ percentile queues that exceed the available storage length by 5 metres or more:

- Westbound Left at Davis Road and Thorold Stone Road (a.m. peak hour)
- Southbound Left at Davis Road and Lundy's Lane (p.m. peak hour)
- Eastbound Left at Thorold Townline Road and Thorold Stone Road (a.m. peak hour)
- Westbound Left at Thorold Townline Road and Thorold Stone Road (a.m. peak hour)
- Southbound Left at Thorold Townline Road and Thorold Stone Road (p.m. peak hour)
- Eastbound Right at Thorold Townline Road and Lundy's Lane (a.m. and p.m. peak hours)
- Northbound Left at Thorold Townline Road and Lundy's Lane (a.m. and p.m. peak hours)
- Southbound Left at Thorold Townline Road and Lundy's Lane (p.m. peak hour)
- Southbound Right at Thorold Townline Road and Lundy's Lane (p.m. peak hour)

The $95^{\text {th }}$ percentile queue lengths that exceed the available storage space under 2035 total conditions are generally longer than the 2025 total conditions because of the sizeable increase in background traffic volumes from 2025 to 2035, which is particularly true at intersections that are not included in the preferred haul route.

Under 2035 future total conditions, the 95th percentile queue for the southbound left movement at the intersection of Thorold Townline Road and the proposed Upper's Quarry access is predicted to be 21 and 19 metres during the weekday a.m. and p.m. peak hours, respectively. Given the minor predicted exceedance, the southbound left turn storage of 30 metres, as proposed in the conceptual site access design, can adequately accommodate the predicted $95^{\text {th }}$ percentile queues under 2035 total conditions. The westbound queues at the site access will be accommodated by internal site roadways.

## 8 QUARRY ACCESS

### 8.1 Location

The intersection of Uppers Lane and Thorold Townline Road is to be modified to accommodate truck traffic and function as the future access to the proposed Upper's Quarry. Access to the proposed Upper's Quarry via Upper's Lane will be achieved regardless as to the ownership of the road allowance, as the location will serve either as a direct access to the quarry, or as a roadway to access the quarry. Aggregate and Asphalt traffic (heavy vehicles) will access Upper's Lane / the proposed Upper's Quarry via Thorold Townline Road to/from the north, and will not access the proposed quarry via Beechwood Road. The quarry access will thus be located approximately one kilometre south of the Beaverdams Road and Thorold Townline Road intersection.

### 8.2 Access Design

The proposed design for the access incorporates engineering design criteria as per the 2017 Transportation of Canada (TAC) geometric design guideline for Canadian roads and The Ontario Ministry of Transportation's (MTO) Commercial Site Access Policy and Standard Designs. The proposed access design provides deceleration and accelerations lanes northbound at the site access. A slip around lane is provided southbound, thus accommodating left-turning vehicles into the site and preventing blockage of through traffic at the site access.

Access design includes curb radii of 16 m and 18 m to accommodate future truck turning movements into and out of the site. The access design can accommodate site-related traffic for both Haul Route Options 1 and 2, although the preferred Haul Route Option 1 will only require heavy vehicle site traffic to be accommodated for the southbound left and westbound right movements.

Of note, while the preferred aggregate haul route is to the north via Thorold Townline (thus the provision of a northbound acceleration lane and southbound left-turn lane in the conceptual design), other forms of site traffic may access the quarry from the south. A dedicated northbound right turn lane has been included in the conceptual design to accommodate non-aggregate site traffic without impeding northbound through traffic.

The design of the site access is provided in Appendix E.

### 8.3 Site Access Operation

Site access operation was reviewed using a heavy single unit (HSU) truck to simulate turning movements of aggregate trucks accessing and departing the site. Turning movement simulations show that all required turning movement operations can be accommodated at the site access.

Truck turning movement simulations at the future site access are provided in Appendix E.

### 8.4 Sightline Assessment

Sight distances were examined in both directions on Thorold Townline Road at the proposed site access. Our examination is based on the criteria contained in the Transportation Association of Canada (TAC) Guideline, 2017 edition. Thorold Townline Road has a posted speed of $80 \mathrm{~km} / \mathrm{h}$ in the vicinity of the subject site. As per industry standard, sight distance was examined a design speed of $100 \mathrm{~km} / \mathrm{h}$ or $20 \mathrm{~km} / \mathrm{h}$ over the posted speed.

The criteria in the TAC guideline is based on passenger car operations and does not explicitly consider a variation for truck movements. Section 2.5.3.1 in the TAC Guideline indicates that although trucks need longer
stopping sight distances than passenger cars, the additional lengths required by trucks is balanced by the fact that a truck driver can generally see further than a passenger car driver due to the eye height advantage. The TAC Guideline goes on to say that "As a result, separate stopping sight distances for trucks are not generally used in highway design".

Our research of the policies employed by other jurisdictions in this regard revealed that a variation for trucks is likewise not applied. According to Section 3-6 in 'A Policy on Geometric Design of Highways and Streets, 6th Edition, 2011, published by the American Association of State Highway and Transportation Officials (AASHTO), the additional lengths required by trucks is balanced by the fact that "the truck driver is able to see substantially farther beyond vertical sight obstructions because of the higher position of the seat in the vehicle." Likewise, passenger cars approaching the site access would have longer sight lines due to the height of the trucks entering and exiting the site. In addition, due to their training, the average truck driver is typically more adept than the average passenger car driver at recognizing potential risks and reacting to same.
Based on the foregoing, we have utilized the criteria as presented in the TAC guideline. However, we have based our analysis on the maximum values contained therein to ensure a conservative analysis.

## Assessment Criteria

Based on Table 2.5.2: Stopping Sight Distance on level roadways for Automobiles contained in the Transportation Association of Canada (TAC) Guideline (see Appendix F) the maximum stopping sight distance for an $100 \mathrm{~km} / \mathrm{h}$ design speed is 185 metres.
Based on Table 2.5.3: Stopping Sight Distance on Grades contained in the Transportation Association of Canada (TAC) Guideline (see Appendix F) the maximum stopping sight distance for an $100 \mathrm{~km} / \mathrm{h}$ design speed on a downgrade of $9 \%$ is 223 metres.
Based on Table 2.5.6 Decision Sight Distance contained in the Transportation Association of Canada (TAC) Guideline (see Appendix F) the maximum decision sight distance for a $100 \mathrm{~km} / \mathrm{h}$ design speed on a roadway is 415 metres for an avoidance manoeuvre.

## Analysis Results

The proposed access is located approximately 1.5 km north of the intersection of Lundy's Lane and 1.1 km south of Beaverdams Road. Based on our online review of Google aerial mapping, Thorold Townline Road is straight roadway with no horizontal curvature and minor vertical deflection gradually sloping upward from south to north, south of the proposed site access via Upper's Lane. The slope does not create any obstacles to drivers approaching the intersection nor to trucks at the site access. The proposed site access via Upper's Lane is located such that drivers approaching on Thorold Townline Road have an unimpeded view in excess of 415 metres in both directions.

Based on our review, the sight lines on Thorold Townline Road at the site access via Upper's Lane exceed those recommended for stopping and decision sight distances as contained in the TAC guideline.

## 9 CONCLUSION

Overall, the traffic generated by the proposed Upper's Quarry can be accommodated by the existing study area road network for the preferred haul route with minimal changes or upgrades to study area intersections. Two possible routes have been considered as appropriate 'haul routes' for material that will be shipped from the proposed Upper's Quarry to serve local and broader markets, however, Haul Route Option 1 (via Thorold Townline Road) was identified as the preferred haul route.

### 9.1 Haul Route Options

## Haul Route Option 1

The first option of a haul route for trucks to / from the proposed Upper's Quarry would utilize Thorold Townline Road to the north of the site, as it is a regional road and provides the most direct route to / from the quarry. The haul route includes the following roads:

- Thorold Townline Road north of the site access to Thorold Stone Road
- Highway 406 via Thorold Stone Road westbound
- Queen Elizabeth Way (QEW) via Taylor Rd northbound
- Queen Elizabeth Way (QEW) via Thorold Stone Road eastbound


## Haul Route Option 2

Davis Road is designated as a provincial highway and is a major boundary road in close proximity to the site. Accordingly, it can also be considered an appropriate roadway to accommodate truck traffic to / from the quarry. The use of Davis Road as a second option for a haul route would result in a more circuitous haul route, as access to Davis Road would require quarry trucks to first travel south on Thorold Townline Road to Lundy's Lane, and then proceed west to Davis Road. The second haul route option includes the following roadways:

- Thorold Townline Road south of the site access to Lundy's Lane
- Lundy's Lane west to Davis Road
- Davis Road north to Thorold Stone Road
- Highway 406 via Thorold Stone Road westbound
- Queen Elizabeth Way (QEW) via Thorold Stone Road (eastbound) and Taylor Road northbound
- Queen Elizabeth Way (QEW) via Thorold Stone Road eastbound


### 9.2 Preferred Haul Route

TMIG recommends that Haul Route Option 1 be chosen as the preferred Haul Route, subject to approval by the Town and an appraisal of the cost of any road improvements required to accommodate truck traffic.
Haul Route Option 1 will also be seen as a preferable route by current and future residents within the vicinity of the proposed Upper's Quarry, as the Rolling Meadows Secondary Plan area represents a large amount of future residential traffic that will travel along Davis Road and Lundy's Lane. As such, it would be ideal to have truck traffic travel north directly on Thorold Townline Road (Haul Route Option 1), compared to the more circuitous route around the boundary of the future Rolling Meadows area (Haul Route Option 2).

Of note, Haul Route Option 1 will direct trucks northbound on Thorold Townline Road through a non-residential area, however, a causeway has been constructed along Thorold Townline Road to cross a waterway immediately south of Beaverdams Road. Depending on the structural properties of the causeway, improvements may need to be made in order to sustain the regular truck traffic associated with the proposed Upper's Quarry. Before the choice of haul route is finalized, it is recommended that Walker Aggregates Inc. and the Town perform a review of the existing load capacity of Thorold Townline Road in order to determine if any upgrades are required, and if so, what cost would be associated with the upgrades. If it is found that
upgrades are required, it should be determined if the upgrades would be needed to service the future Rolling Meadows development regardless of any Upper's Quarry operations. The cost of the roadway upgrades should be assigned proportionately to the parties that will derive direct benefits from the upgrades.

### 9.3 Capacity Analysis Results and Recommendations

Overall, the study area intersections operate well or at acceptable levels under all planning horizons. Some individual movements are approaching capacity, particularly under 2035 conditions, but still operate with acceptable delays of 80 seconds or less, indicating a Level of Service (LOS) ' $E$ ' or better. Some geometric changes and modifications to signal timing plans are recommended in order to address any capacity or queuing issues in order to allow for efficient movement of traffic through the study area.

Haul Route Option 1 via Thorold Townline to the north was identified as the preferred haul route, and accordingly future total traffic operations were analyzed for Haul Route Option 1 only. A summary of recommendations and timing of the improvements are provided below.

## Background Conditions (2025 \& 2035)

- With adjustments to existing signal timing plans, all study intersections operate at acceptable levels under 2025 and 2035 background conditions. Some individual movements are approaching capacity, but operate at acceptable levels of service.
- In general, it is suggested that the Thorold Townline Road and Beaverdams Road intersection be monitored for signalization in 2025, and that signals be installed prior to the 2035 planning horizon (i.e. prior to the combined full build-out of the Rolling Meadows development, Thorold Townline Road Employment Lands, and the proposed Upper's Lane Quarry).
- Construction of an auxiliary southbound right turn lane at the intersection of Thorold Townline Road and Lundy's Lane by the 2035 background planning horizon was found to provide better overall operations at the intersection. Interim adjustments to signal timings and introduction of protected phases could potentially negate the need for a southbound right turn lane, however, high volumes of southbound rightturning vehicles are predicted in 2035 that would benefit from a dedicated lane compared to the existing shared through/right turn lane. Given that the proposed Upper's Quarry is assumed to be active by 2025, quarry related traffic is not the primary cause of the high volume of right-turning vehicles predicted in 2035, particularly based on preferred Haul Route Option 1 (via Thorold Townline Road), as minimal staff site traffic travels through the intersection, and heavy vehicle site traffic will not travel through the Thorold Townline Road and Lundy's Lane intersection. The operational impact of Haul Route Option 1 site-related traffic at this intersection is negligible and will not trigger the aforementioned road improvements.
- There is opportunity to widen the existing 24 metre ROW at the Thorold Townline Road and Lundy's Lane intersection to the designated 26.2 metre road allowance to accommodate a southbound right turn lane. Furthermore, the Region may require road widening dedications in addition to the designated road allowances without the need for amendments to the Official Plan for purposes such as turning lanes at intersections.
- It is recommended the Thorold Townline Road and Lundy's Lane intersection be monitored in the future to determine whether constructing the dedicated southbound right turn lane would be the most appropriate solution to accommodate background development traffic volumes within the vicinity of the intersection.


## Total Conditions (2025 \& 2035)

- With adjustments to existing signal timing plans, all study intersections operate acceptably under 2025 and 2035 total conditions. Some intersections/movements are approaching, or are at capacity, but operate at acceptable levels of service.
- The proposed access design will be constructed in 2025 prior to the quarry becoming active. The proposed access design provides deceleration and accelerations lanes northbound at the site access (via Upper's Lane). A slip around lane is provided southbound, thus accommodating left-turning vehicles into the site and preventing blockage of through traffic at the site access.
- The southbound queue at Thorold Stone Road and Thorold Townline Road should be monitored in 2035 to determine if any upgrades to the intersection are needed to address the potential for long queues to build up (southbound left experiences a queue up to 160 m according to simulations). The long southbound left queue buildup does not occur under 2025 total conditions when Upper's Quarry is active, as such, quarry related traffic is not the cause of the long queues predicted in 2035.


### 9.4 Conceptual Site Access Design

The intersection of Uppers Lane and Thorold Townline Road is to be modified to accommodate truck traffic and function as the future access to the proposed Upper's Quarry. Access to the proposed Upper's Quarry via Upper's Lane will be achieved regardless as to the ownership of the road allowance, as the location will serve either as a direct access to the quarry, or as a roadway to access the quarry. Aggregate and Asphalt traffic (heavy vehicles) will access Upper's Lane / the proposed Upper's Quarry via Thorold Townline Road to/from the north, and will not access the proposed quarry via Beechwood Road. The quarry access will thus be located approximately one kilometre south of the Beaverdams Road and Thorold Townline Road intersection.

The proposed design for the access incorporates engineering design criteria as per the 2017 Transportation of Canada (TAC) geometric design guideline for Canadian roads and The Ontario Ministry of Transportation's (MTO) Commercial Site Access Policy and Standard Designs. The proposed access design provides deceleration and accelerations lanes northbound at the site access. A slip around lane is provided southbound, thus accommodating left-turning vehicles into the site and preventing blockage of through traffic at the site access.

Access design includes curb radii of 16 m and 18 m to accommodate future truck turning movements into and out of the site.

Entrance improvements shall be implemented prior to the haulage of extracted material off-site:

- At the intersection of Upper's Lane and Thorold Townline Road: including the installation of a southbound slip-around lane consisting of a parallel lane with 30 metres of storage plus approach / departure tapers of 150 metres, along with a northbound right-turn lane with a taper of 85 metres and a parallel length of 170 metres.
- Along Upper's Lane: including a widening of approximately 1.0 to 1.5 metres west of any proposed entrance along Upper's Lane and installation of a culvert for the future watercourse realignment.


## APPENDIX A

## Preliminary Site Plan






,
$=2$

1 ,


 $12=2$
 max max Enimerastatem
 = = =
$\pm=5$ $=$
$=9$


 new
 $=2=2$
 $= \pm= \pm=m$
 2amawawawawaw waw waw $=m$
$=5$
2-


 2

 mammemmen
 $\pm=$ vawasawaswive




## APPENDIX B

Traffic Data


| Ontario Traffic Inc. |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Afternoon Peak Diagram |  |  |  |  |  |  |  | Spec <br> From <br> To: |  | Period <br> 6:00:00 <br> 9:00:00 |  |  | ne om: : | $\begin{aligned} & \text { ur Pe } \\ & \text { 16:30:0 } \\ & \text { 17:30:0 } \end{aligned}$ |  |
| Municipality: Thorold <br> Site \#: 1822100007 <br> Intersection: Thorold Stone Rd - RR 58 (Davis Ri <br> TFR File \#: 9 <br> Count date: 19-Jun-18 |  |  |  |  |  |  |  | Weat <br> Perso | her | conditio <br> ) who | On |  |  |  |  |
| ** Signalized Intersection ** |  |  |  |  |  |  |  | Major Road: Thorold Stone Rd-RR 58 (Davis Rı |  |  |  |  |  |  |  |
| North Leg Total: <br> North Entering: <br> North Peds: <br> Peds Cross: | $\begin{aligned} & \text { l: } 51 \\ & 29 \\ & 0 \\ & \hline \end{aligned}$ |  | Heavys <br> Trucks <br> Cars <br> Totals | 0 <br> 1 <br> 23 <br> 24 | 0 0 2 2 | 0 0 3 3 | $\left.\right\|^{0} 1$ |  |  | Heavys <br> Trucks <br> Cars <br> Totals | $\frac{14}{22}$ |  | East Le <br> East En <br> East Pe <br> Peds C | Total: tering: ds: ross | $\begin{aligned} & 2429 \\ & 1183 \\ & 0 \\ & 8 \end{aligned}$ |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Comments |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

## Ontario Traffic Inc.

## Total Count Diagram



Comments

## Ontario Traffic Inc. Traffic Count Summary

| Intersection: Thorold Stone Rd - RR 58 (Davis F | Count Date: 19-Jun-18 | Municipality: Thorold |
| :--- | :--- | :--- | :--- |





## Ontario Traffic Inc.

## Total Count Diagram



Comments

## Ontario Traffic Inc. Traffic Count Summary

| Intersection: Thorold Stone Rd - RR 58 (Davis F | Count Date: 14-Jun-18 | Municipality: Thorold |
| :--- | :--- | :--- | :--- |





## Ontario Traffic Inc.

## Total Count Diagram



Comments

## Ontario Traffic Inc. Traffic Count Summary





## Ontario Traffic Inc.

## Total Count Diagram



Comments

## Ontario Traffic Inc. Traffic Count Summary



| Ontario Traffic Inc. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Morning Peak Diagram |  |  |  | Specified Period <br> From: 6:00:00 <br> To: 9:00:00 |  |  | One Hour Peak  <br> From: 7:30:00 <br> To: $8: 30: 00$ |  |  |
| Municipality: Thorold <br> Site \#: 1822100006 <br> Intersection: RR 58 (Davis Rd) \& Beaverdams R <br> TFR File \#: 9 <br> Count date: 19-Jun-18 |  |  |  | Weather conditions: <br> Person(s) who counted: |  |  |  |  |  |
| ** Signalized Intersection ** |  |  |  | Major Road: RR 58 (Davis Rd) runs N/S |  |  |  |  |  |
| North Leg Total: 832 <br> North Entering: 308 <br> North Peds: 0 <br> Peds Cross: | Heavys 2 <br> Trucks 5 <br> Cars 34 <br> Totals 41 | 8 <br> 88 <br> 137 <br> 183 | 0 10 <br> 1 44 <br> 83 254 <br>   <br> 84  |  | Heavys <br> Trucks <br> Cars <br> Totals | 9 <br> 41 <br> 474 <br> 524 |  | East Leg East En East Pe Peds | Total: 341 <br> ering: 188 <br> ds: 0 <br> loss: $\mathbb{Z}$ |
|  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |
| Comments |  |  |  |  |  |  |  |  |  |



## Ontario Traffic Inc.

## Total Count Diagram



Comments

## Ontario Traffic Inc. Traffic Count Summary

Intersection: RR 58 (Davis Rd) \& Beaverdams | Count Date: 19-Jun-18 Municipality: Thorold


## Ontario Traffic Inc.

Count Date: 19-Jun-18 Site \#: 1822100006

| Interval <br> Time | Passenger Cars - North Approach |  |  |  |  |  | Trucks - North Approach |  |  |  |  |  | Heavys - North Approach |  |  |  |  |  | Pedestrians <br> North Cross |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Left |  | Thru |  | Right |  | Left |  | Thru |  | Right |  | Left |  | Thru |  | Right |  |  |  |
|  | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr |
| 5:45:00 | $0 \quad 0$ |  | $0 \quad 0$ |  | 00 |  | 00 |  | 00 |  | 00 |  | 00 |  | $0 \quad 0$ |  | $0 \quad 0$ |  | $0 \quad 0$ |  |
| 6:00:00 | $0 \quad 0$ |  | $0 \quad 0$ |  | $0 \quad 0$ |  | 0 0 |  | $0 \quad 0$ |  | 00 |  | 00 |  | 00 |  | $0 \quad 0$ |  | $0 \quad 0$ |  |
| 6:15:00 | $1 \quad 1$ |  | $11 \quad 11$ |  | 44 |  | 0 0 |  | $4 \quad 4$ |  | 11 |  | $0 \quad 0$ |  | $0 \quad 0$ |  | $0 \quad 0$ |  | $0 \quad 0$ |  |
| 6:30:00 | 98 |  | $39 \quad 28$ |  | 13 9 |  | $1 \quad 1$ |  | 51 |  | 10 |  | $0 \quad 0$ |  | $0 \quad 0$ |  | $0 \quad 0$ |  | $0 \quad 0$ |  |
| 6:45:00 | $20 \quad 11$ |  | $85 \quad 46$ |  | 2310 |  | 10 |  | 72 |  | 21 |  | $0 \quad 0$ |  | $0 \quad 0$ |  | $0 \quad 0$ |  | $0 \quad 0$ |  |
| 7:00:00 | $31 \quad 11$ |  | 13752 |  | $36 \quad 13$ |  | 10 |  | $11 \quad 4$ |  | 20 |  | $0 \quad 0$ |  | $0 \quad 0$ |  | $0 \quad 0$ |  | $0 \quad 0$ |  |
| 7:15:00 | $38 \quad 7$ |  | 162 25 |  | $40 \quad 4$ |  | 10 |  | $15 \quad 4$ |  | 20 |  | $0 \quad 0$ |  | $0 \quad 0$ |  | 00 |  | $0 \quad 0$ |  |
| 7:30:00 | $49 \quad 11$ |  | 196 34 |  | 48 8 |  | 10 |  | $22 \quad 7$ |  | 53 |  | $0 \quad 0$ |  | $2 \quad 2$ |  | $0 \quad 0$ |  | $0 \quad 0$ |  |
| 7:45:00 | $68 \quad 19$ |  | 226 30 |  | 53 5 |  | 10 |  | 3412 |  | 61 |  | $0 \quad 0$ |  | 53 |  | $0 \quad 0$ |  | $0 \quad 0$ |  |
| 8:00:00 | $90 \quad 22$ |  | 26943 |  | 6411 |  | 2 |  | 4410 |  | 7 |  | $0 \quad 0$ |  | $6 \quad 1$ |  | $2 \quad 2$ |  | $0 \quad 0$ |  |
| 8:15:00 | 113 23 |  | 29930 |  | 72 8 |  | 2 2 0 |  | $50 \quad 6$ |  | 8 |  | $0 \quad 0$ |  | 8 2 |  | 20 |  | 00 |  |
| 8:30:00 | 13219 |  | 333 34 |  | 8210 |  | 20 |  | $60 \quad 10$ |  | 10 2 |  | $0 \quad 0$ |  | $10-2$ |  | 20 |  | $0 \quad 0$ |  |
| 8:45:00 | 151 19 |  | 365 32 |  | $91 \quad 9$ |  | 31 |  | $64 \quad 4$ |  | 12 2 |  | $0 \quad 0$ |  | 11 1 |  | 20 |  | 00 |  |
| 9:00:00 | 17423 |  | $385 \quad 20$ |  | 10211 |  | 30 |  | 73 9 |  | $14 \quad 2$ |  | $0 \quad 0$ |  | $12 \quad 1$ |  | 20 |  | 0 0 |  |
| 9:01:13 | 1740 |  | 389 4 |  | 1031 |  | 30 |  | 730 |  | $14 \quad 0$ |  | $0 \quad 0$ |  | 12 0 |  | 20 |  | 00 |  |
| 15:30:00 | 174 0 |  | 389 | 0 | 103 | 0 | 3 | 0 | 73 | 0 | 14 | 0 | 0 | 0 | 12 | 0 | 2 | 0 | 0 | 0 |
| 15:45:00 | 174 | 0 | 389 | 0 | 103 | 0 | 3 | 0 | 73 | 0 | 14 | 0 | 0 | 0 | 12 | 0 | 2 | 0 | 0 | 0 |
| 16:00:00 | 174 | 0 | 389 | 0 | 103 | 0 | 3 | 0 | 73 | 0 | 14 | 0 | 0 | 0 | 12 | 0 | 2 | 0 | 0 | 0 |
| 16:15:00 | 210 | 36 | 436 | 47 | 124 | 21 | 4 | 1 | 83 | 10 | 15 | 1 | 0 | 0 | 13 | 1 | 2 | 0 | 0 | 0 |
| 16:30:00 | 262 | 52 | 483 | 47 | 152 | 28 | 4 | 0 | 90 | 7 | 16 | 1 | 0 | 0 | 13 | 0 | 2 | 0 | 0 | 0 |
| 16:45:00 | 303 | 41 | 541 | 58 | 172 | 20 | 4 | 0 | 95 | 5 | 16 | 0 | 0 | 0 | 14 | 1 | 2 | 0 | 0 | 0 |
| 17:00:00 | 339 | 36 | 587 | 46 | 192 | 20 | 6 | 2 | 96 | 1 | 17 | 1 | 1 | 1 | 14 | 0 | 2 | 0 | 0 | 0 |
| 17:15:00 | 373 | 34 | 626 | 39 | 211 | 19 | 7 | 1 | 99 | 3 | 17 | 0 | 1 | 0 | 14 | 0 | 2 | 0 | 0 | 0 |
| 17:30:00 | 410 | 37 | 682 | 56 | 236 | 25 | 9 | 2 | 103 | 4 | 17 | 0 | 1 | 0 | 14 | 0 | 2 | 0 | 0 | 0 |
| 17:45:00 | 432 | 22 | 746 | 64 | 261 | 25 | 10 | 1 | 107 | 4 | 18 | 1 | 1 | 0 | 14 | 0 | 2 | 0 | 0 | 0 |
| 18:00:00 | 460 | 28 | 779 | 33 | 276 | 15 | 11 | 1 | 107 | 0 | 19 | 1 | 1 | 0 | 14 | 0 | 2 | 0 | 0 | 0 |
| 18:15:00 | 478 | 18 | 817 | 38 | 302 | 26 | 11 | 0 | 107 | 0 | 19 | 0 | 1 | 0 | 14 | 0 | 2 | 0 | 0 | 0 |
| 18:30:00 | 492 | 14 | 865 | 48 | 333 | 31 | 11 | 0 | 109 | 2 | 19 | 0 | 1 | 0 | 14 | 0 | 3 | 1 | 0 | 0 |
| 18:45:00 | 509 | 17 | 898 | 33 | 355 | 22 | 12 | 1 | 110 | 1 | 19 | 0 | 1 | 0 | 14 | 0 | 3 | 0 | 0 | 0 |
| 19:00:00 | 525 | 16 | 933 | 35 | 375 | 20 | 13 | 1 | 111 | 1 | 19 | 0 | 1 | 0 | 14 | 0 | 3 | 0 | 0 | 0 |
| 19:00:17 | 525 | 0 | 935 | 2 | 375 | 0 | 13 | 0 | 111 | 0 | 19 | 0 | 1 | 0 | 14 | 0 | 3 | 0 | 0 | 0 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

## Ontario Traffic Inc.

Count Date: 19-Jun-18 Site \#: 1822100006

| Interval Time | Passenger Cars - East Approach |  |  |  |  |  | Trucks - East Approach |  |  |  |  |  | Heavys - East Approach |  |  |  |  |  | Pedestrians East Cross |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Left |  | Thru |  | Right |  | Left |  | Thru |  | Right |  | Left |  | Thru |  | Right |  |  |  |
|  | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr |
| 5:45:00 | $0 \quad 0$ |  | $0 \quad 0$ |  | $0 \quad 0$ |  | $0 \quad 0$ |  | $0 \quad 0$ |  | $0 \quad 0$ |  | $0 \quad 0$ |  | $0 \quad 0$ |  | $0 \quad 0$ |  | $0 \quad 0$ |  |
| 6:00:00 | $0 \quad 0$ |  | $0 \quad 0$ |  | 0 | 0 | $0 \quad 0$ |  | $0 \quad 0$ |  | 00 |  | $0 \quad 0$ |  | $0 \quad 0$ |  | 00 |  | $0 \quad 0$ |  |
| 6:15:00 | $3 \quad 3$ |  |  |  | 6 | 6 | $0 \quad 0$ |  | $0 \quad 0$ |  | $0 \quad 0$ |  | $0 \quad 0$ |  | $0 \quad 0$ |  | $0 \quad 0$ |  | $0 \quad 0$ |  |
| 6:30:00 | 63 |  | $\begin{array}{ll}2 & 2 \\ 5 & 3\end{array}$ |  | 18 | 12 | $0 \quad 0$ |  | $0 \quad 0$ |  | $0 \quad 0$ |  | $0 \quad 0$ |  | $0 \quad 0$ |  | $0 \quad 0$ |  | $0 \quad 0$ |  |
| 6:45:00 | $8 \quad 2$ |  | $\begin{array}{ll}5 & 3 \\ 9 & 4\end{array}$ |  | 33 | 15 | $0 \quad 0$ |  | 00 |  | 00 |  | 00 |  | 00 |  | 00 |  | $0 \quad 0$ |  |
| 7:00:00 | 13 5 |  | $\begin{array}{rr}9 & 4 \\ 18 & 9\end{array}$ |  | 48 | 15 | $0 \quad 0$ |  | 11 |  | 00 |  | 00 |  | 00 |  | 00 |  | $0 \quad 0$ |  |
| 7:15:00 | 15 2 |  | $27 \quad 9$ |  | 63 | 15 | 00 |  | 10 |  | 00 |  | 00 |  | 00 |  | 00 |  | $0 \quad 0$ |  |
| 7:30:00 | 23 8 |  | $34 \quad 7$ |  | 83 | 20 | 11 |  | 10 |  | 00 |  | 00 |  | 00 |  | 00 |  | $0 \quad 0$ |  |
| 7:45:00 | $27 \quad 4$ |  | 439 |  | 110 | 27 | 21 |  | 21 |  | 00 |  | 00 |  | 00 |  | 00 |  | $0 \quad 0$ |  |
| 8:00:00 | $35 \quad 8$ |  | 46 3 |  | 149 | 39 | 20 |  | 31 |  | 00 |  | 00 |  | 00 |  | 00 |  | $0 \quad 0$ |  |
| 8:15:00 | $41 \quad 6$ |  | 493 |  | 187 | 38 | 20 |  | 30 |  | 2 2 |  | 00 |  | 00 |  | $0 \quad 0$ |  | $0 \quad 0$ |  |
| 8:30:00 | 49 8 |  | $50 \quad 1$ |  | 223 | 36 | 20 |  | 30 |  | 20 |  | $0 \quad 0$ |  | $0 \quad 0$ |  | 11 |  | $0 \quad 0$ |  |
| 8:45:00 | 51 2 |  | 51 1 |  | 259 | 36 | 20 |  | 30 |  | 42 |  | 00 |  | $0 \quad 0$ |  | 10 |  | 00 |  |
| 9:00:00 | $55 \quad 4$ |  | 57 6 |  | 288 | 29 | 20 |  | 30 |  | 6 2 |  | 00 |  | $0 \quad 0$ |  | 10 |  | 00 |  |
| 9:01:13 | 55 0 |  | 58 1 |  | 293 | 5 | 20 |  | 30 |  | 60 |  | 00 |  | $0 \quad 0$ |  | 10 |  | $0 \quad 0$ |  |
| 15:30:00 | 550 |  | 58 0 |  | 293 | 0 | 20 |  | 30 |  | 60 |  | 00 |  | 00 |  | 10 |  | 00 |  |
| 15:45:00 | 550 |  | 58 0 |  | 293 | 0 | 20 |  | 30 |  | 60 |  | 00 |  | $0 \quad 0$ |  | 1 | 0 | 0 | 0 |
| 16:00:00 | 55 | 0 | 58 | 0 | 293 | 0 | 2 | 0 | 3 | 0 | 6 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 |
| 16:15:00 | 62 | 7 | 68 | 10 | 328 | 35 | 3 | 1 | 3 | 0 | 6 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 |
| 16:30:00 | 68 | 6 | 81 | 13 | 358 | 30 | 3 | 0 | 3 | 0 | 6 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 |
| 16:45:00 | 80 | 12 | 89 | 8 | 394 | 36 | 3 | 0 | 3 | 0 | 7 | 1 | 0 | 0 | 0 | 0 | 2 | 1 | 0 | 0 |
| 17:00:00 | 90 | 10 | 95 | 6 | 427 | 33 | 3 | 0 | 3 | 0 | 8 | 1 | 0 | 0 | 0 | 0 | 3 | 1 | 0 | 0 |
| 17:15:00 | 100 | 10 | 105 | 10 | 457 | 30 | 3 | 0 | 3 | 0 | 8 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 |
| 17:30:00 | 111 | 11 | 112 | 7 | 486 | 29 | 5 | 2 | 3 | 0 | 8 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 |
| 17:45:00 | 115 | 4 | 120 | 8 | 518 | 32 | 5 | 0 | 4 | 1 | 8 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 |
| 18:00:00 | 121 | 6 | 133 | 13 | 539 | 21 | 5 | 0 | 4 | 0 | 9 | 1 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 |
| 18:15:00 | 126 | 5 | 140 | 7 | 563 | 24 | 5 | 0 | 5 | 1 | 9 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 |
| 18:30:00 | 132 | 6 | 166 | 26 | 588 | 25 | 5 | 0 | 6 | 1 | 9 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 |
| 18:45:00 | 139 | 7 | 175 | 9 | 603 | 15 | 5 | 0 | 6 | 0 | 10 | 1 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 |
| 19:00:00 | 142 | 3 | 179 | 4 | 618 | 15 | 5 | 0 | 6 | 0 | 11 | 1 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 |
| 19:00:17 | 142 | 0 | 179 | 0 | 618 | 0 | 5 | 0 | 6 | 0 | 11 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

## Ontario Traffic Inc.

Count Date: 19-Jun-18 Site \#: 1822100006

| Interval <br> Time | Passenger Cars - South Approach |  |  |  |  |  | Trucks - South Approach |  |  |  |  |  | Heavys - South Approach |  |  |  |  |  | Pedestrians South Cross |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Left |  | Thru |  | Right |  | Left |  | Thru |  | Right |  | Left |  | Thru |  | Right |  |  |  |
|  | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr |
| 5:45:00 | $0 \quad 0$ |  | $0 \quad 0$ |  | $0 \quad 0$ |  | 00 |  | 00 |  | 00 |  | $0 \quad 0$ |  | $0 \quad 0$ |  | $0 \quad 0$ |  | $0 \quad 0$ |  |
| 6:00:00 | $0 \quad 0$ |  | 00 |  | $0 \quad 0$ |  | 0 0 |  | $0 \quad 0$ |  | 00 |  | 00 |  | 00 |  | $0 \quad 0$ |  | $0 \quad 0$ |  |
| 6:15:00 | $0 \quad 0$ |  | 1616 |  | 3 3 |  | 0 0 |  | $4 \quad 4$ |  | $0 \quad 0$ |  | $0 \quad 0$ |  | $0 \quad 0$ |  | $0 \quad 0$ |  | $0 \quad 0$ |  |
| 6:30:00 |  |  | $41 \quad 25$ |  | 63 |  | 0 0 |  | 84 |  | $0 \quad 0$ |  | $0 \quad 0$ |  | $0 \quad 0$ |  | $0 \quad 0$ |  | $0 \quad 0$ |  |
| 6:45:00 | $\begin{array}{ll}0 & 0 \\ 0 & 0\end{array}$ |  | 8342 |  | 12 6 |  | 0 0 |  | $12 \quad 4$ |  | $0 \quad 0$ |  | $0 \quad 0$ |  | $0 \quad 0$ |  | $0 \quad 0$ |  | $0 \quad 0$ |  |
| 7:00:00 | $1 \quad 1$ |  | 125 42 |  | $20 \quad 8$ |  | 00 |  | 15 3 |  | $0 \quad 0$ |  | $0 \quad 0$ |  | $0 \quad 0$ |  | 0 0 |  | $0 \quad 0$ |  |
| 7:15:00 | 10 |  | 154 29 |  | $39 \quad 19$ |  | 00 |  | $25 \quad 10$ |  | $0 \quad 0$ |  | $0 \quad 0$ |  | $0 \quad 0$ |  | 0 0 |  | $0 \quad 0$ |  |
| 7:30:00 | 10 |  | 185 31 |  | $45 \quad 6$ |  | 00 |  | $27 \quad 2$ |  | 00 |  | $0 \quad 0$ |  | $0 \quad 0$ |  | $0 \quad 0$ |  | $0 \quad 0$ |  |
| 7:45:00 | 10 |  | 24459 |  | 53 8 |  | $1 \quad 1$ |  | $35 \quad 8$ |  | 11 |  | $0 \quad 0$ |  | 44 |  | 00 |  | $0 \quad 0$ |  |
| 8:00:00 | 10 |  | 29450 |  | 596 |  | 10 |  | $44 \quad 9$ |  | 10 |  | $0 \quad 0$ |  | 51 |  | 0 0 |  | 00 |  |
| 8:15:00 | 21 |  | 363 69 |  | 66 7 |  | 10 |  | 52 8 |  | 2 1 |  | $0 \quad 0$ |  | 61 |  | 00 |  | $0 \quad 0$ |  |
| 8:30:00 | 31 |  | $424 \quad 61$ |  | $75 \quad 9$ |  | 10 |  | 56 4 |  | 20 |  | 00 |  | 71 |  | $0 \quad 0$ |  | $0 \quad 0$ |  |
| 8:45:00 | 30 |  | 483 59 |  | $81 \quad 6$ |  | 21 |  | 63 7 |  | 20 |  | 00 |  | 92 |  | $0 \quad 0$ |  | 00 |  |
| 9:00:00 | 41 |  | 54057 |  | 86 5 |  | 20 |  | 7310 |  | 20 |  | $0 \quad 0$ |  | $10 \quad 1$ |  | $0 \quad 0$ |  | $0 \quad 0$ |  |
| 9:01:13 | 40 |  | 544 4 |  | 860 |  | 20 |  | $74 \quad 1$ |  | 20 |  | 00 |  | 10 0 |  | $0 \quad 0$ |  | 00 |  |
| 15:30:00 | 40 |  | 544 | 0 | 86 | 0 | 2 | 0 | 74 | 0 | 2 | 0 | 0 | 0 | 10 | 0 | 0 | 0 | 0 | 0 |
| 15:45:00 | 4 | 0 | 544 | 0 | 86 | 0 | 2 | 0 | 74 | 0 | 2 | 0 | 0 | 0 | 10 | 0 | 0 | 0 | 0 | 0 |
| 16:00:00 | 4 | 0 | 544 | 0 | 86 | 0 | 2 | 0 | 74 | 0 | 2 | 0 | 0 | 0 | 10 | 0 | 0 | 0 | 0 | 0 |
| 16:15:00 | 4 | 0 | 601 | 57 | 88 | 2 | 2 | 0 | 81 | 7 | 2 | 0 | 0 | 0 | 12 | 2 | 0 | 0 | 0 | 0 |
| 16:30:00 | 7 | 3 | 649 | 48 | 95 | 7 | 2 | 0 | 87 | 6 | 2 | 0 | 0 | 0 | 12 | 0 | 1 | 1 | 0 | 0 |
| 16:45:00 | 7 | 0 | 710 | 61 | 103 | 8 | 2 | 0 | 91 | 4 | 2 | 0 | 0 | 0 | 12 | 0 | 1 | 0 | 0 | 0 |
| 17:00:00 | 9 | 2 | 772 | 62 | 109 | 6 | 2 | 0 | 92 | 1 | 3 | 1 | 0 | 0 | 12 | 0 | 1 | 0 | 0 | 0 |
| 17:15:00 | 11 | 2 | 825 | 53 | 113 | 4 | 2 | 0 | 93 | 1 | 3 | 0 | 0 | 0 | 12 | 0 | 1 | 0 | 0 | 0 |
| 17:30:00 | 13 | 2 | 872 | 47 | 121 | 8 | 2 | 0 | 96 | 3 | 4 | 1 | 0 | 0 | 12 | 0 | 1 | 0 | 0 | 0 |
| 17:45:00 | 14 | 1 | 918 | 46 | 126 | 5 | 2 | 0 | 99 | 3 | 4 | 0 | 0 | 0 | 13 | 1 | 1 | 0 | 0 | 0 |
| 18:00:00 | 16 | 2 | 959 | 41 | 128 | 2 | 2 | 0 | 101 | 2 | 5 | 1 | 0 | 0 | 13 | 0 | 1 | 0 | 0 | 0 |
| 18:15:00 | 16 | 0 | 1005 | 46 | 134 | 6 | 2 | 0 | 102 | 1 | 5 | 0 | 0 | 0 | 13 | 0 | 1 | 0 | 0 | 0 |
| 18:30:00 | 18 | 2 | 1036 | 31 | 136 | 2 | 2 | 0 | 103 | 1 | 5 | 0 | 0 | 0 | 13 | 0 | 1 | 0 | 0 | 0 |
| 18:45:00 | 18 | 0 | 1076 | 40 | 144 | 8 | 2 | 0 | 103 | 0 | 5 | 0 | 0 | 0 | 14 | 1 | 1 | 0 | 0 | 0 |
| 19:00:00 | 19 | 1 | 1114 | 38 | 147 | 3 | 2 | 0 | 104 | 1 | 6 | 1 | 0 | 0 | 14 | 0 | 1 | 0 | 0 | 0 |
| 19:00:17 | 19 | 0 | 1114 | 0 | 147 | 0 | 2 | 0 | 104 | 0 | 6 | 0 | 0 | 0 | 14 | 0 | 1 | 0 | 0 | 0 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

## Ontario Traffic Inc.

Count Date: 19-Jun-18 Site \#: 1822100006

| Interval <br> Time | Passenger Cars - West Approach |  |  |  |  |  | Trucks - West Approach |  |  |  |  |  | Heavys - West Approach |  |  |  |  |  | Pedestrians <br> West Cross |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Left |  | Thru |  | Right |  | Left |  | Thru |  | Right |  | Left |  | Thru |  | Right |  |  |  |
|  | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr |
| 5:45:00 | $0 \quad 0$ |  | $0 \quad 0$ |  | $0 \quad 0$ |  | 00 |  | 00 |  | 00 |  | $0 \quad 0$ |  | $0 \quad 0$ |  | 00 |  | $0 \quad 0$ |  |
| 6:00:00 | $0 \quad 0$ |  | 0 | 0 | $0 \quad 0$ |  | $0 \quad 0$ |  | $0 \quad 0$ |  | 00 |  | $0 \quad 0$ |  | $0 \quad 0$ |  | 00 |  | 00 |  |
| 6:15:00 | $9 \quad 9$ |  | 1 | 1 | $0 \quad 0$ |  | $0 \quad 0$ |  | $0 \quad 0$ |  | 00 |  | $0 \quad 0$ |  | $0 \quad 0$ |  | 00 |  | 00 |  |
| 6:30:00 | 2516 |  | 12 | 11 | 11 |  | $0 \quad 0$ |  | $0 \quad 0$ |  | 00 |  | $0 \quad 0$ |  | $0 \quad 0$ |  | 00 |  | 00 |  |
| 6:45:00 | $54 \quad 29$ |  | 22 | 10 | 2 |  | 11 |  | $0 \quad 0$ |  | 00 |  | $0 \quad 0$ |  | $0 \quad 0$ |  | 00 |  | $0 \quad 0$ |  |
| 7:00:00 | $77 \quad 23$ |  | 27 | 5 | 3 |  | 10 |  | $0 \quad 0$ |  | 00 |  | $0 \quad 0$ |  | $0 \quad 0$ |  | $0 \quad 0$ |  | $0 \quad 0$ |  |
| 7:15:00 | 10124 |  | 32 | 5 | 41 |  | 21 |  | 22 |  | 00 |  | $0 \quad 0$ |  | $0 \quad 0$ |  | 00 |  | $0 \quad 0$ |  |
| 7:30:00 | 11413 |  | 41 | 9 | 51 |  | 20 |  | 31 |  | 00 |  | $0 \quad 0$ |  | $0 \quad 0$ |  | $0 \quad 0$ |  | $0 \quad 0$ |  |
| 7:45:00 | $138 \quad 24$ |  | 54 | 13 | $8 \quad 3$ |  | 42 |  | 41 |  | 00 |  | $0 \quad 0$ |  | $0 \quad 0$ |  | $0 \quad 0$ |  | 00 |  |
| 8:00:00 | $164 \quad 26$ |  | 62 | 8 | $10 \quad 2$ |  | 51 |  | 40 |  | 00 |  | 11 |  | 00 |  | 00 |  | 00 |  |
| 8:15:00 | 18420 |  | 70 | 8 | 10 0 |  | 11 6 |  | 40 |  | 00 |  | 10 |  | $0 \quad 0$ |  | $0 \quad 0$ |  | $0 \quad 0$ |  |
| 8:30:00 | 20925 |  | 76 | 6 | 11 1 |  | 12 |  | 51 |  | 00 |  | 10 |  | 00 |  | 00 |  | 00 |  |
| 8:45:00 | 237 28 |  | 88 | 12 | 13 2 |  | 14 2 |  | 50 |  | 00 |  | 10 |  | $0 \quad 0$ |  | 00 |  | $0 \quad 0$ |  |
| 9:00:00 | $266 \quad 29$ |  | 95 | 7 | 130 |  | 15 |  | 50 |  | 00 |  | 21 |  | 00 |  | 00 |  | 00 |  |
| 9:01:13 | 268 2 |  | 95 | 0 | 130 |  | 15 0 |  | 50 |  | 00 |  | 20 |  | 00 |  | $0 \quad 0$ |  | $0 \quad 0$ |  |
| 15:30:00 | 268 0 |  | 95 | 0 | 130 |  | 15 0 |  | 50 |  | 00 |  | 20 |  | 00 |  | 00 |  | $0 \quad 0$ |  |
| 15:45:00 | 268 0 |  | 95 | 0 | 130 |  | 15 0 |  | 50 |  | 00 |  | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 16:00:00 | 268 | 0 | 95 | 0 | 13 | 0 | 15 | 0 | 5 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 16:15:00 | 295 | 27 | 105 | 10 | 13 | 0 | 15 | 0 | 5 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 16:30:00 | 315 | 20 | 113 | 8 | 15 | 2 | 16 | 1 | 5 | 0 | 0 | 0 | 3 | 1 | 0 | 0 | 0 | 0 | 0 | 0 |
| 16:45:00 | 337 | 22 | 120 | 7 | 16 | 1 | 16 | 0 | 5 | 0 | 1 | 1 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 17:00:00 | 355 | 18 | 127 | 7 | 16 | 0 | 16 | 0 | 5 | 0 | 1 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 17:15:00 | 379 | 24 | 135 | 8 | 17 | 1 | 16 | 0 | 6 | 1 | 1 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 17:30:00 | 399 | 20 | 143 | 8 | 17 | 0 | 16 | 0 | 7 | 1 | 1 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 17:45:00 | 421 | 22 | 151 | 8 | 19 | 2 | 16 | 0 | 7 | 0 | 1 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 18:00:00 | 440 | 19 | 167 | 16 | 22 | 3 | 16 | 0 | 8 | 1 | 1 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 18:15:00 | 455 | 15 | 183 | 16 | 22 | 0 | 16 | 0 | 8 | 0 | 1 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 18:30:00 | 474 | 19 | 190 | 7 | 26 | 4 | 17 | 1 | 8 | 0 | 1 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 18:45:00 | 493 | 19 | 198 | 8 | 27 | 1 | 17 | 0 | 8 | 0 | 1 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 19:00:00 | 510 | 17 | 202 | 4 | 29 | 2 | 17 | 0 | 9 | 1 | 1 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 19:00:17 | 510 | 0 | 202 | 0 | 29 | 0 | 17 | 0 | 9 | 0 | 1 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |




## Ontario Traffic Inc.

## Total Count Diagram



Comments

## Ontario Traffic Inc. Traffic Count Summary

| Intersection: RR 58 (Davis Rd) \& Beaverdams \| Count Date: 14-Jun-18 | Municipality: Thorold |
| :--- | :--- | :--- |



## Ontario Traffic Inc.

Count Date: 14-Jun-18 Site \#: 1822100012

| Interval <br> Time | Passenger Cars - North Approach |  |  |  |  |  | Trucks - North Approach |  |  |  |  |  | Heavys - North Approach |  |  |  |  |  | Pedestrians |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Left |  | Thru |  | Right |  | Left |  | Thru |  | Right |  | Left |  | Thru |  | Right |  | North Cross |  |
|  | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr |
| 6:00:00 | $0 \quad 0$ |  | $0 \quad 0$ |  | $0 \quad 0$ |  | 00 |  | $0 \quad 0$ |  | 00 |  | $0 \quad 0$ |  | 0 0 |  | 00 |  | $0 \quad 0$ |  |
| 6:15:00 | $3 \quad 3$ |  | $17 \quad 17$ |  | $4 \quad 4$ |  | $0 \quad 0$ |  | $2 \quad 2$ |  | 00 |  | $0 \quad 0$ |  | $0 \quad 0$ |  | 00 |  | 00 |  |
| 6:30:00 | $7 \quad 4$ |  | $56 \quad 39$ |  | $10 \quad 6$ |  | $0 \quad 0$ |  | 42 |  | 00 |  | $0 \quad 0$ |  | $0 \quad 0$ |  | $0 \quad 0$ |  | 00 |  |
| 6:45:00 | 2215 |  | 10650 |  | 19 9 |  | $0 \quad 0$ |  | 6 2 |  | 11 |  | $0 \quad 0$ |  | $0 \quad 0$ |  | $0 \quad 0$ |  | 00 |  |
| 7:00:00 | $32 \quad 10$ |  | 157 51 |  | $36 \quad 17$ |  | $0 \quad 0$ |  | $8 \quad 2$ |  | 10 |  | $0 \quad 0$ |  | 11 |  | $0 \quad 0$ |  | 00 |  |
| 7:15:00 | 408 |  | 193 36 |  | $42 \quad 6$ |  | $0 \quad 0$ |  | $12 \quad 4$ |  | 21 |  | $0 \quad 0$ |  | 10 |  | $0 \quad 0$ |  | $0 \quad 0$ |  |
| 7:30:00 | 48 8 |  | 234 41 |  | 5614 |  | 11 |  | 208 |  | 31 |  | 11 |  | 43 |  | 11 |  | $0 \quad 0$ |  |
| 7:45:00 | 6416 |  | 270 36 |  | 64 8 |  | 21 |  | $29 \quad 9$ |  | 30 |  | 10 |  | 6 2 |  | 10 |  | $0 \quad 0$ |  |
| 8:00:00 | $86 \quad 22$ |  | 308 38 |  | $77 \quad 13$ |  | 20 |  | $38 \quad 9$ |  | 41 |  | 10 |  | $8 \quad 2$ |  | $3 \quad 2$ |  | 00 |  |
| 8:15:00 | 10216 |  | 341 33 |  | 83 6 |  | 20 |  | $40 \quad 2$ |  | 51 |  | 21 |  | 102 |  | 30 |  | $0 \quad 0$ |  |
| 8:30:00 | 126 24 |  | 369 28 |  | $92 \quad 9$ |  | 20 |  | $44 \quad 4$ |  | 6 1 |  | 20 |  | 11 1 |  | 41 |  | $0 \quad 0$ |  |
| 8:45:00 | 14216 |  | 403 34 |  | 10412 |  | 20 |  | $51 \quad 7$ |  | 71 |  | 20 |  | 12 1 |  | 40 |  | $0 \quad 0$ |  |
| 9:00:00 | 157 15 |  | 435 32 |  | 118 14 |  | 42 |  | $54 \quad 3$ |  | 81 |  | 20 |  | 13 1 |  | 40 |  | $0 \quad 0$ |  |
| 9:00:08 | 157 0 |  | 4350 |  | 118 0 |  | 40 |  | 540 |  | 80 |  | 20 |  | 130 |  | 40 |  | $0 \quad 0$ |  |
| 16:00:00 | 157 0 |  | 4350 |  | 118 0 |  | 40 |  | $54 \quad 0$ |  | 80 |  | 20 |  | 130 |  | 40 |  | $0 \quad 0$ |  |
| 16:15:00 | 20043 |  | 479 | 44 | 139 | 21 | 4 | 0 | 57 | 3 | 11 | 3 | 2 | 0 | 14 | 1 | 4 | 0 | 0 | 0 |
| 16:30:00 | 236 | 36 | 532 | 53 | 175 | 36 | 4 | 0 | 65 | 8 | 12 | 1 | 2 | 0 | 15 | 1 | 5 | 1 | 0 | 0 |
| 16:45:00 | 280 | 44 | 589 | 57 | 194 | 19 | 4 | 0 | 69 | 4 | 12 | 0 | 3 | 1 | 15 | 0 | 5 | 0 | 0 | 0 |
| 17:00:00 | 327 | 47 | 651 | 62 | 226 | 32 | 5 | 1 | 71 | 2 | 12 | 0 | 3 | 0 | 15 | 0 | 5 | 0 | 0 | 0 |
| 17:15:00 | 370 | 43 | 720 | 69 | 254 | 28 | 6 | 1 | 72 | 1 | 12 | 0 | 3 | 0 | 15 | 0 | 5 | 0 | 0 | 0 |
| 17:30:00 | 404 | 34 | 783 | 63 | 291 | 37 | 6 | 0 | 78 | 6 | 12 | 0 | 3 | 0 | 15 | 0 | 6 | 1 | 0 | 0 |
| 17:45:00 | 433 | 29 | 860 | 77 | 317 | 26 | 6 | 0 | 79 | 1 | 12 | 0 | 3 | 0 | 15 | 0 | 6 | 0 | 0 | 0 |
| 18:00:00 | 459 | 26 | 921 | 61 | 338 | 21 | 6 | 0 | 81 | 2 | 12 | 0 | 3 | 0 | 15 | 0 | 6 | 0 | 0 | 0 |
| 18:15:00 | 494 | 35 | 974 | 53 | 356 | 18 | 6 | 0 | 83 | 2 | 13 | 1 | 3 | 0 | 15 | 0 | 6 | 0 | 0 | 0 |
| 18:30:00 | 517 | 23 | 1018 | 44 | 377 | 21 | 6 | 0 | 85 | 2 | 13 | 0 | 3 | 0 | 15 | 0 | 7 | 1 | 0 | 0 |
| 18:45:00 | 534 | 17 | 1057 | 39 | 402 | 25 | 6 | 0 | 86 | 1 | 13 | 0 | 3 | 0 | 15 | 0 | 7 | 0 | 0 | 0 |
| 19:00:00 | 551 | 17 | 1096 | 39 | 418 | 16 | 6 | 0 | 90 | 4 | 13 | 0 | 3 | 0 | 15 | 0 | 7 | 0 | 0 | 0 |
| 19:00:04 | 551 | 0 | 1096 | 0 | 418 | 0 | 6 | 0 | 90 | 0 | 13 | 0 | 3 | 0 | 15 | 0 | 7 | 0 | 0 | 0 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

## Ontario Traffic Inc.

Count Date: 14-Jun-18 Site \#: 1822100012

| Interval <br> Time | Passenger Cars - East Approach |  |  |  |  |  | Trucks - East Approach |  |  |  |  |  | Heavys - East Approach |  |  |  |  |  | Pedestrians <br> East Cross |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Left |  | Thru |  | Right |  | Left |  | Thru |  | Right |  | Left |  | Thru |  | Right |  |  |  |
|  | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr |
| 6:00:00 | $0 \quad 0$ |  | $0 \quad 0$ |  | $0 \quad 0$ |  | 00 |  | $0 \quad 0$ |  | $0 \quad 0$ |  | $0 \quad 0$ |  | $0 \quad 0$ |  | 00 |  | 00 |  |
| 6:15:00 | $2 \quad 2$ |  | $3 \quad 3$ |  | $7 \begin{array}{ll}7 & 7\end{array}$ |  | $0 \quad 0$ |  | 00 |  | 00 |  | $0 \quad 0$ |  | $0 \quad 0$ |  | 00 |  | $0 \quad 0$ |  |
| 6:30:00 | 97 |  | $5 \quad 2$ |  | $17 \quad 10$ |  | $0 \quad 0$ |  | 00 |  | 00 |  | $0 \quad 0$ |  | $0 \quad 0$ |  | 00 |  | 00 |  |
| 6:45:00 | 11 2 |  | $7 \quad 2$ |  | $37 \quad 20$ |  | $0 \quad 0$ |  | 00 |  | 11 |  | $0 \quad 0$ |  | $0 \quad 0$ |  | $0 \quad 0$ |  | $0 \quad 0$ |  |
| 7:00:00 | 12 1 |  | 13 6 |  | $51 \quad 14$ |  | $2 \quad 2$ |  | 00 |  | 10 |  | $0 \quad 0$ |  | $0 \quad 0$ |  | 00 |  | 00 |  |
| 7:15:00 | 131 |  | 23 | 10 | $62 \quad 11$ |  | 20 |  | $0 \quad 0$ |  | 10 |  | $0 \quad 0$ |  | $0 \quad 0$ |  | $0 \quad 0$ |  | $0 \quad 0$ |  |
| 7:30:00 | 15 2 |  | 46 | 23 | 7513 |  | 20 |  | $0 \quad 0$ |  | 21 |  | $0 \quad 0$ |  | 11 |  | $0 \quad 0$ |  | $0 \quad 0$ |  |
| 7:45:00 | 18 3 |  | 50 | 4 | 102 27 |  | 42 |  | $0 \quad 0$ |  | 20 |  | $0 \quad 0$ |  | 10 |  | $0 \quad 0$ |  | $0 \quad 0$ |  |
| 8:00:00 | $20 \quad 2$ |  | 55 | 5 | 150 48 |  | 51 |  | $0 \quad 0$ |  | 20 |  | $0 \quad 0$ |  | 10 |  | 00 |  | 00 |  |
| 8:15:00 | $24 \quad 4$ |  | 57 | 2 | 205 55 |  | 6 1 |  | 11 |  | 31 |  | $0 \quad 0$ |  | 10 |  | 00 |  | 00 |  |
| 8:30:00 | $34 \quad 10$ |  | 62 | 5 | 241 36 |  | 60 |  | 21 |  | 30 |  | 00 |  | 10 |  | 00 |  | $0 \quad 0$ |  |
| 8:45:00 | $36 \quad 2$ |  | 64 | 2 | 287 46 |  | $6 \quad 0$ |  | 20 |  | 41 |  | $0 \quad 0$ |  | 10 |  | 11 |  | $0 \quad 0$ |  |
| 9:00:00 | $45 \quad 9$ |  | 67 | 3 | 322 35 |  | 60 |  | 20 |  | 6 2 |  | $0 \quad 0$ |  | 10 |  | 10 |  | $0 \quad 0$ |  |
| 9:00:08 | 450 |  | 67 | 0 | 3220 |  | 60 |  | 20 |  | 60 |  | $0 \quad 0$ |  | 10 |  | 10 |  | 00 |  |
| 16:00:00 | 450 |  | 67 | 0 | 3220 |  | 60 |  | 20 |  | 60 |  | $0 \quad 0$ |  | 10 |  | 10 |  | $0 \quad 0$ |  |
| 16:15:00 | 51 6 |  | 86 | 19 | 353 31 |  | 60 |  | 31 |  | 60 |  | 00 |  | 21 |  | 10 |  | 00 |  |
| 16:30:00 | 59 8 |  | 98 | 12 | 388 35 |  | 6 | 0 | 3 | 0 | 6 | 0 | 0 | 0 | 2 | 0 | 1 | 0 | 0 | 0 |
| 16:45:00 | 63 | 4 | 108 | 10 | 424 | 36 | 7 | 1 | 4 | 1 | 6 | 0 | 0 | 0 | 2 | 0 | 2 | 1 | 0 | 0 |
| 17:00:00 | 74 | 11 | 120 | 12 | 462 | 38 | 7 | 0 | 4 | 0 | 7 | 1 | 0 | 0 | 2 | 0 | 2 | 0 | 0 | 0 |
| 17:15:00 | 93 | 19 | 131 | 11 | 505 | 43 | 7 | 0 | 4 | 0 | 7 | 0 | 0 | 0 | 2 | 0 | 2 | 0 | 0 | 0 |
| 17:30:00 | 105 | 12 | 147 | 16 | 542 | 37 | 7 | 0 | 4 | 0 | 7 | 0 | 0 | 0 | 2 | 0 | 2 | 0 | 0 | 0 |
| 17:45:00 | 112 | 7 | 159 | 12 | 573 | 31 | 7 | 0 | 4 | 0 | 7 | 0 | 0 | 0 | 2 | 0 | 2 | 0 | 0 | 0 |
| 18:00:00 | 114 | 2 | 177 | 18 | 603 | 30 | 7 | 0 | 5 | 1 | 7 | 0 | 0 | 0 | 2 | 0 | 2 | 0 | 0 | 0 |
| 18:15:00 | 120 | 6 | 187 | 10 | 634 | 31 | 7 | 0 | 5 | 0 | 7 | 0 | 0 | 0 | 2 | 0 | 2 | 0 | 0 | 0 |
| 18:30:00 | 128 | 8 | 190 | 3 | 664 | 30 | 7 | 0 | 5 | 0 | 8 | 1 | 0 | 0 | 2 | 0 | 2 | 0 | 0 | 0 |
| 18:45:00 | 130 | 2 | 195 | 5 | 680 | 16 | 7 | 0 | 5 | 0 | 8 | 0 | 0 | 0 | 2 | 0 | 2 | 0 | 0 | 0 |
| 19:00:00 | 134 | 4 | 200 | 5 | 704 | 24 | 7 | 0 | 5 | 0 | 8 | 0 | 0 | 0 | 2 | 0 | 2 | 0 | 0 | 0 |
| 19:00:04 | 134 | 0 | 200 | 0 | 704 | 0 | 7 | 0 | 5 | 0 | 8 | 0 | 0 | 0 | 2 | 0 | 2 | 0 | 0 | 0 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

## Ontario Traffic Inc.

Count Date: 14-Jun-18 Site \#: 1822100012

| Interval <br> Time | Passenger Cars - South Approach |  |  |  |  |  | Trucks - South Approach |  |  |  |  |  | Heavys - South Approach |  |  |  |  |  | Pedestrians South Cross |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Left |  | Thru |  | Right |  | Left |  | Thru |  | Right |  | Left |  | Thru |  | Right |  |  |  |
|  | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr |
| 6:00:00 | $0 \quad 0$ |  | $0 \quad 0$ |  | $0 \quad 0$ |  | 00 |  | 00 |  | $0 \quad 0$ |  | $0 \quad 0$ |  | 0 0 |  | 00 |  | $0 \quad 0$ |  |
| 6:15:00 | 00 |  | 18 18 |  | $0 \quad 0$ |  | $0 \quad 0$ |  | $3 \quad 3$ |  | 00 |  | $0 \quad 0$ |  | $0 \quad 0$ |  | 00 |  | 00 |  |
| 6:30:00 | $0 \quad 0$ |  | $59 \quad 41$ |  | $4 \quad 4$ |  | $0 \quad 0$ |  | 6 3 |  | 00 |  | $0 \quad 0$ |  | $0 \quad 0$ |  | 00 |  | 00 |  |
| 6:45:00 | 11 |  | 100 41 |  | 95 |  | $0 \quad 0$ |  | 14 8 |  | 11 |  | $0 \quad 0$ |  | 00 |  | $0 \quad 0$ |  | 00 |  |
| 7:00:00 | 21 |  | 138 38 |  | 15 6 |  | $0 \quad 0$ |  | $20 \quad 6$ |  | 10 |  | $0 \quad 0$ |  | 11 |  | $0 \quad 0$ |  | 00 |  |
| 7:15:00 | 20 |  | 177 | 39 | 20 5 |  | $0 \quad 0$ |  | $29 \quad 9$ |  | 21 |  | $0 \quad 0$ |  | 21 |  | 00 |  | $0 \quad 0$ |  |
| 7:30:00 | 42 |  | 225 | 48 | 23 3 |  | $0 \quad 0$ |  | $38 \quad 9$ |  | 20 |  | $0 \quad 0$ |  | 20 |  | $0 \quad 0$ |  | $0 \quad 0$ |  |
| 7:45:00 | 51 |  | 268 | 43 | $31 \quad 8$ |  | $0 \quad 0$ |  | 43 5 |  | 20 |  | 11 |  | $6 \quad 4$ |  | $1 \begin{array}{ll}1 & 1\end{array}$ |  | $0 \quad 0$ |  |
| 8:00:00 | 61 |  | 327 | 59 | $37 \quad 6$ |  | 11 |  | $52 \quad 9$ |  | 20 |  | 10 |  | 8 2 |  | 10 |  | 00 |  |
| 8:15:00 | 60 |  | 368 | 41 | 425 |  | 21 |  | 61 9 |  | 20 |  | 10 |  | 11 3 |  | 10 |  | 00 |  |
| 8:30:00 | $6 \quad 0$ |  | 438 | 70 | $53 \quad 11$ |  | 20 |  | 68 7 |  | 31 |  | 10 |  | $13-2$ |  | 10 |  | $0 \quad 0$ |  |
| 8:45:00 | $8 \quad 2$ |  | 484 | 46 | $57 \quad 4$ |  | 20 |  | $77 \quad 9$ |  | 41 |  | 10 |  | 15 2 |  | 10 |  | $0 \quad 0$ |  |
| 9:00:00 | 91 |  | 534 | 50 | 60 3 |  | 20 |  | 86 9 |  | 40 |  | 10 |  | 16 1 |  | 10 |  | $0 \quad 0$ |  |
| 9:00:08 | 90 |  | 535 | 1 | $60 \quad 0$ |  | 20 |  | 860 |  | 40 |  | 10 |  | 160 |  | 10 |  | $0 \quad 0$ |  |
| 16:00:00 | 90 |  | 535 | 0 | $60 \quad 0$ |  | 20 |  | 860 |  | 40 |  | 10 |  | 16 0 |  | 10 |  | 00 |  |
| 16:15:00 | 90 |  | 590 | 55 | $70 \quad 10$ |  | 20 |  | $94 \quad 8$ |  | 40 |  | 10 |  | 17 1 |  | 10 |  | $0 \quad 0$ |  |
| 16:30:00 | 10 1 |  | 641 | 51 | 73 | 3 | 2 | 0 | 97 | 3 | 6 | 2 | 1 | 0 | 18 | 1 | 1 | 0 | 0 | 0 |
| 16:45:00 | 11 | 1 | 702 | 61 | 80 | 7 | 2 | 0 | 104 | 7 | 6 | 0 | 1 | 0 | 19 | 1 | 1 | 0 | 0 | 0 |
| 17:00:00 | 13 | 2 | 770 | 68 | 86 | 6 | 2 | 0 | 109 | 5 | 6 | 0 | 1 | 0 | 19 | 0 | 1 | 0 | 0 | 0 |
| 17:15:00 | 13 | 0 | 840 | 70 | 105 | 19 | 2 | 0 | 113 | 4 | 6 | 0 | 1 | 0 | 19 | 0 | 1 | 0 | 0 | 0 |
| 17:30:00 | 14 | 1 | 920 | 80 | 108 | 3 | 2 | 0 | 118 | 5 | 7 | 1 | 1 | 0 | 19 | 0 | 1 | 0 | 0 | 0 |
| 17:45:00 | 16 | 2 | 980 | 60 | 109 | 1 | 2 | 0 | 121 | 3 | 7 | 0 | 1 | 0 | 20 | 1 | 1 | 0 | 0 | 0 |
| 18:00:00 | 17 | 1 | 1036 | 56 | 114 | 5 | 2 | 0 | 124 | 3 | 7 | 0 | 1 | 0 | 20 | 0 | 1 | 0 | 0 | 0 |
| 18:15:00 | 26 | 9 | 1103 | 67 | 117 | 3 | 2 | 0 | 126 | 2 | 7 | 0 | 1 | 0 | 20 | 0 | 1 | 0 | 0 | 0 |
| 18:30:00 | 28 | 2 | 1162 | 59 | 117 | 0 | 2 | 0 | 128 | 2 | 7 | 0 | 1 | 0 | 20 | 0 | 1 | 0 | 0 | 0 |
| 18:45:00 | 28 | 0 | 1200 | 38 | 119 | 2 | 2 | 0 | 130 | 2 | 7 | 0 | 1 | 0 | 21 | 1 | 1 | 0 | 0 | 0 |
| 19:00:00 | 29 | 1 | 1229 | 29 | 120 | 1 | 2 | 0 | 130 | 0 | 7 | 0 | 1 | 0 | 21 | 0 | 1 | 0 | 0 | 0 |
| 19:00:04 | 29 | 0 | 1229 | 0 | 120 | 0 | 2 | 0 | 130 | 0 | 7 | 0 | 1 | 0 | 21 | 0 | 1 | 0 | 0 | 0 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

## Ontario Traffic Inc.

Count Date: 14-Jun-18 Site \#: 1822100012

| Interval <br> Time | Passenger Cars - West Approach |  |  |  |  |  | Trucks - West Approach |  |  |  |  |  | Heavys - West Approach |  |  |  |  |  | Pedestrians <br> West Cross |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Left |  | Thru |  | Right |  | Left |  | Thru |  | Right |  | Left |  | Thru |  | Right |  |  |  |
|  | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr |
| 6:00:00 | $0 \quad 0$ |  | $0 \quad 0$ |  | $0 \quad 0$ |  | 00 |  | $0 \quad 0$ |  | $0 \quad 0$ |  | $0 \quad 0$ |  | $0 \quad 0$ |  | 00 |  | $0 \quad 0$ |  |
| 6:15:00 | $13 \quad 13$ |  | $3 \quad 3$ |  | $0 \quad 0$ |  | 00 |  | $0 \quad 0$ |  | 00 |  | $0 \quad 0$ |  | $0 \quad 0$ |  | 00 |  | 00 |  |
| 6:30:00 | $35 \quad 22$ |  | $5 \quad 2$ |  | 00 |  | 00 |  | $0 \quad 0$ |  | 00 |  | $0 \quad 0$ |  | $0 \quad 0$ |  | 00 |  | 00 |  |
| 6:45:00 | $60 \quad 25$ |  | 11 6 |  | $3 \quad 3$ |  | $0 \quad 0$ |  | $0 \quad 0$ |  | 00 |  | $0 \quad 0$ |  | $0 \quad 0$ |  | 00 |  | 00 |  |
| 7:00:00 | $76 \quad 16$ |  | 16 5 |  | 4 |  | $0 \quad 0$ |  | $0 \quad 0$ |  | 00 |  | $0 \quad 0$ |  | $0 \quad 0$ |  | 00 |  | 00 |  |
| 7:15:00 | $105 \quad 29$ |  | $23 \quad 7$ |  | 5 |  | $1 \quad 1$ |  | $0 \quad 0$ |  | 00 |  | $0 \quad 0$ |  | $0 \quad 0$ |  | 00 |  | $0 \quad 0$ |  |
| 7:30:00 | $121 \quad 16$ |  | 3310 |  | 50 |  | 43 |  | 22 |  | $0 \quad 0$ |  | 11 |  | $0 \quad 0$ |  | $0 \quad 0$ |  | 11 |  |
| 7:45:00 | 157 36 |  | $40 \quad 7$ |  | 8 3 |  | 51 |  | 20 |  | 11 |  | 10 |  | 22 |  | $0 \quad 0$ |  | 10 |  |
| 8:00:00 | 17619 |  | $44 \quad 4$ |  | 11 3 |  | 50 |  | 20 |  | 10 |  | 21 |  | 31 |  | 00 |  | 10 |  |
| 8:15:00 | $205 \quad 29$ |  | 48 4 |  | 110 |  | $7 \quad 2$ |  | 20 |  | 10 |  | 31 |  | 30 |  | 00 |  | 10 |  |
| 8:30:00 | 236 31 |  | 54 6 |  | 14 3 |  | $10 \quad 3$ |  | 20 |  | 21 |  | 30 |  | 30 |  | 00 |  | 10 |  |
| 8:45:00 | 261 25 |  | 63 9 |  | 140 |  | 12 2 |  | 3 |  | 20 |  | 41 |  | 30 |  | 00 |  | 10 |  |
| 9:00:00 | 287 26 |  | 68 5 |  | 19 5 |  | 14 2 |  | 30 |  | 20 |  | 6 2 |  | 30 |  | 00 |  | 10 |  |
| 9:00:08 | 287 0 |  | 68 0 |  | 190 |  | 14 0 |  | 30 |  | 20 |  | 60 |  | 30 |  | 00 |  | 10 |  |
| 16:00:00 | 287 0 |  | 68 0 |  | 19 0 |  | 14 0 |  | 30 |  | 20 |  | 60 |  | 30 |  | 00 |  | 10 |  |
| 16:15:00 | 31023 |  | 74 | 6 | 20 | 1 | 14 | 0 | 4 | 1 | 2 | 0 | 7 | 1 | 3 | 0 | 0 | 0 | 1 | 0 |
| 16:30:00 | 335 | 25 | 87 | 13 | 21 | 1 | 15 | 1 | 4 | 0 | 2 | 0 | 7 | 0 | 3 | 0 | 0 | 0 | 1 | 0 |
| 16:45:00 | 361 | 26 | 96 | 9 | 21 | 0 | 15 | 0 | 5 | 1 | 3 | 1 | 7 | 0 | 3 | 0 | 1 | 1 | 1 | 0 |
| 17:00:00 | 376 | 15 | 105 | 9 | 21 | 0 | 16 | 1 | 5 | 0 | 3 | 0 | 7 | 0 | 3 | 0 | 1 | 0 | 1 | 0 |
| 17:15:00 | 401 | 25 | 111 | 6 | 22 | 1 | 16 | 0 | 5 | 0 | 3 | 0 | 7 | 0 | 3 | 0 | 1 | 0 | 1 | 0 |
| 17:30:00 | 425 | 24 | 118 | 7 | 23 | 1 | 16 | 0 | 5 | 0 | 3 | 0 | 7 | 0 | 3 | 0 | 1 | 0 | 1 | 0 |
| 17:45:00 | 444 | 19 | 122 | 4 | 24 | 1 | 16 | 0 | 5 | 0 | 3 | 0 | 7 | 0 | 3 | 0 | 1 | 0 | 1 | 0 |
| 18:00:00 | 467 | 23 | 125 | 3 | 25 | 1 | 17 | 1 | 5 | 0 | 3 | 0 | 7 | 0 | 3 | 0 | 1 | 0 | 1 | 0 |
| 18:15:00 | 494 | 27 | 128 | 3 | 27 | 2 | 18 | 1 | 5 | 0 | 3 | 0 | 7 | 0 | 3 | 0 | 1 | 0 | 2 | 1 |
| 18:30:00 | 511 | 17 | 132 | 4 | 28 | 1 | 18 | 0 | 5 | 0 | 3 | 0 | 7 | 0 | 3 | 0 | 1 | 0 | 2 | 0 |
| 18:45:00 | 531 | 20 | 134 | 2 | 28 | 0 | 18 | 0 | 5 | 0 | 3 | 0 | 7 | 0 | 3 | 0 | 1 | 0 | 2 | 0 |
| 19:00:00 | 546 | 15 | 137 | 3 | 29 | 1 | 18 | 0 | 5 | 0 | 3 | 0 | 7 | 0 | 3 | 0 | 1 | 0 | 2 | 0 |
| 19:00:04 | 546 | 0 | 137 | 0 | 29 | 0 | 18 | 0 | 5 | 0 | 3 | 0 | 7 | 0 | 3 | 0 | 1 | 0 | 2 | 0 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |




## Ontario Traffic Inc.

## Total Count Diagram



Comments

## Ontario Traffic Inc. Traffic Count Summary





## Ontario Traffic Inc.

## Total Count Diagram



Comments

## Ontario Traffic Inc. Traffic Count Summary





## Ontario Traffic Inc.

## Total Count Diagram



Comments

## Ontario Traffic Inc. Traffic Count Summary

Intersection: Hwy 20 (Lundy's Lane) \& RR 58 ([ Count Date: 19-Jun-18 $\quad$ Municipality: Thorold




## Ontario Traffic Inc.

## Total Count Diagram



Comments

## Ontario Traffic Inc. Traffic Count Summary

Intersection: Hwy 20 (Lundy's Lane) \& RR 58 ([ Count Date: 14-Jun-18 $\quad$ Municipality: Thorold




## Ontario Traffic Inc.

## Total Count Diagram



Comments

## Ontario Traffic Inc. Traffic Count Summary





## Ontario Traffic Inc.

## Total Count Diagram



Comments

## Ontario Traffic Inc. Traffic Count Summary





## Ontario Traffic Inc.

## Total Count Diagram



Comments

## Ontario Traffic Inc. Traffic Count Summary



| Signal Code: H58DVS |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Intersection: HWY 58 \& DAVIS RD./THOROLD STONE RD. |  |  |  |  |  |  |
| Municipality: thorold |  |  |  |  |  |  |
| Owner: MTO |  |  |  |  |  |  |
| Last Modified: 4/24/2019 10:46:51 AM |  |  |  |  |  |  |
| Timing Parameters | EBD \& WBD THOROLD STONE RD. | NBD HWY 58 (SPLIT) | SBD DAVIS RD. (SPLIT) | n/a | n/a | n/a |
| Min Green | 20 | 10 | 10 | 0 | 0 | 0 |
| Walk | 15 | 15 | 15 | 0 | 0 | 0 |
| Ped Clearance | 7 | 7 | 7 | 0 | 0 | 0 |
| Vehicle Ext. | 4.5 | 3 | 3 | 0 | 0 | 0 |
| Max Green | 32 | 38 | 15 | 0 | 0 | 0 |
| Yellow | 5.7 | 5.4 | 5.4 | 0 | 0 | 0 |
| All Red | 2 | 2 | 1.5 | 0 | 0 | 0 |


|  |  | Offset |
| :--- | :---: | :---: |
| Minimum Cycle | 45.1 | 0 |
| Pedestrian Cycle | 59.1 |  |
| Maximum Cycle | 107 | 0 |
| Operation | FA |  |

Installed On:
8/23/1999
Count Date:
--/--/----
FA = Fully Actuated
SA = Semi Actuated
FT = Fixed Time
*Note: you need to change the paper orientation from Portriat to Landscape

| Signal Code: 057070 |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Intersection: RR57 (THOROLD STONE RD, ) \& RR70 (THOROLD TOWNLINE RD.) |  |  |  |  |  |  |
| Municipality: thorold |  |  |  |  |  |  |
| Owner: MTO |  |  |  |  |  |  |
| Last Modified: 12/10/2013 9:50:43 AM |  |  |  |  |  |  |
| Timing Parameters | $\begin{aligned} & \hline \text { EBD ADVANCE } \\ & \text { THOROLD } \\ & \text { STONE RD. } \\ & \hline \end{aligned}$ | EBD \& WBD <br> THRU THOROLD <br> STONE RD. | NBD \& SBD <br> THRU THOROLD <br> TOWNLINE RD. | n/a | n/a | n/a |
| Min Green | 8 | 10 | 10 | 0 | 0 | 0 |
| Walk | 0 | 11 | 15 | 0 | 0 | 0 |
| Ped Clearance | 0 | 18 | 25 | 0 | 0 | 0 |
| Vehicle Ext. | 2.5 | 6 | 2.3 | 0 | 0 | 0 |
| Max Green | 20 | 44 | 35 | 0 | 0 | 0 |
| Yellow | 3 | 4.1 | 4.1 | 0 | 0 | 0 |
| All Red | 0 | 2 | 2.3 | 0 | 0 | 0 |


|  |  | Offset |
| :--- | :---: | :---: |
| Minimum Cycle | 32.5 | 0 |
| Pedestrian Cycle | 81.5 |  |
| Maximum Cycle | 114.5 | 0 |
| Operation | FA |  |

Installed On:
6/12/2003
Count Date:
5/10/2012
FA = Fully Actuated
SA = Semi Actuated
FT = Fixed Time

* Note: you need to change the paper orientation from Portriat to Landscape

| Signal Code: H58BVR |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Intersection: Highway 58 \& Beaverdams Rd. |  |  |  |  |  |  |
| Municipality: thorold |  |  |  |  |  |  |
| Owner: mto |  |  |  |  |  |  |
| Last Modified: 5/29/2015 8:46:42 AM |  |  |  |  |  |  |
| Timing Parameters | NBD \& SBD THRU HWY 58 | EBD \& WBD THRU BEAVERDAMS RD. | n/a | n/a | n/a | n/a |
| Min Green | 25 | 10 | 0 | 0 | 0 | 0 |
| Walk | 10 | 11 | 0 | 0 | 0 | 0 |
| Ped Clearance | 15 | 19 | 0 | 0 | 0 | 0 |
| Vehicle Ext. | 5 | 3 | 0 | 0 | 0 | 0 |
| Max Green | 45 | 35 | 0 | 0 | 0 | 0 |
| Yellow | 5 | 5 | 0 | 0 | 0 | 0 |
| All Red | 2 | 3.1 | 0 | 0 | 0 | 0 |


|  |  | Offset |
| :--- | :---: | :---: |
| Minimum Cycle | 50.1 | 0 |
| Pedestrian Cycle | 70.1 |  |
| Maximum Cycle | 95.1 | 0 |
| Operation | FA |  |

Installed On:
5/29/2015
Count Date:
--/--/----
FA = Fully Actuated
SA = Semi Actuated
FT = Fixed Time

* Note: you need to change the paper orientation from Portriat to Landscape

Copyright 2001 © Regional Niagara


* Note: you need to change the paper orientation from Portriat to Landscape

Copyright 2001 © Regional Niagara

| Signal Code: 070H20 |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Intersection: RR70 (TOWNLINE RD.) \& HWY 20 (LUNDYS LANE) |  |  |  |  |  |  |
| Municipality: thorold |  |  |  |  |  |  |
| Owner: MTO |  |  |  |  |  |  |
| Last Modified: 3/28/2018 11:28:16 AM |  |  |  |  |  |  |
| Timing Parameters | $\begin{array}{\|c\|} \hline \text { EBD \& WBD } \\ \text { LUNDY'S LANE } \\ \hline \end{array}$ | NBD \& SBD TOWNLINE RD. | -- | n/a | -- | -- |
| Min Green | 20 | 10 | 0 | 0 | 0 | 0 |
| Walk | 15 | 15 | 0 | 0 | 0 | 0 |
| Ped Clearance | 7 | 14 | 0 | 0 | 0 | 0 |
| Vehicle Ext. | 5 | 5 | 0 | 0 | 0 | 0 |
| Max Green | 50 | 40 | 0 | 0 | 0 | 0 |
| Yellow | 5 | 4 | 0 | 0 | 0 | 0 |
| All Red | 2 | 2 | 0 | 0 | 0 | 0 |


|  |  | Offset |
| :--- | :---: | :---: |
| Minimum Cycle | 43 | 0 |
| Pedestrian Cycle | 64 |  |
| Maximum Cycle | 103 | 0 |
| Operation | FA |  |

Installed On:
5/2/2001
Count Date:
5/14/2008
FA = Fully Actuated
SA = Semi Actuated
FT = Fixed Time
*Note: you need to change the paper orientation from Portriat to Landscape
Copyright 2001 © Regional Niagara

## APPENDIX C

## Capacity Analysis

## Timings

1: Davis Road \& Thorold Stone Road
<2018 Existing> AM Peak Hour

|  | $\rangle$ | $\rightarrow$ | 7 | $\dagger$ |  | 4 | $\uparrow$ | 1 | $\checkmark$ | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \% | ¢ $\uparrow$ | $\overline{7}$ | \% | 个t | \% | $\uparrow$ | 7 | \% | $\uparrow$ | F |
| Traffic Volume (vph) | 21 | 866 | 226 | 67 | 1053 | 398 | 15 | 149 | 1 | 2 | 18 |
| Future Volume (vph) | 21 | 866 | 226 | 67 | 1053 | 398 | 15 | 149 | 1 | 2 | 18 |
| Turn Type | Perm | NA | Perm | Perm | NA | Split | NA | Perm | Split | NA | Perm |
| Protected Phases |  | 2 |  |  | 6 | 4 | 4 |  | 8 | 8 |  |
| Permitted Phases | 2 |  | 2 | 6 |  |  |  | 4 |  |  | 8 |
| Detector Phase | 2 | 2 | 2 | 6 | 6 | 4 | 4 | 4 | 8 | 8 | 8 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 20.0 | 20.0 | 20.0 | 20.0 | 20.0 | 10.0 | 10.0 | 10.0 | 10.0 | 10.0 | 10.0 |
| Minimum Split (s) | 28.9 | 28.9 | 28.9 | 28.9 | 28.9 | 29.7 | 29.7 | 29.7 | 21.7 | 21.7 | 21.7 |
| Total Split (s) | 39.7 | 39.7 | 39.7 | 39.7 | 39.7 | 45.4 | 45.4 | 45.4 | 21.9 | 21.9 | 21.9 |
| Total Split (\%) | 37.1\% | 37.1\% | 37.1\% | 37.1\% | 37.1\% | 42.4\% | 42.4\% | 42.4\% | 20.5\% | 20.5\% | 20.5\% |
| Yellow Time (s) | 5.4 | 5.4 | 5.4 | 5.4 | 5.4 | 5.7 | 5.7 | 5.7 | 5.7 | 5.7 | 5.7 |
| All-Red Time (s) | 1.5 | 1.5 | 1.5 | 1.5 | 1.5 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 6.9 | 6.9 | 6.9 | 6.9 | 6.9 | 7.7 | 7.7 | 7.7 | 7.7 | 7.7 | 7.7 |
| Lead/Lag |  |  |  |  |  |  |  |  |  |  |  |
| Lead-Lag Optimize? |  |  |  |  |  |  |  |  |  |  |  |
| Recall Mode | C-Max | C-Max | C-Max | Max | Max | None | None | None | None | None | None |
| Act Efft Green (s) | 62.8 | 62.8 | 62.8 | 62.8 | 62.8 | 22.5 | 22.5 | 22.5 | 10.0 | 10.0 | 10.0 |
| Actuated g/C Ratio | 0.59 | 0.59 | 0.59 | 0.59 | 0.59 | 0.21 | 0.21 | 0.21 | 0.09 | 0.09 | 0.09 |
| $\mathrm{V} / \mathrm{C}$ Ratio | 0.12 | 0.45 | 0.26 | 0.29 | 0.55 | 0.66 | 0.66 | 0.36 | 0.01 | 0.01 | 0.08 |
| Control Delay | 18.8 | 16.4 | 6.0 | 21.4 | 18.2 | 47.5 | 47.7 | 7.3 | 44.0 | 44.5 | 0.7 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 18.8 | 16.4 | 6.0 | 21.4 | 18.2 | 47.5 | 47.7 | 7.3 | 44.0 | 44.5 | 0.7 |
| LOS | B | B | A | C | B | D | D | A | D | D | A |

Approach Delay
Approach Delay
Approach LOS
Intersection Summary
Cycle Length: 107
th: 107
ffset: 0 ( $0 \%$ ), Referenced to phase 2:EBTL, Start of Green
Natural Cycle: 85
$\begin{array}{ll}\text { Control Type: Actuated-Coordinated } & \\ \text { Maximum v/C Ratio: } 0.66 & \\ \text { Intersection Signal Delay: 20.4 } & \text { Intersection LOS: C } \\ \begin{array}{ll}\text { Intersection Capacity } & \text { Utilization } 82.0 \% \\ \text { Analysis Period (min) } 15 & \text { ICU Level of Service D }\end{array}\end{array}$
Analysis Period (min) 15


[^0]Synchro 10 Report
1: Davis Road \& Thorold Stone Road
 $\begin{array}{lrrrrrrrrrrrr}18 \\ \text { Future Volume (vph) } & 21 & 866 & 226 & 67 & 1053 & 6 & 398 & 15 & 149 & 1 & 2 & 18 \\ \text { Ideat Flow (vphpl) } & 1900 & 1900 & 1900 & 1900 & 1900 & 1900 & 1900 & 1900 & 1900 & 1900 & 1900 & 1900 \\ \text { Total Lost time (s) } & 6.9 & 6.9 & 6.9 & 6.9 & 6.9 & & 7.7 & 7.7 & 7.7 & 7.7 & 7.7 & 7.7 \\ \text { Las } & 100 & & 105 & \end{array}$

|  |  |  |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Total Lost time (s) | 6.9 | 6.9 | 6.9 | 6.9 | 6.9 | 7.7 | 7.7 | 7.7 | 7.7 | 7.7 | 7.7 |
| Lane Util. Factor | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 0.95 | 0.95 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.99 | 1.00 | 1.00 | 0.99 |


| Frpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.99 | 1.00 | 1.00 | 0.99 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
|  | 1.00 | 1.00 | 0.05 | 1.00 | 1.00 | 1.0 | 1.00 | 00 | 1.00 | 1.00 | 0.05 |


|  | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| FIt | Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 0.95 | 0.96 | 1.00 | 0.95 | 1.00 |


| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 0.95 | 0.96 | 1.00 | 0.95 | 1.00 | 1.00 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Satd. Flow (prot) | 1640 | 3406 | 1442 | 1530 | 3398 | 1559 | 1549 | 1475 | 1388 | 1624 | 1338 |
| Flt Permitted | 0.19 | 1.00 | 1.00 | 0.26 | 1.00 | 0.95 | 0.96 | 1.00 | 0.95 | 1.00 | 1.00 |


|  |  |  |  |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Satd. Flow (perm) | 321 | 3406 | 1442 | 416 | 3398 |  | 1559 | 1549 | 1475 | 1388 | 1624 | 1338 |
| Peak-hour factor, PHF | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | Adj. Flow (vph) dJ. How Reduction


| TOR Reduction (vph) | 0 | 0 | 79 | 0 | 0 | 0 | 0 | 0 | 122 | 0 | 0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 22 | 902 | 156 | 70 | 03 | 0 | 216 | 15 | 33 | 1 | 2 |



| Heary Vehicles (\%) | $10 \%$ | $6 \%$ | $12 \%$ | $18 \%$ | $6 \%$ | $30 \%$ | $10 \%$ | $28 \%$ | $8 \%$ | $30 \%$ | $17 \%$ | $19 \%$ |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Uurn Type | Perm | NA | Perm | Perm | NA |  | Split | NA | Perm | Split | NA | Perm |

$$
\begin{aligned}
& \text { Iurn Iype } \\
& \text { Protected Phases }
\end{aligned}
$$

Potetected Phases
Actuated Green, G (s) 58

Effective Green, $g$ (s)


Clearance Time (s)

|  |  |  |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
|  | 6.9 | 6.9 | 6.9 | 6.9 | 6.9 | 7.7 | 7.7 | 7.7 | 7.7 | 7.7 | 7.7 |
| Lanicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 |
| s Ratio Prot | 174 | 1852 | 784 | 226 | 1848 | 327 | 325 | 310 | 51 | 60 | 50 |
|  |  | 0.26 |  |  | co 32 | 0.14 | co 0.14 |  | 0.00 | c 0.00 |  |

v/s Ratio Prot
/s Ratio Perm $\quad 0.07$

|  | 0.13 | 0.49 | 0.20 | 0.31 | 0.60 | 0.66 | 0.66 | 0.11 | 0.02 | 0.03 | 0.01 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


|  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


| Incremental Delay, d2 | 1.5 | 0.9 | 0.6 | 3.5 | 1.4 | 5.9 | 6.0 | 0.3 | 0.3 | 0.4 | 0.2 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


| Delay (s) | 13.4 | 16.1 | 13.0 | 16.9 | 17.9 |  | 44.6 | 44.7 | 34.4 | 49.9 | 50.0 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
|  |  | 49 | 8 |  |  |  |  |  |  |  |  |


| Level of Service | B | B | B | B | B | D | D | C | D |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Approach Delay (s) | 15.4 |  | 17.8 |  | 42.0 |  | 49 |  |  |
| Approach LOS | B |  |  | B |  | D |  | D |  |


| Intersection Summary |  |  |  |
| :--- | ---: | :--- | ---: |
| HCM 2000 Control Delay | 21.9 | HCM 2000 Level of Service | C |
| HCM 2000 Volume to Capacity ratio | 0.59 | Sum of lost time (s) | 22.3 |
| Actuated Cycle Length (s) | 107.0 |  |  |


| Actuated Cycle Length (s) | 0.59 |
| :--- | ---: |

Intersection Capacity Utilization
82.0\%

CU Level of Service
D
c Critical Lane Group

Timings
2: Davis Road \& Niagara Falls Road/Beaverdams Road



[^1]Synchro 10 Report

HCM Signalized Intersection Capacity Analysis
2: Davis Road \& Niagara Falls Road/Beaverdams Road
2. Davis Road \& Niagara Falls Road/Beaverdams Road 0 09-14-2021
 otal Lost time (s) Lane

| Lane Util. Factor | 1.00 | 1.00 |
| :--- | ---: | ---: |
| Frt | 0.09 | 0.89 |
| Flt Protected | 0.96 | 0.99 |


| Fit Protected | 0.96 | 0.99 |
| :--- | :--- | :--- |
| Satd. Flow (prot) | 1667 | 1629 |
| FIt Permitted | 0.66 | 0.96 |


|  | 0.66 |  |  | 0.96 |  |  | $\begin{aligned} & 1388 \\ & 0.64 \end{aligned}$ | 1.00 |  | $\begin{array}{r} 1787 \\ 0.56 \end{array}$ | 1.00 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Flt Permitted |  |  |  |  | 1 |  |  |  |  |  |
| Satd. Flow (perm) |  | 1138 |  |  |  |  | 1569 |  | 932 | 3113 |  | 1054 | 2983 | 13 |
| Peak-hour factor, PHF | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |  |
| Adj. Flow (vph) | 116 | 33 | 7 | 25 | 18 | 175 | 4 | 281 | 32 | 86 | 181 |  |


| RTOR Reduction (vph) | 0 | 1 | 0 | 0 | 74 | 0 | 0 | 13 | 0 | 0 | 0 | 34 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |


| ane Group Flow (vph) | 0 | 155 | 0 | 0 | 144 | 0 | 4 | 300 | 0 | 86 | 181 | 12 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Heavy Vehicles (\%) | $10 \%$ | $7 \%$ | $7 \%$ | $7 \%$ | $12 \%$ | $2 \%$ | $30 \%$ | $15 \%$ | $7 \%$ | $1 \%$ | $21 \%$ | $16 \%$ |
| Turn Type | Perm | NA |  | Perm | NA |  | Perm | NA |  | Perm | NA | Perm | Turn Ty



| Actuated Green, G $(\mathbf{s})$ | 55.0 | 55.0 | 25.0 | 25.0 | 25.0 | 25.0 | 25.0 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Effective Green, $(\mathrm{s})$ | 55.0 | 5.0 | 25.0 | 25.0 | 25.0 | 25.0 | 25.0 |
| Actuated g/C Ratio | 0.58 | 0.58 | 0.26 | 0.26 | 0.26 | 0.26 | 0.2 |

Actuated g/C Ratio
Vehicle Extension (s)
ane Grp Cap (vph)
/s Ratio Perm
V/s Ratio
$m$ Delay, d
Progression Factor
ncremental Delay, d2
Delay (s)
Level of Service
Approach Delay (s)
Approach LOS

| Intersection Summary |  |  |  |
| :--- | ---: | :--- | ---: |
| HCM 2000 Control Delay | 21.7 | HCM 2000 Level of Service | C |
| HCM 2000 Volume to Capacity ratio | 0.28 | Sum of lost time (s) | 15.1 |
| Actuated Cycle Length (s) | 95.1 | Sum |  |
| Intersection Capacity Utilization | $87.6 \%$ | ICU Level of Service | E |
| Analysis Period (min) | 15 |  |  |

c Critical Lane Group

Timings
3: Davis Road \& Lundys Lane

| Lane Group | EBL | EBT | WBL | WBT | WBR | NBL | NBT | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \% | F | 7 | $\uparrow$ | 7 | \% | F | \% | $\uparrow$ | 7 |
| Traffic Volume (vph) | 118 | 433 | 29 | 305 | 47 | 22 | 137 | 58 | 89 | 74 |
| Future Volume (vph) | 118 | 433 | 29 | 305 | 47 | 22 | 137 | 58 | 89 | 74 |
| Turn Type | Perm | NA | Perm | NA | Perm | Perm | NA | Perm | NA | Perm |
| Protected Phases |  | 2 |  | 6 |  |  | 4 |  | 8 |  |
| Permitted Phases | 2 |  | 6 |  | 6 | 4 |  | 8 |  | 8 |
| Detector Phase | 2 | 2 | 6 | 6 | 0 | 4 | 4 | 8 | 8 | 8 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 22.0 | 22.0 | 22.0 | 22.0 | 22.0 | 15.0 | 15.0 | 15.0 | 15.0 | 15.0 |
| Minimum Split (s) | 36.0 | 36.0 | 36.0 | 36.0 | 36.0 | 32.0 | 32.0 | 32.0 | 32.0 | 32.0 |
| Total Split (s) | 52.0 | 52.0 | 52.0 | 52.0 | 52.0 | 42.0 | 42.0 | 42.0 | 42.0 | 42.0 |
| Total Split (\%) | 55.3\% | 55.3\% | 55.3\% | 55.3\% | 55.3\% | 44.7\% | 44.7\% | 44.7\% | 44.7\% | 44.7\% |
| Yellow Time (s) | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| All-Red Time (s) | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |
| Lead/Lag |  |  |  |  |  |  |  |  |  |  |
| Lead-Lag Optimize? |  |  |  |  |  |  |  |  |  |  |
| Recall Mode | C-Max | C-Max | Max | Max | Max | None | None | None | None | None |
| Act Effct Green (s) | 63.5 | 63.5 | 63.5 | 63.5 | 63.5 | 16.5 | 16.5 | 16.5 | 16.5 | 16.5 |
| Actuated g/C Ratio | 0.68 | 0.68 | 0.68 | 0.68 | 0.68 | 0.18 | 0.18 | 0.18 | 0.18 | 0.18 |
| v/c Ratio | 0.19 | 0.39 | 0.06 | 0.28 | 0.05 | 0.12 | 0.61 | 0.36 | 0.35 | 0.26 |
| Control Delay | 7.0 | 8.2 | 6.3 | 7.2 | 2.0 | 33.2 | 43.2 | 39.6 | 37.4 | 9.8 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 7.0 | 8.2 | 6.3 | 7.2 | 2.0 | 33.2 | 43.2 | 39.6 | 37.4 | 9.8 |
| LOS | A | A | A | A | A | C | D | D | D | A |
| Approach Delay |  | 7.9 |  | 6.5 |  |  | 42.0 |  | 28.7 |  |
| Approach LOS |  | A |  | A |  |  | D |  | C |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 94 |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 94 |  |  |  |  |  |  |  |  |  |  |
| Offset: $0(0 \%)$, Referenced to phase 2:EBTL, Start of Green |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 70 |  |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Coordinated |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.61 |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 15.5 |  |  |  |  | tersection | LOS: B |  |  |  |  |
| Intersection Capacity Utilization 90.8\% |  |  |  |  | U Level | f Servic |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |



[^2]Synchro 10 Report

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \% | $\hat{\dagger}$ |  | \% | $\uparrow$ | F' | 7 | $\uparrow$ |  | \% | $\uparrow$ | 「 |
| Traffic Volume (vph) | 118 | 433 | 18 | 29 | 305 | 47 | 22 | 137 | 21 | 58 | 89 | 74 |
| Future Volume (vph) | 118 | 433 | 18 | 29 | 305 | 47 | 22 | 137 | 21 | 58 | 89 | 74 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 7.0 | 7.0 |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  | 7.0 | 7.0 | 7.0 |
| Lane Util. Factor | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 |
| Frpb, ped/bikes | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 |
| Flpb, ped/bikes | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 |
| Frt | 1.00 | 0.99 |  | 1.00 | 1.00 | 0.85 | 1.00 | 0.98 |  | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 |  | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |  | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1656 | 1821 |  | 1466 | 1743 | 1442 | 1444 | 1535 |  | 1530 | 1532 | 1392 |
| Flt Permitted | 0.56 | 1.00 |  | 0.46 | 1.00 | 1.00 | 0.70 | 1.00 |  | 0.61 | 1.00 | 1.00 |
| Satd. Flow (perm) | 984 | 1821 |  | 706 | 1743 | 1442 | 1057 | 1535 |  | 986 | 1532 | 1392 |
| Peak-hour factor, PHF | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 |
| Adj. Flow (vph) | 126 | 461 | 19 | 31 | 324 | 50 | 23 | 146 | 22 | 62 | 95 | 79 |
| RTOR Reduction (vph) | 0 | 1 | 0 | 0 | 0 | 16 | 0 | 7 | 0 | 0 | 0 | 65 |
| Lane Group Flow (vph) | 126 | 479 | 0 | 31 | 324 | 34 | 23 | 161 | 0 | 62 | 95 | 14 |
| Confl. Peds. (\#/hr) |  |  | 1 | 1 |  |  |  |  |  |  |  |  |
| Heavy Vehicles (\%) | 9\% | 3\% | 19\% | 23\% | 9\% | 12\% | 25\% | 20\% | 30\% | 18\% | 24\% | 16\% |
| Turn Type | Perm | NA |  | Perm | NA | Perm | Perm | NA |  | Perm | NA | Perm |
| Protected Phases |  | 2 |  |  | 6 |  |  | 4 |  |  | 8 |  |
| Permitted Phases | 2 |  |  | 6 |  | 6 | 4 |  |  | 8 |  | 8 |
| Actuated Green, G (s) | 63.5 | 63.5 |  | 63.5 | 63.5 | 63.5 | 16.5 | 16.5 |  | 16.5 | 16.5 | 16.5 |
| Effective Green, $\mathrm{g}(\mathrm{s})$ | 63.5 | 63.5 |  | 63.5 | 63.5 | 63.5 | 16.5 | 16.5 |  | 16.5 | 16.5 | 16.5 |
| Actuated g/C Ratio | 0.68 | 0.68 |  | 0.68 | 0.68 | 0.68 | 0.18 | 0.18 |  | 0.18 | 0.18 | 0.18 |
| Clearance Time (s) | 7.0 | 7.0 |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  | 7.0 | 7.0 | 7.0 |
| Vehicle Extension (s) | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 | 2.0 | 2.0 |  | 2.0 | 2.0 | 2.0 |
| Lane Grp Cap (vph) | 664 | 1230 |  | 476 | 1177 | 974 | 185 | 269 |  | 173 | 268 | 244 |
| v/s Ratio Prot |  | c0.26 |  |  | 0.19 |  |  | c0. 10 |  |  | 0.06 |  |
| v/s Ratio Perm | 0.13 |  |  | 0.04 |  | 0.02 | 0.02 |  |  | 0.06 |  | 0.01 |
| v/c Ratio | 0.19 | 0.39 |  | 0.07 | 0.28 | 0.03 | 0.12 | 0.60 |  | 0.36 | 0.35 | 0.06 |
| Uniform Delay, d1 | 5.7 | 6.7 |  | 5.2 | 6.1 | 5.1 | 32.7 | 35.7 |  | 34.1 | 34.1 | 32.3 |
| Progression Factor | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 0.6 | 0.9 |  | 0.3 | 0.6 | 0.1 | 0.1 | 2.4 |  | 0.5 | 0.3 | 0.0 |
| Delay (s) | 6.3 | 7.6 |  | 5.4 | 6.7 | 5.1 | 32.8 | 38.1 |  | 34.6 | 34.4 | 32.3 |
| Level of Service | A | A |  | A | A | A | C | D |  | C | C | C |
| Approach Delay (s) |  | 7.4 |  |  | 6.4 |  |  | 37.4 |  |  | 33.7 |  |
| Approach LOS |  | A |  |  | A |  |  | D |  |  | C |  |

## Approach LOS

Intersection Summary

| HCM 2000 Control Delay | 15.4 | HCM 2000 Level of Service | B |
| :--- | ---: | :--- | ---: |
| HCM 2000 Volume to Capacity ratio | 0.43 | Sum of lost time (s) | 14.0 |
| Actuated Cycle Length (s) | 94.0 | E |  |
| Intersection Capacity Utilization | $90.8 \%$ | ICU Level of Service | E |

tersection Ce Length (s)
tersection Capacity Utilization
90.8\%

ICU Level of Service
E

C Critical Lane Group

Timings
4: Thorold Townline Road \& Thorold Stone Road



[^3]HCM Signalized Intersection Capacity Analysis
<2018 Existing> AM Peak Hour 4: Thorold Townline Road \& Thorold Stone Road

9-14-202

|  | $\Rightarrow$ | $\rightarrow$ |  | $\downarrow$ |  |  |  | $\uparrow$ | $p$ | - | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \% | 个4 | $\stackrel{7}{ }$ | \% | 个4 | F | \% | F |  | 7 | F |  |
| Traffic Volume (vph) | 323 | 659 | 34 | 20 | 807 | 73 | 64 | 112 | 24 | 52 | 81 | 205 |
| Future Volume (vph) | 323 | 659 | 34 | 20 | 807 | 73 | 64 | 112 | 24 | 52 | 81 | 205 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 3.0 | 6.1 | 6.1 | 6.1 | 6.1 | 6.1 | 6.4 | 6.4 |  | 6.4 | 6.4 |  |
| Lane Util. Factor | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 |  |
| Frpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.97 | 1.00 | 1.00 |  | 1.00 | 1.00 |  |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 |  |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 0.97 |  | 1.00 | 0.89 |  |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |  | 0.95 | 1.00 |  |
| Satd. Flow (prot) | 1640 | 3471 | 1369 | 1444 | 3505 | 1454 | 1492 | 1596 |  | 1641 | 1446 |  |
| FIt Permitted | 0.27 | 1.00 | 1.00 | 0.39 | 1.00 | 1.00 | 0.23 | 1.00 |  | 0.61 | 1.00 |  |
| Satd. Flow (perm) | 460 | 3471 | 1369 | 594 | 3505 | 1454 | 365 | 1596 |  | 1058 | 1446 |  |
| Peak-hour factor, PHF | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 |
| Adj. Flow (vph) | 336 | 686 | 35 | 21 | 841 | 76 | 67 | 117 | 25 | 54 | 84 | 214 |
| RTOR Reduction (vph) | 0 | 0 | 10 | 0 | 0 | 34 | 0 | 8 | 0 | 0 | 94 | 0 |
| Lane Group Flow (vph) | 336 | 686 | 25 | 21 | 841 | 42 | 67 | 134 | 0 | 54 | 204 | 0 |
| Confl. Peds. (\#hr) | 4 |  |  |  |  | 4 |  |  |  |  |  |  |
| Heavy Vehicles (\%) | 10\% | 4\% | 18\% | 25\% | 3\% | 8\% | 21\% | 14\% | 25\% | 10\% | 18\% | 17\% |
| Turn Type | pm+pt | NA | Perm | Perm | NA | Perm | Perm | NA |  | Perm | NA |  |
| Protected Phases | 5 | 2 |  |  | 6 |  |  | 4 |  |  | 8 |  |
| Permitted Phases | 2 |  | 2 | 6 |  | 6 | 4 |  |  | 8 |  |  |
| Actuated Green, G (s) | 81.5 | 81.5 | 81.5 | 63.3 | 63.3 | 63.3 | 20.5 | 20.5 |  | 20.5 | 20.5 |  |
| Effective Green, g (s) | 81.5 | 81.5 | 81.5 | 63.3 | 63.3 | 63.3 | 20.5 | 20.5 |  | 20.5 | 20.5 |  |
| Actuated g/C Ratio | 0.71 | 0.71 | 0.71 | 0.55 | 0.55 | 0.55 | 0.18 | 0.18 |  | 0.18 | 0.18 |  |
| Clearance Time (s) | 3.0 | 6.1 | 6.1 | 6.1 | 6.1 | 6.1 | 6.4 | 6.4 |  | 6.4 | 6.4 |  |
| Vehicle Extension (s) | 2.5 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 2.3 | 2.3 |  | 2.3 | 2.3 |  |
| Lane Grp Cap (vph) | 484 | 2470 | 974 | 328 | 1937 | 803 | 65 | 285 |  | 189 | 258 |  |
| v/s Ratio Prot | c0.09 | 0.20 |  |  | 0.24 |  |  | 0.08 |  |  | 0.14 |  |
| v/s Ratio Perm | c0.40 |  | 0.02 | 0.04 |  | 0.03 | c0. 18 |  |  | 0.05 |  |  |
| v/c Ratio | 0.69 | 0.28 | 0.03 | 0.06 | 0.43 | 0.05 | 1.03 | 0.47 |  | 0.29 | 0.79 |  |
| Uniform Delay, d1 | 7.9 | 5.9 | 4.8 | 11.9 | 15.1 | 11.8 | 47.0 | 42.1 |  | 40.7 | 44.9 |  |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 |  |
| Incremental Delay, d2 | 4.0 | 0.3 | 0.0 | 0.4 | 0.7 | 0.1 | 120.5 | 0.7 |  | 0.5 | 14.0 |  |
| Delay (s) | 11.9 | 6.2 | 4.9 | 12.2 | 15.8 | 11.9 | 167.5 | 42.8 |  | 41.2 | 59.0 |  |
| Level of Service | B | A | A | B | B | B | F | D |  | D | E |  |
| Approach Delay (s) |  | 8.0 |  |  | 15.4 |  |  | 82.8 |  |  | 56.2 |  |
| Approach LOS |  | A |  |  | B |  |  | F |  |  | E |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 23.5 |  | CM 2000 | Level of | ervice |  | C |  |  |  |
| HCM 2000 Volume to Capacity ratio |  |  | 0.78 |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length (s) |  |  | 114.5 |  | um of los | time (s) |  |  | 15.5 |  |  |  |
| Intersection Capacity Utilization |  |  | 86.3\% |  | CU Level | of Service |  |  | E |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |
| c Critical Lane Group |  |  |  |  |  |  |  |  |  |  |  |  |

Uppers Quarry Traffic Impact Study
TMIG

Synchro 10 Report

Timings
5: Thorold Townline Road \& Lundys Lane



[^4]Synchro 10 Report

HCM Signalized Intersection Capacity Analysis 5: Thorold Townline Road \& Lundys Lane
<2018 Existing> AM Peak Hour

 |  | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Ideat Flow (vphpl) | 19.0 | 7.0 | 7.0 | 7.0 | 7.0 |  | 6.0 | 6.0 |  | 6.0 | 6.0 |  |

| Total Lost time (s) | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 6.0 | 6.0 | 6.0 | 6.0 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |


|  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frpb, ped/bikes | 1.0 | 1.00 | 10 | 1.00 | 1.0 | 1.0 |  |  |  |


| Frpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 1.00 | 0.97 | 1.00 | 0.96 |


|  | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 1.00 | 0.97 | 1.00 | 0.96 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 0.95 | 1.00 | 0.95 | 1.00 |
|  | 1581 | 1810 | 1495 | 1752 | 1786 | 1612 | 1608 | 1671 | 1540 |


| Satd. Flow (prot) | 1581 | 1810 | 1495 | 1752 | 1786 | 1612 | 1608 | 1671 | 1540 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Flt Permitted | 0.56 | 1.00 | 1.00 | 0.51 | 1.00 | 0.68 | 1.00 | 0.50 | 1.00 |
| Satd. Flow (perm) | 924 | 1810 | 1495 | 932 | 1786 | 1152 | 1608 | 877 | 1540 |


|  |  |  |  |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Peak-hour factor, PHF | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 |
| Adi-Flow (vph) | 67 | 409 | 92 | 41 | 327 | 10 | 71 | 152 | 40 | 14 | 92 | 28 |


| Adj. Flow (vph) | 67 | 409 | 92 | 41 | 327 | 10 | 71 | 152 | 40 | 14 | 92 | 28 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| RTOR Reduction (vph) | 0 | 0 | 16 | 0 | 1 | 0 | 0 | 12 | 0 | 0 | 14 |  |


| Lane Group Flow (vph) | 67 | 409 | 76 | 41 | 336 | 0 | 71 | 180 | 0 | 14 | 106 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |


|  | $14 \%$ | $5 \%$ | $8 \%$ | $3 \%$ | $6 \%$ | $0 \%$ | $12 \%$ | $17 \%$ | $5 \%$ | $8 \%$ | $16 \%$ | $29 \%$ |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Teary Vehicles (\%) | Perm | NA | Perm | Perm | NA |  | Perm | NA |  | Perm | NA |  |

Protected Phases

| Permitted Phases | 2 |
| :--- | :--- |

Actuated Green, G (s)
Effective Green, $\mathrm{g}(\mathrm{s})$
Clearance Time (s)

|  | 71.3 | 7.3 | 7.3 | 7.3 | 71.3 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Clearance Time (s) | 0.69 | 0.69 | 0.69 | 0.69 | 0.69 |
|  | 7.0 | 7.0 | 70 | 7.0 | 7.0 |


| Clearance Time (s) | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 6.0 | 6.0 | 6.0 | 6.0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Vehicle Extension (s) | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| Lane Grp Cap (vph) | 639 | 1252 | 1034 | 645 | 1236 | 209 | 291 | 159 | 279 |
| v/s Ratio Prot |  | c0.23 |  |  | 0.19 |  | c0.11 |  | 0.07 |


|  | $\mathrm{co.23}$ |  | 0.19 |  | $c 0.11$ |  | 0.07 |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| v/s Ratio Prot | 0.07 |  | 0.05 | 0.04 |  | 0.06 |  | 0.02 |  |
| v/s Ratio Perm | 0.10 | 0.33 | 0.07 | 0.06 | 0.27 | 0.34 | 0.62 | 0.09 | 0.38 |


|  | 0.10 | 0.33 | 0.07 | 0.06 | 0.27 | 0.34 | 0.62 | 0.09 | 0.38 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | :--- |
| Uniform Delay, d1 | 5.3 | 6.3 | 5.1 | 5.1 | 6.0 | 36.8 | 38.9 | 35.1 | 37.1 |


| rogression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


|  | 0.3 | 0.7 | 0.1 | 0.2 | 0.5 | 2.0 | 5.5 | 0.5 | 1.8 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


| Delay (s) | 5.6 | 7.0 | 5.3 | 5.3 | 6.6 | 38.8 | 44.4 | 35.6 | 38.9 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |

A A

Approach Delay (s) 6.6

| Intersection Summary |  |  |  |
| :--- | ---: | :--- | ---: |
| HCM 2000 Control Delay | 16.8 | HCM 2000 Level of Service | B |
| HCM 2000 Volume to Capacity ratio | 0.39 | Sum of lost time (s) | 13.0 |


| HCM 2000 Volume to Capacity ratio | 0.39 |  |  |
| :--- | ---: | :--- | ---: |
| Actuated Cycle Length (s) | 103.0 | Sum of lost time (s) | 13.0 |
| Intersection Capacity Utilization | $64.1 \%$ | ICU Level of Service | C |

Intersection Capacity Utilization
64.1\%

C
c Critical Lane Group


[^5]HCM Unsignalized Intersection Capacity Analysis
7: Thorold Townline Road \& Uppers Lane
<2018 Existing> AM Peak Hou 7: Thorold Townline Road \& Uppers Lane 09-14-2021

|  | $\dagger$ | 4 | $\dagger$ | $p$ |  | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | \% |  | $\dagger$ |  |  | 4 |
| Traffic Volume (veh/h) | 1 | 0 | 211 | 1 | 0 | 124 |
| Future Volume (Veh/h) | 1 | 0 | 211 | 1 | 0 | 124 |
| Sign Control | Stop |  | Free |  |  | Free |
| Grade | 0\% |  | 0\% |  |  | 0\% |
| Peak Hour Factor | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 |
| Hourly flow rate (vph) | 1 | 0 | 227 | 1 | 0 | 133 |

$\begin{array}{lrrrrrr}\text { Peak Hour Factor } & 0.93 & 0.93 & 0.93 & 0.93 & 0.93 & 0.93 \\ \text { Hourly flow rate (vph) } & 1 & 0 & 227 & 1 & 0 & 133\end{array}$
Pedestrians
Pedestrians Width ( m )
Walking Speed (m/s)
Walking Speed (m/s)
Percent Blockage
Right turn flare (veh)
Right turn flare (veh)
Median storage veh)
Upstream signal ( m )
DX, platoon unblocked

| VC, conflicting volume | 360 | 228 |
| :--- | :--- | :--- |
| $\mathrm{VC1}$, stage 1 conf vol |  |  |
| $\mathrm{vC2}$, stage 2 conf vol |  |  |


| VC 2, stage 2 conf vol |  |  |  |
| :--- | :--- | :--- | :--- |
| VC, unblocked vol | 360 | 228 | 228 |
| CC , single (s) | 6.4 | 6.2 | 4.1 |
| C 2 stage (s) |  |  |  |


| VCu, unblocked vol | 360 | 228 | 228 |
| :--- | ---: | ---: | ---: |
| tC, single (s) | 6.4 | 6.2 | 4.1 |
| tC, 2 stage (s) | 3.5 | 3.3 | 2.2 |
| tF (s) | 100 | 100 | 100 |
| p0 queue free \% | 642 | 817 | 1352 |


| Direction, Lane \# | WB 1 | NB 1 | SB 1 |  |  |
| :--- | ---: | ---: | ---: | ---: | :--- |
| Volume Total | 1 | 228 | 133 |  |  |
| Volume Left | 1 | 0 | 0 |  |  |
| Volume Right | 0 | 1 | 0 |  |  |
| cSH | 642 | 1700 | 1352 |  |  |
| Volume to Capacity | 0.00 | 0.13 | 0.00 |  |  |
| Queue Length 95th (m) | 0.0 | 0.0 | 0.0 |  |  |
| Control Delay (s) | 10.6 | 0.0 | 0.0 |  |  |
| Lane LOS | B |  |  |  |  |
| Approach Delay (s) | 10.6 | 0.0 | 0.0 |  |  |
| Approach LOS | $B$ |  |  |  |  |
| Intersection Summary |  |  | 0.0 |  |  |
| Average Delay |  |  | $01.2 \%$ | ICU Level of Service |  |
| Intersection Capacity Utilization |  | 15 |  |  |  |

## Timings

1: Davis Road \& Thorold Stone Road
<2018 Existing> PM Peak Hour


Turn Type
Portected Phases
Detectittor Phase
Switch Phase
Minimum Initial (s)

| Minimum Initial (s) | 20.0 | 20.0 | 20.0 | 20.0 | 20.0 | 10.0 | 10.0 | 10.0 | 10.0 | 10.0 | 10.0 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Minimum Split (s) | 28.9 | 28.9 | 28.9 | 28.9 | 28.9 | 29.7 | 29.7 | 29.7 | 21.7 | 21.7 | 21.7 |


| Minimum Spit (s) | 28.9 | 28.9 | 28.9 | 28.9 | 28.9 | 29.7 | 29.7 | 29.7 | 21.7 | 21.7 | 21.7 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Total Split (s) | 39.7 | 39.7 | 39.7 | 39.7 | 39.7 | 45.4 | 45.4 | 45.4 | 21.9 | 21.9 | 21.9 |


$\begin{array}{rrrrrrrrrr}15 & 3.1 \% & 3.1 \% & 37.1 \% & 37.1 \% & 42.4 \% & 42.4 \% & 42.4 \% & 20.5 \% & 20.5 \% \\ 5.4 & 5.4 & 5.4 & 5.4 & 5.4 & 5.7 & 5.7 & 5.7 & 5.7 & 5.7 \\ 5.7\end{array}$
$\begin{array}{llllllllllll} & 5.4 & 5.4 & 5.4 & 5.4 & 5.4 & 5.7 & 5.7 & 5.7 & 5.7 & 5.7 & 5.7 \\ \text { Yellow Time (s) } & 1.5 & 1.5 & 1.5 & 1.5 & 1.5 & 2.0 & 2.0 & 2.0 & 2.0 & 2.0 & 2.0 \\ \text { All-Red Time (s) } & 0.0 & 0.0 & 0.0 & 0.0 & 0.0 & 0.0 & 0.0 & 0.0 & 0.0 & 0.7 & 0.7\end{array}$

| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Total Lost Time (s) | 6.9 | 6.9 | 6.9 | 6.9 | 6.9 | 7.7 | 7.7 | 7.7 | 7.7 | 7.7 | 7.7 |

ead/Lag

| Lead-Lag Optimize? |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Recall Mode | C-Max | C-Max | C-Max | Max | Max | None | None | None | None | None | None |
| Act Efft Green (s) | 60.3 | 60.3 | 60.3 | 60.3 | 60.3 | 21.5 | 21.5 | 21.5 | 10.0 | 10.0 | 10.0 |
| Actuated g/C Ratio | 0.56 | 0.56 | 0.56 | 0.56 | 0.56 | 0.20 | 0.20 | 0.20 | 0.09 | 0.09 | 0.09 |
| v/c Ratio | 0.18 | 0.64 | 0.46 | 0.63 | 0.59 | 0.66 | 0.65 | 0.23 | 0.02 | 0.04 | 0.12 |
| Control Delay | 22.1 | 21.0 | 9.9 | 48.7 | 19.8 | 48.0 | 47.6 | 4.3 | 44.5 | 44.8 | 0.9 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 22.1 | 21.0 | 9.9 | 48.7 | 19.8 | 48.0 | 47.6 | 4.3 | 44.5 | 44.8 | 0.9 |
| LOS | c | c | A | D | B | D | D | A | D | D | A |

Approach Delay Approach LOS

## ntersection Summar

ycle Length: 107
Actuated Cycle Length: 107
Ifset: O (0\%), Referenced to phase 2:EBTL, Start of Green
Natural Cycle: 105
Control Type: Actuated-Coordinated
$\begin{array}{ll}\text { Control Type: Actuated-Coordinated } & \\ \begin{array}{ll}\text { Maximum v/c Ratio: } 0.66 & \\ \text { Intersection Signal Delay: } 22.6 & \text { Intersection LOS: } C \\ \text { Intersection Capacity Utilzation } 86.2 \% & \text { ICU Level of Service E }\end{array}\end{array}$
Analysis Period (min) 15


[^6]|  | 7 | $\rightarrow$ |  | 7 |  |  | 4 |  | $P$ |  |  | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{*}$ | $\uparrow \uparrow$ | F | * | 个分 |  | ${ }_{1}$ | $\uparrow$ | F | 7 | $\uparrow$ | F |
| Traffic Volume (vph) | 24 | 1209 | 427 | 78 | 1108 | 1 | 412 | 5 | 86 | 4 | 6 | 28 |
| Future Volume (vph) | 24 | 1209 | 427 | 78 | 1108 | 1 | 412 | 5 | 86 | 4 | 6 | 28 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 900 |
| Total Lost time (s) | 6.9 | 6.9 | 6.9 | 6.9 | 6.9 |  | 7.7 | 7.7 | 7.7 | 7.7 | 7.7 | 7.7 |
| Lane Util. Factor | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 |  | 0.95 | 0.95 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.99 |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 |  | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |  | 0.95 | 0.95 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1433 | 3539 | 1568 | 1671 | 3539 |  | 1681 | 1677 | 1482 | 1805 | 1810 | 1531 |
| FIt Permitted | 0.16 | 1.00 | 1.00 | 0.13 | 1.00 |  | 0.95 | 0.95 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (perm) | 245 | 3539 | 1568 | 232 | 3539 |  | 1681 | 1677 | 1482 | 1805 | 1810 | 1531 |
| Peak-hour factor, PHF | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Adj. Flow (vph) | 25 | 1273 | 449 | 82 | 1166 | 1 | 434 | 5 | 91 | 4 | 6 | 29 |
| RTOR Reduction (vph) | 0 | 0 | 110 | 0 | 0 | 0 | 0 | 0 | 73 | 0 | 0 | 27 |
| Lane Group Flow (vph) | 25 | 1273 | 339 | 82 | 1167 | 0 | 221 | 218 | 18 | 4 | 6 |  |


| Lane Group Flow (vph) | 25 | 1273 | 339 | 82 | 1167 | 0 | 221 | 218 | 18 | 4 | 6 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Confl. Peds. (\#hr) | $26 \%$ | $2 \%$ | $3 \%$ | $8 \%$ | $2 \%$ | $0 \%$ | $2 \%$ | $30 \%$ | $9 \%$ | $0 \%$ | $5 \%$ |
| Heavy Vehicles (\%) | $26 \%$ | $4 \%$ |  |  |  |  |  |  |  |  |  |

$$
\begin{aligned}
& \text { Heavy Vehicles (\% } \\
& \hline \text { urrn Tyne }
\end{aligned}
$$

Turn Type
rotected Phases
Permitted Phases
Actuated Green, G (s)
$\begin{array}{lrrrr} & 2 & 2 & 2 & 6\end{array}$
Effective Green, $g$ (s)


Clearance Time (s)

|  |  |  |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Venicle Extension (s) | 6.9 | 6.9 | 6.9 | 6.9 | 6.9 | 7.7 | 7.7 | 7.7 | 7.7 | 7.7 | 7.1 |
| Lane Gre Cap (vph) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 |
| v/s Ratio Prot | 130 | 1891 | 838 | 124 | 1891 | 337 | 336 | 297 | 101 | 101 | 85 |
| VIs Ratio Perm |  | 0.36 |  |  | 0.33 | $c 0.13$ | 0.13 |  | 0.00 | $c 0.00$ |  |

v/s Ratio Prot
s Ratio Perm 0.10
$\begin{array}{lllll} & 0.19 & 0.67 & 0.40 & 0.66\end{array}$
$\begin{array}{llllll} & 12.9 & 18.1 & 14.8 & 17.9\end{array}$

|  | 1.9 | 1.1 | 14.8 | 17.9 | 17.3 | 39.3 | 39.3 | 34.6 | 47.8 | 47.8 | 47.7 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |


| ncremental Delay, d2 | 3.3 | 1.9 | 1.5 | 24.4 | 1.5 | 5.5 | 5.2 | 0.2 | 0.3 | 0.4 | 0.2 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


| Level of Service | B | C | B | D | B | D | D | C | D |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Approach Delay (s) | 19.0 |  | 20.4 |  | 43.0 |  | 48 |  |  |
| Approach LOS | B |  |  | C |  | D |  |  |  |


| Intersection Summary |  |  |  |
| :--- | ---: | :--- | ---: |
| HCM 2000 Control Delay | 23.4 | HCM 2000 Level of Service | C |
| HCM 2000 Volume to Capacity ratio | 0.62 |  | 22.3 |
| Actuated Cycle Length (s) | 107.0 | Sum of lost time (s) | E |
| Intersection Capacity Utilization | $86.2 \%$ | ICU Level of Service |  |

Acluated Cycle Length (s)
86.2\%

CU Level of Service
E
c Critical Lane Group

Timings
2：Davis Road \＆Niagara Falls Road／Beaverdams Road

| Lane Group | EBL | EBT | WBL | WBT | NBL | NBT | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations |  | $\dagger$ |  | ¢ | ${ }^{1}$ | 个施 | ＊ | 个 $\uparrow$ | F |
| Traffic Volume（vph） | 90 | 32 | 42 | 44 | 5 | 275 | 170 | 244 | 105 |
| Future Volume（vph） | 90 | 32 | 42 | 44 | 5 | 275 | 170 | 244 | 105 |
| Turn Type | Perm | NA | Perm | NA | Perm | NA | Perm | NA | Perm |
| Protected Phases |  | 2 |  | 6 |  | 4 |  | 8 |  |
| Permitted Phases | 2 |  | 6 |  | 4 |  | 8 |  | 8 |
| Detector Phase | 2 | 2 | 6 | 6 | 4 | 4 | 8 | 8 | 8 |
| Switch Phase |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 10.0 | 10.0 | 10.0 | 10.0 | 25.0 | 25.0 | 25.0 | 25.0 | 25.0 |
| Minimum Split（s） | 38.1 | 38.1 | 38.1 | 38.1 | 32.0 | 32.0 | 32.0 | 32.0 | 32.0 |
| Total Split（s） | 43.1 | 43.1 | 43.1 | 43.1 | 52.0 | 52.0 | 52.0 | 52.0 | 52.0 |
| Total Split（\％） | 45．3\％ | 45．3\％ | 45．3\％ | 45．3\％ | 54．7\％ | 54．7\％ | 54．7\％ | 54．7\％ | 54．7\％ |
| Yellow Time（s） | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| All－Red Time（s） | 3.1 | 3.1 | 3.1 | 3.1 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |
| Lost Time Adjust（s） |  | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time（s） |  | 8.1 |  | 8.1 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |
| Lead／Lag |  |  |  |  |  |  |  |  |  |
| Lead－Lag Optimize？ |  |  |  |  |  |  |  |  |  |
| Recall Mode | C－Max | C－Max | Max | Max | None | None | None | None | None |
| Act Effict Green（s） |  | 51.9 |  | 51.9 | 28.1 | 28.1 | 28.1 | 28.1 | 28.1 |
| Actuated g／C Ratio |  | 0.55 |  | 0.55 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 |
| v／c Ratio |  | 0.20 |  | 0.27 | 0.02 | 0.33 | 0.58 | 0.26 | 0.20 |
| Control Delay |  | 13.1 |  | 8.2 | 20.8 | 24.9 | 36.1 | 25.5 | 5.1 |
| Queue Delay |  | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay |  | 13.1 |  | 8.2 | 20.8 | 24.9 | 36.1 | 25.5 | 5.1 |
| LOS |  | B |  | A | C | C | D | C | A |
| Approach Delay |  | 13.1 |  | 8.2 |  | 24.8 |  | 24.8 |  |
| Approach LOS |  | B |  | A |  | C |  | C |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |
| Cycle Length： 95.1 |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length： 95.1 |  |  |  |  |  |  |  |  |  |
| Offset： 0 （0\％），Referenced to phase 2：EBTL，Start of Green |  |  |  |  |  |  |  |  |  |
| Natural Cycle： 75 |  |  |  |  |  |  |  |  |  |
| Control Type：Actuated－Coordinated |  |  |  |  |  |  |  |  |  |
| Maximum v／c Ratio： 0.58 |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay： 20.3 |  |  |  | Intersection LOS：C |  |  |  |  |  |
| Intersection Capacity Utilization 81．2\％ |  |  |  | ICU Level of Service D |  |  |  |  |  |
| Analysis Period（min） 15 |  |  |  |  |  |  |  |  |  |



[^7]Synchro 10 Report

HCM Signalized Intersection Capacity Analysis
2：Davis Road \＆Niagara Falls Road／Beaverdams Road
＜2018 Existing＞PM Peak Hou 09－14－2021


Uppers Quarry Traffic Impact Study

Timings
3: Davis Road \& Lundys Lane

| Lane Group | EBL | EBT | WBL | WBT | WBR | NBL | NBT | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | 7 | F | \% | $\uparrow$ | 7 | \% | F | 7 | $\uparrow$ | F |
| Traffic Volume (vph) | 105 | 464 | 24 | 452 | 59 | 46 | 134 | 74 | 122 | 113 |
| Future Volume (vph) | 105 | 464 | 24 | 452 | 59 | 46 | 134 | 74 | 122 | 113 |
| Turn Type | Perm | NA | Perm | NA | Perm | Perm | NA | Perm | NA | Perm |
| Protected Phases |  | 2 |  | 6 |  |  | 4 |  | 8 |  |
| Permitted Phases | 2 |  | 6 |  | 6 | 4 |  | 8 |  | 8 |
| Detector Phase | 2 | 2 | 6 | 6 | 6 | 4 | 4 | 8 | 8 | 8 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 22.0 | 22.0 | 22.0 | 22.0 | 22.0 | 15.0 | 15.0 | 15.0 | 15.0 | 15.0 |
| Minimum Split (s) | 36.0 | 36.0 | 36.0 | 36.0 | 36.0 | 32.0 | 32.0 | 32.0 | 32.0 | 32.0 |
| Total Split (s) | 52.0 | 52.0 | 52.0 | 52.0 | 52.0 | 42.0 | 42.0 | 42.0 | 42.0 | 42.0 |
| Total Split (\%) | 55.3\% | 55.3\% | 55.3\% | 55.3\% | 55.3\% | 44.7\% | 44.7\% | 44.7\% | 44.7\% | 44.7\% |
| Yellow Time (s) | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| All-Red Time (s) | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |
| Lead/Lag |  |  |  |  |  |  |  |  |  |  |
| Lead-Lag Optimize? |  |  |  |  |  |  |  |  |  |  |
| Recall Mode | C-Max | C-Max | Max | Max | Max | Max | Max | Max | Max | Max |
| Act Effct Green (s) | 45.0 | 45.0 | 45.0 | 45.0 | 45.0 | 35.0 | 35.0 | 35.0 | 35.0 | 35.0 |
| Actuated g/C Ratio | 0.48 | 0.48 | 0.48 | 0.48 | 0.48 | 0.37 | 0.37 | 0.37 | 0.37 | 0.37 |
| V/C Ratio | 0.36 | 0.61 | 0.10 | 0.55 | 0.09 | 0.11 | 0.28 | 0.19 | 0.20 | 0.19 |
| Control Delay | 19.6 | 21.7 | 14.8 | 20.2 | 4.0 | 20.2 | 20.4 | 21.4 | 21.1 | 4.6 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 19.6 | 21.7 | 14.8 | 20.2 | 4.0 | 20.2 | 20.4 | 21.4 | 21.1 | 4.6 |
| LOS | B | C | B | C | A | C | C | C | C | A |
| Approach Delay |  | 21.3 |  | 18.1 |  |  | 20.4 |  | 15.1 |  |
| Approach LOS |  | C |  | B |  |  | C |  | B |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 94 |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 94 |  |  |  |  |  |  |  |  |  |  |
| Offset: $0(0 \%)$, Referenced to phase 2:EBTL, Start of Green |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 70 |  |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Coordinated |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.61 |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 19.0 |  |  |  |  | Intersection LOS: B |  |  |  |  |  |
| Intersection Capacity Utilization 101.1\% |  |  |  |  | ICU Level of Service G |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |



[^8]Synchro 10 Report

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \% | $\hat{F}$ |  | \% | $\uparrow$ | F' | 7 | $\stackrel{1}{6}$ |  | 7 | $\uparrow$ | 7 |
| Traffic Volume (vph) | 105 | 464 | 28 | 24 | 452 | 59 | 46 | 134 | 30 | 74 | 122 | 113 |
| Future Volume (vph) | 105 | 464 | 28 | 24 | 452 | 59 | 46 | 134 | 30 | 74 | 122 | 113 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 7.0 | 7.0 |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  | 7.0 | 7.0 | 7.0 |
| Lane Util. Factor | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 |
| Frpb, ped/bikes | 1.00 | 1.00 |  | 1.00 | 1.00 | 0.98 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 |
| Flpb, ped/bikes | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 |
| Frt | 1.00 | 0.99 |  | 1.00 | 1.00 | 0.85 | 1.00 | 0.97 |  | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 |  | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |  | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1717 | 1804 |  | 1611 | 1863 | 1474 | 1736 | 1680 |  | 1700 | 1743 | 1553 |
| Flt Permitted | 0.37 | 1.00 |  | 0.33 | 1.00 | 1.00 | 0.67 | 1.00 |  | 0.65 | 1.00 | 1.00 |
| Satd. Flow (perm) | 662 | 1804 |  | 557 | 1863 | 1474 | 1230 | 1680 |  | 1156 | 1743 | 1553 |
| Peak-hour factor, PHF | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 |
| Adj. Flow (vph) | 113 | 499 | 30 | 26 | 486 | 63 | 49 | 144 | 32 | 80 | 131 | 122 |
| RTOR Reduction (vph) | 0 | 2 | 0 | 0 | 0 | 33 | 0 | 9 | 0 | 0 | 0 | 77 |
| Lane Group Flow (vph) | 113 | 527 | 0 | 26 | 486 | 30 | 49 | 167 | 0 | 80 | 131 | 45 |
| Confl. Peds. (\#/hr) | 2 |  | 1 | 1 |  | 2 |  |  | 1 | 1 |  |  |
| Heavy Vehicles (\%) | 5\% | 3\% | 26\% | 12\% | 2\% | 7\% | 4\% | 9\% | 12\% | 6\% | 9\% | 4\% |
| Turn Type | Perm | NA |  | Perm | NA | Perm | Perm | NA |  | Perm | NA | Perm |
| Protected Phases |  | 2 |  |  | 6 |  |  | 4 |  |  | 8 |  |
| Permitted Phases | 2 |  |  | 6 |  | 6 | 4 |  |  | 8 |  |  |
| Actuated Green, G (s) | 45.0 | 45.0 |  | 45.0 | 45.0 | 45.0 | 35.0 | 35.0 |  | 35.0 | 35.0 | 35.0 |
| Effective Green, g (s) | 45.0 | 45.0 |  | 45.0 | 45.0 | 45.0 | 35.0 | 35.0 |  | 35.0 | 35.0 | 35.0 |
| Actuated g/C Ratio | 0.48 | 0.48 |  | 0.48 | 0.48 | 0.48 | 0.37 | 0.37 |  | 0.37 | 0.37 | 0.37 |
| Clearance Time (s) | 7.0 | 7.0 |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  | 7.0 | 7.0 | 7.0 |
| Vehicle Extension (s) | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 | 2.0 | 2.0 |  | 2.0 | 2.0 | 2.0 |
| Lane Grp Cap (vph) | 316 | 863 |  | 266 | 891 | 705 | 457 | 625 |  | 430 | 648 | 578 |
| v/s Ratio Prot |  | c0.29 |  |  | 0.26 |  |  | c0.10 |  |  | 0.08 |  |
| v/s Ratio Perm | 0.17 |  |  | 0.05 |  | 0.02 | 0.04 |  |  | 0.07 |  | 0.03 |
| v/c Ratio | 0.36 | 0.61 |  | 0.10 | 0.55 | 0.04 | 0.11 | 0.27 |  | 0.19 | 0.20 | 0.08 |
| Uniform Delay, d1 | 15.4 | 18.0 |  | 13.4 | 17.3 | 13.0 | 19.3 | 20.6 |  | 19.9 | 20.0 | 19.1 |
| Progression Factor | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 3.1 | 3.2 |  | 0.7 | 2.4 | 0.1 | 0.5 | 1.0 |  | 1.0 | 0.7 | 0.3 |
| Delay (s) | 18.5 | 21.3 |  | 14.1 | 19.7 | 13.2 | 19.8 | 21.6 |  | 20.8 | 20.7 | 19.3 |
| Level of Service | B | C |  | B | B | B | B | C |  | C | C | B |
| Approach Delay (s) |  | 20.8 |  |  | 18.7 |  |  | 21.2 |  |  | 20.2 |  |
| Approach LOS |  | C |  |  | B |  |  | C |  |  | C |  |

## Apoch

HCM 2000 Control Delay
$\begin{array}{lll}\text { HCM } 2000 \text { Vonume to Capacity ratio } & 20.1 & \text { HCM } 2000 \text { Level of Service }\end{array}$
Actuated Cycle Length (s)

101.1\%

Sum of lost time (s)
ICU Level of Service
tersection Capacity Utilization
C
c Critical Lane Group

Timings
4：Thorold Townline Road \＆Thorold Stone Road 09－14－2021

| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | SBL | SBT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \％ | 个 $\uparrow$ | 「 | \％ | 个 $\uparrow$ | F | \％ | $\hat{}$ | ${ }^{7}$ | $\uparrow$ |
| Traffic Volume（vph） | 231 | 1036 | 32 | 30 | 821 | 35 | 69 | 83 | 48 | 138 |
| Future Volume（vph） | 231 | 1036 | 32 | 30 | 821 | 35 | 69 | 83 | 48 | 138 |
| Turn Type | pm＋pt | NA | Perm | Perm | NA | Perm | Perm | NA | Perm | NA |
| Protected Phases | 5 | 2 |  |  | 6 |  |  | 4 |  | ， |
| Permitted Phases | 2 |  | 2 | 6 |  |  | 4 |  | 8 |  |
| Detector Phase | 5 | 2 | 2 | 6 | 6 | 6 | 4 | 4 | 8 | 8 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 8.0 | 10.0 | 10.0 | 10.0 | 10.0 | 10.0 | 10.0 | 10.0 | 10.0 | 10.0 |
| Minimum Split（s） | 11.0 | 35.1 | 35.1 | 35.1 | 35.1 | 35.1 | 41.4 | 41.4 | 41.4 | 41.4 |
| Total Split（s） | 23.0 | 73.1 | 73.1 | 50.1 | 50.1 | 50.1 | 41.4 | 41.4 | 41.4 | 41.4 |
| Total Split（\％） | 20．1\％ | 63．8\％ | 63．8\％ | 43．8\％ | 43．8\％ | 43．8\％ | 36．2\％ | 36．2\％ | 36．2\％ | 36．2\％ |
| Yellow Time（s） | 3.0 | 4.1 | 4.1 | 4.1 | 4.1 | 4.1 | 4.1 | 4.1 | 4.1 | 4.1 |
| All－Red Time（s） | 0.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.3 | 2.3 | 2.3 | 2.3 |
| Lost Time Adjust（s） | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time（s） | 3.0 | 6.1 | 6.1 | 6.1 | 6.1 | 6.1 | 6.4 | 6.4 | 6.4 | 6.4 |
| Lead／Lag | Lead |  |  | Lag | Lag | Lag |  |  |  |  |
| Lead－Lag Optimize？ | Yes |  |  | Yes | Yes | Yes |  |  |  |  |
| Recall Mode | None | C－Max | C－Max | C－Max | C－Max | C－Max | None | None | None | None |
| Act Efft Green（s） | 76.3 | 73.2 | 73.2 | 58.0 | 58.0 | 58.0 | 28.8 | 28.8 | 28.8 | 28.8 |
| Actuated g／C Ratio | 0.67 | 0.64 | 0.64 | 0.51 | 0.51 | 0.51 | 0.25 | 0.25 | 0.25 | 0.25 |
| v／c Ratio | 0.57 | 0.47 | 0.03 | 0.13 | 0.48 | 0.04 | 1.04 | 0.26 | 0.17 | 0.90 |
| Control Delay | 14.1 | 12.3 | 3.6 | 21.1 | 21.3 | 2.1 | 162.2 | 30.1 | 32.3 | 54.1 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 14.1 | 12.3 | 3.6 | 21.1 | 21.3 | 2.1 | 162.2 | 30.1 | 32.3 | 54.1 |
| LOS | B | B | A | C | C | A | F | C | C | D |
| Approach Delay |  | 12.4 |  |  | 20.5 |  |  | 82.1 |  | 51.8 |
| Approach LOS |  | B |  |  | C |  |  | F |  | D |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |
| Cycle Length： 114.5 |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length： 114.5 |  |  |  |  |  |  |  |  |  |  |
| Offset： $0(0 \%)$ ，Referenced to phase 2：EBTL and 6：WBTL，Start of Green |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle： 90 |  |  |  |  |  |  |  |  |  |  |
| Control Type：Actuated－Coordinated |  |  |  |  |  |  |  |  |  |  |
| Maximum v／c Ratio： 1.04 |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay： 25.7 |  |  |  |  | tersection | LOS：C |  |  |  |  |
| Intersection Capacity Utilization 90．1\％ |  |  |  |  |  |  |  |  |  |  |
| Analysis Period（min） 15 |  |  |  | ICU Level of Service E |  |  |  |  |  |  |



[^9]Synchro 10 Report

HCM Signalized Intersection Capacity Analysis
＜2018 Existing＞PM Peak Hou 4：Thorold Townline Road \＆Thorold Stone Road

9－14－202


Uppers Quarry Traffic Impact Study

Timings
5: Thorold Townline Road \& Lundys Lane
$\downarrow \downarrow$



[^10]Synchro 10 Report

HCM Signalized Intersection Capacity Analysis 5: Thorold Townline Road \& Lundys Lane
<2018 Existing> PM Peak Hour
09-14-2021


| Traffic Volume (vph) | 37 | 434 | 96 | 44 | 401 | 21 | 100 | 132 | 50 | 25 | 118 | 38 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Future Volume (vph) | 37 | 434 | 96 | 44 | 401 | 21 | 100 | 132 | 50 | 25 | 118 | 38 |



| Total Lost time (s) | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 6.0 | 6.0 | 6.0 | 6.0 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |


| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
|  | 1.00 | 1.00 | 1.00 | 100 | 100 | 1.00 | 1.00 | 1.00 | 1.00 |


| Frpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |


| Ipb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 0.99 | 1.00 | 0.96 | 1.00 | 0.96 |


| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 0.99 | 1.00 | 0.96 | 1.00 | 0.96 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 0.95 | 1.00 | 0.95 | 1.00 |
| Satd Flow (prot) | 1624 | 1827 | 1553 | 1752 | 1835 | 1687 | 1746 | 1736 | 1715 |


| Satd. Flow (prot) | 1624 | 1827 | 1553 | 1752 | 1835 | 1687 | 1746 | 1736 | 1715 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Flt Permitted | 0.47 | 1.00 | 1.00 | 0.46 | 1.00 | 0.54 | 1.00 | 0.47 | 1.00 |
| Satd. Flow (perm) | 804 | 1827 | 1553 | 852 | 1835 | 963 | 1746 | 861 | 1715 |


| Satd. Flow (perm) | 804 | 1827 | 1553 | 852 | 1835 | 963 | 1746 | 861 | 1715 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |

$\left.\begin{array}{lrlllllllllll} & 0.91 & .910\end{array}\right)$

| TOR Reduction (vph) | 0 | 0 | 16 | 0 | 1 | 0 | 0 | 18 | 0 | 0 | 15 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ane Group Flow (vph) | 41 | 477 | 89 |  | 46 |  | 110 |  | 0 |  |  |


| Lane Group Flow (vph) | 41 | 477 | 89 | 48 | 463 | 0 | 110 | 182 | 0 | 27 | 157 |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | :--- |
| Confl. Peds. (\#hr) | 1 | $11 \%$ | $4 \%$ | $4 \%$ | $3 \%$ | $2 \%$ | $15 \%$ | $7 \%$ | $6 \%$ | $0 \%$ | $4 \%$ | $7 \%$ |
| Heavy Vehicles (\%) | $11 \%$ | $6 \%$ |  |  |  |  |  |  |  |  |  |  |


| Heavy Vehicles (\%) | $11 \%$ | $4 \%$ | $4 \%$ | $3 \%$ | $2 \%$ | $15 \%$ | $7 \%$ | $6 \%$ | $0 \%$ | $4 \%$ | $7 \%$ | 6 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Turn Type | Perm | NA | Perm | Perm | NA |  | Perm | NA |  | Perm | NA |  |

rotected Phases
$\begin{array}{lllll}\text { Permitted Phases } & 2 & 2 & 2 & 0\end{array}$
$\begin{array}{llllll}\text { ctuated Green, G (s) } & 71.9 & 71.9 & 71.9 & 71.9 & 71.9\end{array}$
$\begin{array}{lllllll}\text { Effective Green, } \mathrm{g}(\mathrm{s}) & 71.9 & 71.9 & 71.9 & 71.9 & 71.9 \\ & 0.70 & 0.70 & 0.70 & 0.70 & 0.70\end{array}$
Aclualed g/ Raio

|  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 0.18 | 0.18 | 0.18 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


|  |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Cehicle Extension $(\mathrm{s})$ | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 6.0 | 6.0 | 6.0 | 5.0 |
| ane Grp Cap (vph) | 561 | 1275 | 1084 | 594 | 1280 | 169 | 306 | 5.0 | 5.0 |


|  | 561 |  |  |  |  |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Lane Grp Cap (vph) | 1275 | 1084 | 594 | 1280 | 169 | 306 | 151 | 301 |  |
| V/s Ratio Prot | 0.05 |  |  | 0.06 | 0.06 | 0.25 |  | 0.11 | 0.10 |
| V/s Ratio Perm | 0.05 |  | 0.11 |  | 0.03 | 0.09 |  |  |  |


|  | 0.05 | 0.06 | 0.06 |  | $c$ |  | 0.11 | 0.03 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| s Ratio Perm | 0.07 | 0.37 | 0.08 | 0.08 | 0.36 | 0.65 | 0.59 | 0.18 |


| Uniform Delay, d1 | 4.9 | 6.4 | 5.0 | 5.0 | 6.3 | 39.5 | 39.1 | 36.1 | 38.5 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | :--- |
|  | 100 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 3. |


| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


|  | 0.3 | 0.8 | 0.1 | 0.3 | 0.8 | 11.5 | 4.6 | 1.2 | 3.1 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


| Delay (s) | 5.2 | 7.2 | 5.1 | 5.2 | 7.1 | 51.0 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |


| Level of Service | A | A | A | A | A |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Approach Delay (s) |  | 6.7 |  |  | 6.9 |
| Approach LOS |  | A |  |  | A |

Intersection Summary

| HCM 2000 Control Delay | 18.4 | HCM 2000 Level of Service | B |
| :--- | ---: | :--- | ---: |
| HCM 2000 Volume to Capacity ratio | 0.43 |  |  |
| Actuated Cycle Length (s) | 103.0 | Sum of lost time (s) | 13.0 |
| Intersection Capacity Utilization | $70.7 \%$ | ICU Level of Service | C |

tered Cycle Length (s)
70.7\%

ICU Level of Service
C
Analysis Period (min)

HCM Unsignalized Intersection Capacity Analysis
<2018 Existing> PM Peak Hour
6: Thorold Townline Road \& Beaverdams Road

|  | $\rangle$ |  |  | $\dagger$ |  |  | 4 | 4 | 7 |  | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\dagger$ |  |  | ${ }_{\text {¢ }}$ |  |  | ${ }_{\$}$ |  |  | ${ }_{4}$ |  |
| Sign Control |  | Stop |  |  | Stop |  |  | Stop |  |  | Stop |  |
| Trafic Volume (vph) | 24 | 197 | 16 | 11 | 166 | 21 | 32 | 148 | 7 | 20 | 150 | 35 |
| Future Volume (vph) | 24 | 197 | 16 | 11 | 166 | 21 | 32 | 148 | 7 | 20 | 150 | 35 |
| Peak Hour Factor | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 |
| Hourly flow rate (vph) | 26 | 212 | 17 | 12 | 178 | 23 | 34 | 159 | 8 | 22 | 161 | 38 |
| Direction, Lane \# | EB 1 | WB 1 | NB 1 | SB 1 |  |  |  |  |  |  |  |  |
| Volume Total (vph) | 255 | 213 | 201 | 221 |  |  |  |  |  |  |  |  |
| Volume Left (vph) | 26 | 12 | 34 | 22 |  |  |  |  |  |  |  |  |
| Volume Right (vph) | 17 | 23 | 8 | 38 |  |  |  |  |  |  |  |  |
| Hadj (s) | 0.02 | -0.04 | 0.16 | 0.01 |  |  |  |  |  |  |  |  |
| Departure Headway (s) | 5.5 | 5.6 | 5.8 | 5.6 |  |  |  |  |  |  |  |  |
| Degree Utilization, x | 0.39 | 0.33 | 0.32 | 0.34 |  |  |  |  |  |  |  |  |
| Capacity (veh/h) | 601 | 592 | 562 | 585 |  |  |  |  |  |  |  |  |
| Control Delay (s) | 12.0 | 11.2 | 11.5 | 11.5 |  |  |  |  |  |  |  |  |
| Approach Delay (s) | 12.0 | 11.2 | 11.5 | 11.5 |  |  |  |  |  |  |  |  |
| Approach LOS | B | B | B | B |  |  |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Delay |  |  | 11.6 |  |  |  |  |  |  |  |  |  |
| Level of Service |  |  | B |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 42.3\% | ICU Level of Service |  |  |  |  | A |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |

[^11]HCM Unsignalized Intersection Capacity Analysis
7: Thorold Townline Road \& Uppers Lane
<2018 Existing> PM Peak Hou 7: Thorold Townline Road \& Uppers Lane 09-14-2021


Pedestrians
Walking Speed ( $\mathrm{m} / \mathrm{s}$ )
Waking Speed ( $\mathrm{m} / \mathrm{s}$ )
Right turn flare (veh)
Median type
Median storage veh)
Upstream signal ( m )
pX , platoon unblocked

| VC, conflicting volume | 408 | 208 | 209 |
| :--- | :--- | :--- | :--- |
| VC 1, stage 1 conf vol |  |  |  |

vC2, stage 2 conf vol
Cu, unblocked vol 408

| tC, single (s) | 6.4 | 6.2 | 4.1 |
| :--- | ---: | ---: | ---: |
| tC, 2 stage (s) | 3.5 | 3.3 | 2.2 |
| tF (s) | 100 | 100 | 100 |
| p0 queue free \% | 6.3 | 8 |  |


| $\mathrm{FF}(\mathrm{s})$ | 3.5 | 3.3 | 2.2 |
| :--- | ---: | ---: | ---: |
| po queue free \% | 100 | 100 | 100 |
| cM capacity (veh/h) | 603 | 837 | 1374 |


| cM capacity (veh/h) | 603 | 837 |  | 1374 |
| :--- | ---: | ---: | ---: | :--- |
| Direction, Lane \# | WB 1 | NB 1 | SB 1 |  |
| Volume Total | 1 | 209 | 198 |  |
| Volume Left | 0 | 0 | 1 |  |
| Volume Right | 1 | 1 | 0 |  |
| cSH | 837 | 1700 | 1374 |  |
| Volume to Capacity | 0.00 | 0.12 | 0.00 |  |
| Queue Length 95th (m) | 0.0 | 0.0 | 0.0 |  |
| Control Delay (s) | 9.3 | 0.0 | 0.0 | A |
| Lane LOS | A |  |  |  |
| Approach Delay (s) | 9.3 | 0.0 | 0.0 |  |
| Approach LOS | A |  |  |  |

ntersection Summary
$\begin{array}{lrl}\text { Average Delay } & 0.0 & \\ \text { Intersection Capacity Utilization } & 20.2 \% & \text { ICU Level of Senvic }\end{array}$
Analysis Period (min)


| Lane Group | EBL | EBT | EBR | WBL | WBT | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \% | $\uparrow \uparrow$ | F | \% | 中 ${ }^{\text {a }}$ | 7 | $\uparrow$ | F | \% | $\uparrow$ | 7 |
| Traffic Volume (vph) | 21 | 929 | 274 | 87 | 1076 | 542 | 15 | 211 | 1 | 2 | 18 |
| Future Volume (vph) | 21 | 929 | 274 | 87 | 1076 | 542 | 15 | 211 | 1 | 2 | 18 |
| Turn Type | Perm | NA | Perm | pm+pt | NA | Split | NA | Perm | Split | NA | Perm |
| Protected Phases |  | 2 |  | 1 | 6 | 4 | 4 |  | 8 | 8 |  |
| Permitted Phases | 2 |  | 2 | 6 |  |  |  | 4 |  |  | 8 |
| Detector Phase | 2 | 2 | 2 | 1 | 6 | 4 | 4 | 4 | 8 | 8 | 8 |

## Switch Phase

$\begin{array}{llllrlllllll}\text { Minimum Initial (s) } & 20.0 & 20.0 & 20.0 & 8.0 & 20.0 & 10.0 & 10.0 & 10.0 & 10.0 & 10.0 & 10.0 \\ \text { Minimum Split (s) } & 28.9 & 28.9 & 28.9 & 12.5 & 28.9 & 29.7 & 29.7 & 29.7 & 21.7 & 21.7 & 21.7\end{array}$

| Minimum Split (s) | 28.9 | 28.9 | 28.9 | 12.5 | 28.9 | 29.7 | 29.7 | 29.7 | 21.7 | 21.7 | 21.7 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Total Split (s) | 46.3 | 46.3 | 46.3 | 13.0 | 59.3 | 39.0 | 39.0 | 39.0 | 21.7 | 21.7 | 21.7 |


| Total Split $(\%)$ | $38.6 \%$ | $38.6 \%$ | $38.6 \%$ | $10.8 \%$ | $49.4 \%$ | $32.5 \%$ | $32.5 \%$ | $32.5 \%$ | $18.1 \%$ | $18.1 \%$ | $18.1 \%$ |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Yellow Time (s) | 5.4 | 5.4 | 5.4 | 3.0 | 5.4 | 5.7 | 5.7 | 5.7 | 5.7 | 5.7 | 5.7 |


|  | 1.5 | 1.5 | 1.5 | 0.0 | 1.5 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| All-Red Time (s) | 1.5 |  | s. |  |  |  |  |  |  |  |  |


|  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


|  | Lost Time Adjust(s) | 6.9 | 6.9 | 6.9 | 3.0 | 6.9 | 7.7 | 7.7 | 7.7 | 7.7 | 7.7 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Total Lost Time (s) | 6.9 | 6.7 |  |  |  |  |  |  |  |  |  |
| Lead/Lag | Lag | Lag | Lag | Lead |  |  |  |  |  |  |  |


| Lead/Lag | Lag | Lag | Lag | Lead |
| :--- | :---: | :---: | :---: | :---: |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes |


|  | C-Max | C-Max | C-Max | None | Max | None | None | None | None | None | None |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


| Act Effct Green (s) | 58.3 | 58.3 | 58.3 | 74.3 | 70.4 | 27.9 | 27.9 | 27.9 | 10.0 | 10.0 |  | 0.0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  |  |  |  |  |

I/c Ratio
Control Delay


Total Delay
LOS Approach Delay
Approach LOS $\begin{array}{lllllllllll}0.12 & 0.49 & 0.49 & 0.62 & 0.59 & 0.23 & 0.23 & 0.23 & 0.08 & 0.08 & 0.08 \\ 26.1 & 27.0 & 0.36 & 0.33 & 0.57 & 0.80 & 0.81 & 0.43 & 0.01 & 0.01 & 0.08 \\ & 27.4 & 326 & 59.5 & 01.1 & 7.3 & & & \end{array}$

## tersection Sum <br> Intersection Summa

Actuated Cycle Length: 120
Offset: 0 ( $0 \%$ ), Referenced to phase 2:EBTL, Start of Green
Natural Cycle: 95
$\begin{array}{ll}\text { Control Type: Actuated-Coordinated } & \\ \text { Maximum v/c Ratio: } 0.81 & \\ \begin{array}{ll}\text { Intersection Signal Delay: } 31.9 & \text { Intersection LOS: C } \\ \text { Intersection Capacity Utiization 86.6\% } & \text { ICU Level of Service E }\end{array}\end{array}$
Splits and Phases: 1: Davis Road \& Thorold Stone Road


[^12]Synchro 10 Report

1. Davis Road \& Thorold Stone Road
 $\begin{array}{lrrrrrrrrrrrr} & 21 & & \\ \text { Future Volume (vph) } & 21 & 929 & 274 & 87 & 1076 & 6 & 542 & 15 & 211 & 1 & 2 & 18 \\ \text { Ideal Flow (vphpl) } & 1900 & 1900 & 1900 & 1900 & 1900 & 1900 & 1900 & 1900 & 1900 & 1900 & 1900 & 1900 \\ \text { Total Lost time (s) } & 6.9 & 6.9 & 6.9 & 3.0 & 6.9 & & 7.7 & 7.7 & 7.7 & 7.7 & 7.7 & 7.7\end{array}$

|  | 6.9 | 6.9 | 6.9 | 3.0 | 6.9 | 7.7 | 7.7 | 7.7 | 7.7 | 7.7 | 7.7 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Total Lost time (s) | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 0.95 | 0.95 | 1.00 | 1.00 | 1.00 | 1.00 |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.99 | 1.00 | 1.00 | 090 |


| Frpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.99 | 1.00 | 1.00 | 0.99 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Fit | 1.00 | 1.00 | 0.05 | 1.00 | 1.00 | 1.00 | 1.00 | 0.05 | 100 | 100 | 0.05 |


| ift | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| FIt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 0.95 | 0.95 | 1.00 | 0.95 | 1.00 | 1.00 |


|  | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 0.95 | 0.95 | 1.00 | 0.95 | 1.00 | 1.00 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Satd. Flow (prot) | 1640 | 3406 | 1442 | 1530 | 3398 | 1559 | 1553 | 1475 | 1388 | 1624 | 1337 |
| FIt Permitted | 0.22 | 1.00 | 1.00 | 0.18 | 1.00 | 0.95 | 0.95 | 1.00 | 0.95 | 1.00 | 1.00 |


| Satd. Flow (perm) | 374 | 3406 | 1442 | 289 | 3398 |  | 1559 | 1553 | 1475 | 1388 | 1624 | 1337 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Peak-hour factor, PHF | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | ddj. Flow (vph) TOR Reduction

0.96
22

| Lane Group Flow (vph) | 22 | 968 | 185 | 91 | 1127 | 0 | 288 | 293 | 51 | 1 | 2 |
| :--- | ---: | :--- | :--- | :--- | :--- | :--- | :--- | :--- | ---: | :--- | :--- |


| Heavy Vehicles (\%) | $10 \%$ | $6 \%$ | $12 \%$ | $18 \%$ | $6 \%$ | $30 \%$ | $10 \%$ | $28 \%$ | $8 \%$ | $30 \%$ | $17 \%$ | $19 \%$ |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Turn Type | Perm | NA | Perm | pm + pt | NA |  | Split | NA | Perm | Split | NA | Perm |

$$
\begin{aligned}
& \text { Turn Type } \\
& \text { Protected Phases } \\
& \text { Permitted Phases }
\end{aligned}
$$

$$
\begin{aligned}
& \text { Permitted Phases } \\
& \text { Actuated Green, G (s) }
\end{aligned}
$$

$$
\begin{aligned}
& \text { Actuated Green, G (s) } \\
& \text { Effective Green. (s) }
\end{aligned}
$$

$$
\begin{aligned}
& \text { Effective Green, } g(s) \text { s) } \\
& \hline \text { Actuated } g / C \text { Ration }
\end{aligned}
$$

|  |  |  |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
|  | 6.9 | 6.9 | 6.9 | 3.0 | 6.9 | 7.7 | 7.7 | 7.7 | 7.7 | 7.7 | 7.7 |
|  | 3.0 | 3.0 | 3.0 | 2.5 | 3.0 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 |
| Lane Grp Cap (vph) | 167 | 1524 | 645 | 252 | 1863 | 362 | 361 | 342 | 46 | 54 | 44 |
| v/s Ratio Prot |  | co 28 |  | 0.03 | co 33 | 0.18 | $\mathrm{co.19}$ |  | 0.00 | $c 0.00$ |  |

$$
\begin{aligned}
& \text { Actuarea git raio } \\
& \text { Clearance Time (s) }
\end{aligned}
$$

$$
\begin{aligned}
& \text { Clearance Time (s) } \\
& \text { Vehicle Extension (s) }
\end{aligned}
$$

| V/s Ratio Perm | 0.06 |  | 0.13 | 0.17 |  | 0.30 | 0.80 | 0.81 | 0.03 | 0.15 | 0.02 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
|  | 0.13 | 0.64 | 0.29 | 0.36 | 0.60 | 0.04 | 0.0 |  |  |  |  |


| Uniform Delay, d1 | 19.5 | 25.6 | 21.0 | 15.6 | 18.3 | 43.4 | 43.6 | 36.6 | 56.1 | 56.1 | 56.1 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


| Progression Factor | 1.00 | 1.00 | 1.00 | 1.99 | 1.76 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| ncremental Delay, d2 | 1.6 | 2.0 | 1.1 | 0.5 | 1.2 | 12.7 | 14.2 | 0.4 | 0.3 | 0.5 | 0.0 |


|  | 1.6 | 2.0 | 1.1 | 0.5 | 1.2 | 12.7 | 14.2 | 0.4 | 0.3 | 0.5 | 0.2 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


| Delay (s) | 21.1 | 27.6 | 22.1 | 31.5 | 33.5 | 56.1 | 57.8 | 37.0 | 56.4 | 56.6 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Level of Service | C | C | C | C | C | E | E | D | E | E |
| Approach Delay (s) |  | 26.3 |  |  | 33.3 |  | 51.4 |  |  | 56.4 |
| Approach LOS |  | C |  |  | C |  | D |  |  | E | Approach LOS


| Intersection Summary |  |  |  |
| :--- | ---: | :--- | ---: |
| HCM 2000 Control Delay | 35.1 | HCM 2000 Level of Service | D |
| HCM 2000 Volume to Capacity ratio | 0.66 | Sum of lost time (s) | 25.3 |
| Actuated Ccyle Length (s) | 120.0 | E |  |
| Intersection Capacity Utilization | $86.6 \%$ | ICU Level of Service | E |

Intersection Capacity Utilization 86.6\%

CU Level of Service
E
c Critical Lane Group

2: Davis Road \& Niagara Falls Road/Beaverdams Road



[^13]Synchro 10 Report

HCM Signalized Intersection Capacity Analysis
2: Davis Road \& Niagara Falls Road/Beaverdams Road
<2025 Background> AM Peak Hou 2. Davis Road \& Niagara Falls Road/Beaverdams Road 09-14-2021
 deal Flow (vphpl) otal Lost time (s) Lane

| Total Lost time (s) | 8.1 | 8.1 |
| :--- | ---: | ---: |
| Lane Util. Factor | 1.00 | 1.00 |
| Frt | 0.99 | 0.90 |
| Flt Protected | 0.97 | 0.99 |


| FIt Protected | 0.97 |
| :--- | ---: |
| Satd. Flow (prot) | 1662 |

FIt Permitted


|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| RTOR Reduction (vph) | 0 | 2 | 0 | 0 | 74 | 0 | 0 | 13 | 0 | 0 | 0 | 0 | 33 |


| Lane Group Flow (vph) | 0 | 160 | 0 | 0 | 155 | 0 | 17 | 547 | 0 | 86 | 253 |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Heavy Vehicles (\%) | $10 \%$ | $7 \%$ | $7 \%$ | $7 \%$ | $12 \%$ | $2 \%$ | $30 \%$ | $15 \%$ | $7 \%$ | $1 \%$ | $21 \%$ | 16 |
| Turn Type | Perm | NA |  | Perm | NA |  | Perm | NA |  | Perm | NA | Per |

Tum Type Protected Phases

| Permitted Phases | 2 |  | 6 |  | 4 |  | 8 |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Actuated Green, G (s) | 57.5 | 57.5 | 27.4 | 27.4 | 27.4 | 27.4 | 27.4 |  |
| Effective Green, $\mathrm{g}(\mathrm{s})$ | 57.5 | 57.5 | 27.4 | 27.4 | 27.4 | 27.4 | 27.4 |  |
| Actuated g/C Ratio | 0.58 |  | 0.58 | 0.27 | 0.27 | 0.27 | 0.27 | 0.27 |


| Effective Green, g (s) | 57.5 | 57.5 | 27.4 | 27.4 | 27.4 | 27.4 | 27.4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Actuated g/C Ratio | 0.58 | 0.58 | 0.27 | 0.27 | 0. 27 | 0.27 | 0.27 |
| Clearance Time (s) | 8.1 | 8.1 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |


| Clearance Time (s) | 8.1 | 8.1 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Vehicle Extension (s) | 3.0 | 3.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| Lane Grp Cap (vph) | 653 | 884 | 238 | 852 | 167 | 817 | 38 |

ane Grp Cap (vph)
v/s Ratio Perm
Catio
Uniform Delay, d
rogression Factor
Progression Factor
Delay (s)
-evel of Service
Approach Delay (s)
Approach LOS

| Intersection Summary |  |  |  |
| :--- | ---: | :--- | ---: |
| HCM 200 Control Delay | 26.3 | HCM 2000 Level of Service | C |
| HCM 2000 Volume to Capacity ratio | 0.37 |  | 15.1 |
| Actuated Cycle Length (s) | 100.0 | Sum of lost time (s) | E |
| Intersection Capacity Utilization | $88.3 \%$ | ICU Level of Service |  |
| Analysis Period (min) | 15 |  |  |

nalysis Period (min)
c Critical Lane Group

Timings 3: Davis Road \& Lundys Lane

| Lane Group | EBL | EBT | WBL | WBT | WBR | NBL | NBT | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \% | F | 7 | $\uparrow$ | 7 | \% | $\stackrel{1}{6}$ | \% | $\uparrow$ | 7 |
| Traffic Volume (vph) | 140 | 518 | 36 | 395 | 233 | 22 | 139 | 181 | 94 | 143 |
| Future Volume (vph) | 140 | 518 | 36 | 395 | 233 | 22 | 139 | 181 | 94 | 143 |
| Turn Type | Perm | NA | Perm | NA | Perm | Perm | NA | Perm | NA | Perm |
| Protected Phases |  | 2 |  | 6 |  |  | 4 |  | 8 |  |
| Permitted Phases | 2 |  | 6 |  | 6 | 4 |  | 8 |  | 8 |
| Detector Phase | 2 | 2 | 6 | 6 | 6 | 4 | 4 | 8 | 8 | 8 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 22.0 | 22.0 | 22.0 | 22.0 | 22.0 | 15.0 | 15.0 | 15.0 | 15.0 | 15.0 |
| Minimum Split (s) | 36.0 | 36.0 | 36.0 | 36.0 | 36.0 | 32.0 | 32.0 | 32.0 | 32.0 | 32.0 |
| Total Split (s) | 46.0 | 46.0 | 46.0 | 46.0 | 46.0 | 44.0 | 44.0 | 44.0 | 44.0 | 44.0 |
| Total Split (\%) | 51.1\% | 51.1\% | 51.1\% | 51.1\% | 51.1\% | 48.9\% | 48.9\% | 48.9\% | 48.9\% | 48.9\% |
| Yellow Time (s) | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| All-Red Time (s) | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |
| Lead/Lag |  |  |  |  |  |  |  |  |  |  |
| Lead-Lag Optimize? |  |  |  |  |  |  |  |  |  |  |
| Recall Mode | C-Max | C-Max | Max | Max | Max | None | None | None | None | None |
| Act Efft Green (s) | 53.8 | 53.8 | 53.8 | 53.8 | 53.8 | 22.2 | 22.2 | 22.2 | 22.2 | 22.2 |
| Actuated g/C Ratio | 0.60 | 0.60 | 0.60 | 0.60 | 0.60 | 0.25 | 0.25 | 0.25 | 0.25 | 0.25 |
| V/C Ratio | 0.30 | 0.52 | 0.11 | 0.40 | 0.26 | 0.09 | 0.45 | 0.76 | 0.27 | 0.33 |
| Control Delay | 12.8 | 14.2 | 11.3 | 12.5 | 2.4 | 23.5 | 29.0 | 49.5 | 27.1 | 5.9 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 12.8 | 14.2 | 11.3 | 12.5 | 2.4 | 23.5 | 29.0 | 49.5 | 27.1 | 5.9 |
| LOS | B | B | B | B | A | C | C | D | C | A |
| Approach Delay |  | 13.9 |  | 8.9 |  |  | 28.4 |  | 29.6 |  |
| Approach LOS |  | B |  | A |  |  | C |  | C |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 90 |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 90 |  |  |  |  |  |  |  |  |  |  |
| Offset: $0(0 \%)$, Referenced to phase 2:EBTL, Start of Green |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 70 |  |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Coordinated |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.76 |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 16.9 |  |  |  |  | tersection | LOS: B |  |  |  |  |
| Intersection Capacity Utilization 95.0\% |  |  |  | ICU Level of Service F |  |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |



[^14]Synchro 10 Report

HCM Signalized Intersection Capacity Analysis
3: Davis Road \& Lundys Lane
<2025 Background> AM Peak Hour 3. Davis Road \& Lundys Lane

 | Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Total Lost time (s) | 7.0 | 7.0 |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  | 7.0 | 7.0 | 7.0 | $\begin{array}{lrrrrrrrrrr}\text { Total Lost time (s) } & 7.0 & 7.0 & 7.0 & 7.0 & 7.0 & 7.0 & 7.0 & 7.0 & 7.0 & 7.0 \\ \text { Lane Util. Factor } & 1.00 & 1.00 & 1.00 & 1.00 & 1.00 & 1.00 & 1.00 & 1.00 & 1.00 & 1.00 \\ & 1.00 & 1.00 & 1.00 & 1.00 & 1.00 & 1.00 & 100 & 1.00 & 100 & 100\end{array}$

| Frpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt | 1.00 | 0.99 | 1.00 | 1.00 | 0.85 | 1.00 | 0.98 | 1.00 | 1.00 | 0.85 |


|  | 1.00 | 0.99 | 1.00 | 1.00 | 0.85 | 1.00 | 0.98 | 1.00 | 1.00 | 0.85 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| FIt | Protected | 0.95 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 0.95 | 1.00 |


| Flt Protected | 0.95 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 0.95 | 1.00 | 1.00 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Satd. Flow (prot) | 1656 | 1825 | 1467 | 1743 | 1442 | 1444 | 1529 | 1530 | 1532 | 1392 |
| Flt Permitted | 0.48 | 1.00 | 0.37 | 1.00 | 1.00 | 0.69 | 1.00 | 0.64 | 1.00 | 1.00 |


| Satd. Flow (perm) | 834 | 1825 | 569 | 1743 | 1442 | 1052 | 1529 | 1030 | 1532 | 1392 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |

Adj. Flow (vph)


|  |  |  |  |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| ane Group Flow (vph) | 149 | 1 | 0 | 0 | 0 | 100 | 0 | 9 | 0 | 0 | 0 | 115 |



| Heavy Vehicles (\%) | $9 \%$ | $3 \%$ | $19 \%$ | $23 \%$ | $9 \%$ | $12 \%$ | $25 \%$ | $20 \%$ | $30 \%$ | $18 \%$ | $24 \%$ | $16 \%$ |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Turn Tyye | Perm | NA |  | Perm | NA | Perm | Perm | NA |  | Perm | NA | Perm |

Type
rotected Phases


#### Abstract

Permitted Phases


$\begin{array}{lll} & 53.8 & 53.8\end{array}$
Effective Green, $g$ (s)
Actuated g/C Ratio
Clearance Time (s)

|  |  |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Lane Grp Cap (vph) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |
| v/s Ratio Prot | 498 | 1090 | 340 | 1041 | 861 | 259 | 377 | 254 | 377 | 343 |
|  |  | c 0.31 |  | 0.24 |  |  | 0.11 |  | 0.07 |  |


|  | co.31 |  | 0.24 |  |  | 0.11 |  | 0.07 | 0.19 | 0.07 | 0.03 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


|  | 0.30 | 0.52 | 0.11 | 0.40 | 0.17 | 0.09 | 0.44 | 0.76 | 0.27 | 0.6 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Uniform Delay, d1 | 8.9 | 10.6 |  | 7.8 | 9.6 | 8.1 | 26.1 | 28.6 | 31.4 | 27.3 |


| Progression Factor | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


| ncremental Delay, d2 | 1.5 | 1.8 | 0.7 | 1.2 | 0.4 | 0.1 | 0.3 | 11.0 | 0.1 | 0.1 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


| Level of Service | B | B | A | B | A | C | C | D |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Approach Delay (s) | 12.0 |  | 9.9 |  |  | 28.6 | C |  |
| Approach LOS |  | B |  |  |  |  |  |  |


| Intersection Summary |  |  |  |
| :--- | :--- | :--- | ---: |
| HCM 2000 Control Delay | 17.5 | HCM 2000 Level of Service | B |
| HCM 2000 Volume to Capacity ratio | 0.59 | Sum of lost time (s) | 14.0 |


| HCM 2000 Volume to Capacity ratio | 0.59 |  |  |
| :--- | ---: | :--- | ---: |
| Actuated Cycle Length (s) | 90.0 | Sum of lost time (s) | 14.0 |
| Intersection Capacity Utilization | $95.0 \%$ | ICU Level of Service | F |

Intersection Capacity Utilization
95.0\%

F
c Critical Lane Group

Timings
4：Thorold Townline Road \＆Thorold Stone Road

|  |  |  |  |  |  |  |  | 4 |  | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | SBL | SBT |
| Lane Configurations | \％ | 个个 | 「 | \％ | 个 $\uparrow$ | 7 | ${ }^{7}$ | A | ${ }^{7}$ | $\hat{\square}$ |
| Traffic Volume（vph） | 323 | 659 | 95 | 110 | 807 | 73 | 82 | 130 | 52 | 141 |
| Future Volume（vph） | 323 | 659 | 95 | 110 | 807 | 73 | 82 | 130 | 52 | 141 |
| Turn Type | pm＋pt | NA | Perm | pm＋pt | NA | Perm | pm＋pt | NA | Perm | NA |
| Protected Phases | 5 | 2 |  | 1 | 6 |  | 7 | 4 |  | 8 |
| Permitted Phases | 2 |  | 2 | 6 |  | 6 | 4 |  | 8 |  |
| Detector Phase | 5 | 2 | 2 | 1 | 6 | 6 | 7 | 4 | 8 | 8 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 8.0 | 10.0 | 10.0 | 8.0 | 10.0 | 10.0 | 8.0 | 10.0 | 10.0 | 10.0 |
| Minimum Split（s） | 11.0 | 35.1 | 35.1 | 12.5 | 35.1 | 35.1 | 11.0 | 41.4 | 41.4 | 41.4 |
| Total Split（s） | 30.0 | 49.2 | 49.2 | 17.8 | 37.0 | 37.0 | 11.0 | 53.0 | 42.0 | 42.0 |
| Total Split（\％） | 25．0\％ | 41．0\％ | 41．0\％ | 14．8\％ | 30．8\％ | 30．8\％ | 9．2\％ | 44．2\％ | 35．0\％ | 35．0\％ |
| Yellow Time（s） | 3.0 | 4.1 | 4.1 | 3.0 | 4.1 | 4.1 | 3.0 | 4.1 | 4.1 | 4.1 |
| All－Red Time（s） | 0.0 | 2.0 | 2.0 | 0.0 | 2.0 | 2.0 | 0.0 | 2.3 | 2.3 | 2.3 |
| Lost Time Adjust（s） | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time（s） | 3.0 | 6.1 | 6.1 | 3.0 | 6.1 | 6.1 | 3.0 | 6.4 | 6.4 | 6.4 |
| Lead／Lag | Lead | Lag | Lag | Lead | Lag | Lag | Lead |  | Lag | Lag |
| Lead－Lag Optimize？ | Yes | Yes | Yes | Yes | Yes | Yes | Yes |  | Yes | Yes |
| Recall Mode | None | C－Max | C－Max | None | C－Max | C－Max | None | None | None | None |
| Act Effict Green（s） | 72.5 | 56.6 | 56.6 | 58.2 | 45.1 | 45.1 | 41.3 | 37.9 | 29.1 | 29.1 |
| Actuated g／C Ratio | 0.60 | 0.47 | 0.47 | 0.48 | 0.38 | 0.38 | 0.34 | 0.32 | 0.24 | 0.24 |
| v／c Ratio | 0.79 | 0.42 | 0.14 | 0.32 | 0.64 | 0.12 | 0.44 | 0.37 | 0.20 | 0.89 |
| Control Delay | 51.1 | 37.5 | 22.0 | 16.4 | 37.3 | 2.5 | 31.7 | 28.6 | 35.6 | 60.2 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 51.1 | 37.5 | 22.0 | 16.4 | 37.3 | 2.5 | 31.7 | 28.6 | 35.6 | 60.2 |
| LOS | D | D | C | B | D | A | C | C | D | E |
| Approach Delay |  | 40.2 |  |  | 32.4 |  |  | 29.6 |  | 57.0 |
| Approach LOS |  | D |  |  | C |  |  | C |  | E |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |
| Cycle Length： 120 |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length： 120 |  |  |  |  |  |  |  |  |  |  |
| Offset： 0 （0\％），Referenced to phase 2：EBTL and 6：WBTL，Start of Green |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle： 100 |  |  |  |  |  |  |  |  |  |  |
| Control Type：Actuated－Coordinated |  |  |  |  |  |  |  |  |  |  |
| Maximum v／c Ratio： 0.89 |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay： 38.8 |  |  |  |  | Itersection | LOS：D |  |  |  |  |
| Intersection Capacity Utilization 85．8\％ |  |  |  |  |  |  |  |  |  |  |
| Analysis Period（min） 15 |  |  |  | ICU Level of Service E |  |  |  |  |  |  |



|  | 4 |  |  | $\checkmark$ |  |  | 4 | $\uparrow$ | $p$ |  | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \％ | ¢ $\uparrow$ | $\overline{7}$ | \％ | ¢ $\uparrow$ | F | \％ | ¢ |  | \％ | $\dagger$ |  |
| Traffic Volume（vph） | 323 | 659 | 95 | 110 | 807 | 73 | 82 | 130 | 51 | 52 | 141 | 205 |
| Future Volume（vph） | 323 | 659 | 95 | 110 | 807 | 73 | 82 | 130 | 51 | 52 | 141 | 205 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time（s） | 3.0 | 6.1 | 6.1 | 3.0 | 6.1 | 6.1 | 3.0 | 6.4 |  | 6.4 | 6.4 |  |
| Lane Util．Factor | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 |  |
| Frpb，ped／bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.97 | 1.00 | 1.00 |  | 1.00 | 1.00 |  |
| Flpb，ped／bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 |  |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 0.96 |  | 1.00 | 0.91 |  |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |  | 0.95 | 1.00 |  |
| Satd．Flow（prot） | 1641 | 3471 | 1369 | 1444 | 3505 | 1453 | 1492 | 1554 |  | 1641 | 1474 |  |
| Flt Permitted | 0.18 | 1.00 | 1.00 | 0.39 | 1.00 | 1.00 | 0.22 | 1.00 |  | 0.64 | 1.00 |  |
| Satd．Flow（perm） | 317 | 3471 | 1369 | 594 | 3505 | 1453 | 339 | 1554 |  | 1104 | 1474 |  |
| Peak－hour factor，PHF | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 |
| Adj．Flow（vph） | 336 | 686 | 99 | 115 | 841 | 76 | 85 | 135 | 53 | 54 | 147 | 214 |
| RTOR Reduction（vph） | 0 | 0 | 50 | 0 | 0 | 48 | 0 | 13 | 0 | 0 | 47 |  |
| Lane Group Flow（vph） | 336 | 686 | 49 | 115 | 841 | 28 | 85 | 175 | 0 | 54 | 314 |  |
| Confl．Peds．（\＃／hr） | 4 |  |  |  |  | 4 |  |  |  |  |  |  |
| Heavy Vehicles（\％） | 10\％ | 4\％ | 18\％ | 25\％ | 3\％ | 8\％ | 21\％ | 14\％ | 25\％ | 10\％ | 18\％ | 17\％ |
| Turn Type | pm＋pt | NA | Perm | pm＋pt | NA | Perm | pm＋pt | NA |  | Perm | NA |  |
| Protected Phases | 5 | 2 |  | 1 | 6 |  | 7 | 4 |  |  | 8 |  |
| Permitted Phases | 2 |  | 2 | 6 |  | 6 | 4 |  |  | 8 |  |  |
| Actuated Green，G（s） | 69.0 | 56.0 | 56.0 | 54.5 | 44.5 | 44.5 | 38.5 | 38.5 |  | 29.1 | 29.1 |  |
| Effective Green， $\mathrm{g}(\mathrm{s})$ | 69.0 | 56.0 | 56.0 | 54.5 | 44.5 | 44.5 | 38.5 | 38.5 |  | 29.1 | 29.1 |  |
| Actuated g／C Ratio | 0.58 | 0.47 | 0.47 | 0.45 | 0.37 | 0.37 | 0.32 | 0.32 |  | 0.24 | 0.24 |  |
| Clearance Time（s） | 3.0 | 6.1 | 6.1 | 3.0 | 6.1 | 6.1 | 3.0 | 6.4 |  | 6.4 | 6.4 |  |
| Vehicle Extension（s） | 2.5 | 6.0 | 6.0 | 2.5 | 6.0 | 6.0 | 2.5 | 2.3 |  | 2.3 | 2.3 |  |
| Lane Grp Cap（vph） | 419 | 1619 | 638 | 340 | 1299 | 538 | 170 | 498 |  | 267 | 357 |  |
| $\mathrm{v} / \mathrm{s}$ Ratio Prot | c0．14 | 0.20 |  | 0.03 | 0.24 |  | c0．03 | 0.11 |  |  | c0．21 |  |
| $\mathrm{v} / \mathrm{s}$ Ratio Perm | c0．32 |  | 0.04 | 0.13 |  | 0.02 | 0.13 |  |  | 0.05 |  |  |
| v／c Ratio | 0.80 | 0.42 | 0.08 | 0.34 | 0.65 | 0.05 | 0.50 | 0.35 |  | 0.20 | 0.88 |  |
| Uniform Delay，d1 | 19.6 | 21.3 | 17.7 | 19.4 | 31.3 | 24.2 | 31.1 | 31.2 |  | 36.2 | 43.8 |  |
| Progression Factor | 2.18 | 1.58 | 3.81 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 |  |
| Incremental Delay，d2 | 8.8 | 0.7 | 0.2 | 0.4 | 2.5 | 0.2 | 1.7 | 0.3 |  | 0.2 | 20.7 |  |
| Delay（s） | 51.5 | 34.3 | 67.6 | 19.9 | 33.8 | 24.4 | 32.8 | 31.4 |  | 36.4 | 64.5 |  |
| Level of Service | D | c | E | B | C | c | C | c |  | D | E |  |
| Approach Delay（s） |  | 42.4 |  |  | 31.5 |  |  | 31.9 |  |  | 60.8 |  |
| Approach LOS |  | D |  |  | C |  |  | C |  |  | E |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 2000 Control Delay |  |  | 40.1 |  | HCM 2000 | Level of S | Service |  | D |  |  |  |
| HCM 2000 Volume to Capacity ratio |  |  | 0.83 |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length（s） |  |  | 120.0 |  | Sum of lost | time（s） |  |  | 18.5 |  |  |  |
| Intersection Capacity Utilization |  |  | 85．8\％ |  | CU Level | of Service |  |  | E |  |  |  |
| Analysis Period（min） |  |  | 15 |  |  |  |  |  |  |  |  |  |
| c Critical Lane Group |  |  |  |  |  |  |  |  |  |  |  |  |

Timings
<2025 Background> AM Peak Hour
09-14-202
5: Thorold Townline Road \& Lundys Lane
$\uparrow \downarrow \downarrow \downarrow$

| Lane Group | EBL | EBT | EBR | WBL | WBT | NBL | NBT | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ${ }^{*}$ | $\uparrow$ | F' | * | $\hat{\beta}$ | ${ }^{7}$ | ${ }_{6}$ | * | $\uparrow$ | F |
| Traffic Volume (vph) | 157 | 521 | 98 | 38 | 348 | 71 | 140 | 22 | 85 | 56 |
| Future Volume (vph) | 157 | 521 | 98 | 38 | 348 | 71 | 140 | 22 | 85 | 56 |
| Turn Type | Perm | NA | Perm | Perm | NA | Perm | NA | Perm | NA | Perm |
| Protected Phases |  | 2 |  |  | 6 |  | 4 |  | 8 |  |
| Permitted Phases | 2 |  | 2 | 6 |  | 4 |  | 8 |  | 8 |
| Detector Phase | 2 | 2 | 2 | 6 | 6 | 4 | 4 | 8 | 8 | 8 |
| witch Phase |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 20.0 | 20.0 | 20.0 | 20.0 | 20.0 | 10.0 | 10.0 | 10.0 | 10.0 | 10.0 |
| Minimum Split (s) | 29.0 | 29.0 | 29.0 | 29.0 | 29.0 | 35.0 | 35.0 | 35.0 | 35.0 | 35.0 |
| Total Split (s) | 65.0 | 65.0 | 65.0 | 65.0 | 65.0 | 35.0 | 35.0 | 35.0 | 35.0 | 35.0 |
| Total Split (\%) | 65.0\% | 65.0\% | 65.0\% | 65.0\% | 65.0\% | 35.0\% | 35.0\% | 35.0\% | 35.0\% | 35.0\% |
| Yellow Time (s) | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| All-Red Time (s) | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 |
| Lead/Lag |  |  |  |  |  |  |  |  |  |  |
| Lead-Lag Optimize? |  |  |  |  |  |  |  |  |  |  |
| Recall Mode | C-Max | C-Max | C-Max | Max | Max | None | None | None | None | None |
| Act Efft Green (s) | 68.8 | 68.8 | 68.8 | 68.8 | 68.8 | 18.2 | 18.2 | 18.2 | 18.2 | 18.2 |
| Actuated g/C Ratio | 0.69 | 0.69 | 0.69 | 0.69 | 0.69 | 0.18 | 0.18 | 0.18 | 0.18 | 0.18 |
| v/c Ratio | 0.29 | 0.45 | 0.10 | 0.08 | 0.34 | 0.35 | 0.63 | 0.15 | 0.31 | 0.22 |
| Control Delay | 8.8 | 9.2 | 3.6 | 6.9 | 7.8 | 38.8 | 43.8 | 34.1 | 36.6 | 10.3 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 8.8 | 9.2 | 3.6 | 6.9 | 7.8 | 38.8 | 43.8 | 34.1 | 36.6 | 10.3 |
| LOS | A | A | A | A | A | D | D | c | D | B |
| Approach Delay |  | 8.4 |  |  | 7.7 |  | 42.4 |  | 27.3 |  |
| Approach LOS |  | A |  |  | A |  | D |  | C |  |

$\frac{\text { Intersection Summary }}{\text { Cycle Length } 100}$
ycle Length: 100
Offset: 0 ( $0 \%$ ), Referenced to phase 2:EBTL, Start of Green
Natural Cycle: 65
$\begin{array}{ll}\text { Control Type: Actuated-Coordinated } & \\ \text { Maximum v/c Ratio: } 0.63 & \text { Intersection LOS: B } \\ \text { Intersection Signal Delay: } 15.4 & \text { ICU Level of Service D } \\ \text { Intersection Capacity Utilization 79.0\% }\end{array}$
Analysis Period (min) 15


[^15]Synchro 10 Report

HCM Signalized Intersection Capacity Analysis
5: Thorold Townline Road \& Lundys Lane
<2025 Background> AM Peak Hour

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \% | $\uparrow$ | F | \% | $\hat{F}$ |  | 7 | A |  | 7 | $\uparrow$ | 「 |
| Traffic Volume (vph) | 157 | 521 | 98 | 38 | 348 | 39 | 71 | 140 | 37 | 22 | 85 | 56 |
| Future Volume (vph) | 157 | 521 | 98 | 38 | 348 | 39 | 71 | 140 | 37 | 22 | 85 | 56 |


|  | Future Volume (vph) | 157 | 521 | 98 | 38 | 348 | 39 | 71 | 140 | 37 | 22 | 85 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
|  | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 190 |


| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 19000 | 1900 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Total Lost time (s) | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  | 6.0 | 6.0 |  | 6.0 | 6.0 | 6.0 |


| ane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
|  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |


| Frpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
|  |  | 1.00 | 1.05 |  |  |  | 1.0 | 10 | 1.00 | 10 |


|  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Fipb, ped/bikes | 1.00 | 1.00 | 0.85 | 1.00 | 0.98 | 1.00 | 0.97 | 1.00 | 1.00 | 0.85 |
|  | 0.05 | 1.00 | 1.00 | 005 | 1.00 | 0.05 | 1.00 |  |  |  |


|  | 1.00 | 1.00 | 0.85 | 1.00 | 0.98 | 1.00 | 0.97 | 1.00 | 1.00 | 0.80 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| FIt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 0.95 | 1.00 | 0.95 | 1.00 | 1.00 |
|  | 1581 | 1810 | 1495 | 1752 | 1771 | 1612 | 1607 | 1671 | 1638 | 1252 |


|  | 1581 | 1810 | 1495 | 1752 | 1771 | 1612 | 1607 | 1671 | 1638 | 1252 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Satd. Flow (prot) | 0.50 | 1.00 | 1.00 | 0.41 | 1.00 | 0.70 | 1.00 | 0.51 | 1.00 | 1.00 |


|  | 834 | 1810 | 1495 | 752 | 1771 |  | 1184 | 1607 |  | 893 | 1638 | 1252 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Peak-how (pactor) | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 |

Adj. Flow (vph)

|  |  |  |  |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| VOR Reduction (vph) | 0 | 0 | 17 | 0 | 3 | 0 | 0 | 0 | 11 | 0 | 0 | 0 |
| 49 | 169 | 560 | 88 | 41 | 413 | 0 | 76 | 180 | 0 | 24 | 91 | 11 |


| Lane Group Flow (vph) | 169 | 560 | 88 | 41 | 413 | 0 | 76 | 180 | 0 | 24 | 91 | 11 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Confl. Peds. (\#hr) | 1 |  | $14 \%$ | $5 \%$ | $8 \%$ | $3 \%$ | $6 \%$ | $0 \%$ | $12 \%$ | $17 \%$ | $5 \%$ | $8 \%$ |
| Heavy Vehicles (\%) | $14 \%$ | $16 \%$ | $29 \%$ |  |  |  |  |  |  |  |  |  |


| Heavy Vehicles (\%) | $14 \%$ | $5 \%$ | $8 \%$ | $3 \%$ | $6 \%$ | $0 \%$ | $12 \%$ | $17 \%$ | $5 \%$ | $8 \%$ | $16 \%$ | $29 \%$ |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Turn Type | Perm | NA | Perm | Perm | NA |  | Perm | NA |  | Perm | NA | Perm |

Protected Phases
Permitted Phases
Permitted Phases
Actuated Green, G (s)
Effective Green, $g$ (s)
Clearance Time (s)
Vehicle Extension (s)
Lane Grp Cap (vph)
v/s Ratio Prot
v/s Ratio Perm
v/c Ratio

|  | 0.20 |  | 0.06 | 0.05 |  | 0.06 |  | 0.03 | 0.06 | 0.01 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| $V C R$ Ratio | 0.29 | 0.45 | 0.09 | 0.08 | 0.34 | 0.35 | 0.62 | 0.015 | 0.31 | 0.05 |


|  | 6.1 | 7.0 | 5.2 | 5.1 | 6.3 | 35.8 | 37.7 | 34.4 | 35.4 | 33.2 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | :--- |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.0 | 1.0 | 1.0 |


|  | 1.00 | 1.00 | 1.00 | 1.0 | 1.00 | 1.00 | 1.0 | 1.00 | 1.00 | 1.00 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| hcremental Delay, d2 | 1.3 | 1.2 | 0.2 | 0.3 | 0.8 | 2.1 | 5.5 | 0.9 | 1.2 | 0.2 |


| Delay (s) | 7.4 | 8.2 | 5.3 | 5.4 | 7.1 | 37.8 | 43.2 | 35.3 | 1.2 | 0.2 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


| Level of Service | A | A | A | A | A | D | D | D | D |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Approach Delay (s) | 7.7 |  |  | 7.0 | A |  | 41.7 | D |  |


| Approach LOS | 7.7 | A | A | A |
| :--- | ---: | ---: | ---: | ---: |
|  | A | D | D | D |


| Intersection Summary |  |  |  |
| :--- | ---: | :--- | ---: |
| HCM 2000 Control Delay | 15.5 | HCM 2000 Level of Service | B |
| HCM 2000 Volume to Capacity ratio | 0.48 |  | 13.0 |
| Actuated Cycle Length (s) | 100.0 | Sum of lost time (s) | D |
| Intersection Capacity Utilization | $79.0 \%$ | ICU Level of Service |  |
| Analysis Period (min) | 15 |  |  |

Intersection Capacity Utilization 79.0\%

CU Level of Service
c Critical Lane Group

HCM Unsignalized Intersection Capacity Analysis
<2025 Background> AM Peak Hour
6: Thorold Townline Road \& Beaverdams Road


[^16]HCM Unsignalized Intersection Capacity Analysi
<2025 Background> AM Peak Hour 7: Thorold Townline Road \& Uppers Lane

|  | $\checkmark$ |  |  | $p$ |  | $\downarrow$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |  |
| Lane Configurations | M |  | $f$ |  |  | $\uparrow$ |  |
| Traffic Volume (veh/h) | - | 0 | 323 | 0 | 0 | 256 |  |
| Future Volume (Veh/h) | 0 | 0 | 323 | 0 | 0 | 256 |  |
| Sign Control | Stop |  | Free |  |  | Free |  |
| Grade | 0\% |  | 0\% |  |  | 0\% |  |
| Peak Hour Factor | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 |  |
| Hourly flow rate (vph) | 0 | 0 | 347 | 0 | 0 | 275 |  |
| Pedestrians |  |  |  |  |  |  |  |
| Lane Width (m) |  |  |  |  |  |  |  |
| Walking Speed (m/s) |  |  |  |  |  |  |  |
| Percent Blockage |  |  |  |  |  |  |  |
| Right turn flare (veh) |  |  |  |  |  |  |  |
| Median type |  |  | None |  |  | None |  |
| Median storage veh) |  |  |  |  |  |  |  |
| Upstream signal ( $m$ ) |  |  |  |  |  |  |  |
| pX, platoon unblocked |  |  |  |  |  |  |  |
| vC , conflicting volume | 622 | 347 |  |  | 347 |  |  |
| vC1, stage 1 conf vol |  |  |  |  |  |  |  |
| $v C 2$, stage 2 conf vol |  |  |  |  |  |  |  |
| vCu , unblocked vol | 622 | 347 |  |  | 347 |  |  |
| tC, single (s) | 6.4 | 6.2 |  |  | 4.1 |  |  |
| tC, 2 stage (s) |  |  |  |  |  |  |  |
| tF (s) | 3.5 | 3.3 |  |  | 2.2 |  |  |
| po queue free \% | 100 | 100 |  |  | 100 |  |  |
| cM capacity (veh/h) | 454 | 701 |  |  | 1223 |  |  |
| Direction, Lane \# | WB 1 | NB 1 | SB 1 |  |  |  |  |
| Volume Total | 0 | 347 | 275 |  |  |  |  |
| Volume Left | 0 | 0 | 0 |  |  |  |  |
| Volume Right | 0 | 0 | 0 |  |  |  |  |
| cSH | 1700 | 1700 | 1223 |  |  |  |  |
| Volume to Capacity | 0.00 | 0.20 | 0.00 |  |  |  |  |
| Queue Length 95th ( m ) | 0.0 | 0.0 | 0.0 |  |  |  |  |
| Control Delay (s) | 0.0 | 0.0 | 0.0 |  |  |  |  |
| Lane LOS | A |  |  |  |  |  |  |
| Approach Delay (s) | 0.0 | 0.0 | 0.0 |  |  |  |  |
| Approach LOS | A |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |
| Average Delay |  |  | 0.0 |  |  |  |  |
| Intersection Capacity UtilizationAnalysis Period (min) |  |  | 20.3\% | ICU Level of Service |  |  | A |
|  |  |  | 15 |  |  |  |  |

<2025 Background> PM Peak Hour 1: Davis Road \& Thorold Stone Road


## Intersection Summa

Cycle Length: 140
ngth: 140
Offset: $0(0 \%)$, Referenced to phase 2:EBTL and 6 :WBTL, Start of Green
Control Type: Actuated-Coordinated

| Control Type: Actuated-Coordinated |  |
| :--- | :--- |
| Maximum v/c Ratio: 0.79 |  |
| Intersection Signal Delay: 30.6 Intersection LOS: C <br> Intersection Capacity Utilization 87.6\% ICU Level of Service E <br> Analysis Period (min) 15  |  |

Intersection Capacity Utilization 87.6\% ICU Level of Service E
Analysis Period (min) 15


[^17]Synchro 10 Report

1. Davis Road \& Thorold Stone Road


|  | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Ideal Flow (vphpl) | 6.9 | 6.9 | 6.9 | 3.0 | 6.9 |  | 7.7 | 7.7 | 7.7 | 7.7 | 7.7 | 7.7 |
| Total Lost time (s) | 100 | 0.95 | 100 | 100 | 0.95 |  | 0.95 | 0.95 | 100 | 100 | 100 | 100 |


| Lane Util. Factor | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 0.95 | 0.95 | 1.00 | 1.00 | 1.00 | 1.00 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Frob, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.98 |


| Frpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.98 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
|  | 1.00 | 100 | 0.05 | 1.00 | 1.00 | 1.00 | 1.00 | 0.05 | 1.00 | 1.00 | 0.85 |


|  | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Frt | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 0.95 | 0.95 | 1.00 | 0.95 | 1.00 | 1.00 |
| Flt Protected | 0.1 .05 |  |  |  |  |  |  |  |  |  |  |


|  | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 0.95 | 0.95 | 1.00 | 0.95 | 1.00 | 1.00 |
| :--- | :--- | :--- | :--- | :--- | :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Satd. Flow (prot) | 1433 | 3539 | 1568 | 1671 | 3539 | 1681 | 1678 | 1482 | 1805 | 1810 | 1524 |
| FIt Permitted | 0.19 | 1.00 | 1.00 | 0.09 | 1.00 | 0.95 | 0.95 | 1.00 | 0.95 | 1.00 | 1.00 |


| Satd. Flow (perm) | 294 | 3539 | 1568 | 163 | 3539 |  | 1681 | 1678 | 1482 | 1805 | 1810 | 1524 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Peak-hour factor, PHF | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | eak-hour factor, PHF

Adj. Flow (vph)

|  | 25 | 1298 | 617 | 154 | 1225 |
| :--- | ---: | ---: | ---: | ---: | ---: |


| Lane Group Flow (vph) | 25 | 1298 | 472 | 154 | 1226 | 0 | 266 | 272 | 27 | 4 | 6 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


|  | $26 \%$ | $2 \%$ | $3 \%$ | $8 \%$ | $2 \%$ | $0 \%$ | $2 \%$ | $30 \%$ | $9 \%$ | $0 \%$ | $5 \%$ | $4 \%$ |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


| Turn Type | Perm | NA | Perm | pm +pt | NA | Split | NA | Perm | Split | NA |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | rotected Phases


| Permitted Phases | 2 | 2 | 2 | 6 |  | 4 | 4 | 4 | 8 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |


| Actuated Green, G (s) | 68.0 | 68.0 | 68.0 | 82.9 | 82.9 | 28.8 | 28.8 | 28.8 | 6.0 | 6.0 | 6.0 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Effective Green, $g(s)$ | 68.0 | 68.0 | 68.0 | 82.9 | 82.9 | 28.8 | 28.8 | 28.8 | 6.0 | 6.0 | 6.0 |


|  | 68.0 | 68.0 | 68.0 | 82.9 | 82.9 | 28.8 | 28.8 | 28.0 | 0.0 | 0.0 | 6.0 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Acfective Green, $g / C$ Ratio | 0.49 | 0.49 | 0.49 | 0.59 | 0.59 | 0.21 | 0.21 | 0.21 | 0.04 | 0.04 | 0.04 |


| Actuated ge Cime (s) | 0.49 | 6.9 | 6.9 | 3.0 | 6.9 |  | 7.7 | 7.7 | 7.7 | 7.7 | 7.7 | 7.7 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


|  |  |  |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Clearance Time (s) | 6.9 | 6.9 | 6.9 | 3.0 | 6.9 | 7.7 | 7.7 | 7.7 | 7.7 | 7.7 | 7.7 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 |


| Lane Grp Cap (vph) | 142 | 1718 | 761 | 224 | 2095 | 345 | 345 | 304 | 77 | 77 | 60 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| v/s Ratio Prot |  | $\mathrm{co.37}$ |  | $\mathrm{co.06}$ | 0.35 | 0.16 | $\mathrm{co.16}$ |  | 0.00 | $\mathrm{c0} 00$ |  |
| v/s Ratio Perm | 0.09 |  | 0.30 | 0.35 |  |  |  | 0.02 |  |  | 0.00 |


|  |  |  |  |  |  |  |  |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| W/C Ratio Perm | 0.09 | 0.18 | 0.76 | 0.62 | 0.69 | 0.59 | 0.77 | 0.79 | 0.09 | 0.05 | 0.08 |


| Uniform Delay, d1 | 20.2 | 29.2 | 26.5 | 22.6 | 17.8 | 52.5 | 52.7 | 45.0 | 64.3 | 64.3 | 64.2 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
|  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 100 | 100 | 100 | 10.0 |


| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


|  | 2.7 | 3.1 | 3.8 | 8.5 | 1.2 | 1.4 | 12.6 | 0.2 | 0.5 | 0.7 | 0.2 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


| Delay (s) | 22.9 | 32.4 | 30.3 | 31.1 | 19.0 | 63.8 | 65.3 | 45.2 | 64.8 | 65.1 | 64.4 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| evel of Service | C | C | C | C | B | E | E | D | E | E | E |
| Approach Delay (s) |  | 31.6 |  |  | 20.4 |  | 60.7 |  |  | 64.5 |  |
| Approach LOS |  | C |  |  | C |  | E |  |  | E |  | Approach LOS


| Intersection Summary |  |  |  |
| :--- | ---: | :--- | ---: |
| HCM 2000 Control Delay | 32.9 | HCM 2000 Level of Service | C |
| HCM 2000 Volume to Capacity ratio | 0.72 |  | 25.3 |
| Actuated Cycle Length (s) | 140.0 | Sum of lost time (s) | E |
| Intersection Capacity Utilization | $87.6 \%$ | ICU Level of Service |  |
| Analysis Period (min) | 15 |  |  |

Intersection Capacity Utilization 87.6\%

ICU Level of Service
c Critical Lane Group

2: Davis Road \& Niagara Falls Road/Beaverdams Road


Splits and Phases: 2: Davis Road \& Niagara Falls Road/Beaverdams Road


[^18]Synchro 10 Report

HCM Signalized Intersection Capacity Analysis
2: Davis Road \& Niagara Falls Road/Beaverdams Road

<2025 Background> PM Peak Hour 2. Davis Road \& Niagara Falls Road/Beaverdams Road 09-14-2021 $\begin{array}{lrrrrrrrrrrrr} & & \text { EBL } & \text { EBT } & \text { EBR } & \text { WBL } & \text { WBT } & \text { WBR } & \text { NBL } & \text { NBT } & \text { NBR } & \text { SBL } & \text { SBT } \\ \text { Mover }\end{array}$ |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Trafíc Volume (vph) | 90 | 32 | 17 | 74 | 44 | 147 | 12 | 409 | 50 | 170 | 471 | 105 |
| Future Volume (vph) | 90 | 32 | 19 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 |  |  |  |  |  |  |  |  | $\begin{array}{lrrrrrrr}\text { Total Lost time (s) } & 8.1 & 8.1 & 7.0 & 7.0 & 7.0 & 7.0 & 7.0 \\ \text { ane Util. Factor } & 1.00 & 1.00 & 1.00 & 0.95 & 1.00 & 0.95 & 1.00\end{array}$

| ne Util. Factor | . 00 | 1.00 | 1.00 | 0.95 | 1.00 | 0.95 | . 00 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Frt | 98 | 0.93 | 1.00 |  | 10 |  |  |


|  | 1.98 | 0.93 | 1.00 | 0.98 | 1.00 | 1.00 | 0.85 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| FIt Protected | 0.97 | 0.99 | 0.95 | 1.00 | 0.95 | 1.00 | 1.00 |
|  | 0.97 | 1717 | 0 |  | 180 | 170 | 33 |


|  | 0.97 | 0.99 | 0.95 | 1.00 | 0.95 | 1.00 | 1.09 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Satd. Flow (prot) | 1717 | 1702 | 1805 | 3298 | 1770 | 3343 | 1583 |


|  |  | 0.67 |  |  | 0.87 |  | 0.41 | 1.00 |  | 0.42 | 1.00 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Flt Permiitted |  | 1180 |  |  | 1499 |  | 771 | 3298 |  | 773 | 3343 |
| Satd. Flow (perm) | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Peak-hour factor, PHF | 0.95 | 0.95 |  |  |  |  |  |  |  |  |  |


| Peak-hour factor, PHF | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Adj. Flow (vph) | 95 | 34 | 18 | 78 | 46 | 155 | 13 | 431 | 53 | 179 | 496 | 11 |
| RTOR Reduction (vph) | 0 | 3 | 0 | 0 | 31 | 0 | 0 | 14 | 0 | 0 | 0 | 75 |

0

| Lane Group Flow (vph) | 0 | 144 | 0 | 0 | 248 | 0 | 13 | 470 | 0 | 179 | 496 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |

urn Type
隹cted Phases
Actuated Green, G (s) $\quad 2$
Effective Green, $g$ (s)
Actuated g/C Ratio
Clearance Time (s)
$\frac{\text { Venicle Extension (s) }}{\text { Lane Grp Cap (vph) }}$
s Ratio Prot
IC Ratio
Uniform Delay, d
Progression Factor
ncremental Delay, d2
Delay (s)
Level of Service
Approach Delay (s)
Approach LOS

| Intersection Summary |  |  |  |
| :--- | ---: | :--- | ---: |
| HCM 2000 Control Delay | 25.3 | HCM 2000 Level of Service | C |
| HCM 2000 Volume to Capacity ratio | 0.47 |  | 15.1 |
| Actuated Cycle Length (s) | 100.0 | Sum of lost time (s) | D |
| Intersection Capacity Utilization | $76.1 \%$ | ICU Level of Service |  |
| Analysis Period (min) | 15 |  |  |

Critical Lane Gro 3: Davis Road \& Lundys Lane

| Lane Group | EBL | EBT | WBL | WBT | WBR | NBL | NBT | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \% | f | \% | $\uparrow$ | 7 | 7 | F | \% | $\uparrow$ | F |
| Traffic Volume (vph) | 179 | 565 | 28 | 553 | 241 | 46 | 141 | 300 | 125 | 157 |
| Future Volume (vph) | 179 | 565 | 28 | 553 | 241 | 46 | 141 | 300 | 125 | 157 |
| Turn Type | pm+pt | NA | Perm | NA | Perm | Perm | NA | pm+pt | NA | Perm |
| Protected Phases | 5 | 2 |  | 6 |  |  | 4 | 3 | 8 |  |
| Permitted Phases | 2 |  | 6 |  | 6 | 4 |  | 8 |  | 8 |
| Detector Phase | 5 | 2 | 6 | 6 | 6 | 4 | 4 | 3 | 8 | 8 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 22.0 | 22.0 | 22.0 | 22.0 | 15.0 | 15.0 | 5.0 | 15.0 | 15.0 |
| Minimum Split (s) | 8.0 | 36.0 | 36.0 | 36.0 | 36.0 | 32.0 | 32.0 | 8.0 | 32.0 | 32.0 |
| Total Split (s) | 12.0 | 66.0 | 54.0 | 54.0 | 54.0 | 32.0 | 32.0 | 22.0 | 54.0 | 54.0 |
| Total Split (\%) | 10.0\% | 55.0\% | 45.0\% | 45.0\% | 45.0\% | 26.7\% | 26.7\% | 18.3\% | 45.0\% | 45.0\% |
| Yellow Time (s) | 3.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 3.0 | 5.0 | 5.0 |
| All-Red Time (s) | 0.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 0.0 | 2.0 | 2.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 3.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 3.0 | 7.0 | 7.0 |
| Lead/Lag | Lead |  | Lag | Lag | Lag | Lag | Lag | Lead |  |  |
| Lead-Lag Optimize? | Yes |  | Yes | Yes | Yes | Yes | Yes | Yes |  |  |
| Recall Mode | None | C-Max | Max | Max | Max | Max | Max | None | Max | Max |
| Act Effct Green (s) | 63.0 | 59.0 | 47.0 | 47.0 | 47.0 | 26.0 | 26.0 | 51.0 | 47.0 | 47.0 |
| Actuated g/C Ratio | 0.52 | 0.49 | 0.39 | 0.39 | 0.39 | 0.22 | 0.22 | 0.42 | 0.39 | 0.39 |
| V/c Ratio | 0.75 | 0.72 | 0.16 | 0.82 | 0.36 | 0.18 | 0.52 | 0.66 | 0.20 | 0.24 |
| Control Delay | 35.1 | 29.4 | 28.8 | 45.2 | 9.1 | 41.4 | 45.5 | 32.0 | 25.0 | 4.3 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 35.1 | 29.4 | 28.8 | 45.2 | 9.1 | 41.4 | 45.5 | 32.0 | 25.0 | 4.3 |
| LOS | D | C | C | D | A | D | D | C | C | A |
| Approach Delay |  | 30.7 |  | 34.1 |  |  | 44.7 |  | 23.0 |  |
| Approach LOS |  | C |  | C |  |  | D |  | C |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 120 |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 120 |  |  |  |  |  |  |  |  |  |  |
| Offset: $0(0 \%)$, Referenced to phase 2:EBTL, Start of Green |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 85 |  |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Coordinated |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.82 |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 31.3 |  |  |  |  | Intersection LOS: C |  |  |  |  |  |
| Intersection Capacity Utilization 108.1\% Analysis Period (min) 15 |  |  |  |  | ICU Level of Service G |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |


$\square$

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \% | $\dagger$ |  | \% | $\uparrow$ | 「 | ${ }^{7}$ | $\stackrel{\rightharpoonup}{1}$ |  | \% | $\uparrow$ |  |
| Traffic Volume (vph) | 179 | 565 | 28 | 28 | 553 | 241 | 46 | 141 | 37 | 300 | 125 | 57 |
| Future Volume (vph) | 179 | 565 | 28 | 28 | 553 | 241 | 46 | 141 | 37 | 300 | 125 | 157 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 3.0 | 7.0 |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  | 3.0 | 7.0 | 7.0 |
| Lane Util. Factor | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 |
| Frpb, ped/bikes | 1.00 | 1.00 |  | 1.00 | 1.00 | 0.98 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 |
| Flpb, ped/bikes | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 |
| Frt | 1.00 | 0.99 |  | 1.00 | 1.00 | 0.85 | 1.00 | 0.97 |  | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 |  | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |  | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1719 | 1811 |  | 1611 | 1863 | 1473 | 1736 | 1671 |  | 1702 | 1743 | 1553 |
| Flt Permitted | 0.16 | 1.00 |  | 0.29 | 1.00 | 1.00 | 0.67 | 1.00 |  | 0.48 | 1.00 | 1.00 |
| Satd. Flow (perm) | 286 | 1811 |  | 496 | 1863 | 1473 | 1226 | 1671 |  | 857 | 1743 | 1553 |
| Peak-hour factor, PHF | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 |
| Adj. Flow (vph) | 192 | 608 | 30 | 30 | 595 | 259 | 49 | 152 | 40 | 323 | 134 | 169 |
| RTOR Reduction (vph) | 0 | 2 | 0 | 0 | 0 | 144 | 0 | 8 | 0 | 0 | 0 | 103 |
| Lane Group Flow (vph) | 192 | 636 | 0 | 30 | 595 | 115 | 49 | 184 | 0 | 323 | 134 | 66 |
| Confl. Peds. (\#/hr) | 2 |  | 1 | 1 |  | 2 |  |  | 1 | 1 |  |  |
| Heavy Vehicles (\%) | 5\% | 3\% | 26\% | 12\% | 2\% | 7\% | 4\% | 9\% | 12\% | 6\% | 9\% | 4\% |


|  | $5 \%$ | $3 \%$ | $26 \%$ | $12 \%$ | $2 \%$ | $7 \%$ | $4 \%$ | $9 \%$ | $12 \%$ | $6 \%$ | $9 \%$ | $4 \%$ |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Heary Vehicles (\%) | pm+pt | NA |  | Perm | NA | Perm | Perm | NA |  | pm+pt | NA | Perm |

urn Type $\qquad$
Permitted Phases
Actuated Green, G (s)
Effective Green, $\mathrm{g}(\mathrm{s})$


Clearance Time (s)
Lane Grp Cap (vph)
Lane Grp Cap (
v/s Ratio Prot
v/s Ratio Perm
$\begin{array}{ll} & \text { c0.06 } \\ \text { Vs Ratio Perm } & 0.32 \\ \text { VIc Ratio } & 0.77\end{array}$
Uniform Delay, d1 0.77
$\begin{array}{lll} & 23.1 & 23.9\end{array}$

|  | 1.00 | 1.00 |
| :--- | :--- | :--- | :--- |
| cremental Delay, d2 | 14.0 | 4 |

$\begin{array}{llll} & 14.0 & 4.9\end{array}$
(s) Approach Delay (s) Approach LOS
Intersection Summary

| HCM 2000 Control Delay | 36.0 | HCM 2000 Level of Service | D |
| :--- | ---: | :--- | ---: |
| HCM 2000 Volume to Capacity ratio | 0.78 |  | 20.0 |
| Actuated Cycle Length (s) | 120.0 | Sum of lost time (s) | G |

Actualed Cycle Lenght (s)
108.1\%

CU Level of Service
G
Analysis Period (min)
Critical Lane Group

Timings
4: Thorold Townline Road \& Thorold Stone Road

|  | $\rangle$ |  |  |  |  |  |  | 4 |  | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | SBL | SBT |
| Lane Configurations | \% | ¢ $\uparrow$ | F | ${ }^{7}$ | 个 $\uparrow$ | F | \% | A | \% | $\hat{\square}$ |
| Traffic Volume (vph) | 231 | 1036 | 53 | 61 | 821 | 35 | 123 | 135 | 48 | 158 |
| Future Volume (vph) | 231 | 1036 | 53 | 61 | 821 | 35 | 123 | 135 | 48 | 158 |
| Turn Type | pm+pt | NA | Perm | pm+pt | NA | Perm | pm+pt | NA | pm+pt | NA |
| Protected Phases | 5 | 2 |  | 1 | 0 |  | 7 | 4 | 3 | 8 |
| Permitted Phases | 2 |  | 2 | 6 |  | 6 | 4 |  | 8 |  |
| Detector Phase | 5 | 2 | 2 | 1 | 6 | 6 | 7 | 4 | 3 | 8 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 8.0 | 10.0 | 10.0 | 5.0 | 10.0 | 10.0 | 5.0 | 10.0 | 5.0 | 10.0 |
| Minimum Split (s) | 11.0 | 35.1 | 35.1 | 8.0 | 35.1 | 35.1 | 8.0 | 41.4 | 8.0 | 41.4 |
| Total Split (s) | 21.0 | 55.0 | 55.0 | 9.6 | 43.6 | 43.6 | 13.4 | 45.9 | 9.5 | 42.0 |
| Total Split (\%) | 17.5\% | 45.8\% | 45.8\% | 8.0\% | 36.3\% | 36.3\% | 11.2\% | 38.3\% | 7.9\% | 35.0\% |
| Yellow Time (s) | 3.0 | 4.1 | 4.1 | 3.0 | 4.1 | 4.1 | 3.0 | 4.1 | 3.0 | 4.1 |
| All-Red Time (s) | 0.0 | 2.0 | 2.0 | 0.0 | 2.0 | 2.0 | 0.0 | 2.3 | 0.0 | 2.3 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 3.0 | 6.1 | 6.1 | 3.0 | 6.1 | 6.1 | 3.0 | 6.4 | 3.0 | 6.4 |
| Lead/Lag | Lead | Lag | Lag | Lead | Lag | Lag | Lead | Lag | Lead | Lag |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Recall Mode | None | C-Max | C-Max | None | C-Max | C-Max | None | None | None | None |
| Act Effict Green (s) | 65.9 | 54.9 | 54.9 | 55.1 | 45.3 | 45.3 | 48.1 | 37.1 | 41.4 | 31.7 |
| Actuated g/C Ratio | 0.55 | 0.46 | 0.46 | 0.46 | 0.38 | 0.38 | 0.40 | 0.31 | 0.34 | 0.26 |
| v/c Ratio | 0.72 | 0.66 | 0.07 | 0.30 | 0.64 | 0.05 | 0.57 | 0.49 | 0.13 | 0.92 |
| Control Delay | 29.1 | 29.4 | 0.2 | 18.9 | 35.2 | 0.1 | 32.4 | 32.1 | 21.4 | 60.7 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 29.1 | 29.4 | 0.2 | 18.9 | 35.2 | 0.1 | 32.4 | 32.1 | 21.4 | 60.7 |
| LOS | C | C | A | B | D | A | C | C | C | E |
| Approach Delay |  | 28.2 |  |  | 32.8 |  |  | 32.2 |  | 56.8 |
| Approach LOS |  | C |  |  | C |  |  | C |  | E |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 120 |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 120 |  |  |  |  |  |  |  |  |  |  |
| Offset: $0(0 \%)$, Referenced to phase 2:EBTL and 6 :WBTL, Start of Green |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 100 |  |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Coordinated |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.92 |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 34.5 |  |  |  | Intersection LOS: C |  |  |  |  |  |  |
| Intersection Capacity Utilization 84.4\% |  |  |  | ICU Level of Service E |  |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |



[^19]Synchro 10 Report

HCM Signalized Intersection Capacity Analysis
<2025 Background> PM Peak Hour 4: Thorold Townline Road \& Thorold Stone Road

9-14-202


Uppers Quarry Traffic Impact Study

Timings
<2025 Background> PM Peak Hour
09-14-2021
5: Thorold Townline Road \& Lundys Lane
$\uparrow \downarrow \downarrow$ •

| Lane Group | EBL | EBT | EBR | WBL | WBT | NBL | NBT | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ${ }_{1}$ | $\uparrow$ | F' | ${ }^{7}$ | F | ${ }_{1}$ | $\hat{\beta}$ | \% | $\uparrow$ | F |
| Traffic Volume (vph) | 81 | 527 | 103 | 44 | 555 | 113 | 131 | 52 | 118 | 130 |
| Future Volume (vph) | 81 | 527 | 103 | 44 | 555 | 113 | 131 | 52 | 118 | 130 |
| Turn Type | Perm | NA | Perm | Perm | NA | Perm | NA | Perm | NA | Perm |
| Protected Phases |  | 2 |  |  | 6 |  | 4 |  | 8 |  |
| Permitted Phases | 2 |  | 2 | 6 |  | 4 |  | 8 |  | 8 |
| Detector Phase | 2 | 2 | 2 | 6 | 6 | 4 | 4 | 8 | 8 | 8 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 20.0 | 20.0 | 20.0 | 20.0 | 20.0 | 10.0 | 10.0 | 10.0 | 10.0 | 10.0 |
| Minimum Split (s) | 29.0 | 29.0 | 29.0 | 29.0 | 29.0 | 35.0 | 35.0 | 35.0 | 35.0 | 35.0 |
| Total Split (s) | 85.0 | 85.0 | 85.0 | 85.0 | 85.0 | 35.0 | 35.0 | 35.0 | 35.0 | 35.0 |
| Total Split (\%) | 70.8\% | 70.8\% | 70.8\% | 70.8\% | 70.8\% | 29.2\% | 29.2\% | 29.2\% | 29.2\% | 29.2\% |
| Yellow Time (s) | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| All-Red Time (s) | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 |
| Lead/Lag |  |  |  |  |  |  |  |  |  |  |
| Lead-Lag Optimize? |  |  |  |  |  |  |  |  |  |  |
| Recall Mode | C-Max | C-Max | C-Max | C-Max | C-Max | None | None | None | None | None |
| Act Effct Green (s) | 86.6 | 86.6 | 86.6 | 86.6 | 86.6 | 20.4 | 20.4 | 20.4 | 20.4 | 20.4 |
| Actuated g/C Ratio | 0.72 | 0.72 | 0.72 | 0.72 | 0.72 | 0.17 | 0.17 | 0.17 | 0.17 | 0.17 |
| V/c Ratio | 0.20 | 0.44 | 0.10 | 0.09 | 0.49 | 0.67 | 0.65 | 0.43 | 0.43 | 0.38 |
| Control Delay | 8.4 | 10.9 | 4.0 | 6.8 | 9.4 | 63.3 | 51.8 | 52.5 | 47.7 | 9.2 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 8.4 | 10.9 | 4.0 | 6.8 | 9.4 | 63.3 | 51.8 | 52.5 | 47.7 | 9.2 |
| LOS | A | B | A | A | A | E | D | D | D | A |
| Approach Delay |  | 9.6 |  |  | 9.3 |  | 56.2 |  | 31.8 |  |
| Approach LOS |  | A |  |  | A |  | E |  | C |  |

## Intersection Summary

Actuated Cycle Length 120
Offset: $0(0 \%)$, Referenced to phase 2:EBTL and 6 :WBTL, Start of Green
Natural Cycle: 70
$\begin{array}{ll}\text { Control Type: Actuated-Coordinated } & \\ \text { Maximum v/c Ratio: 0.67 } & \\ \text { Intersection Signal Delay: 20.0 } & \text { Intersection LOS: C } \\ \text { Intersection Capacity Utilization } 87.8 \% & \text { ICU Level of Service E }\end{array}$
Analysis Period (min) 15


HCM Signalized Intersection Capacity Analysis 5: Thorold Townline Road \& Lundys Lane 09-14-2021
<2025 Background> PM Peak Hour


|  | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Ideal Flow (vphpl) | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  | 6.0 | 6.0 |  | 6.0 | 6.0 | 6.0 |
| Total Lost time (s) | 10 | 10 |  |  |  |  |  |  |  |  |  |  |


| Total Lost time (s) | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frpb | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |  |  |


|  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


|  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
|  | 1.00 | 1.00 | 0.85 | 1.00 | 0.99 | 1.00 | 0.96 | 1.00 | 1.00 | 0.85 |


|  | 1.00 | 1.00 | 0.85 | 1.00 | 0.99 | 1.00 | 0.96 | 1.00 | 1.00 | 0.89 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| FIt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 0.95 | 1.00 | 0.95 | 1.00 | 1.00 |
|  | 1.625 | 1827 | 1553 | 1752 | 1.03 |  | 0.62 | 170 | 173 | 170 |


| Satd. Flow (prot) | 1625 | 1827 | 1553 | 1752 | 1833 | 1687 | 1745 | 1736 | 1776 | 152 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| It Permitted | 0.36 | 1.00 | 1.00 | 0.40 | 1.00 | 0.62 | 1.00 | 0.43 | 1.00 | 1.00 |


|  | 621 | 1827 | 1553 | 739 | 1833 |  | 1094 | 1745 |  | 794 | 1776 | 152 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Satd. Flow (perm) | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 |

Adj. Flow (vph) TOR Reduction (v

|  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.9 |  |
| 89 | 579 | 113 | 48 | 610 | 35 | 124 | 144 | 55 | 57 | 130 |  |


|  | 16 | 0 | 1 | 0 | 0 | 12 | 0 | 0 | 0 | 119 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


| Lane Group Flow (vph) | 89 | 579 | 97 | 48 | 644 | 0 | 124 | 187 | 0 | 57 | 130 | 24 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Confl. Peds. (\#hr) | 1 |  |  | 1 |  |  |  |  |  |  |  |  |
| Heavy Vehicles (\%) | $11 \%$ | $4 \%$ | $4 \%$ | $3 \%$ | $2 \%$ | $15 \%$ | $7 \%$ | $6 \%$ | $0 \%$ | $4 \%$ | $7 \%$ | 6 |

Teary Vehicles (\%)
Protected Phases

| Permitted Phases | 2 | 2 |  |  | 6 | 4 | 4 | 8 | 8 | 8 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Actuated Green, G (s) | 86.6 | 86.6 | 86.6 | 86.6 | 86.6 | 20.4 | 20.4 | 20.4 | 20.4 | 20.4 |


| Actuated Green, G (s) | 86.6 | 86.6 | 86.6 | 86.6 | 86.6 | 20.4 | 20.4 | 20.4 | 20.4 | 20.4 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Effective Green, g (s) | 86.6 | 86.6 | 86.6 | 86.6 | 86.6 | 20.4 | 20.4 | 20.4 | 20.4 | 20.4 |


|  | Elfective Green, $\mathrm{g}(\mathrm{s})$ | 80.6 | 8.6 | 80.6 | 80.6 | 80.6 | 20.4 | 20.4 | 20.4 | 20.4 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Actuated $\mathrm{g} / \mathrm{C}$ Ratio | 0.72 | 0.72 | 0.72 | 0.72 | 0.72 | 0.17 | 0.17 | 0.17 | 0.17 | 0.17 |


| Clearance Time (s) | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


| Clearance Time (s) | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Vehicle Extension (s) | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| Lane Grp Cap (vph) | 448 | 1318 | 1120 | 533 | 1322 | 185 | 296 | 134 | 301 | 259 |
| v/s Ratio Prot |  | 0.32 |  |  | $c 0.35$ |  | 0.11 |  | 0.07 |  |


| v/s Ratio Prot |  | 0.32 |  | $\mathrm{co.35}$ |  |  |  |  | 0.11 |  | 0.07 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| v/s Ratio Perm | 0.14 |  | 0.06 | 0.06 |  | $c 0.11$ |  | 0.07 |  | 0.02 |  |


| v/c Ratio | 0.20 | 0.44 | 0.09 | 0.09 | 0.49 | 0.67 | 0.63 | 0.43 | 0.43 | 0.09 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


|  | 0.20 | 0.44 | 0.09 | 0.09 | 0.49 | 0.67 | 0.63 | 0.43 | 0.43 | 0.09 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Uniform Delay, d1 | 5.4 | 6.8 | 5.0 | 5.0 | 7.2 | 46.6 | 46.3 | 44.6 | 44.6 | 42.0 |
| Progression Factor | 1.12 | 1.30 | 1.19 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |



| Delay (s) | 6.8 | 9.6 | 6.0 | 5.3 | 8.5 | 58.4 | 52.3 | 49.1 | 46.7 | 42.3 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| evel of Service | A | A | A | A | A | E | D | D | D | D |


| Approach Delay (s) | 8.8 | 8.2 | 54.6 | 45.2 |
| :--- | ---: | ---: | ---: | ---: |
| ppproach LOS | A | A | D | D |


| Intersection Summary |  |  |  |
| :--- | ---: | :--- | ---: |
| HCM 2000 Control Delay | 21.2 | HCM 2000 Level of Service | C |
| HCM 2000 Volume to Capacity ratio | 0.52 |  | 13.0 |
| Actuated Cycle Length (s) | 120.0 | Sum of lost time (s) | E |
| Intersection Capacity Utilization | $87.8 \%$ | ICU Level of Service |  |
| Analysis Period (min) | 15 |  |  |

ICU Level of Service
c Critical Lane Group

HCM Unsignalized Intersection Capacity Analysis
<2025 Background> PM Peak Hour
6: Thorold Townline Road \& Beaverdams Road


[^20]HCM Unsignalized Intersection Capacity Analysis
7: Thorold Townline Road \& Uppers Lane



|  | 0 | f |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | ---: |
| Traffic Volume $($ veh/h) | 0 | 0 | 323 | 0 | 0 | 297 |
| Future Volume $(V \mathrm{Veh} / \mathrm{h})$ | 0 | 0 | 323 | 0 | 0 | 297 |

$\begin{array}{lrrrrrr}\text { Grade } & 0 \% & & 0 \% & & 0 \% \\ \text { Peak Hour Factor } & 0.91 & 0.91 & 0.91 & 0.91 & 0.91 & 0.91 \\ \text { Hourly flow rate (vph) } & 0 & 0 & 355 & 0 & 0 & 326\end{array}$

Pedestrians
Walking Speed ( $\mathrm{m} / \mathrm{s}$ )
Percent Blockage
Right turn flare (veh)

| Right | None fiare (ven) None |
| :--- | :--- | :--- |

Median storage veh)
Upstream signal ( $m$ )
X , platoon unblocked
VC , conflicting volume
vC1, stage 1 conf vol
vC2, stage 2 conf vol

|  |  |  |  |
| :--- | :--- | :--- | :--- |
| Cu, unblocked vol | 681 | 355 | 355 |


| vCu, unblocked vol | 681 | 355 | 355 |
| :--- | ---: | ---: | ---: |
| tC , single (s) | 6.4 | 6.2 | 4.1 |
| $\mathrm{tC}, 2$ stage (s) | 3.5 | 3.3 | 2.2 |
| tF (s) | 100 |  |  |
| po queue free \% | 100 | 100 | 100 |
| cM capacity (veh/h) | 419 | 693 | 1215 |


| Direction, Lane \# | WB 1 | NB 1 | SB 1 |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | :--- |
| Volume Total | 0 | 355 | 326 |  |  |  |
| Volume Left | 0 | 0 | 0 |  |  |  |
| Volume Right | 0 | 0 | 0 |  |  |  |
| cSH | 1700 | 1700 | 1215 |  |  |  |
| Volume to Capacity | 0.00 | 0.21 | 0.00 |  |  |  |
| Queue Length 95th (m) | 0.0 | 0.0 | 0.0 |  |  |  |
| Control Delay (s) | 0.0 | 0.0 | 0.0 |  |  |  |
| Lane LOS | A |  |  |  |  |  |
| Approach Delay (s) | 0.0 | 0.0 | 0.0 |  | A |  |
| Approach LOS | A |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |
| Average Delay |  | 0.0 | ICU Level of Service |  |  |  |
| Intersection Capacity Utilization |  | $20.3 \%$ |  |  |  |  |

Analysis Period (min)
<2025 Total - Thorold Townline> AM Peak Hour
1: Davis Road \& Thorold Stone Road

| Lane Group | EBL | EBT | EBR | WBL | WBT | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \% | $\uparrow \uparrow$ | 7 | \% | 个t | 7 | $\uparrow$ | 「 | ${ }^{7}$ | $\uparrow$ | 7 |
| Traffic Volume (vph) | 21 | 948 | 274 | 87 | 1102 | 542 | 15 | 211 | 1 | 2 | 18 |
| Future Volume (vph) | 21 | 948 | 274 | 87 | 1102 | 542 | 15 | 211 | 1 | 2 | 18 |
| Turn Type | Perm | NA | Perm | Perm | NA | Split | NA | Perm | Split | NA | Perm |
| Protected Phases |  | 2 |  |  | 6 | 4 | 4 |  | 8 | 8 |  |
| Permitted Phases | 2 |  | 2 | 6 |  |  |  | 4 |  |  | 8 |
| Detector Phase | 2 | 2 | 2 | 6 | 6 | 4 | 4 | 4 | 8 | 8 | 8 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 20.0 | 20.0 | 20.0 | 20.0 | 20.0 | 10.0 | 10.0 | 10.0 | 10.0 | 10.0 | 10.0 |
| Minimum Split (s) | 28.9 | 28.9 | 28.9 | 28.9 | 28.9 | 29.7 | 29.7 | 29.7 | 21.7 | 21.7 | 21.7 |
| Total Split (s) | 58.0 | 58.0 | 58.0 | 58.0 | 58.0 | 40.0 | 40.0 | 40.0 | 22.0 | 22.0 | 22.0 |
| Total Split (\%) | 48.3\% | 48.3\% | 48.3\% | 48.3\% | 48.3\% | 33.3\% | 33.3\% | 33.3\% | 18.3\% | 18.3\% | 18.3\% |
| Yellow Time (s) | 5.4 | 5.4 | 5.4 | 5.4 | 5.4 | 5.7 | 5.7 | 5.7 | 5.7 | 5.7 | 5.7 |
| All-Red Time (s) | 1.5 | 1.5 | 1.5 | 1.5 | 1.5 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 6.9 | 6.9 | 6.9 | 6.9 | 6.9 | 7.7 | 7.7 | 7.7 | 7.7 | 7.7 | 7.7 |
| Lead/Lag |  |  |  |  |  |  |  |  |  |  |  |
| Lead-Lag Optimize? |  |  |  |  |  |  |  |  |  |  |  |
| Recall Mode | C-Max | C-Max | C-Max | Max | Max | None | None | None | None | None | None |
| Act Effict Green (s) | 70.1 | 70.1 | 70.1 | 70.1 | 70.1 | 28.3 | 28.3 | 28.3 | 10.0 | 10.0 | 10.0 |
| Actuated g/C Ratio | 0.58 | 0.58 | 0.58 | 0.58 | 0.58 | 0.24 | 0.24 | 0.24 | 0.08 | 0.08 | 0.08 |
| v/c Ratio | 0.13 | 0.51 | 0.31 | 0.44 | 0.59 | 0.78 | 0.80 | 0.43 | 0.01 | 0.01 | 0.09 |
| Control Delay | 19.3 | 18.3 | 6.0 | 33.5 | 24.8 | 58.2 | 59.7 | 7.2 | 51.0 | 51.0 | 0.9 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 19.3 | 18.3 | 6.0 | 33.5 | 24.8 | 58.2 | 59.7 | 7.2 | 51.0 | 51.0 | 0.9 |
| LOS | B | B | A | C | C | E | E | A | D | D | A |
| Approach Delay |  | 15.6 |  |  | 25.4 |  | 44.7 |  |  | 7.7 |  |
| Approach LOS |  | B |  |  | C |  | D |  |  | A |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 120 |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 120 |  |  |  |  |  |  |  |  |  |  |  |
| Offset: 0 (0\%), Referenced to phase 2:EBTL, Start of Green |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 85 |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Coordinated |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.80 |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 26.1 |  |  |  | Intersection LOS: C |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 87.3\% |  |  |  | ICU Level of Service E |  |  |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |  |



[^21]Synchro 10 Report

HCM Signalized Intersection Capacity Analysis<2025 Total - Thorold Townline> AM Peak Hour 1: Davis Road \& Thorold Stone Road


Timings 2: Davis Road \& Niagara Falls Road/Beaverdams Road

|  | $\rangle$ | $\rightarrow$ | $\checkmark$ |  | 4 | $\uparrow$ |  |  | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | WBL | WBT | NBL | NBT | SBL | SBT | SBR |
| Lane Configurations |  | $\dagger$ |  | ¢ | \% | 性 | * | $\uparrow \uparrow$ | 7 |
| Traffic Volume (vph) | 110 | 31 | 34 | 17 | 16 | 473 | 82 | 240 | 44 |
| Future Volume (vph) | 110 | 31 | 34 | 17 | 16 | 473 | 82 | 240 | 44 |
| Turn Type | Perm | NA | Perm | NA | Perm | NA | Perm | NA | Perm |
| Protected Phases |  | 2 |  | 6 |  | 4 |  | 8 |  |
| Permitted Phases | 2 |  |  |  | 4 |  | 8 |  | 8 |
| Detector Phase | 2 | 2 | 6 | 6 | 4 | 4 | 8 | 8 | 8 |
| Switch Phase |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 10.0 | 10.0 | 10.0 | 10.0 | 25.0 | 25.0 | 25.0 | 25.0 | 25.0 |
| Minimum Split (s) | 38.1 | 38.1 | 38.1 | 38.1 | 32.0 | 32.0 | 32.0 | 32.0 | 32.0 |
| Total Split (s) | 50.0 | 50.0 | 50.0 | 50.0 | 50.0 | 50.0 | 50.0 | 50.0 | 50.0 |
| Total Split (\%) | 50.0\% | 50.0\% | 50.0\% | 50.0\% | 50.0\% | 50.0\% | 50.0\% | 50.0\% | 50.0\% |
| Yellow Time (s) | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| All-Red Time (s) | 3.1 | 3.1 | 3.1 | 3.1 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |
| Lost Time Adjust (s) |  | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) |  | 8.1 |  | 8.1 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |
| Lead/Lag |  |  |  |  |  |  |  |  |  |
| Lead-Lag Optimize? |  |  |  |  |  |  |  |  |  |
| Recall Mode | C-Max | C-Max | Max | Max | None | None | None | None | None |
| Act Effict Green (s) |  | 57.5 |  | 57.5 | 27.4 | 27.4 | 27.4 | 27.4 | 27.4 |
| Actuated g/C Ratio |  | 0.58 |  | 0.58 | 0.27 | 0.27 | 0.27 | 0.27 | 0.27 |
| $\mathrm{v} / \mathrm{C}$ Ratio |  | 0.25 |  | 0.24 | 0.07 | 0.65 | 0.51 | 0.31 | 0.11 |
| Control Delay |  | 12.2 |  | 3.9 | 26.1 | 34.6 | 41.8 | 29.4 | 5.8 |
| Queue Delay |  | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay |  | 12.2 |  | 3.9 | 26.1 | 34.6 | 41.8 | 29.4 | 5.8 |
| LOS |  | B |  | A | C | C | D | C | A |
| Approach Delay |  | 12.2 |  | 3.9 |  | 34.3 |  | 29.3 |  |
| Approach LOS |  | B |  | A |  | C |  | C |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |
| Cycle Length: 100 |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 100 |  |  |  |  |  |  |  |  |  |
| Offset: 0 (0\%), Referenced to phase 2:EBTL, Start of Green |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 75 |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Coordinated |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.65 |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 25.1 |  |  |  |  | Itersection | LOS: C |  |  |  |
| Intersection Capacity Utilization 88.3\% |  |  |  |  | CU Level | of Service |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |



[^22]Synchro 10 Report

HCM Signalized Intersection Capacity Analysis<2025 Total - Thorold Townline> AM Peak Hour 2: Davis Road \& Niagara Falls Road/Beaverdams Road


[^23]Synchro 10 Report



[^24]Synchro 10 Report

HCM Signalized Intersection Capacity Analysis<2025 Total - Thorold Townline> AM Peak Hour 3: Davis Road \& Lundys Lane


Timings
<2025 Total - Thorold Townline> AM Peak Hour 4: Thorold Townline Road \& Thorold Stone Road 09-23-2021

| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | SBL | SBT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \% | 个 $\uparrow$ | F | \% | 个 $\uparrow$ | F | \% | $\hat{\dagger}$ | \% | A |
| Traffic Volume (vph) | 323 | 659 | 114 | 124 | 807 | 73 | 108 | 150 | 52 | 154 |
| Future Volume (vph) | 323 | 659 | 114 | 124 | 807 | 73 | 108 | 150 | 52 | 154 |
| Turn Type | pm+pt | NA | Perm | pm+pt | NA | Perm | pm+pt | NA | Perm | NA |
| Protected Phases | 5 | 2 |  | 1 | 6 |  | 7 | 4 |  | 8 |
| Permitted Phases | 2 |  | 2 | 6 |  | 6 | 4 |  | 8 |  |
| Detector Phase | 5 | 2 | 2 | 1 | 6 | 6 | 7 | 4 | 8 | 8 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 8.0 | 10.0 | 10.0 | 8.0 | 10.0 | 10.0 | 8.0 | 10.0 | 10.0 | 10.0 |
| Minimum Split (s) | 11.0 | 35.1 | 35.1 | 12.5 | 35.1 | 35.1 | 11.0 | 41.4 | 41.4 | 41.4 |
| Total Split (s) | 27.0 | 43.0 | 43.0 | 20.0 | 36.0 | 36.0 | 14.0 | 57.0 | 43.0 | 43.0 |
| Total Split (\%) | 22.5\% | 35.8\% | 35.8\% | 16.7\% | 30.0\% | 30.0\% | 11.7\% | 47.5\% | 35.8\% | 35.8\% |
| Yellow Time (s) | 3.0 | 4.1 | 4.1 | 3.0 | 4.1 | 4.1 | 3.0 | 4.1 | 4.1 | 4.1 |
| All-Red Time (s) | 0.0 | 2.0 | 2.0 | 0.0 | 2.0 | 2.0 | 0.0 | 2.3 | 2.3 | 2.3 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 3.0 | 6.1 | 6.1 | 3.0 | 6.1 | 6.1 | 3.0 | 6.4 | 6.4 | 6.4 |
| Lead/Lag | Lead | Lag | Lag | Lead | Lag | Lag | Lead |  | Lag | Lag |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes | Yes | Yes |  | Yes | Yes |
| Recall Mode | None | C-Max | C-Max | None | C-Max | C-Max | None | None | None | None |
| Act Effct Green (s) | 66.3 | 49.0 | 49.0 | 53.2 | 38.9 | 38.9 | 47.7 | 44.3 | 30.9 | 30.9 |
| Actuated g/C Ratio | 0.55 | 0.41 | 0.41 | 0.44 | 0.32 | 0.32 | 0.40 | 0.37 | 0.26 | 0.26 |
| V/C Ratio | 0.87 | 0.48 | 0.21 | 0.40 | 0.74 | 0.14 | 0.54 | 0.43 | 0.20 | 0.90 |
| Control Delay | 62.5 | 42.4 | 23.4 | 20.0 | 43.2 | 2.7 | 32.0 | 26.7 | 34.4 | 60.6 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 62.5 | 42.4 | 23.4 | 20.0 | 43.2 | 2.7 | 32.0 | 26.7 | 34.4 | 60.6 |
| LOS | E | D | C | C | D | A | C | C | C | E |
| Approach Delay |  | 46.4 |  |  | 37.4 |  |  | 28.4 |  | 57.3 |
| Approach LOS |  | D |  |  | D |  |  | C |  | E |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 120 |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 120 |  |  |  |  |  |  |  |  |  |  |
| Offset: $0(0 \%)$, Referenced to phase 2:EBTL and 6 :WBTL, Start of Green |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 100 |  |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Coordinated |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.90 |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 42.7 |  |  |  | Intersection LOS: D |  |  |  |  |  |  |
| Intersection Capacity Utilization 86.5\% |  |  |  | ICU Level of Service E |  |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |



[^25]Synchro 10 Report

HCM Signalized Intersection Capacity Analysis<2025 Total - Thorold Townline> AM Peak Hour 4: Thorold Townline Road \& Thorold Stone Road


Uppers Quarry Traffic Impact Study
Synchro 10 Repor



[^26]Synchro 10 Report

HCM Signalized Intersection Capacity Analysis<2025 Total - Thorold Townline> AM Peak Hour 5: Thorold Townline Road \& Lundys Lane


Timings
<2025 Total - Thorold Townline> AM Peak Hour 6: Thorold Townline Road \& Beaverdams Road 09-23-2021



[^27]Synchro 10 Report

HCM Signalized Intersection Capacity Analysis<2025 Total - Thorold Townline> AM Peak Hour 6: Thorold Townline Road \& Beaverdams Road 09-23-2021


HCM Unsignalized Intersection Capacity Analysi8025 Total - Thorold Townline> AM Peak Hour 7: Thorold Townline Road \& Uppers Lane 09-23-2021

|  | $\checkmark$ | 4 | $\uparrow$ | $p$ |  | $\downarrow$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |  |
| Lane Configurations | M |  | $\hat{F}$ |  | 7 | $\uparrow$ |  |
| Trafic Volume (veh/h) | 3 | 66 | 323 | 3 | 46 | 256 |  |
| Future Volume (Veh/h) | 3 | 66 | 323 | 3 | 46 | 256 |  |
| Sign Control | Stop |  | Free |  |  | Free |  |
| Grade | 0\% |  | 0\% |  |  | 0\% |  |
| Peak Hour Factor | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 |  |
| Hourly flow rate (vph) | 3 | 71 | 347 | 3 | 49 | 275 |  |
| Pedestrians |  |  |  |  |  |  |  |
| Lane Width (m) |  |  |  |  |  |  |  |
| Walking Speed ( $\mathrm{m} / \mathrm{s}$ ) |  |  |  |  |  |  |  |
| Percent Blockage |  |  |  |  |  |  |  |
| Right turn flare (veh) |  |  |  |  |  |  |  |
| Median type |  |  | None |  |  | None |  |
| Median storage veh) |  |  |  |  |  |  |  |
| Upstream signal ( m ) |  |  |  |  |  |  |  |
| pX, platoon unblocked |  |  |  |  |  |  |  |
| vC , conficting volume | 722 | 348 |  |  | 350 |  |  |
| vC1, stage 1 conf vol |  |  |  |  |  |  |  |
| vC2, stage 2 conf vol |  |  |  |  |  |  |  |
| vCu, unblocked vol | 722 | 348 |  |  | 350 |  |  |
| tC, single (s) | 6.4 | 7.1 |  |  | 4.9 |  |  |
| $\mathrm{tC}, 2$ stage (s) |  |  |  |  |  |  |  |
| tF (s) | 3.5 | 4.1 |  |  | 2.9 |  |  |
| p0 queue free \% | 99 | 87 |  |  | 94 |  |  |
| cM capacity (veh/h) | 375 | 537 |  |  | 870 |  |  |
| Direction, Lane\# | WB 1 | NB1 | SB 1 | SB2 |  |  |  |
| Volume Total | 74 | 350 | 49 | 275 |  |  |  |
| Volume Left | 3 | 0 | 49 | 0 |  |  |  |
| Volume Right | 71 | 3 | 0 | 0 |  |  |  |
| cSH | 528 | 1700 | 870 | 1700 |  |  |  |
| Volume to Capacity | 0.14 | 0.21 | 0.06 | 0.16 |  |  |  |
| Queue Length 95th (m) | 3.9 | 0.0 | 1.4 | 0.0 |  |  |  |
| Control Delay (s) | 12.9 | 0.0 | 9.4 | 0.0 |  |  |  |
| Lane LOS | B |  | A |  |  |  |  |
| Approach Delay (s) | 12.9 | 0.0 | 1.4 |  |  |  |  |
| Approach LOS | B |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |
| Average Delay |  |  | 1.9 |  |  |  |  |
| Intersection Capacity Utilization |  |  | 34.8\% | ICU Level of Service |  |  | A |
| Analysis Period (min) |  |  | 15 |  |  |  |  |

<2025 Total - Thorold Townline> PM Peak Hour 1: Davis Road \& Thorold Stone Road


## Intersection Summa

Cycle Length: 120
ength: 120
Offset: 0 (0\%), Referenced to phase 2:EBTL and 6 :WBTL, Start of Green
Natural Cycle: 95
Control Type: Actuated-Coordinated

| Control Type: Actuated-Coordinated |  |
| :--- | :--- |
| Maximum v/c Ratio: 0.82 |  |
| Intersection Signal Delay: 31.4 | Intersection LOS: $C$ |
| Intersection Capacity Utilization $88.1 \%$ | ICU Level of Service E |

Intersection Capacity Utilization 88.1\% ICU Level of Service E
Splits and Phases: 1: Davis Road \& Thorold Stone Road


[^28]Synchro 10 Report

HCM Signalized Intersection Capacity Analysis<2025 Total - Thorold Townline> PM Peak Hour 1: Davis Road \& Thorold Stone Road


[^29]Synchro 10 Report

Timings 2: Davis Road \& Niagara Falls Road/Beaverdams Road

|  | $\rangle$ |  |  |  | 4 | 4 |  |  | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | WBL | WBT | NBL | NBT | SBL | SBT | SBR |
| Lane Configurations |  | $\dagger$ |  | ${ }_{\$}$ | ${ }^{7}$ | $\uparrow{ }^{\text {¢ }}$ | ${ }^{7}$ | ¢ $\uparrow$ | F |
| Traffic Volume (vph) | 90 | 32 | 74 | 44 | 12 | 409 | 170 | 471 | 105 |
| Future Volume (vph) | 90 | 32 | 74 | 44 | 12 | 409 | 170 | 471 | 105 |
| Turn Type | Perm | NA | Perm | NA | Perm | NA | Perm | NA | Perm |
| Protected Phases |  | 2 |  | 6 |  | 4 |  | 8 |  |
| Permitted Phases | 2 |  | 6 |  | 4 |  | 8 |  | 8 |
| Detector Phase | 2 | 2 | 6 | 6 | 4 | 4 | 8 | 8 | 8 |
| Switch Phase |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 10.0 | 10.0 | 10.0 | 10.0 | 25.0 | 25.0 | 25.0 | 25.0 | 25.0 |
| Minimum Split (s) | 38.1 | 38.1 | 38.1 | 38.1 | 32.0 | 32.0 | 32.0 | 32.0 | 32.0 |
| Total Split (s) | 40.0 | 40.0 | 40.0 | 40.0 | 60.0 | 60.0 | 60.0 | 60.0 | 60.0 |
| Total Split (\%) | 40.0\% | 40.0\% | 40.0\% | 40.0\% | 60.0\% | 60.0\% | 60.0\% | 60.0\% | 60.0\% |
| Yellow Time (s) | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| All-Red Time (s) | 3.1 | 3.1 | 3.1 | 3.1 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |
| Lost Time Adjust (s) |  | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) |  | 8.1 |  | 8.1 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |
| Lead/Lag |  |  |  |  |  |  |  |  |  |
| Lead-Lag Optimize? |  |  |  |  |  |  |  |  |  |
| Recall Mode | C-Max | C-Max | Max | Max | None | None | None | None | None |
| Act Effict Green (s) |  | 52.5 |  | 52.5 | 32.4 | 32.4 | 32.4 | 32.4 | 32.4 |
| Actuated g/C Ratio |  | 0.52 |  | 0.52 | 0.32 | 0.32 | 0.32 | 0.32 | 0.32 |
| $\mathrm{v} / \mathrm{C}$ Ratio |  | 0.24 |  | 0.34 | 0.05 | 0.45 | 0.72 | 0.46 | 0.19 |
| Control Delay |  | 15.9 |  | 13.5 | 19.4 | 25.9 | 44.6 | 27.3 | 4.2 |
| Queue Delay |  | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay |  | 15.9 |  | 13.5 | 19.4 | 25.9 | 44.6 | 27.3 | 4.2 |
| LOS |  | B |  | B | B | C | D | c | A |
| Approach Delay |  | 15.9 |  | 13.5 |  | 25.7 |  | 28.0 |  |
| Approach LOS |  | B |  | B |  | C |  | C |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |
| Cycle Length: 100 |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 100 |  |  |  |  |  |  |  |  |  |
| Offset: 0 (0\%), Referenced to phase 2:EBTL, Start of Green |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 75 |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Coordinated |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.72 |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 23.9 |  |  |  |  | tersection | LOS: C |  |  |  |
| Intersection Capacity Utilization 76.1\% |  |  |  | ICU Level of Service D |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |



[^30]Synchro 10 Report

HCM Signalized Intersection Capacity Analysis<2025 Total - Thorold Townline> PM Peak Hour 2: Davis Road \& Niagara Falls Road/Beaverdams Road


[^31]Synchro 10 Report 3: Davis Road \& Lundys Lane 09-23-2021

| Lane Group | EBL | EBT | WBL | WBT | WBR | NBL | NBT | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \% | $\stackrel{1}{ }$ | \% | $\uparrow$ | 7 | 7 | F | \% | $\uparrow$ | F |
| Traffic Volume (vph) | 179 | 567 | 28 | 555 | 241 | 46 | 141 | 300 | 125 | 157 |
| Future Volume (vph) | 179 | 567 | 28 | 555 | 241 | 46 | 141 | 300 | 125 | 157 |
| Turn Type | pm+pt | NA | Perm | NA | Perm | Perm | NA | pm+pt | NA | Perm |
| Protected Phases | 5 | 2 |  | 6 |  |  | 4 | 3 | 8 |  |
| Permitted Phases | 2 |  | 6 |  | 6 | 4 |  | 8 |  | 8 |
| Detector Phase | 5 | 2 | 6 | 6 | 6 | 4 | 4 | 3 | 8 | 8 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 22.0 | 22.0 | 22.0 | 22.0 | 15.0 | 15.0 | 5.0 | 15.0 | 15.0 |
| Minimum Split (s) | 8.0 | 36.0 | 36.0 | 36.0 | 36.0 | 32.0 | 32.0 | 8.0 | 32.0 | 32.0 |
| Total Split (s) | 13.0 | 69.0 | 56.0 | 56.0 | 56.0 | 32.0 | 32.0 | 19.0 | 51.0 | 51.0 |
| Total Split (\%) | 10.8\% | 57.5\% | 46.7\% | 46.7\% | 46.7\% | 26.7\% | 26.7\% | 15.8\% | 42.5\% | 42.5\% |
| Yellow Time (s) | 3.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 3.0 | 5.0 | 5.0 |
| All-Red Time (s) | 0.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 0.0 | 2.0 | 2.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 3.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 3.0 | 7.0 | 7.0 |
| Lead/Lag | Lead |  | Lag | Lag | Lag | Lag | Lag | Lead |  |  |
| Lead-Lag Optimize? | Yes |  | Yes | Yes | Yes | Yes | Yes | Yes |  |  |
| Recall Mode | None | C-Max | Max | Max | Max | Max | Max | None | Max | Max |
| Act Effct Green (s) | 66.0 | 62.0 | 49.3 | 49.3 | 49.3 | 25.2 | 25.2 | 48.0 | 44.0 | 44.0 |
| Actuated g/C Ratio | 0.55 | 0.52 | 0.41 | 0.41 | 0.41 | 0.21 | 0.21 | 0.40 | 0.37 | 0.37 |
| V/c Ratio | 0.66 | 0.68 | 0.14 | 0.78 | 0.35 | 0.19 | 0.53 | 0.72 | 0.21 | 0.25 |
| Control Delay | 25.5 | 26.2 | 26.7 | 41.9 | 9.6 | 41.6 | 46.3 | 37.4 | 27.2 | 4.7 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 25.5 | 26.2 | 26.7 | 41.9 | 9.6 | 41.6 | 46.3 | 37.4 | 27.2 | 4.7 |
| LOS | C | C | C | D | A | D | D | D | C | A |
| Approach Delay |  | 26.1 |  | 31.9 |  |  | 45.3 |  | 26.4 |  |
| Approach LOS |  | C |  | C |  |  | D |  | C |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 120 |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 120 |  |  |  |  |  |  |  |  |  |  |
| Offset: $0(0 \%)$, Referenced to phase 2:EBTL, Start of Green |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 85 |  |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Coordinated |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.78 |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 29.9 |  |  |  |  | Intersection LOS: C |  |  |  |  |  |
| Intersection Capacity Utilization 108.2\% Analysis Period (min) 15 |  |  |  |  | ICU Level of Service G |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |



HCM Signalized Intersection Capacity Analysis<2025 Total - Thorold Townline> PM Peak Hour 3: Davis Road \& Lundys Lane

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \% | $\stackrel{1}{6}$ |  | \% | $\uparrow$ | F | \% |  |  | ${ }^{7}$ | $\uparrow$ | \% |
| Traffic Volume (vph) | 179 | 567 | 28 | 28 | 555 | 241 | 46 | 141 | 37 | 300 | 125 | 157 |
| Future Volume (vph) | 179 | 567 | 28 | 28 | 555 | 241 | 46 | 141 | 37 | 300 | 125 | 157 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 3.0 | 7.0 |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  | 3.0 | 7.0 | 7.0 |
| Lane Util. Factor | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 |
| Frpb, ped/bikes | 1.00 | 1.00 |  | 1.00 | 1.00 | 0.98 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 |
| Flpb, ped/bikes | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 |
| Frt | 1.00 | 0.99 |  | 1.00 | 1.00 | 0.85 | 1.00 | 0.97 |  | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 |  | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |  | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1719 | 1811 |  | 1611 | 1863 | 1473 | 1736 | 1671 |  | 1702 | 1743 | 1553 |
| Flt Permitted | 0.18 | 1.00 |  | 0.32 | 1.00 | 1.00 | 0.67 | 1.00 |  | 0.47 | 1.00 | 1.00 |
| Satd. Flow (perm) | 322 | 1811 |  | 537 | 1863 | 1473 | 1226 | 1671 |  | 845 | 1743 | 1553 |
| Peak-hour factor, PHF | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 |
| Adj. Flow (vph) | 192 | 610 | 30 | 30 | 597 | 259 | 49 | 152 | 40 | 323 | 134 | 169 |
| RTOR Reduction (vph) | 0 | 1 | 0 | 0 | 0 | 143 | 0 | 8 | 0 | 0 | 0 | 107 |
| Lane Group Flow (vph) | 192 | 639 | 0 | 30 | 597 | 116 | 49 | 184 | 0 | 323 | 134 | 62 |
| Confl. Peds. (\#/hr) | 2 |  | 1 | 1 |  | 2 |  |  | 1 | 1 |  |  |
| Heavy Vehicles (\%) | 5\% | 3\% | 26\% | 12\% | 2\% | 7\% | 4\% | 9\% | 12\% | 6\% | 9\% | 4\% |
| Turn Type | pm+pt | NA |  | Perm | NA | Perm | Perm | NA |  | pm+pt | NA | Perm |
| Protected Phases | 5 | 2 |  |  | 6 |  |  | 4 |  | 3 | 8 |  |
| Permitted Phases | 2 |  |  | 6 |  | 6 | 4 |  |  | 8 |  |  |
| Actuated Green, G (s) | 62.0 | 62.0 |  | 49.3 | 49.3 | 49.3 | 25.2 | 25.2 |  | 44.0 | 44.0 | 44.0 |
| Effective Green, g (s) | 62.0 | 62.0 |  | 49.3 | 49.3 | 49.3 | 25.2 | 25.2 |  | 44.0 | 44.0 | 44.0 |
| Actuated g/C Ratio | 0.52 | 0.52 |  | 0.41 | 0.41 | 0.41 | 0.21 | 0.21 |  | 0.37 | 0.37 | 0.37 |
| Clearance Time (s) | 3.0 | 7.0 |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  | 3.0 | 7.0 | 7.0 |
| Vehicle Extension (s) | 3.0 | 4.0 |  | 4.0 | 4.0 | 4.0 | 2.0 | 2.0 |  | 3.0 | 2.0 | 2.0 |
| Lane Grp Cap (vph) | 279 | 935 |  | 220 | 765 | 605 | 257 | 350 |  | 422 | 639 | 569 |
| v/s Ratio Prot | 0.06 | c0.35 |  |  | c0.32 |  |  | 0.11 |  | c0.10 | 0.08 |  |
| v/s Ratio Perm | 0.30 |  |  | 0.06 |  | 0.08 | 0.04 |  |  | c0.18 |  | 0.04 |
| $\mathrm{v} / \mathrm{C}$ Ratio | 0.69 | 0.68 |  | 0.14 | 0.78 | 0.19 | 0.19 | 0.53 |  | 0.77 | 0.21 | 0.11 |
| Uniform Delay, d1 | 21.1 | 21.7 |  | 22.1 | 30.7 | 22.6 | 39.0 | 42.1 |  | 30.8 | 26.1 | 25.1 |
| Progression Factor | 1.00 | 1.00 |  | 1.10 | 1.10 | 2.28 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 6.9 | 4.0 |  | 1.2 | 7.1 | 0.6 | 1.6 | 5.6 |  | 8.1 | 0.7 | 0.4 |
| Delay (s) | 28.0 | 25.7 |  | 25.5 | 40.8 | 52.1 | 40.7 | 47.7 |  | 38.9 | 26.8 | 25.5 |
| Level of Service | C | C |  | C | D | D | D | D |  | D | C |  |
| Approach Delay (s) |  | 26.2 |  |  | 43.6 |  |  | 46.2 |  |  | 32.7 |  |
| Approach LOS |  | C |  |  | D |  |  | D |  |  | C |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 2000 Control Delay |  |  | 35.6 |  | HCM 2000 | Level of | ervice |  | D |  |  |  |
|  |  |  | 0.79 |  |  |  |  |  |  |  |  |  |
| HCM 2000 Volume to Capacity ratio |  |  | 120.0 |  | Sum of los | time (s) |  |  | 20.0 |  |  |  |
| Intersection Capacity Utilization |  |  | 108.2\% |  | CU Level | of Service |  |  | G |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |
| c Critical Lane Group |  |  |  |  |  |  |  |  |  |  |  |  |

Timings
<2025 Total - Thorold Townline> PM Peak Hour 4: Thorold Townline Road \& Thorold Stone Road 09-23-2021

| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | SBL | SBT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \% | 个 $\uparrow$ | F | \% | 个 $\uparrow$ | F | \% | $\hat{F}$ | 7 | A |
| Traffic Volume (vph) | 231 | 1036 | 72 | 75 | 821 | 35 | 142 | 148 | 48 | 171 |
| Future Volume (vph) | 231 | 1036 | 72 | 75 | 821 | 35 | 142 | 148 | 48 | 171 |
| Turn Type | pm+pt | NA | Perm | pm+pt | NA | Perm | pm+pt | NA | pm+pt | NA |
| Protected Phases | 5 | 2 |  | 1 | 6 |  | 7 | 4 | 3 | 8 |
| Permitted Phases | 2 |  | 2 | 6 |  | 6 | 4 |  | 8 |  |
| Detector Phase | 5 | 2 | 2 | 1 | 6 | 6 | 7 | 4 | 3 | 8 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 8.0 | 10.0 | 10.0 | 5.0 | 10.0 | 10.0 | 5.0 | 10.0 | 5.0 | 10.0 |
| Minimum Split (s) | 11.0 | 35.1 | 35.1 | 8.0 | 35.1 | 35.1 | 8.0 | 41.4 | 8.0 | 41.4 |
| Total Split (s) | 21.0 | 54.4 | 54.4 | 9.6 | 43.0 | 43.0 | 13.0 | 46.0 | 10.0 | 43.0 |
| Total Split (\%) | 17.5\% | 45.3\% | 45.3\% | 8.0\% | 35.8\% | 35.8\% | 10.8\% | 38.3\% | 8.3\% | 35.8\% |
| Yellow Time (s) | 3.0 | 4.1 | 4.1 | 3.0 | 4.1 | 4.1 | 3.0 | 4.1 | 3.0 | 4.1 |
| All-Red Time (s) | 0.0 | 2.0 | 2.0 | 0.0 | 2.0 | 2.0 | 0.0 | 2.3 | 0.0 | 2.3 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 3.0 | 6.1 | 6.1 | 3.0 | 6.1 | 6.1 | 3.0 | 6.4 | 3.0 | 6.4 |
| Lead/Lag | Lead | Lag | Lag | Lead | Lag | Lag | Lead | Lag | Lead | Lag |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Recall Mode | None | C-Max | C-Max | None | C-Max | C-Max | None | None | None | None |
| Act Efft Green (s) | 64.4 | 53.4 | 53.4 | 53.3 | 43.5 | 43.5 | 49.6 | 38.2 | 43.3 | 33.2 |
| Actuated g/C Ratio | 0.54 | 0.44 | 0.44 | 0.44 | 0.36 | 0.36 | 0.41 | 0.32 | 0.36 | 0.28 |
| v/c Ratio | 0.73 | 0.68 | 0.12 | 0.42 | 0.67 | 0.06 | 0.71 | 0.56 | 0.13 | 0.93 |
| Control Delay | 49.3 | 51.1 | 24.5 | 23.2 | 36.8 | 0.2 | 42.0 | 34.0 | 20.9 | 61.9 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 49.3 | 51.1 | 24.5 | 23.2 | 36.8 | 0.2 | 42.0 | 34.0 | 20.9 | 61.9 |
| LOS | D | D | C | C | D | A | D | C | C | E |
| Approach Delay |  | 49.4 |  |  | 34.4 |  |  | 36.8 |  | 57.9 |
| Approach LOS |  | D |  |  | C |  |  | D |  | E |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 120 |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 120 |  |  |  |  |  |  |  |  |  |  |
| Offset: $0(0 \%)$, Referenced to phase 2:EBTL and 6 :WBTL, Start of Green |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 100 |  |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Coordinated |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.93 |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 44.7 |  |  |  | Intersection LOS: D |  |  |  |  |  |  |
| Intersection Capacity Utilization 86.1\% |  |  |  | ICU Level of Service E |  |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |



[^32]Synchro 10 Report

4: Thorold Townline Road \& Thorold Stone Road




HCM Signalized Intersection Capacity Analysis<2025 Total - Thorold Townline> PM Peak Hou 5: Thorold Townline Road \& Lundys Lane


Timings
<2025 Total - Thorold Townline> PM Peak Hour 6: Thorold Townline Road \& Beaverdams Road 09-23-2021



[^33]Synchro 10 Report

HCM Signalized Intersection Capacity Analysis<2025 Total - Thorold Townline> PM Peak Hour 6: Thorold Townline Road \& Beaverdams Road

|  | $\Rightarrow$ | $\rightarrow$ |  | $\dagger$ |  |  | 4 | 4 | 7 |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | ¢ |  |  | $\uparrow$ |  |  | ¢ |  |  | ${ }_{\text {¢ }}$ |  |
| Traffic Volume (vph) | 27 | 213 | 16 | 43 | 192 | 21 | 32 | 384 | 26 | 20 | 275 | 41 |
| Future Volume (vph) | 27 | 213 | 16 | 43 | 192 | 21 | 32 | 384 | 26 | 20 | 275 | 41 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) |  | 6.0 |  |  | 6.0 |  |  | 6.0 |  |  | 6.0 |  |
| Lane Util. Factor |  | 1.00 |  |  | 1.00 |  |  | 1.00 |  |  | 1.00 |  |
| Frpb, ped/bikes |  | 1.00 |  |  | 1.00 |  |  | 1.00 |  |  | 1.00 |  |
| Flpb, ped/bikes |  | 1.00 |  |  | 1.00 |  |  | 1.00 |  |  | 1.00 |  |
| Frt |  | 0.99 |  |  | 0.99 |  |  | 0.99 |  |  | 0.98 |  |
| Flt Protected |  | 0.99 |  |  | 0.99 |  |  | 1.00 |  |  | 1.00 |  |
| Satd. Flow (prot) |  | 1831 |  |  | 1832 |  |  | 1605 |  |  | 1594 |  |
| Flt Permitted |  | 0.95 |  |  | 0.91 |  |  | 0.95 |  |  | 0.96 |  |
| Satd. Flow (perm) |  | 1745 |  |  | 1677 |  |  | 1534 |  |  | 1530 |  |
| Peak-hour factor, PHF | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 |
| Adj. Flow (vph) | 29 | 229 | 17 | 46 | 206 | 23 | 34 | 413 | 28 | 22 | 296 | 44 |
| RTOR Reduction (vph) | 0 |  | 0 | 0 | 3 | 0 | 0 |  | 0 | 0 | 7 | 0 |
| Lane Group Flow (vph) | 0 | 273 | 0 | 0 | 272 | 0 | 0 | 472 | 0 | 0 | 355 | 0 |
| Confl. Peds. (\#hr) | 1 |  | 5 | 5 |  | 1 | 8 |  | 3 | 3 |  | 8 |
| Heavy Vehicles (\%) | 10\% | 1\% | 4\% | 4\% | 1\% | 0\% | 4\% | 19\% | 0\% | 2\% | 19\% | 6\% |
| Turn Type | Perm | NA |  | Perm | NA |  | Perm | NA |  | Perm | NA |  |
| Protected Phases |  | 2 |  |  | 6 |  |  | 4 |  |  | 8 |  |
| Permitted Phases | 2 |  |  | 6 |  |  | 4 |  |  | 8 |  |  |
| Actuated Green, G (s) |  | 41.7 |  |  | 41.7 |  |  | 36.3 |  |  | 36.3 |  |
| Effective Green, g (s) |  | 41.7 |  |  | 41.7 |  |  | 36.3 |  |  | 36.3 |  |
| Actuated g/C Ratio |  | 0.46 |  |  | 0.46 |  |  | 0.40 |  |  | 0.40 |  |
| Clearance Time (s) |  | 6.0 |  |  | 6.0 |  |  | 6.0 |  |  | 6.0 |  |
| Vehicle Extension (s) |  | 5.0 |  |  | 5.0 |  |  | 5.0 |  |  | 5.0 |  |
| Lane Grp Cap (vph) |  | 808 |  |  | 777 |  |  | 618 |  |  | 617 |  |
| v/s Ratio Prot |  |  |  |  |  |  |  |  |  |  |  |  |
| v/s Ratio Perm |  | 0.16 |  |  | c0.16 |  |  | c0.31 |  |  | 0.23 |  |
| v/c Ratio |  | 0.34 |  |  | 0.35 |  |  | 0.76 |  |  | 0.58 |  |
| Uniform Delay, d1 |  | 15.4 |  |  | 15.5 |  |  | 23.2 |  |  | 20.9 |  |
| Progression Factor |  | 1.00 |  |  | 1.00 |  |  | 1.00 |  |  | 1.00 |  |
| Incremental Delay, d2 |  | 1.1 |  |  | 1.2 |  |  | 6.6 |  |  | 2.1 |  |
| Delay (s) |  | 16.5 |  |  | 16.7 |  |  | 29.7 |  |  | 22.9 |  |
| Level of Service |  | B |  |  | B |  |  | C |  |  | C |  |
| Approach Delay (s) |  | 16.5 |  |  | 16.7 |  |  | 29.7 |  |  | 22.9 |  |
| Approach LOS |  | B |  |  | B |  |  | C |  |  | C |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 2000 Control Delay |  |  | 22.7 |  | CM 2000 | Level of S | ervice |  | C |  |  |  |
| HCM 2000 Volume to Capacity ratio |  |  | 0.54 |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length (s) |  |  | 90.0 |  | um of lost | time (s) |  |  | 12.0 |  |  |  |
| Intersection Capacity Utilization |  |  | 63.3\% |  | CU Level of | Service |  |  | B |  |  |  |
|  |  |  | 15 |  |  |  |  |  |  |  |  |  |
| c Critical Lane Group |  |  |  |  |  |  |  |  |  |  |  |  |

HCM Unsignalized Intersection Capacity Analysi8025 Total - Thorold Townline> PM Peak Hour 7: Thorold Townline Road \& Uppers Lane 09-23-2021

|  | $\dagger$ | 4 | $\uparrow$ | $p$ | $\checkmark$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | M |  | $\hat{}$ |  | ${ }^{7}$ | $\uparrow$ |
| Trafic Volume (veh/h) |  | 46 | 323 | 3 | 46 | 297 |
| Future Volume (Veh/h) | 3 | 46 | 323 | 3 | 46 | 297 |
| Sign Control | Stop |  | Free |  |  | Free |
| Grade | 0\% |  | 0\% |  |  | 0\% |
| Peak Hour Factor | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 |
| Hourly flow rate (vph) | 3 | 51 | 355 | 3 | 51 | 326 |

$\begin{array}{lrrrrrr}\text { Peak Hour Factor } & 0.91 & 0.91 & 0.91 & 0.91 & 0.91 & 0.91 \\ \text { Hourly flow rate (vph) } & 3 & 51 & 355 & 3 & 51 & 326\end{array}$
Hourly flow rate (vph)
Lane Width ( $m$ )
Walking Speed ( $\mathrm{m} / \mathrm{s}$ )
Waking Speed ( $\mathrm{m} / \mathrm{s}$ )
Percent Blockage
Right turn flare (veh)
Right turn flare (veh)

| Right turn flare (veh) |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Median type |  | None |  | None |  |
| Median storage veh) |  |  |  |  |  |
| Upstream signal ( m ) |  |  |  |  |  |
| pX, platoon unblocked |  |  |  |  |  |
| VC, conflicting volume 784 | 356 |  |  | 358 |  |
| $\mathrm{vC1}$, stage 1 conf vol |  |  |  |  |  |
| vC2, stage 2 conf vol |  |  |  |  |  |
| vCu, unblocked vol 784 | 356 |  |  | 358 |  |
| tC, single (s) 6.4 | 7.0 |  |  | 4.9 |  |
| $\mathrm{tC}, 2$ stage (s) |  |  |  |  |  |
| $\mathrm{tF}(\mathrm{s}) \quad 3.5$ | 4.0 |  |  | 2.9 |  |
| p0 queue free \% 99 | 91 |  |  | 94 |  |
| cM capacity (veh/h) 343 | 538 |  |  | 863 |  |
| Direction, Lane \# WB 1 | NB1 | SB 1 | SB 2 |  |  |
| Volume Total 54 | 358 | 51 | 326 |  |  |
| Volume Left 3 | 0 | 51 | 0 |  |  |
| Volume Right 51 | 3 | 0 | 0 |  |  |
| CSH 522 | 1700 | 863 | 1700 |  |  |
| Volume to Capacity 0.10 | 0.21 | 0.06 | 0.19 |  |  |
| Queue Length 95th ( m ) 2.8 | 0.0 | 1.5 | 0.0 |  |  |
| Control Delay (s) 12.7 | 0.0 | 9.4 | 0.0 |  |  |
| Lane LOS B |  | A |  |  |  |
| Approach Delay (s) 12.7 | 0.0 | 1.3 |  |  |  |
| Approach LOS B |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |
| Average Delay |  | 1.5 |  |  |  |
| Intersection Capacity Utilization |  | 33.8\% |  | CU Level of Service | A |

Analysis Period (min)


| Lane Group | EBL | EBT | EBR | WBL | WBT | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ${ }^{1}$ | 个 $\uparrow$ | 「 | ＊ | 个 ${ }_{\text {d }}$ | \％ | $\uparrow$ | 「 | 1 | $\uparrow$ | F＇ |
| Traffic Volume（vph） | 21 | 991 | 336 | 114 | 1096 | 649 | 15 | 257 | 1 | 2 | 18 |
| Future Volume（vph） | 21 | 991 | 336 | 114 | 1096 | 649 | 15 | 257 | 1 | 2 | 18 |
| Turn Type | Perm | NA | Perm | pm＋pt | NA | Split | NA | Perm | Split | NA | Perm |
| Protected Phases |  | 2 |  | 1 | 6 | 4 | 4 |  | 8 | 8 |  |
| Permitted Phases | 2 |  | 2 | 6 |  |  |  | 4 |  |  | 8 |
| Detector Phase | 2 | 2 | 2 | 1 | 6 | 4 | 4 | 4 | 8 | 8 | 8 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 20.0 | 20.0 | 20.0 | 8.0 | 20.0 | 10.0 | 10.0 | 10.0 | 10.0 | 10.0 | 10.0 |
| Minimum Split（s） | 28.9 | 28.9 | 28.9 | 12.5 | 28.9 | 29.7 | 29.7 | 29.7 | 21.7 | 21.7 | 21.7 |
| Total Split（s） | 46.3 | 46.3 | 46.3 | 13.0 | 59.3 | 39.0 | 39.0 | 39.0 | 21.7 | 21.7 | 21.7 |
| Total Split（\％） | 38．6\％ | 38．6\％ | 38．6\％ | 10．8\％ | 49．4\％ | 32．5\％ | 32．5\％ | 32．5\％ | 18．1\％ | 18．1\％ | 18．1\％ |
| Yellow Time（s） | 5.4 | 5.4 | 5.4 | 3.0 | 5.4 | 5.7 | 5.7 | 5.7 | 5.7 | 5.7 | 5.7 |
| All－Red Time（s） | 1.5 | 1.5 | 1.5 | 0.0 | 1.5 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |
| Lost Time Adjust（s） | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time（s） | 6.9 | 6.9 | 6.9 | 3.0 | 6.9 | 7.7 | 7.7 | 7.7 | 7.7 | 7.7 | 7.7 |
| Lead／Lag | Lag | Lag | Lag | Lead |  |  |  |  |  |  |  |
| Lead－Lag Optimize？ | Yes | Yes | Yes | Yes |  |  |  |  |  |  |  |
| Recall Mode | C－Max | C－Max | C－Max | None | Max | None | None | None | None | None | None |
| Act Efft Green（s） | 55.0 | 55.0 | 55.0 | 72.0 | 68.1 | 30.2 | 30.2 | 30.2 | 10.0 | 10.0 | 10.0 |
| Actuated g／C Ratio | 0.46 | 0.46 | 0.46 | 0.60 | 0.57 | 0.25 | 0.25 | 0.25 | 0.08 | 0.08 | 0.08 |
| $\mathrm{v} / \mathrm{C}$ Ratio | 0.14 | 0.66 | 0.45 | 0.48 | 0.60 | 0.88 | 0.89 | 0.47 | 0.01 | 0.01 | 0.08 |
| Control Delay | 28.2 | 30.5 | 12.7 | 33.8 | 38.7 | 67.1 | 68.2 | 7.1 | 51.0 | 51.0 | 0.7 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 28.2 | 30.5 | 12.7 | 33.8 | 38.7 | 67.1 | 68.2 | 7.1 | 51.0 | 51.0 | 0.7 |
| LOS | C | C | B | C | D | E | E | A | D | D | A |
| Approach Delay |  | 26.0 |  |  | 38.3 |  | 50.8 |  |  | 7.5 |  |
| Approach LOS |  | C |  |  | D |  | D |  |  | A |  |

## Intersection Summa

Cycle Length： 120
ngth： 120
Offset：O（0\％），Referenced to phase 2：EBTL，Start of Green
Natural Cycle： 105

| Control Type：Actuated－Coordinated |  |
| :--- | :--- |
| Maximum v／c Ratio： 0.89 |  |
| Intersection Signal Delay： |  |
| Intersection Capacity Utilization $90.1 \%$ | Intersection LOS：D |
| Analysis Period（min） 15 | ICU Level of Service E |

Intersection Capacity Utilization 90．1\％ ICU Level of Service E

Splits and Phases：1：Davis Road \＆Thorold Stone Road

1．Davis Road \＆Thorold Stone Road


|  |  |  |  |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Future Volume（vph） | 21 | 991 | 336 | 114 | 1096 | 6 | 649 | 15 | 257 | 1 | 2 | 18 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time（s） | 6.9 | 6.9 | 6.9 | 3.0 | 6.9 |  | 7.7 | 7.7 | 7.7 | 7.7 | 7.7 | 7.7 |


| Total Lost time（s） | 6.9 | 6.9 | 6.9 | 3.0 | 6.9 | 7.7 | 7.7 | 7.7 | 7.7 | 7.7 | 7.7 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Lane Util．Factor | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 0.95 | 0.95 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frob thedbikes | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 0.99 | 100 | 100 | 0.99 |


| Frpb，ped／bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.99 | 1.00 | 1.00 | 0.99 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Flpb，ped／bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Fit | 1.00 | 1.00 | 0.05 | 1.00 | 1.00 | 1.00 | 1.00 | 0.05 | 1.00 | 100 | 0.05 |


| FIt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| FIt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 0.95 | 0.95 | 1.00 | 0.95 | 1.00 | 1.00 |


| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 0.95 | 0.95 | 1.00 | 0.95 | 1.00 | 1.00 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Satd．Flow（prot） | 1640 | 3406 | 1442 | 1530 | 3399 | 1559 | 1554 | 1475 | 1388 | 1624 | 1337 |
| Flt Permitted | 0.21 | 1.00 | 1.00 | 0.14 | 1.00 | 0.95 | 0.95 | 1.00 | 0.95 | 1.00 | 1.00 |


| Satd．Flow（perm） | 0.21 | 1.00 | 1.00 | 0.14 | 1.00 |  | 0.95 | 0.95 | 1.00 | 0.95 | 1.00 | 1539 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Peak－hour factor，PHF | 0.96 | 0.96 | 1442 | 228 | 3399 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | Adj．Flow（vph） TOR Reduction

0.96
22

| Lane Group Flow（vph） | 22 | 1032 | 121 | 029 | 119 | 1148 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
|  | 1 |  |  |  |  | 0 |


|  |  |  |  |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Confl．Peds．（\＃lhr） | 1 |  |  | 119 | 1148 | 0 | 345 | 347 | 67 | 1 | 2 | 1 |
| Heavy Vehicles（\％） | $10 \%$ | $6 \%$ | $12 \%$ | $18 \%$ | $6 \%$ | 1 | 1 |  | $10 \%$ | $10 \%$ | $28 \%$ | $8 \%$ |


|  | Heary Venicles（\％） | Perm | NA | Perm | pm +pt | NA |  | Split | NA | Perm | Split |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Turn Type | NA | Perm |  |  |  |  |  |  |  |  |  | Protected Phases Permitted Phases


| Actuated Green，G（s） | 50.4 | 50.4 | 50.4 | 63.5 | 63.5 | 30.2 | 30.2 | 30.2 | 4.0 | 4.0 | 4.0 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |


| Effective Green，$g(s)$ | 50.4 | 50.4 | 50.4 | 63.5 | 63.5 | 30.2 | 30.2 | 30.2 | 4.0 | 4.0 | 4.0 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
|  | 50.4 | 50.4 | 50.4 | 63.5 | 63.5 | 30.2 | 30.2 | 30.2 | 4.0 | 4.0 | 4.0 |



|  | 6.9 | 6.9 | 6.9 | 3.0 | 6.9 | 7.7 | 7.7 | 7.7 | 7.7 | 7.7 | 7.7 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Vehicle Extension（s） | 3.0 | 3.0 | 3.0 | 2.5 | 3.0 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 |
| Lane Grp Cap（vph） | 148 | 1430 | 605 | 230 | 1798 | 392 | 391 | 371 | 46 | 54 | 44 |
| Vs Ratio Prot |  | c 0.30 |  | 0.04 | $\mathrm{co.34}$ | 0.22 | $\mathrm{co.22}$ |  | 0.00 | $\mathrm{c0.00}$ |  |


s Ratio Perm

|  |  |  |  |  |  |  |  |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| C Ratio | 0.15 | 0.72 | 0.38 | 0.52 | 0.64 | 0.88 | 0.89 | 0.18 | 0.02 | 0.04 | 0.01 |
|  | 0.015 | 0.23 |  |  |  |  |  |  |  |  |  |


|  | Uniform Delay，d1 | 21.5 | 29.0 | 24.0 | 18.3 | 20.1 | 43.2 | 43.3 | 35.2 | 56.1 | 56.1 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 56.1 |  |  |  |  |  |  |  |  |  |  |  |
| Progression Factor | 1.00 | 1.00 | 1.00 | 2.30 | 1.99 | 1.00 | 1.00 | 100 | 100 | 100 |  |


|  | 1.00 | 1.00 | 1.00 | 2.30 | 1.99 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Incremental Delay，d2 | 2.1 | 3.2 | 1.8 | 0.9 | 1.1 | 20.8 | 21.7 | 0.4 | 0.3 | 0.5 | 0.2 |
|  | 2.6 | 32 | 2.8 | 4.0 | 4.0 |  | 0 | 3 |  |  |  |


| Delay（s） | 23.6 | 32.1 | 25.8 | 43.0 | 41.0 | 64.0 | 65.0 | 35.6 | 56.4 | 56.6 | 56.3 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Level of Service | C | C | C | D | D | E | E | D | E | E | E |
| Approach Delay（s） |  | 30.4 |  |  | 41.2 |  | 56.4 |  |  | 56.4 | E |
| Approach LOS |  | C |  |  | D |  | E |  |  | E |  | Approach LOS

Intersection Summary

| HCM 2000 Control Delay | 41.2 | HCM 2000 Level of Service | D |
| :--- | ---: | :--- | ---: |
| HCM 2000 Volume to Capacity ratio | 0.74 |  | 25.3 |
| Actuated Cycle Length（s） | 120.0 | Sum of lost time（s） | E |
| Intersection Capacity Utilization | $90.1 \%$ | ICU Level of Service |  |

Actuated Cycle Length（s）
90．1\％
ICU Level of Service
E
Analysis Period（min）
c Critical Lane Group

2: Davis Road \& Niagara Falls Road/Beaverdams Road



[^34]Synchro 10 Report

HCM Signalized Intersection Capacity Analysis
2: Davis Road \& Niagara Falls Road/Beaverdams Road
<2035 Background> AM Peak Hour 2. Davis Road \& Niagara Falls Road/Beaverdams Road 09-14-2021
 deal Flow (vphpl) otal Lost time (s) Ert

|  | 8.1 | 1.0 |
| :--- | :--- | :--- |
| Frt | 1.00 | 1.00 |
| Flt Protected | 0.98 | 0.89 |


| Flt Protected | 0.98 | 0.89 |
| :--- | :--- | :--- |
|  | 0.97 | 0.99 |


| Flt Protected | 0.97 | 0.99 |
| :--- | :--- | :--- |
| Satd. Flow (prot) | 1658 | 1631 |


| Satd. Flow (prot) |  | 1658 |  |  | 1631 |  | 1388 | 3122 |  | 1787 | 2983 | 139 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Flt Permitted |  | 0.67 |  |  | 0.94 |  | 0.53 | 1.00 |  | 0.26 | 1.00 | 1 |
| Satd. Flow (perm) |  | 1155 |  |  | 1549 |  | 779 | 3122 |  | 480 | 2983 | 13 |
| Peak-hour factor, PHF | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |  |
| Adj. Flow (vph) | 116 | 33 | 19 | 31 | 18 | 175 | 26 | 659 | 48 | 86 | 346 |  |


|  |  |  |  |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Adj. Flow (vph) | 116 | 33 | 19 | 31 | 18 | 175 | 26 | 659 | 48 | 86 | 346 |  |
| RTOR Reduction (vph) | 0 | 3 | 0 | 0 | 82 | 0 | 0 | 7 | 0 | 0 | 0 | 31 |


| Heary Vehicles (\%) | $10 \%$ | $7 \%$ | $7 \%$ | $7 \%$ | $12 \%$ | $2 \%$ | $30 \%$ | $15 \%$ | $7 \%$ | $1 \%$ | $21 \%$ | $16 \%$ |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Turn Type | Perm | NA | Perm | NA |  | Perm | NA |  | Perm | NA | Perm |  |


| Turn Type | Perm | A | Perm | NA | Perm | NA | Perm | NA |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| tec |  | 2 |  | 6 |  |  |  |  |

2
Acfuctive Green, $\mathrm{G}(\mathrm{s})$
Actuated $\mathrm{g} / \mathrm{C}$ Ratio
Clearance Time (s)
Venicle Extension (s)
Lane Grp Cap (vph)
/s Ratio Prot
/s Ratio Perm
/ Ratio
Uniform Delay, d
rogression Factor
hcremental Delay, d2
Delay (s)
Level of Service
Approach Delay (s)
Approach LOS

| Intersection Summary |  |  |  |
| :--- | ---: | :--- | ---: |
| HCM 200 Control Delay | 26.3 | HCM 2000 Level of Service | C |
| HCM 2000 Volume to Capacity ratio | 0.43 |  | 15.1 |
| Actuated Cycle Length (s) | 100.0 | Sum of lost time (s) | E |
| Intersection Capacity Utilization | $88.4 \%$ | ICU Level of Service |  |
| Analysis Period (min) | 15 |  |  |

nalysis Period (min)
c Critical Lane Group

Timings 3: Davis Road \& Lundys Lane


| Lane Group | EBL | EBT | WBL | WBT | WBR | NBL | NBT | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ${ }^{1}$ | $\uparrow$ | * | $\uparrow$ | F | \% | $\hat{\beta}$ | 7 | $\uparrow$ | F |
| Traffic Volume (vph) | 153 | 633 | 45 | 500 | 132 | 22 | 139 | 136 | 94 | 159 |
| Future Volume (vph) | 153 | 633 | 45 | 500 | 132 | 22 | 139 | 136 | 94 | 159 |
| Turn Type | Perm | NA | Perm | NA | Perm | Perm | NA | Perm | NA | Perm |
| Protected Phases |  | 2 |  | 6 |  |  | 4 |  | 8 |  |
| Permitted Phases | 2 |  | 6 |  | 6 | 4 |  | 8 |  | 8 |
| Detector Phase | 2 | 2 | 6 | 6 | 6 | 4 | 4 | 8 | 8 | 8 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 22.0 | 22.0 | 22.0 | 22.0 | 22.0 | 15.0 | 15.0 | 15.0 | 15.0 | 15.0 |
| Minimum Split (s) | 36.0 | 36.0 | 36.0 | 36.0 | 36.0 | 32.0 | 32.0 | 32.0 | 32.0 | 32.0 |
| Total Split (s) | 53.0 | 53.0 | 53.0 | 53.0 | 53.0 | 37.0 | 37.0 | 37.0 | 37.0 | 37.0 |
| Total Split (\%) | 58.9\% | 58.9\% | 58.9\% | 58.9\% | 58.9\% | 41.1\% | 41.1\% | 41.1\% | 41.1\% | 41.1\% |
| Yellow Time (s) | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| All-Red Time (s) | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |
| Lead/Lag |  |  |  |  |  |  |  |  |  |  |
| Lead-Lag Optimize? |  |  |  |  |  |  |  |  |  |  |
| Recall Mode | C-Max | C-Max | Max | Max | Max | None | None | None | None | None |
| Act Effct Green (s) | 57.4 | 57.4 | 57.4 | 57.4 | 57.4 | 18.6 | 18.6 | 18.6 | 18.6 | 18.6 |
| Actuated g/C Ratio | 0.64 | 0.64 | 0.64 | 0.64 | 0.64 | 0.21 | 0.21 | 0.21 | 0.21 | 0.21 |
| V/c Ratio | 0.36 | 0.59 | 0.16 | 0.48 | 0.14 | 0.11 | 0.56 | 0.71 | 0.32 | 0.40 |
| Control Delay | 11.6 | 13.1 | 9.6 | 11.2 | 2.0 | 27.9 | 35.6 | 52.0 | 31.8 | 7.4 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 11.6 | 13.1 | 9.6 | 11.2 | 2.0 | 27.9 | 35.6 | 52.0 | 31.8 | 7.4 |
| LOS | B | B | A | B | A | C | D | D | C | A |

Approach Delay
Approach Delay
Approach LOS

## ntersection Summa

ycle Length: 90
ength: 90
Ifset: $0(0 \%)$, Referenced to phase 2:EBTL, Start of Green
Control Type: Actuated-Coordinated

```
Maximum v/c Ratio: 0.71
\begin{tabular}{ll} 
Intersection Signal Delay: 16.7 & Intersection LOS: B \\
Intersection Capacity Utilization 101.1\% & ICU Level of Service G \\
Analysis Period (min) 15 &
\end{tabular}
Analysis Period (min) 15
```



[^35]Synchro 10 Report

HCM Signalized Intersection Capacity Analysis
<2035 Background> AM Peak Hour 3: Davis Road \& Lundys Lane 3: Davis Road \& Lundys Lane

 $\begin{array}{lrrrrrrrrrrrr}\text { Ideal Flow (vphpl) } & 1900 & 1900 & 1900 & 1900 & 1900 & 1900 & 1900 & 1900 & 1900 & 1900 & 1900 & 1900 \\ \text { Total Lost time (s) } & 7.0 & 7.0 & & 7.0 & 7.0 & 7.0 & 7.0 & 7.0 & & 7.0 & 7.0 & 7.0\end{array}$ | Total Lost time (s) | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |

| Frpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt | 1.00 | 1.00 | 1.00 | 1.00 | 0.85 | 1.00 | 0.97 | 1.00 | 1.00 | 0.85 |


| FIt | 1.00 | 1.00 | 1.00 | 1.00 | 0.85 | 1.00 | 0.97 | 1.00 | 1.00 | 0.85 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| FIt Protected | 0.95 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 0.95 | 1.00 | 1.00 |


| Fit Protected | 0.95 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 0.95 | 1.00 | 1.00 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Satd. Flow (prot) | 1656 | 1828 | 1467 | 1743 | 1442 | 1444 | 1519 | 1530 | 1532 | 1392 |
| FIt Permitted | 0.41 | 1.00 | 0.31 | 1.00 | 1.00 | 0.69 | 1.00 | 0.61 | 1.00 | 1.00 |


|  |  |  |  |  |  |  |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Satd. Flow (perm) | 718 | 1828 | 476 | 1743 | 1442 | 1052 | 1519 | 985 | 1532 | 1392 |


|  | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Peak--hour factor, PHF | 163 | 673 | 19 | 48 | 532 | 140 | 23 | 148 | 32 | 145 | 100 | 169 |
| Adj. Fow (vph) | 0 | 1 | 0 |  |  |  |  |  |  |  |  |  |


|  |  |  |  |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| RTOR Reduction (vph) | 16 | 1 | 0 | 0 | 0 | 51 | 0 | 10 | 0 | 0 | 0 | 134 |


| Lane Group Flow (vph) | 163 | 691 | 0 | 48 | 532 | 89 | 23 | 170 | 0 | 145 | 100 | 35 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


| Heavy Vehicles (\%) | $9 \%$ | $3 \%$ | $19 \%$ | $23 \%$ | $9 \%$ | $12 \%$ | $25 \%$ | $20 \%$ | $30 \%$ | $18 \%$ | $24 \%$ | $16 \%$ |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Turn Type | Perm | NA |  | Perm | NA | Perm | Perm | NA |  | Perm | NA | Perm |

Turn Type

| NA | Perm |
| :--- | :--- |

Protected Phases
Permitted Phases
Permitted Phases 2
Actuated Green, G (s)
Effective Green, $g$ (s)


Clearance Time (s)

|  |  |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
|  | 4.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |
|  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |
| Cenicle Extension (s) | 457 | 1165 | 303 | 1111 | 919 | 217 | 313 | 203 | 316 | 28 |
| Lane Grp Cap (vph) | co |  |  | 0.31 |  |  | 0.11 |  | 0.07 |  |

v/s Ratio Prot
v/s Ratio Perm
$\begin{array}{lrr} & 0.36 & 0.59 \\ \text { Uniform Delay, d1 } & 7.6 & 9.5\end{array}$
Progression Factor
$\begin{array}{rr}7.6 & 9.5 \\ 1.00 & 1.00\end{array}$
$\begin{array}{llr}\text { elay (s) } & 2.2 & 2.2 \\ & 9.8 & 11.7\end{array}$
$\begin{array}{lr}\text { Level of Service } & \text { A }\end{array}$ Approach Delay (s) Approach LOS
Intersection Summary

| HCM 2000 Control Delay | 16.9 | HCM 2000 Level of Service | B |
| :--- | ---: | :--- | ---: |
| HCM 2000 Volume to Capacity ratio | 0.62 | Sum of lost time (s) | 14.0 |
| Actuated CCcle Length (s) | 90.0 | ICU Level of Service | G |

Actualed Cycle Length (s)
ICU Level of Service
G
Analysis Period (min)
c Critical Lane Group

Timings
4：Thorold Townline Road \＆Thorold Stone Road

|  |  |  |  |  |  |  |  | 4 |  | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | SBL | SBT |
| Lane Configurations | \％ | 个 $\uparrow$ | F | \％ | ¢ $\uparrow$ | F | \％ | $\stackrel{\square}{4}$ | ${ }^{7}$ | $\stackrel{1}{ }$ |
| Traffic Volume（vph） | 323 | 767 | 159 | 203 | 854 | 73 | 107 | 160 | 52 | 209 |
| Future Volume（vph） | 323 | 767 | 159 | 203 | 854 | 73 | 107 | 160 | 52 | 209 |
| Turn Type | pm＋pt | NA | Perm | pm＋pt | NA | Perm | pm＋pt | NA | Perm | NA |
| Protected Phases | 5 | 2 |  | 1 | 6 |  | 7 | 4 |  | 8 |
| Permitted Phases | 2 |  | 2 | 6 |  | 6 | 4 |  | 8 |  |
| Detector Phase | 5 | 2 | 2 | 1 | 6 | 6 | 7 | 4 | 8 | 8 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 8.0 | 10.0 | 10.0 | 8.0 | 10.0 | 10.0 | 8.0 | 10.0 | 10.0 | 10.0 |
| Minimum Split（s） | 11.0 | 35.1 | 35.1 | 12.5 | 35.1 | 35.1 | 11.0 | 41.4 | 41.4 | 41.4 |
| Total Split（s） | 27.0 | 48.6 | 48.6 | 17.4 | 39.0 | 39.0 | 11.0 | 54.0 | 43.0 | 43.0 |
| Total Split（\％） | 22．5\％ | 40．5\％ | 40．5\％ | 14．5\％ | 32．5\％ | 32．5\％ | 9．2\％ | 45．0\％ | 35．8\％ | 35．8\％ |
| Yellow Time（s） | 3.0 | 4.1 | 4.1 | 3.0 | 4.1 | 4.1 | 3.0 | 4.1 | 4.1 | 4.1 |
| All－Red Time（s） | 0.0 | 2.0 | 2.0 | 0.0 | 2.0 | 2.0 | 0.0 | 2.3 | 2.3 | 2.3 |
| Lost Time Adjust（s） | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time（s） | 3.0 | 6.1 | 6.1 | 3.0 | 6.1 | 6.1 | 3.0 | 6.4 | 6.4 | 6.4 |
| Lead／Lag | Lead | Lag | Lag | Lead | Lag | Lag | Lead |  | Lag | Lag |
| Lead－Lag Optimize？ | Yes | Yes | Yes | Yes | Yes | Yes | Yes |  | Yes | Yes |
| Recall Mode | None | C－Max | C－Max | None | C－Max | C－Max | None | None | None | None |
| Act Effict Green（s） | 65.2 | 46.1 | 46.1 | 53.6 | 37.5 | 37.5 | 48.8 | 45.4 | 34.4 | 34.4 |
| Actuated g／C Ratio | 0.54 | 0.38 | 0.38 | 0.45 | 0.31 | 0.31 | 0.41 | 0.38 | 0.29 | 0.29 |
| v／c Ratio | 0.92 | 0.60 | 0.27 | 0.71 | 0.81 | 0.14 | 0.56 | 0.42 | 0.18 | 0.94 |
| Control Delay | 72.0 | 44.9 | 23.9 | 31.0 | 46.4 | 2.6 | 33.5 | 26.6 | 32.9 | 67.9 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 72.0 | 44.9 | 23.9 | 31.0 | 46.4 | 2.6 | 33.5 | 26.6 | 32.9 | 67.9 |
| LOS | E | D | C | C | D | A | C | C | C | E |
| Approach Delay |  | 49.2 |  |  | 40.8 |  |  | 28.7 |  | 64.0 |
| Approach LOS |  | D |  |  | D |  |  | C |  | E |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |
| Cycle Length： 120 |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length： 120 |  |  |  |  |  |  |  |  |  |  |
| Offset： 0 （0\％），Referenced to phase 2：EBTL and 6：WBTL，Start of Green |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle： 100 |  |  |  |  |  |  |  |  |  |  |
| Control Type：Actuated－Coordinated |  |  |  |  |  |  |  |  |  |  |
| Maximum v／c Ratio： 0.94 |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay： 46.2 |  |  |  | Intersection LOS：D |  |  |  |  |  |  |
| Intersection Capacity Utilization 89．3\％ |  |  |  | ICU Level of Service E |  |  |  |  |  |  |
| Analysis Period（min） 15 |  |  |  |  |  |  |  |  |  |  |



HCM Signalized Intersection Capacity Analysis
＜2035 Background＞AM Peak Hour 4：Thorold Townline Road \＆Thorold Stone Road

9－14－202

|  | $\Rightarrow$ |  |  | 7 |  |  |  | 4 | 1 |  | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \％ | 个 $\uparrow$ | $\overline{7}$ | \％ | ¢ 4 | 「 | \％ | F |  | 7 | F |  |
| Traffic Volume（vph） | 323 | 767 | 159 | 203 | 854 | 73 | 107 | 160 | 80 | 52 | 209 | 205 |
| Future Volume（vph） | 323 | 767 | 159 | 203 | 854 | 73 | 107 | 160 | 80 | 52 | 209 | 205 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time（s） | 3.0 | 6.1 | 6.1 | 3.0 | 6.1 | 6.1 | 3.0 | 6.4 |  | 6.4 | 6.4 |  |
| Lane Util．Factor | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 |  |
| Frpb，ped／bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.97 | 1.00 | 1.00 |  | 1.00 | 1.00 |  |
| Flpb，ped／bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 |  |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 0.95 |  | 1.00 | 0.93 |  |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |  | 0.95 | 1.00 |  |
| Satd．Flow（prot） | 1641 | 3471 | 1369 | 1444 | 3505 | 1453 | 1492 | 1535 |  | 1641 | 1497 |  |
| Flt Permitted | 0.11 | 1.00 | 1.00 | 0.28 | 1.00 | 1.00 | 0.19 | 1.00 |  | 0.60 | 1.00 |  |
| Satd．Flow（perm） | 197 | 3471 | 1369 | 422 | 3505 | 1453 | 296 | 1535 |  | 1043 | 1497 |  |
| Peak－hour factor，PHF | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 |
| Adj．Flow（vph） | 336 | 799 | 166 | 211 | 890 | 76 | 111 | 167 | 83 | 54 | 218 | 214 |
| RTOR Reduction（vph） | 0 | 0 | 82 | 0 | 0 | 52 | 0 | 16 | 0 | 0 | 30 |  |
| Lane Group Flow（vph） | 336 | 799 | 84 | 211 | 890 | 24 | 111 | 234 | 0 | 54 | 402 |  |
| Confl．Peds．（\＃／hr） | 4 |  |  |  |  | 4 |  |  |  |  |  |  |
| Heavy Vehicles（\％） | 10\％ | 4\％ | 18\％ | 25\％ | 3\％ | 8\％ | 21\％ | 14\％ | 25\％ | 10\％ | 18\％ | 17\％ |
| Turn Type | pm＋pt | NA | Perm | pm＋pt | NA | Perm | pm＋pt | NA |  | Perm | NA |  |
| Protected Phases | 5 | 2 |  | 1 | 6 |  | 7 | 4 |  |  | 8 |  |
| Permitted Phases | 2 |  | 2 | 6 |  | 6 | 4 |  |  | 8 |  |  |
| Actuated Green，G（s） | 62.1 | 46.1 | 46.1 | 50.4 | 37.4 | 37.4 | 45.4 | 45.4 |  | 34.4 | 34.4 |  |
| Effective Green， g （s） | 62.1 | 46.1 | 46.1 | 50.4 | 37.4 | 37.4 | 45.4 | 45.4 |  | 34.4 | 34.4 |  |
| Actuated g／C Ratio | 0.52 | 0.38 | 0.38 | 0.42 | 0.31 | 0.31 | 0.38 | 0.38 |  | 0.29 | 0.29 |  |
| Clearance Time（s） | 3.0 | 6.1 | 6.1 | 3.0 | 6.1 | 6.1 | 3.0 | 6.4 |  | 6.4 | 6.4 |  |
| Vehicle Extension（s） | 2.5 | 6.0 | 6.0 | 2.5 | 6.0 | 6.0 | 2.5 | 2.3 |  | 2.3 | 2.3 |  |
| Lane Grp Cap（vph） | 363 | 1333 | 525 | 287 | 1092 | 452 | 191 | 580 |  | 298 | 429 |  |
| $\mathrm{v} / \mathrm{s}$ Ratio Prot | c0． 17 | 0.23 |  | 0.08 | 0.25 |  | c0．04 | 0.15 |  |  | c0．27 |  |
| v／s Ratio Perm | c0．31 |  | 0.06 | 0.23 |  | 0.02 | 0.18 |  |  | 0.05 |  |  |
| v／c Ratio | 0.93 | 0.60 | 0.16 | 0.74 | 0.82 | 0.05 | 0.58 | 0.40 |  | 0.18 | 0.94 |  |
| Uniform Delay，d1 | 33.4 | 29.6 | 24.2 | 24.1 | 38.1 | 28.9 | 27.8 | 27.4 |  | 32.2 | 41.7 |  |
| Progression Factor | 1.63 | 1.41 | 3.12 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 |  |
| Incremental Delay，d2 | 24.4 | 1.6 | 0.5 | 8.9 | 6.7 | 0.2 | 3.7 | 0.3 |  | 0.2 | 27.8 |  |
| Delay（s） | 78.8 | 43.2 | 76.3 | 32.9 | 44.8 | 29.1 | 31.4 | 27.6 |  | 32.4 | 69.6 |  |
| Level of Service | E | D | E | C | D | C | C | C |  | C | E |  |
| Approach Delay（s） |  | 56.6 |  |  | 41.7 |  |  | 28.8 |  |  | 65.4 |  |
| Approach LOS |  | E |  |  | D |  |  | C |  |  | E |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 2000 Control Delay |  |  | 49.6 |  | CM 2000 | Level of | Service |  | D |  |  |  |
| HCM 2000 Volume to Capacity ratio |  |  | 0.93 |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length（s） |  |  | 120.0 |  | Sum of los | time（s） |  |  | 18.5 |  |  |  |
| Intersection Capacity Utilization |  |  | 89．3\％ |  | CU Level | of Service |  |  | E |  |  |  |
| Analysis Period（min） |  |  | 15 |  |  |  |  |  |  |  |  |  |
| c Critical Lane Group |  |  |  |  |  |  |  |  |  |  |  |  |

Ippers Quarry Traffic Impact Study
TMIG

Synchro 10 Report

Timings
<2035 Background> AM Peak Hour 09-14-2021



[^36]Synchro 10 Report

HCM Signalized Intersection Capacity Analysis 5: Thorold Townline Road \& Lundys Lane
<2035 Background> AM Peak Hour


| Lane Configurations | \% | $\uparrow$ | F' | ${ }^{7}$ | $\stackrel{\rightharpoonup}{1}$ |  | \% | $\stackrel{\rightharpoonup}{1}$ |  | \% | $\uparrow$ | 1 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Traffic Volume (vph) | 203 | 607 | 107 | 38 | 422 | 78 | 77 | 140 | 37 | 44 | 85 | 82 |
| Future Volume (vph) | 203 | 607 | 107 | 38 | 422 | 78 | 77 | 140 | 37 | 44 | 5 |  |


|  | 607 | 107 | 38 | 422 | 78 | 77 | 140 | 37 | 44 | 85 | 82 |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Future Volume (vph) | 203 | 607 | 1000 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |


|  | 1900 | 1900 |  |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  | 6.0 | 6.0 |  | 6.0 | 6.0 | 6.0 |


| Total Lost time (s) | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
|  | 100 | 100 | 100 | 100 | 100 | 10 | 1.00 | 1.00 | 1.0 | 1.0 |


|  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Frpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |


|  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Flpb, ped ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
|  | 1.00 | 1.00 | 0.85 | 1.00 | 0.98 | 1.00 | 0.97 | 1.00 | 1.00 | 0.85 |


|  | 1.00 | 1.00 | 0.85 | 1.00 | 0.98 | 1.00 | 0.97 | 1.00 | 1.00 | 0.85 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| FIt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 0.95 | 1.00 | 0.95 | 1.00 | 1.00 |


|  | 1.95 | 1.00 | 1.00 | 0.95 | 1.00 | 0.95 | 1.00 | 0.95 | 1.00 | 1.00 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Slt Protected | Flow (prot) | 1582 | 1810 | 1495 | 1752 | 1760 | 1612 | 1607 | 1671 | 1638 |
| Falt | 0.42 | 1.00 | 1.00 | 0.35 | 1.00 | 0.70 | 1.00 | 0.51 | 1.00 | 1.00 |
| Flt Permitted | 701 | 1810 | 14 | 68 | 170 | 1184 | 100 |  | 1038 | 1250 |


| Satd. Flow (perm) | 701 | 1810 | 1495 | 648 | 1760 | 1184 | 1607 | 893 | 1638 | 1252 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


|  |  |  |  |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| dj. Flow (vph) | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 |
|  | 218 | 653 | 115 | 41 | 454 | 84 | 83 | 151 | 40 | 47 | 91 | 81 |


| RTOR Reduction (vph) | 0 | 0 | 17 | 0 | 5 | 0 | 0 | 11 | 0 | 0 | 0 | 72 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


| Lane Group Flow (vph) | 218 | 653 | 98 | 41 | 533 | 0 | 83 | 180 | 0 | 47 | 91 | 1 |
| :--- | ---: | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


| Heavy Vehicles (\%) | $14 \%$ | $5 \%$ | $8 \%$ | $3 \%$ | $6 \%$ | $0 \%$ | $12 \%$ | $17 \%$ | $5 \%$ | $8 \%$ | $16 \%$ | 29 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Turn Type | Perm | NA | Perm | Perm | NA |  | Perm | NA |  | Perm | NA | Perm |

urn Type
Protected Phases
Permitted Phases
Actuated Green, G (s)
Effective Green, $g$ (s)
Clearance Time (s)

|  | 0.69 |
| :--- | ---: |
| Clearancle Exiension (s) | 7.0 |
|  | 5.0 |


|  |  |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Lane Grp Cap (vph) | 482 | 1245 | 1028 | 445 | 1210 | 215 | 292 | 162 | 298 | 227 |
| v/s Ratio Prot | c0.36 |  |  | 0.30 |  | $c 0.11$ |  | 0.06 |  |  |


| N/s Ratio Perm | 0.31 | 0.07 | 0.06 | 0.44 | 0.07 |  | 0.05 | 0.01 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


|  | 0.45 | 0.52 | 0.10 | 0.09 | 0.44 | 0.39 | 0.62 | 0.29 | 0.31 | 0.07 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| V/c Ratio | Uniform Delay, d1 | 7.1 | 7.6 | 5.2 | 5.2 | 7.0 | 36.0 | 37.7 | 35.3 | 35.4 |


| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
|  | 3.0 | 1.6 | 0.2 | 0.4 | 12 | 2.4 | 5.5 | 2.1 | 1.2 | 0.3 |


| Level of Service | B | A | A | A | A | D | D | D |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Approach Delay (s) | 9.0 |  | 8.0 |  | D |  |  |  |
| Approach LOS |  | A |  |  | A |  | D |  |


| Intersection Summary |  |  |  |
| :--- | ---: | :--- | ---: |
| HCM 2000 Control Delay | 16.0 | HCM 2000 Level of Service | B |
| HCM 2000 Volume to Capacity ratio | 0.54 | Sum of lost time (s) | 13.0 |
| Actuated Cycle Length (s) | 100.0 | E |  |
| Intersection Capacity Utilization | $88.2 \%$ | ICU Level of Service | E |
| Analysis Period (min) | 15 |  |  |
| C Critical Lane Group |  |  |  |

C Critical Lane Group

Timings
6: Thorold Townline Road \& Beaverdams Road

| Lane Group | EBL | EBT | WBL | WBT | NBL | NBT | SBL | SBT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations |  | ${ }_{\text {¢ }}$ |  | ${ }_{\text {¢ }}$ |  | ¢ |  | $\dagger$ |
| Traffic Volume (vph) | 19 | 126 | 52 | 170 | 24 | 317 | 11 | 538 |
| Future Volume (vph) | 19 | 126 | 52 | 170 | 24 | 317 | 11 | 538 |
| Turn Type | Perm | NA | Perm | NA | Perm | NA | Perm | NA |
| Protected Phases |  | 2 |  | 6 |  | 4 |  | 8 |
| Permitted Phases | 2 |  | 6 |  | 4 |  | 8 |  |
| Detector Phase | 2 | 2 | 6 | 6 | 4 | 4 | 8 | 8 |
| Switch Phase |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| Minimum Split (s) | 30.5 | 30.5 | 30.5 | 30.5 | 34.0 | 34.0 | 30.5 | 30.5 |
| Total Split (s) | 31.0 | 31.0 | 31.0 | 31.0 | 59.0 | 59.0 | 59.0 | 59.0 |
| Total Split (\%) | 34.4\% | 34.4\% | 34.4\% | 34.4\% | 65.6\% | 65.6\% | 65.6\% | 65.6\% |
| Yellow Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| All-Red Time (s) | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |
| Lost Time Adjust (s) |  | 0.0 |  | 0.0 |  | 0.0 |  | 0.0 |
| Total Lost Time (s) |  | 6.0 |  | 6.0 |  | 6.0 |  | 6.0 |
| Lead/Lag |  |  |  |  |  |  |  |  |
| Lead-Lag Optimize? |  |  |  |  |  |  |  |  |
| Recall Mode | C-Max | C-Max | Max | Max | Max | Max | Max | Max |
| Act Effict Green (s) |  | 25.0 |  | 25.0 |  | 53.0 |  | 53.0 |
| Actuated g/C Ratio |  | 0.28 |  | 0.28 |  | 0.59 |  | 0.59 |
| v/c Ratio |  | 0.36 |  | 0.57 |  | 0.50 |  | 0.68 |
| Control Delay |  | 27.9 |  | 33.0 |  | 12.4 |  | 17.2 |
| Queue Delay |  | 0.0 |  | 0.0 |  | 0.0 |  | 0.0 |
| Total Delay |  | 27.9 |  | 33.0 |  | 12.4 |  | 17.2 |
| LOS |  | C |  | C |  | B |  | B |
| Approach Delay |  | 27.9 |  | 33.0 |  | 12.4 |  | 17.2 |
| Approach LOS |  | C |  | c |  | B |  | B |

## -

## ycle Length: 90

Actuated Cycle Length. 90
Offset: $0(0 \%)$, Referenced to phase 2:EBTL, Start of Green
Natural Cycle: 70
$\begin{array}{ll}\text { Control Type: Actuated-Coordinated } & \\ \text { Maximum v/c Ratio: } 0.68 & \\ \text { Intersection Signal Delay: } 19.8 & \text { Intersection LOS: } B \\ \text { Intersection Capacity Utilization 66.7\% } & \text { ICU Level of Service }\end{array}$
ntersection Capacity Utilization 66.7\% ICU Level of Service C
Analysis Period (min) 15


[^37]HCM Signalized Intersection Capacity Analysis
<2035 Background> AM Peak Hour
. Thorold Townline Road \& Beaverdams Road


Ippers Quarry Traffic Impact Study

HCM Unsignalized Intersection Capacity Analysis <2035 Background> AM Peak Hou 7: Thorold Townline Road \& Uppers Lane

| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Lane Configurations | 0 |  | $\hat{7}$ |  | $\uparrow$ | $\uparrow$ |
| Traffic Volume (veh/h) | 0 | 0 | 458 | 0 | 0 | 419 |
| Future Volume (Veh/h) | 0 | 0 | 458 | 0 | 0 | 419 |
| Sign Control | Stop |  | Free |  |  | Free |
| Grade | $0 \%$ |  | $0 \%$ |  | $0 \%$ |  |
| Peak Hour Factor | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 |
| Hourly flow rate (vph) | 0 | 0 | 492 | 0 | 0 | 451 |
| Pedestrians |  |  |  |  |  |  |

Pedestrians
Lane Width ( m )
Walking Speed ( $\mathrm{m} / \mathrm{s}$ )
Waking Speed ( $\mathrm{m} / \mathrm{s}$ )
Right turn flare (veh)


Analysis Period (min)
pravary Traffic Impact Study
Synchro 10 Report
TMIG


| Lane Group | EBL | EBT | EBR | WBL | WBT | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \％ | 个 $\uparrow$ | 7 | \％ | 个t | \％ | $\uparrow$ | 「 | \％ | $\uparrow$ | $\overline{7}$ |
| Traffic Volume（vph） | 24 | 1255 | 736 | 211 | 1223 | 627 | 5 | 178 | 4 | 6 | 28 |
| Future Volume（vph） | 24 | 1255 | 736 | 211 | 1223 | 627 | 5 | 178 | 4 | 6 | 28 |
| Turn Type | Perm | NA | Perm | pm＋pt | NA | Split | NA | Perm | Split | NA | Perm |
| Protected Phases |  | 2 |  | 1 | 6 | 4 | 4 |  | 8 | 8 |  |
| Permitted Phases | 2 |  | 2 | 6 |  |  |  | 4 |  |  | 8 |
| Detector Phase | 2 | 2 | 2 | 1 | 6 | 4 | 4 | 4 | 8 | 8 | 8 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 20.0 | 20.0 | 20.0 | 5.0 | 20.0 | 10.0 | 10.0 | 10.0 | 10.0 | 10.0 | 10.0 |
| Minimum Split（s） | 28.9 | 28.9 | 28.9 | 8.0 | 28.9 | 29.7 | 29.7 | 29.7 | 17.7 | 17.7 | 17.7 |
| Total Split（s） | 55.0 | 55.0 | 55.0 | 14.0 | 69.0 | 33.3 | 33.3 | 33.3 | 17.7 | 17.7 | 17.7 |
| Total Split（\％） | 45．8\％ | 45．8\％ | 45．8\％ | 11．7\％ | 57．5\％ | 27．8\％ | 27．8\％ | 27．8\％ | 14．8\％ | 14．8\％ | 14．8\％ |
| Yellow Time（s） | 5.4 | 5.4 | 5.4 | 3.0 | 5.4 | 5.7 | 5.7 | 5.7 | 5.7 | 5.7 | 5.7 |
| All－Red Time（s） | 1.5 | 1.5 | 1.5 | 0.0 | 1.5 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |
| Lost Time Adjust（s） | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time（s） | 6.9 | 6.9 | 6.9 | 3.0 | 6.9 | 7.7 | 7.7 | 7.7 | 7.7 | 7.7 | 7.7 |
| Lead／Lag | Lag | Lag | Lag | Lead |  |  |  |  |  |  |  |
| Lead－Lag Optimize？ | Yes | Yes | Yes | Yes |  |  |  |  |  |  |  |
| Recall Mode | C－Max | C－Max | C－Max | None | C－Max | None | None | None | None | None | None |
| Act Efft Green（s） | 52.2 | 52.2 | 52.2 | 73.1 | 69.2 | 25.6 | 25.6 | 25.6 | 10.0 | 10.0 | 10.0 |
| Actuated g／C Ratio | 0.44 | 0.44 | 0.44 | 0.61 | 0.58 | 0.21 | 0.21 | 0.21 | 0.08 | 0.08 | 0.08 |
| $\mathrm{v} / \mathrm{C}$ Ratio | 0.22 | 0.86 | 0.85 | 0.85 | 0.63 | 0.92 | 0.94 | 0.40 | 0.03 | 0.04 | 0.12 |
| Control Delay | 29.6 | 38.4 | 25.2 | 55.8 | 28.5 | 78.2 | 80.8 | 8.3 | 51.2 | 51.3 | 1.0 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 29.6 | 38.4 | 25.2 | 55.8 | 28.5 | 78.2 | 80.8 | 8.3 | 51.2 | 51.3 | 1.0 |
| LOS | C | D | C | E | C | E | F | A | D | D | A |
| Approach Delay |  | 33.5 |  |  | 32.5 |  | 63.9 |  |  | 13.9 |  |
| Approach LOS |  | C |  |  | C |  | E |  |  | B |  |

## Itersection Sum

## Cycle Length： 120

Actuated Cycle Length 120
Offset： $0(0 \%)$ ，Referenced to phase 2：EBTL and 6 ：WBTL，Start of Green
Natural Cycle： 105
Control Type：Actuated－Coordinated

| Conirol Type：Actuated－Coordinated |  |
| :--- | :--- |
| Maximum v／c Ratio：0．94  <br> Intersection Signal Delay： 38.7 Intersection LOS：D <br> Intersection Capacity Utiization 92．6\％ ICU Level of Service F <br> Analysis Period（min） 15  |  |

Intersection Capacity Utilization 92．6\％ ICU Level of Service F

Splits and Phases：1：Davis Road \＆Thorold Stone Road


[^38]Synchro 10 Report
$\xrightarrow{\text { ．Davis Road \＆Thorold Stone Road }}$
 $\begin{array}{lrrrrrrrrrrrr}\text { Future Volume（vph）} & 24 & 1255 & 736 & 211 & 1223 & 1 & 627 & 5 & 178 & 4 & 6 & 28 \\ \text { Ideal Flow（vphl）} & 1900 & 1900 & 1900 & 1900 & 1900 & 1900 & 1900 & 1900 & 1900 & 1900 & 1900 & 1900 \\ \text { Total Lost time（s）} & 6.9 & 6.9 & 6.9 & 3.0 & 6.9 & & 7.7 & 7.7 & 7.7 & 7.7 & 7.7 & 7.7\end{array}$

|  | 6.9 | 6.9 | 6.9 | 3.0 | 6.9 | 7.7 | 7.7 | 7.7 | 7.7 | 7.7 | 7.7 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Total Lost time（s） | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 0.95 | 0.95 | 1.00 | 1.00 | 1.00 | 1.00 |
| Lane Util．Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 100 | 0.98 |


| Frpb，ped／bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.98 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Flpb，ped／bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
|  | 1.00 | 100 | 0.85 | 1.00 | 1.00 | 1.0 | 1.00 | 00 | 1.00 | 1.00 | 105 |


| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| FIt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 0.95 | 0.95 | 1.00 | 0.95 | 1.00 | 1.00 |


|  |  |  |  |  |  |  |  |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | ---: | ---: | ---: | ---: |
| Satd．Flow（prot） | 1433 | 3539 | 1568 | 1671 | 3539 | 1681 | 1680 | 1482 | 1805 | 1810 | 1525 |
| FIt Permitted | 0.18 | 1.00 | 1.00 | 0.08 | 1.00 | 0.95 | 0.95 | 1.00 | 0.95 | 1.00 | 1.00 |


| Satd．Flow（perm） | 267 | 3539 | 1568 | 135 | 3539 |  | 1681 | 1680 | 1482 | 1805 | 1810 | 1525 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Peak－hour factor，PHF | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | Adj．Flow（vph） TOR Reductio


|  | 0 | 0 | 239 | 0 | 0 | 0 | 0 | 0 | 147 | 0 | 0 | 28 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |



| Heary Vehicles（\％） | $26 \%$ | $2 \%$ | $3 \%$ | $8 \%$ | $2 \%$ | $0 \%$ | $2 \%$ | $30 \%$ | $9 \%$ | $0 \%$ | $5 \%$ | $4 \%$ |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Turn Type | Perm | NA | Perm | pm＋pt | NA |  | Split | NA | Perm | Split | NA | Perm |

Cum rype

Potected Phases

| Permitted Phases | 2 | 2 | 6 |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Actuated Green，G（s） | 49.1 | 49.1 | 49.1 | 66.1 | 66.1 | 25.6 | 25.6 | 25.6 | 6.0 | 6.0 | 6.0 |


| actuated Green，$G(s)$ | 49.1 | 49.1 | 49.1 | 66.1 | 66.1 | 25.6 | 25.6 | 25.6 | 6.0 | 6.0 | 6.0 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Effective Green，$g(s)$ | 49.1 | 49.1 | 49.1 | 66.1 | 66.1 | 25.6 | 25.6 | 25.6 | 6.0 | 6.0 | 6.0 |


| Effective Green， $\mathrm{g}(\mathrm{s})$ | 49.1 | 49.1 | 49.1 | 66.1 | 66.1 | 25.6 | 25.6 | 25.6 | 6.0 | 6.0 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Actuated g／C Ratio | 0 | 0 | 0.41 | 55 | 0.55 | 0.21 | 0.21 | 0.21 | 0.05 | 005 | 0.0 |


|  | 0.41 | 0.41 | 0.41 | 0.55 | 0.55 | 0.21 | 0.21 | 0.21 | 0.05 | 0.05 | 0.05 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Cleaarance Time（s） | 6.9 | 6.9 | 6.9 | 3.0 | 6.9 | 7.7 | 7.7 | 7.7 | 7.7 | 7.7 | 7.7 |
|  | 3.0 | 3.0 | 3.0 | 30 | 30 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4. |


|  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Lane Grp Cap（vph） | 109 | 1448 | 641 | 253 | 1949 | 358 | 358 | 316 | 90 | 90 | 76 |
| v／s Ratio Prot |  | 0.37 |  | $c 0.10$ | 0.36 | 0.20 | $c 0.20$ |  | 0.00 | $c 0.00$ |  |


| v／s Ratio Perm | 0.09 | 0.34 | $c 0.38$ |  |  |  | 0.03 |  | 0.02 | 0.02 | 0.09 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


| Uniform Delay，d1 | 0．23．1 | 33.4 | 31.8 | 34.6 | 19.0 | 46.2 | 46.4 | 38.2 | 54.3 | 54.3 | 54.2 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


| Progression Factor | 1.00 | 1.00 | 1.00 | 1.45 | 1.48 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


|  | 4.8 | 10.3 | 12.3 | 17.0 | 1.0 |  | 2.3 | 31.9 | 0.3 | 0.4 | 0.5 | 0.2 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


| Delay（s） | 28.0 | 43.7 | 44.1 | 67.2 | 29.2 |  | 75.5 | 78.3 | 38.5 | 54.6 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Level of Service | C | D | D | E | C | E | E | D | D | D |
| Approach Delay（s） |  | 43.6 |  |  | 34.8 |  | 68.5 |  |  | 54.5 |


| Approach LOS | 43.6 |
| :--- | ---: |
| D |  |


| Intersection Summary |  |  |  |
| :--- | ---: | :--- | ---: |
| HCM 2000 Controro Delay | 45.5 | HCM 2000 Level of Service | D |
| HCM 2000 Volume to Capacity ratio | 0.86 |  | 25.3 |
| Actuated Cycle Length（s） | 120.0 | Sum of lost time（s） | F |
| Intersection Capacity Utilization | $92.6 \%$ | ICU Level of Service |  |
| Analysis Period（min） | 15 |  |  | 92．6\％

CU Level of Service
$\stackrel{25}{ } \mathrm{~F}$
C Critical Lane Group

2: Davis Road \& Niagara Falls Road/Beaverdams Road


Splits and Phases: 2: Davis Road \& Niagara Falls Road/Beaverdams Road


[^39]Synchro 10 Report

HCM Signalized Intersection Capacity Analysis
2: Davis Road \& Niagara Falls Road/Beaverdams Road
<2035 Background> PM Peak Hour 2. Davis Road \& Niagara Falls Road/Beaverdams Road 09-14-2021


Uppers Quarry Traffic Impact Study 3: Davis Road \& Lundys Lane 09-14-2021

| Lane Group | EBL | EBT | WBL | WBT | WBR | NBL | NBT | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ${ }_{1}$ | ¢ | ${ }^{*}$ | $\uparrow$ | F | ${ }_{1}$ | ${ }_{6}$ | \% | $\uparrow$ | 「 |
| Traffic Volume (vph) | 208 | 717 | 42 | 718 | 216 | 46 | 141 | 239 | 125 | 184 |
| Future Volume (vph) | 208 | 717 | 42 | 718 | 216 | 46 | 141 | 239 | 125 | 184 |
| Turn Type | pm+pt | NA | Perm | NA | Perm | Perm | NA | pm+pt | NA | Perm |
| Protected Phases | 5 | 2 |  | 6 |  |  | 4 | 3 | 8 |  |
| Permitted Phases | 2 |  | 6 |  | 6 | 4 |  | 8 |  | 8 |
| Detector Phase | 5 | 2 | 6 | 6 | 6 | 4 | 4 | 3 | 8 | 8 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 22.0 | 22.0 | 22.0 | 22.0 | 15.0 | 15.0 | 5.0 | 15.0 | 15.0 |
| Minimum Split (s) | 8.0 | 36.0 | 36.0 | 36.0 | 36.0 | 32.0 | 32.0 | 8.0 | 32.0 | 32.0 |
| Total Split (s) | 14.0 | 78.0 | 64.0 | 64.0 | 64.0 | 32.0 | 32.0 | 10.0 | 42.0 | 42.0 |
| Total Split (\%) | 11.7\% | 65.0\% | 53.3\% | 53.3\% | 53.3\% | 26.7\% | 26.7\% | 8.3\% | 35.0\% | 35.0\% |
| Yellow Time (s) | 3.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 3.0 | 5.0 | 5.0 |
| All-Red Time (s) | 0.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 0.0 | 2.0 | 2.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 3.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 3.0 | 7.0 | 7.0 |
| Lead/Lag | Lead |  | Lag | Lag | Lag | Lag | Lag | Lead |  |  |
| Lead-Lag Optimize? | Yes |  | Yes | Yes | Yes | Yes | Yes | Yes |  |  |
| Recall Mode | None | C-Max | Max | Max | Max | Max | Max | None | Max | Max |
| Act Effct Green (s) | 75.0 | 71.0 | 57.0 | 57.0 | 57.0 | 25.0 | 25.0 | 39.0 | 35.0 | 35.0 |
| Actuated g/C Ratio | 0.62 | 0.59 | 0.48 | 0.48 | 0.48 | 0.21 | 0.21 | 0.32 | 0.29 | 0.29 |
| V/C Ratio | 0.87 | 0.74 | 0.23 | 0.87 | 0.29 | 0.19 | 0.58 | 0.83 | 0.26 | 0.33 |
| Control Delay | 51.7 | 23.2 | 23.4 | 43.1 | 8.7 | 41.6 | 47.3 | 58.5 | 34.4 | 6.0 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 51.7 | 23.2 | 23.4 | 43.1 | 8.7 | 41.6 | 47.3 | 58.5 | 34.4 | 6.0 |
| LOS | D | C | C | D | A | D | D | E | C | A |
| Approach Delay |  | 29.4 |  | 34.7 |  |  | 46.2 |  | 35.3 |  |
| Approach LOS |  | C |  | C |  |  | D |  | D |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 120 |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 120 |  |  |  |  |  |  |  |  |  |  |
| Offset: $0(0 \%)$, Referenced to phase 2:EBTL, Start of Green |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 95 |  |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Coordinated |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.87 |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 34.0 |  |  |  |  | Intersection LOS: C |  |  |  |  |  |
| Intersection Capacity Utilization 112.7\% |  |  |  |  | CU Level of Service H |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |



[^40]Synchro 10 Report

HCM Signalized Intersection Capacity Analysis
<2035 Background> PM Peak Hour 3: Davis Road \& Lundys Lane

09-14-202

|  | $y$ | $\rightarrow$ |  | $\checkmark$ |  |  |  | $\uparrow$ |  | $\checkmark$ | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \% | F |  | \% | $\uparrow$ | F | \% | $\dagger$ |  | \% | $\uparrow$ | F |
| Traffic Volume (vph) | 208 | 717 | 28 | 42 | 718 | 216 | 46 | 141 | 51 | 239 | 125 | 184 |
| Future Volume (vph) | 208 | 717 | 28 | 42 | 718 | 216 | 46 | 141 | 51 | 239 | 125 | 184 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 3.0 | 7.0 |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  | 3.0 | 7.0 | 7.0 |
| Lane Util. Factor | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 |
| Frpb, ped/bikes | 1.00 | 1.00 |  | 1.00 | 1.00 | 0.98 | 1.00 | 0.99 |  | 1.00 | 1.00 | 1.00 |
| Flpb, ped/bikes | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 |
| Frt | 1.00 | 0.99 |  | 1.00 | 1.00 | 0.85 | 1.00 | 0.96 |  | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 |  | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |  | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1719 | 1818 |  | 1611 | 1863 | 1473 | 1736 | 1652 |  | 1702 | 1743 | 1553 |
| Flt Permitted | 0.10 | 1.00 |  | 0.25 | 1.00 | 1.00 | 0.67 | 1.00 |  | 0.44 | 1.00 | 1.00 |
| Satd. Flow (perm) | 188 | 1818 |  | 418 | 1863 | 1473 | 1226 | 1652 |  | 790 | 1743 | 1553 |
| Peak-hour factor, PHF | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 |
| Adj. Flow (vph) | 224 | 771 | 30 | 45 | 772 | 232 | 49 | 152 | 55 | 257 | 134 | 198 |
| RTOR Reduction (vph) | 0 | 1 | 0 | 0 | 0 | 99 | 0 | 11 | 0 | 0 | 0 | 140 |
| Lane Group Flow (vph) | 224 | 800 | 0 | 45 | 772 | 133 | 49 | 196 | 0 | 257 | 134 | 58 |
| Confl. Peds. (\#/hr) | 2 |  | 1 | 1 |  | 2 |  |  | 1 | 1 |  |  |
| Heavy Vehicles (\%) | 5\% | 3\% | 26\% | 12\% | 2\% | 7\% | 4\% | 9\% | 12\% | 6\% | 9\% | 4\% |
| Turn Type | pm+pt | NA |  | Perm | NA | Perm | Perm | NA |  | pm+pt | NA | Perm |
| Protected Phases | 5 | 2 |  |  | - |  |  | , |  | 3 | 8 |  |
| Permitted Phases | 2 |  |  | 6 |  | 6 | 4 |  |  | 8 |  | 8 |
| Actuated Green, G (s) | 71.0 | 71.0 |  | 57.0 | 57.0 | 57.0 | 25.0 | 25.0 |  | 35.0 | 35.0 | 35.0 |
| Effective Green, g (s) | 71.0 | 71.0 |  | 57.0 | 57.0 | 57.0 | 25.0 | 25.0 |  | 35.0 | 35.0 | 35.0 |
| Actuated g/C Ratio | 0.59 | 0.59 |  | 0.48 | 0.48 | 0.48 | 0.21 | 0.21 |  | 0.29 | 0.29 | 0.29 |
| Clearance Time (s) | 3.0 | 7.0 |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  | 3.0 | 7.0 | 7.0 |
| Vehicle Extension (s) | 3.0 | 4.0 |  | 4.0 | 4.0 | 4.0 | 2.0 | 2.0 |  | 3.0 | 2.0 | 2.0 |
| Lane Grp Cap (vph) | 251 | 1075 |  | 198 | 884 | 699 | 255 | 344 |  | 283 | 508 | 452 |
| v/s Ratio Prot | c0.08 | 0.44 |  |  | 0.41 |  |  | 0.12 |  | c0.05 | 0.08 |  |
| v/s Ratio Perm | c0.45 |  |  | 0.11 |  | 0.09 | 0.04 |  |  | c0.21 |  | 0.04 |
| $\mathrm{v} / \mathrm{C}$ Ratio | 0.89 | 0.74 |  | 0.23 | 0.87 | 0.19 | 0.19 | 0.57 |  | 0.91 | 0.26 | 0.13 |
| Uniform Delay, d1 | 27.6 | 17.9 |  | 18.5 | 28.3 | 18.2 | 39.2 | 42.7 |  | 41.0 | 32.6 | 31.3 |
| Progression Factor | 1.00 | 1.00 |  | 1.07 | 1.15 | 1.81 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 30.2 | 4.7 |  | 2.2 | 9.8 | 0.5 | 1.7 | 6.7 |  | 30.4 | 1.3 | 0.6 |
| Delay (s) | 57.8 | 22.5 |  | 22.1 | 42.4 | 33.5 | 40.8 | 49.4 |  | 71.4 | 33.9 | 31.9 |
| Level of Service | E | C |  | C | D | C | D | D |  | E | C | C |
| Approach Delay (s) |  | 30.3 |  |  | 39.5 |  |  | 47.7 |  |  | 49.6 |  |
| Approach LOS |  | C |  |  | D |  |  | D |  |  | D |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 2000 Control Delay |  |  | 39.0 |  | CM 2000 | Level of S | ervice |  | D |  |  |  |
| HCM 2000 Volume to Capacity ratio |  |  | 0.94 |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length (s) |  |  | 120.0 |  | um of los | time (s) |  |  | 20.0 |  |  |  |
| Intersection Capacity Utilization |  |  | 112.7\% |  | CU Level | Service |  |  | H |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |
| c Critical Lane Group |  |  |  |  |  |  |  |  |  |  |  |  |

Tppers Quarry Traffic Impact Study
TMIG
Synchro 10 Report

Timings
4: Thorold Townline Road \& Thorold Stone Road



[^41]Synchro 10 Report

HCM Signalized Intersection Capacity Analysis
<2035 Background> PM Peak Hour 4: Thorold Townline Road \& Thorold Stone Road

9-14-202


Uppers Quarry Traffic Impact Study
Synchro 10 Report

Timings
<2035 Background> PM Peak Hour
09-14-2021
5: Thorold Townline Road \& Lundys Lane
$\uparrow \downarrow \downarrow \downarrow$

| Lane Group | EBL | EBT | EBR | WBL | WBT | NBL | NBT | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \% | $\uparrow$ | F | \% | F | \% | $\hat{\square}$ | \% | $\uparrow$ | F |
| Traffic Volume (vph) | 114 | 673 | 117 | 44 | 711 | 117 | 142 | 95 | 118 | 183 |
| Future Volume (vph) | 114 | 673 | 117 | 44 | 711 | 117 | 142 | 95 | 118 | 183 |
| Turn Type | Perm | NA | Perm | Perm | NA | Perm | NA | Perm | NA | Perm |
| Protected Phases |  | 2 |  |  | 6 |  | 4 |  | 8 |  |
| Permitted Phases | 2 |  | 2 | 6 |  | 4 |  | 8 |  | 8 |
| Detector Phase | 2 | 2 | 2 | 6 | 6 | 4 | 4 | 8 | 8 | 8 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 20.0 | 20.0 | 20.0 | 20.0 | 20.0 | 10.0 | 10.0 | 10.0 | 10.0 | 10.0 |
| Minimum Split (s) | 29.0 | 29.0 | 29.0 | 29.0 | 29.0 | 35.0 | 35.0 | 35.0 | 35.0 | 35.0 |
| Total Split (s) | 85.0 | 85.0 | 85.0 | 85.0 | 85.0 | 35.0 | 35.0 | 35.0 | 35.0 | 35.0 |
| Total Split (\%) | 70.8\% | 70.8\% | 70.8\% | 70.8\% | 70.8\% | 29.2\% | 29.2\% | 29.2\% | 29.2\% | 29.2\% |
| Yellow Time (s) | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| All-Red Time (s) | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 |
| Lead/Lag |  |  |  |  |  |  |  |  |  |  |
| Lead-Lag Optimize? |  |  |  |  |  |  |  |  |  |  |
| Recall Mode | C-Max | C-Max | C-Max | C-Max | C-Max | None | None | None | None | None |
| Act Effct Green (s) | 85.7 | 85.7 | 85.7 | 85.7 | 85.7 | 21.3 | 21.3 | 21.3 | 21.3 | 21.3 |
| Actuated g/C Ratio | 0.71 | 0.71 | 0.71 | 0.71 | 0.71 | 0.18 | 0.18 | 0.18 | 0.18 | 0.18 |
| v/c Ratio | 0.41 | 0.57 | 0.11 | 0.12 | 0.65 | 0.66 | 0.66 | 0.77 | 0.41 | 0.46 |
| Control Delay | 13.9 | 13.5 | 4.5 | 7.6 | 13.3 | 61.1 | 51.7 | 79.8 | 46.3 | 8.8 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 13.9 | 13.5 | 4.5 | 7.6 | 13.3 | 61.1 | 51.7 | 79.8 | 46.3 | 8.8 |
| LOS | B | B | A | A | B | E | D | E | D | A |
| Approach Delay |  | 12.4 |  |  | 13.0 |  | 55.3 |  | 37.0 |  |
| Approach LOS |  | B |  |  | B |  | E |  | D |  |

Cycle Length: 120
Actuated Cycle Length: 120
Offset: $0(0 \%)$, Referenced to phase 2:EBTL and 6 :WBTL, Start of Green
Natural Cycle: 90
$\begin{array}{ll}\text { Control Type: Actuated-Coordinated } & \\ \text { Maximum v/c Ratio: 0.77 } & \\ \text { Intersection Signal Delay: 22.1 } & \text { Intersection LOS: C } \\ \text { Intersection Capacity Utilization 98.4\% } & \text { ICU Level of Service F }\end{array}$
Analysis Period (min) 15


HCM Signalized Intersection Capacity Analysis 5: Thorold Townline Road \& Lundys Lane
<2035 Background> PM Peak Hour


|  | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Ideal Flow (vphpl) | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  | 6.0 | 6.0 |  | 6.0 | 6.0 | 6.0 |


| Total Lost time (s) | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frpb | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |  |  |


|  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |


| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Ftt | 1.00 | 1.00 | 0.85 | 1.00 | 0.99 | 1.00 | 0.96 | 1.00 | 1.00 | 0.85 |


| Flt Protected | 1.00 | 1.00 | 0.85 | 1.00 | 0.99 | 1.00 | 0.96 | 1.00 | 1.00 | 0.89 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
|  | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 0.95 | 1.00 | 0.95 | 1.00 | 1.00 |
| 1626 | 1827 | 1553 | 1752 | 1818 | 1.087 | 1748 |  | 170 |  |  |


|  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Satd. Flow (prot) | 1626 | 1827 | 1553 | 1752 | 1818 | 1687 | 1748 | 1736 | 1776 | 152 |
| It Permitted | 0.25 | 1.00 | 1.00 | 0.31 | 1.00 | 0.62 | 1.00 | 0.42 | 1.00 | 1.00 |


| Satd. Flow (perm) | 430 | 1827 | 1553 | 569 | 1818 |  | 1102 | 1748 |  | 762 | 1776 | 1524 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Peak-hour factor, PHF | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 |

dj. Flow (vph)
TOR Reduction (v
$\qquad$

|  |  |  |  |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Lane Group Flow (vph) | 125 | 740 | 114 | 48 | 848 | 0 | 129 | 199 | 0 | 104 | 130 | 36 |
| Confl. Peds. (\#/hr) | 1 |  |  |  |  | 1 |  |  |  |  |  | 0 |


| Heavy Vehicles (\%) | $11 \%$ | $4 \%$ | $4 \%$ | $3 \%$ | $2 \%$ | $15 \%$ | $7 \%$ | $6 \%$ | $0 \%$ | $4 \%$ | $7 \%$ | $6 \%$ |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Turn Type | Perm | NA | Perm | Perm | NA |  | Perm | NA |  | Perm | NA | Perm |

urn yype
Protected Phases

| Permitted Phases | 2 | 2 | 2 | 6 | 6 | 4 | 4 | 8 | 8 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |


| Actuated Green, G (s) | 85.7 | 85.7 | 85.7 | 85.7 | 85.7 | 21.3 | 21.3 | 21.3 | 21.3 | 21.3 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


| Effective Green, $\mathrm{g}(\mathrm{s})$ | 85.7 | 85.7 | 85.7 | 85.7 | 85.7 | 21.3 | 21.3 | 21.3 | 21.3 | 21.3 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


|  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


|  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Clearance Time (s) | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| Vehicle Extension (s) |  |  |  |  |  |  |  |  |  |  |


| Lane Grp Cap (vph) | 307 | 1304 | 1109 | 406 | 1298 | 195 | 310 | 135 | 315 | 27 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| v/s Ratio Prot |  | 0.41 |  |  | $c 0.47$ |  | 0.11 |  | 0.07 |  |
| v/s Ratio Porm | 0.09 |  | 0.07 | 0.08 |  | 0.12 |  | $c 0.14$ |  | 0.02 |


| I/s Ratio Perm | 0.29 | 0.07 | 0.08 | 0.65 | 0.12 |  | $c 0.14$ | 0.02 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


|  | 0.41 | 0.57 | 0.10 | 0.12 | 0.65 | 0.66 | 0.64 | 0.77 | 0.41 | 0.13 |
| :--- | ---: | ---: | ---: | ---: | ---: | :--- | :--- | :--- | :--- | :--- |
| Uniform Delay, d1 | 6.9 | 8.2 | 5.3 | 5.4 | 9.2 | 46.0 | 45.8 | 47.0 | 43.8 | 41.6 |


| Progression Factor | 1.22 | 1.30 | 1.09 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


|  | 2.5 | 1.1 | 0.1 | 0.6 | 2.6 | 10.7 | 6.1 | 26.7 | 1.8 | 0.5 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


|  | B | B | A | A | B | E | D | E | D |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Level of Service | 11.0 |  | 11.4 |  | 53.7 | 50.7 |  |  |  |
| Approach Delay (s) |  | B |  | B |  | D |  |  |  |
| Approach LOS |  |  |  |  |  | D |  |  |  |


| Intersection Summary |  |  |  |
| :--- | ---: | :--- | ---: |
| HCM 2000 Control Delay | 23.1 | HCM 2000 Level of Service | C |
| HCM 2000 Volume to Capacity ratio | 0.68 |  |  |
| Actuated Cycle Length (s) | 120.0 | Sum of lost time (s) | 13.0 |
| Intersection Capacity Utilization | $98.4 \%$ | ICU Level of Service | F |
| Analysis Period (min) | 15 |  |  |

Intersection Capacity $\mathbf{~ s}$ )
CU Level of Service
c Critical Lane Group

Timings
6: Thorold Townline Road \& Beaverdams Road



[^42]Synchro 10 Report

HCM Signalized Intersection Capacity Analysis
<2035 Background> PM Peak Hour
6: Thorold Townline Road \& Beaverdams Road

|  | $\Rightarrow$ |  |  |  |  |  |  | $\uparrow$ |  |  |  | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | ¢ |  |  | ¢ |  |  | ${ }_{\text {A }}$ |  |  | $\uparrow$ |  |
| Traffic Volume (vph) | 27 | 205 | 16 | 124 | 178 | 21 | 32 | 538 | 94 | 20 | 317 | 41 |
| Future Volume (vph) | 27 | 205 | 16 | 124 | 178 | 21 | 32 | 538 | 94 | 20 | 317 | 41 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) |  | 6.0 |  |  | 6.0 |  |  | 6.0 |  |  | 6.0 |  |
| Lane Util. Factor |  | 1.00 |  |  | 1.00 |  |  | 1.00 |  |  | 1.00 |  |
| Frpb, ped/bikes |  | 1.00 |  |  | 1.00 |  |  | 1.00 |  |  | 1.00 |  |
| Flpb, ped/bikes |  | 1.00 |  |  | 1.00 |  |  | 1.00 |  |  | 1.00 |  |
| Frt |  | 0.99 |  |  | 0.99 |  |  | 0.98 |  |  | 0.99 |  |
| Flt Protected |  | 0.99 |  |  | 0.98 |  |  | 1.00 |  |  | 1.00 |  |
| Satd. Flow (prot) |  | 1830 |  |  | 1803 |  |  | 1710 |  |  | 1758 |  |
| Flt Permitted |  | 0.93 |  |  | 0.73 |  |  | 0.97 |  |  | 0.95 |  |
| Satd. Flow (perm) |  | 1720 |  |  | 1333 |  |  | 1656 |  |  | 1670 |  |
| Peak-hour factor, PHF | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 |
| Adj. Flow (vph) | 29 | 220 | 17 | 133 | 191 | 23 | 34 | 578 | 101 | 22 | 341 | 44 |
| RTOR Reduction (vph) | 0 | 2 | 0 | 0 | 2 | 0 | 0 | 7 | 0 | 0 | 5 |  |
| Lane Group Flow (vph) | 0 | 264 | 0 | 0 | 345 | 0 | 0 | 706 | 0 | 0 | 402 |  |
| Confl. Peds. (\#/hr) | 1 |  | 5 | 5 |  | 1 | 8 |  | 3 | 3 |  |  |
| Heavy Vehicles (\%) | 10\% | 1\% | 4\% | 4\% | 1\% | 0\% | 4\% | 10\% | 0\% | 2\% | 6\% | 6\% |
| Turn Type | Perm | NA |  | Perm | NA |  | Perm | NA |  | Perm | NA |  |
| Protected Phases |  | 2 |  |  | 6 |  |  | 4 |  |  | 8 |  |
| Permitted Phases | 2 |  |  |  |  |  | 4 |  |  | 8 |  |  |
| Actuated Green, G (s) |  | 34.1 |  |  | 34.1 |  |  | 43.9 |  |  | 43.9 |  |
| Effective Green, $\mathrm{g}(\mathrm{s})$ |  | 34.1 |  |  | 34.1 |  |  | 43.9 |  |  | 43.9 |  |
| Actuated g/C Ratio |  | 0.38 |  |  | 0.38 |  |  | 0.49 |  |  | 0.49 |  |
| Clearance Time (s) |  | 6.0 |  |  | 6.0 |  |  | 6.0 |  |  | 6.0 |  |
| Vehicle Extension (s) |  | 5.0 |  |  | 5.0 |  |  | 5.0 |  |  | 5.0 |  |
| Lane Grp Cap (vph) |  | 651 |  |  | 505 |  |  | 807 |  |  | 814 |  |
| v/s Ratio Prot |  |  |  |  |  |  |  |  |  |  |  |  |
| v/s Ratio Perm |  | 0.15 |  |  | c0.26 |  |  | c0.43 |  |  | 0.24 |  |
| v/c Ratio |  | 0.40 |  |  | 0.68 |  |  | 0.87 |  |  | 0.49 |  |
| Uniform Delay, d1 |  | 20.5 |  |  | 23.4 |  |  | 20.6 |  |  | 15.6 |  |
| Progression Factor |  | 1.00 |  |  | 1.00 |  |  | 1.00 |  |  | 1.00 |  |
| Incremental Delay, d2 |  | 1.9 |  |  | 7.3 |  |  | 11.2 |  |  | 1.0 |  |
| Delay (s) |  | 22.4 |  |  | 30.7 |  |  | 31.8 |  |  | 16.5 |  |
| Level of Service |  | C |  |  | C |  |  | C |  |  | B |  |
| Approach Delay (s) |  | 22.4 |  |  | 30.7 |  |  | 31.8 |  |  | 16.5 |  |
| Approach LOS |  | C |  |  | C |  |  | C |  |  | B |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 26.6 |  | HCM 2000 | Level of S | ervice |  | C |  |  |  |
| HCM 2000 Volume to Capacity ratio |  |  | 0.79 |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length (s) |  |  | 90.0 |  | Sum of lost | time (s) |  |  | 12.0 |  |  |  |
| Intersection Capacity Utilization |  |  | 96.3\% |  | CU Level | f Service |  |  | F |  |  |  |
|  |  |  | 15 |  |  |  |  |  |  |  |  |  |
| Analysis Period (min) <br> c Critical Lane Group |  |  |  |  |  |  |  |  |  |  |  |  |

Uppers Quarry Traffic Impact Study
Synchro 10 Report

<2035 Total - Thorold Townline> AM Peak Hour
1: Davis Road \& Thorold Stone Road

| Lane Group | EBL | EBT | EBR | WBL | WBT | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \% | 个 $\uparrow$ | F | \% | $\uparrow \uparrow$ | 7 | $\uparrow$ | F | 7 | $\uparrow$ | F |
| Traffic Volume (vph) | 21 | 1010 | 336 | 114 | 1122 | 649 | 15 | 257 | 1 | 2 | 18 |
| Future Volume (vph) | 21 | 1010 | 336 | 114 | 1122 | 649 | 15 | 257 | 1 | 2 | 18 |
| Turn Type | Perm | NA | Perm | Perm | NA | Split | NA | Perm | Split | NA | Perm |
| Protected Phases |  | 2 |  |  | 6 | 4 | 4 |  | 8 | 8 |  |
| Permitted Phases | 2 |  | 2 | 6 |  |  |  | 4 |  |  | 8 |
| Detector Phase | 2 | 2 | 2 | 6 | 6 | 4 | 4 | 4 | 8 | 8 | 8 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 20.0 | 20.0 | 20.0 | 20.0 | 20.0 | 10.0 | 10.0 | 10.0 | 10.0 | 10.0 | 10.0 |
| Minimum Split (s) | 28.9 | 28.9 | 28.9 | 28.9 | 28.9 | 29.7 | 29.7 | 29.7 | 21.7 | 21.7 | 21.7 |
| Total Split (s) | 58.0 | 58.0 | 58.0 | 58.0 | 58.0 | 40.0 | 40.0 | 40.0 | 22.0 | 22.0 | 22.0 |
| Total Split (\%) | 48.3\% | 48.3\% | 48.3\% | 48.3\% | 48.3\% | 33.3\% | 33.3\% | 33.3\% | 18.3\% | 18.3\% | 18.3\% |
| Yellow Time (s) | 5.4 | 5.4 | 5.4 | 5.4 | 5.4 | 5.7 | 5.7 | 5.7 | 5.7 | 5.7 | 5.7 |
| All-Red Time (s) | 1.5 | 1.5 | 1.5 | 1.5 | 1.5 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 6.9 | 6.9 | 6.9 | 6.9 | 6.9 | 7.7 | 7.7 | 7.7 | 7.7 | 7.7 | 7.7 |
| Lead/Lag |  |  |  |  |  |  |  |  |  |  |  |
| Lead-Lag Optimize? |  |  |  |  |  |  |  |  |  |  |  |
| Recall Mode | C-Max | C-Max | C-Max | Max | Max | None | None | None | None | None | None |
| Act Effct Green (s) | 67.6 | 67.6 | 67.6 | 67.6 | 67.6 | 30.7 | 30.7 | 30.7 | 10.0 | 10.0 | 10.0 |
| Actuated g/C Ratio | 0.56 | 0.56 | 0.56 | 0.56 | 0.56 | 0.26 | 0.26 | 0.26 | 0.08 | 0.08 | 0.08 |
| v/c Ratio | 0.15 | 0.55 | 0.38 | 0.68 | 0.63 | 0.86 | 0.87 | 0.47 | 0.01 | 0.01 | 0.09 |
| Control Delay | 20.4 | 20.0 | 7.1 | 47.1 | 27.7 | 64.3 | 65.3 | 7.0 | 51.0 | 51.0 | 0.9 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 20.4 | 20.0 | 7.1 | 47.1 | 27.7 | 64.3 | 65.3 | 7.0 | 51.0 | 51.0 | 0.9 |
| LOS | C | B | A | D | C | E | E | A | D | D | A |
| Approach Delay |  | 16.8 |  |  | 29.4 |  | 48.7 |  |  | 7.7 |  |
| Approach LOS |  | B |  |  | C |  | D |  |  | A |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 120 |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 120 |  |  |  |  |  |  |  |  |  |  |  |
| Offset: 0 (0\%), Referenced to phase 2:EBTL, Start of Green |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 115 |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Coordinated |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.87 |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 29.4 |  |  |  |  | ntersectio | LOS: C |  |  |  |  |  |
| Intersection Capacity Utilization 90.8\% |  |  |  | ICU Level of Service E |  |  |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |  |



[^43]Synchro 10 Report

HCM Signalized Intersection Capacity Analysis<2035 Total - Thorold Townline> AM Peak Hour 1: Davis Road \& Thorold Stone Road

|  | 4 | $\rightarrow$ |  | $t$ |  |  | 4 | $\uparrow$ | 1 | $\checkmark$ | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \% | ¢ $\uparrow$ | F | ${ }^{7}$ | 个t |  | \% | $\uparrow$ | F | ${ }^{7}$ | $\uparrow$ | F |
| Traffic Volume (vph) | 21 | 1010 | 336 | 114 | 1122 | 6 | 649 | 15 | 257 | 1 | 2 | 18 |
| Future Volume (vph) | 21 | 1010 | 336 | 114 | 1122 | 6 | 649 | 15 | 257 | 1 | 2 | 18 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 6.9 | 6.9 | 6.9 | 6.9 | 6.9 |  | 7.7 | 7.7 | 7.7 | 7.7 | 7.7 | 7.7 |
| Lane Util. Factor | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 |  | 0.95 | 0.95 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 | 0.99 | 1.00 | 1.00 | 0.99 |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 |  | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |  | 0.95 | 0.95 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1641 | 3374 | 1442 | 1530 | 3336 |  | 1559 | 1554 | 1475 | 1388 | 1624 | 1337 |
| Flt Permitted | 0.15 | 1.00 | 1.00 | 0.19 | 1.00 |  | 0.95 | 0.95 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (perm) | 264 | 3374 | 1442 | 310 | 3336 |  | 1559 | 1554 | 1475 | 1388 | 1624 | 1337 |
| Peak-hour factor, PHF | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 |
| Adj. Flow (vph) | 22 | 1052 | 350 | 119 | 1169 | 6 | 676 | 16 | 268 | 1 | 2 | 19 |
| RTOR Reduction (vph) | 0 | 0 | 114 | 0 | 0 | 0 | , | 0 | 199 | 0 | 0 | 18 |
| Lane Group Flow (vph) | 22 | 1052 | 236 | 119 | 1175 | 0 | 345 | 347 | 69 | 1 | 2 | 1 |
| Confl. Peds. (\#/hr) | 1 |  |  |  |  | 1 | 1 |  | 1 | 1 |  | 1 |
| Heavy Vehicles (\%) | 10\% | 7\% | 12\% | 18\% | 8\% | 30\% | 10\% | 28\% | 8\% | 30\% | 17\% | 19\% |
| Turn Type | Perm | NA | Perm | Perm | NA |  | Split | NA | Perm | Split | NA | Perm |
| Protected Phases |  | 2 |  |  | 6 |  | 4 | 4 |  | 8 | 8 |  |
| Permitted Phases | 2 |  | 2 | 6 |  |  |  |  | 4 |  |  | 8 |
| Actuated Green, G (s) | 63.0 | 63.0 | 63.0 | 63.0 | 63.0 |  | 30.7 | 30.7 | 30.7 | 4.0 | 4.0 | 4.0 |
| Effective Green, g (s) | 63.0 | 63.0 | 63.0 | 63.0 | 63.0 |  | 30.7 | 30.7 | 30.7 | 4.0 | 4.0 | 4.0 |
| Actuated g/C Ratio | 0.52 | 0.52 | 0.52 | 0.52 | 0.52 |  | 0.26 | 0.26 | 0.26 | 0.03 | 0.03 | 0.03 |
| Clearance Time (s) | 6.9 | 6.9 | 6.9 | 6.9 | 6.9 |  | 7.7 | 7.7 | 7.7 | 7.7 | 7.7 | 7.7 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 |
| Lane Grp Cap (vph) | 138 | 1771 | 757 | 162 | 1751 |  | 398 | 397 | 377 | 46 | 54 | 44 |
| v/s Ratio Prot |  | 0.31 |  |  | 0.35 |  | 0.22 | c0.22 |  | 0.00 | c0.00 |  |
| $\mathrm{v} / \mathrm{s}$ Ratio Perm | 0.08 |  | 0.16 | c0.38 |  |  |  |  | 0.05 |  |  | 0.00 |
| v/c Ratio | 0.16 | 0.59 | 0.31 | 0.73 | 0.67 |  | 0.87 | 0.87 | 0.18 | 0.02 | 0.04 | 0.01 |
| Uniform Delay, d1 | 14.8 | 19.7 | 16.2 | 22.0 | 20.9 |  | 42.7 | 42.8 | 34.9 | 56.1 | 56.1 | 56.1 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.44 | 1.34 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 2.5 | 1.5 | 1.1 | 14.9 | 1.1 |  | 18.7 | 19.7 | 0.4 | 0.3 | 0.5 | 0.2 |
| Delay (s) | 17.2 | 21.1 | 17.3 | 46.6 | 29.1 |  | 61.4 | 62.5 | 35.3 | 56.4 | 56.6 | 56.3 |
| Level of Service | , | C | B | D | C |  | E | E | D | E | E | E |
| Approach Delay (s) |  | 20.1 |  |  | 30.7 |  |  | 54.5 |  |  | 56.4 |  |
| Approach LOS |  | C |  |  | C |  |  | D |  |  | E |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 2000 Control Delay |  |  | 33.0 |  | HCM 2000 | Level of S | ervice |  | C |  |  |  |
| HCM 2000 Volume to Capacity ratio |  |  | 0.75 |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length (s) |  |  | 120.0 |  | Sum of los | time (s) |  |  | 22.3 |  |  |  |
| Intersection Capacity Utilization |  |  | 90.8\% |  | CU Level | of Service |  |  | E |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |
| c Critical Lane Group |  |  |  |  |  |  |  |  |  |  |  |  |

Timings 2: Davis Road \& Niagara Falls Road/Beaverdams Road



[^44]Synchro 10 Report

HCM Signalized Intersection Capacity Analysis<2035 Total - Thorold Townline> AM Peak Hour 2: Davis Road \& Niagara Falls Road/Beaverdams Road


[^45]| Lane Group | EBL | EBT | WBL | WBT | WBR | NBL | NBT | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \% | f | \% | $\uparrow$ | F' | ${ }^{7}$ | $\uparrow$ | \% | $\uparrow$ | 「 |
| Traffic Volume (vph) | 153 | 635 | 45 | 502 | 132 | 22 | 139 | 136 | 94 | 159 |
| Future Volume (vph) | 153 | 635 | 45 | 502 | 132 | 22 | 139 | 136 | 94 | 159 |
| Turn Type | Perm | NA | Perm | NA | Perm | Perm | NA | Perm | NA | Perm |
| Protected Phases |  | 2 |  | 6 |  |  | 4 |  | 8 |  |
| Permitted Phases | 2 |  | 6 |  | 6 | 4 |  | 8 |  | 8 |
| Detector Phase | 2 | 2 | 6 | 6 | 6 | 4 | 4 | 8 | 8 | 8 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 22.0 | 22.0 | 22.0 | 22.0 | 22.0 | 15.0 | 15.0 | 15.0 | 15.0 | 15.0 |
| Minimum Split (s) | 36.0 | 36.0 | 36.0 | 36.0 | 36.0 | 32.0 | 32.0 | 32.0 | 32.0 | 32.0 |
| Total Split (s) | 58.0 | 58.0 | 58.0 | 58.0 | 58.0 | 32.0 | 32.0 | 32.0 | 32.0 | 32.0 |
| Total Split (\%) | 64.4\% | 64.4\% | 64.4\% | 64.4\% | 64.4\% | 35.6\% | 35.6\% | 35.6\% | 35.6\% | 35.6\% |
| Yellow Time (s) | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| All-Red Time (s) | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |
| Lead/Lag |  |  |  |  |  |  |  |  |  |  |
| Lead-Lag Optimize? |  |  |  |  |  |  |  |  |  |  |
| Recall Mode | C-Max | C-Max | Max | Max | Max | None | None | None | None | None |
| Act Efft Green (s) | 57.5 | 57.5 | 57.5 | 57.5 | 57.5 | 18.5 | 18.5 | 18.5 | 18.5 | 18.5 |
| Actuated g/C Ratio | 0.64 | 0.64 | 0.64 | 0.64 | 0.64 | 0.21 | 0.21 | 0.21 | 0.21 | 0.21 |
| v/c Ratio | 0.36 | 0.60 | 0.16 | 0.48 | 0.14 | 0.11 | 0.56 | 0.72 | 0.32 | 0.40 |
| Control Delay | 11.5 | 13.0 | 9.5 | 11.1 | 1.9 | 28.0 | 36.1 | 52.5 | 32.0 | 7.5 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 11.5 | 13.0 | 9.5 | 11.1 | 1.9 | 28.0 | 36.1 | 52.5 | 32.0 | 7.5 |
| LOS | B | B | A | B | A | C | D | D | C | A |
| Approach Delay |  | 12.7 |  | 9.2 |  |  | 35.2 |  | 29.2 |  |
| Approach LOS |  | B |  | A |  |  | D |  | C |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 90 |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 90 |  |  |  |  |  |  |  |  |  |  |
| Offset: $0(0 \%)$, Referenced to phase 2:EBTL, Start of Green |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 70 |  |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Coordinated |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.72 |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 16.7 |  |  |  |  | Intersection LOS: B |  |  |  |  |  |
| Intersection Capacity Utilization 101.2\% |  |  |  |  | ICU Level of Service G |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |



[^46]Synchro 10 Report

HCM Signalized Intersection Capacity Analysis<2035 Total - Thorold Townline> AM Peak Hour 3: Davis Road \& Lundys Lane

|  | $\stackrel{ }{ }$ |  |  | $\checkmark$ |  |  | 4 | $\dagger$ | $p$ |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | F |  | ${ }^{7}$ | $\uparrow$ | F | 7 | F |  | 7 | $\uparrow$ | 「 |
| Traffic Volume (vph) | 153 | 635 | 18 | 45 | 502 | 132 | 22 | 139 | 30 | 136 | 94 | 159 |
| Future Volume (vph) | 153 | 635 | 18 | 45 | 502 | 132 | 22 | 139 | 30 | 136 | 94 | 159 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 7.0 | 7.0 |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  | 7.0 | 7.0 | 7.0 |
| Lane Util. Factor | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 |
| Frpb, ped/bikes | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 |
| Flpb, ped/bikes | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 |
| Frt | 1.00 | 1.00 |  | 1.00 | 1.00 | 0.85 | 1.00 | 0.97 |  | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 |  | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |  | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1656 | 1828 |  | 1467 | 1743 | 1442 | 1444 | 1519 |  | 1530 | 1532 | 1392 |
| Flt Permitted | 0.41 | 1.00 |  | 0.31 | 1.00 | 1.00 | 0.69 | 1.00 |  | 0.61 | 1.00 | 1.00 |
| Satd. Flow (perm) | 716 | 1828 |  | 474 | 1743 | 1442 | 1052 | 1519 |  | 984 | 1532 | 1392 |
| Peak-hour factor, PHF | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 |
| Adj. Flow (vph) | 163 | 676 | 19 | 48 | 534 | 140 | 23 | 148 | 32 | 145 | 100 | 169 |
| RTOR Reduction (vph) | 0 | 1 | 0 | 0 | 0 | 51 | 0 | 10 | 0 | 0 | 0 | 134 |
| Lane Group Flow (vph) | 163 | 694 | 0 | 48 | 534 | 89 | 23 | 170 | 0 | 145 | 100 | 35 |
| Confl. Peds. (\#\#hr) |  |  | 1 | 1 |  |  |  |  |  |  |  |  |
| Heavy Vehicles (\%) | 9\% | 3\% | 19\% | 23\% | 9\% | 12\% | 25\% | 20\% | 30\% | 18\% | 24\% | 16\% |
| Turn Type | Perm | NA |  | Perm | NA | Perm | Perm | NA |  | Perm | NA | Perm |
| Protected Phases |  | 2 |  |  | 6 |  |  | 4 |  |  | 8 |  |
| Permitted Phases | 2 |  |  | 6 |  | 6 | 4 |  |  | 8 |  | 8 |
| Actuated Green, G (s) | 57.5 | 57.5 |  | 57.5 | 57.5 | 57.5 | 18.5 | 18.5 |  | 18.5 | 18.5 | 18.5 |
| Effective Green, g (s) | 57.5 | 57.5 |  | 57.5 | 57.5 | 57.5 | 18.5 | 18.5 |  | 18.5 | 18.5 | 18.5 |
| Actuated g/C Ratio | 0.64 | 0.64 |  | 0.64 | 0.64 | 0.64 | 0.21 | 0.21 |  | 0.21 | 0.21 | 0.21 |
| Clearance Time (s) | 7.0 | 7.0 |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  | 7.0 | 7.0 | 7.0 |
| Vehicle Extension (s) | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 | 2.0 | 2.0 |  | 2.0 | 2.0 | 2.0 |
| Lane Grp Cap (vph) | 457 | 1167 |  | 302 | 1113 | 921 | 216 | 312 |  | 202 | 314 | 286 |
| v/s Ratio Prot |  | c0.38 |  |  | 0.31 |  |  | 0.11 |  |  | 0.07 |  |
| $\mathrm{v} / \mathrm{s}$ Ratio Perm | 0.23 |  |  | 0.10 |  | 0.06 | 0.02 |  |  | c0.15 |  | 0.02 |
| v/c Ratio | 0.36 | 0.59 |  | 0.16 | 0.48 | 0.10 | 0.11 | 0.55 |  | 0.72 | 0.32 | 0.12 |
| Uniform Delay, d1 | 7.6 | 9.5 |  | 6.5 | 8.5 | 6.3 | 29.0 | 32.0 |  | 33.3 | 30.4 | 29.1 |
| Progression Factor | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 2.2 | 2.2 |  | 1.1 | 1.5 | 0.2 | 0.1 | 1.1 |  | 9.7 | 0.2 | 0.1 |
| Delay (s) | 9.8 | 11.7 |  | 7.7 | 9.9 | 6.5 | 29.1 | 33.0 |  | 43.0 | 30.6 | 29.2 |
| Level of Service | A | B |  | A | A | A | c | C |  | D | C |  |
| Approach Delay (s) |  | 11.3 |  |  | 9.1 |  |  | 32.6 |  |  | 34.4 |  |
| Approach LOS |  | B |  |  | A |  |  | C |  |  | C |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 2000 Control Delay |  |  | 16.9 |  | HCM 2000 | Level of S | ervice |  | B |  |  |  |
| HCM 2000 Volume to Capacity ratio |  |  | 0.62 |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length (s) |  |  | 90.0 |  | Sum of los | time (s) |  |  | 14.0 |  |  |  |
| Intersection Capacity Utilization |  |  | 101.2\% |  | CU Level | Service |  |  | G |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |
| c Critical Lane Group |  |  |  |  |  |  |  |  |  |  |  |  |

Timings
<2035 Total - Thorold Townline> AM Peak Hour 4: Thorold Townline Road \& Thorold Stone Road 09-23-2021

| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | SBL | SBT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \% | 个 $\uparrow$ | 7 | * | ¢ $\uparrow$ | 「 | \% | $\hat{F}$ | * | $\hat{F}$ |
| Traffic Volume (vph) | 323 | 767 | 178 | 217 | 854 | 73 | 133 | 180 | 52 | 222 |
| Future Volume (vph) | 323 | 767 | 178 | 217 | 854 | 73 | 133 | 180 | 52 | 222 |
| Turn Type | pm+pt | NA | Perm | pm+pt | NA | Perm | $\mathrm{pm}+\mathrm{pt}$ | NA | Perm | NA |
| Protected Phases | 5 | 2 |  | 1 | 6 |  | 7 | 4 |  | 8 |
| Permitted Phases | 2 |  | 2 | 6 |  | 6 | 4 |  | 8 |  |
| Detector Phase | 5 | 2 | 2 | 1 | 6 | 6 | 7 | 4 | 8 | 8 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 8.0 | 10.0 | 10.0 | 8.0 | 10.0 | 10.0 | 8.0 | 10.0 | 10.0 | 10.0 |
| Minimum Split (s) | 11.0 | 35.1 | 35.1 | 12.5 | 35.1 | 35.1 | 11.0 | 41.4 | 41.4 | 41.4 |
| Total Split (s) | 28.5 | 44.5 | 44.5 | 20.0 | 36.0 | 36.0 | 11.0 | 55.5 | 44.5 | 44.5 |
| Total Split (\%) | 23.8\% | 37.1\% | 37.1\% | 16.7\% | 30.0\% | 30.0\% | 9.2\% | 46.3\% | 37.1\% | 37.1\% |
| Yellow Time (s) | 3.0 | 4.1 | 4.1 | 3.0 | 4.1 | 4.1 | 3.0 | 4.1 | 4.1 | 4.1 |
| All-Red Time (s) | 0.0 | 2.0 | 2.0 | 0.0 | 2.0 | 2.0 | 0.0 | 2.3 | 2.3 | 2.3 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 3.0 | 6.1 | 6.1 | 3.0 | 6.1 | 6.1 | 3.0 | 6.4 | 6.4 | 6.4 |
| Lead/Lag | Lead | Lag | Lag | Lead | Lag | Lag | Lead |  | Lag | Lag |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes | Yes | Yes |  | Yes | Yes |
| Recall Mode | None | C-Max | C-Max | None | C-Max | C-Max | None | None | None | None |
| Act Efft Green (s) | 63.6 | 42.3 | 42.3 | 53.9 | 35.6 | 35.6 | 50.4 | 47.0 | 36.0 | 36.0 |
| Actuated g/C Ratio | 0.53 | 0.35 | 0.35 | 0.45 | 0.30 | 0.30 | 0.42 | 0.39 | 0.30 | 0.30 |
| $\mathrm{v} / \mathrm{C}$ Ratio | 0.93 | 0.65 | 0.34 | 0.77 | 0.86 | 0.15 | 0.75 | 0.51 | 0.18 | 0.95 |
| Control Delay | 73.6 | 49.4 | 25.7 | 38.2 | 50.7 | 2.8 | 49.0 | 28.1 | 31.8 | 67.7 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 73.6 | 49.4 | 25.7 | 38.2 | 50.7 | 2.8 | 49.0 | 28.1 | 31.8 | 67.7 |
| LOS | E | D | C | D | D | A | D | C | C | E |
| Approach Delay |  | 52.2 |  |  | 45.3 |  |  | 34.9 |  | 63.8 |
| Approach LOS |  | D |  |  | D |  |  | C |  | E |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 120 |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 120 |  |  |  |  |  |  |  |  |  |  |
| Offset: $0(0 \%)$, Referenced to phase 2:EBTL and 6 :WBTL, Start of Green |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 100 |  |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Coordinated |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.95 |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 49.3 |  |  |  | Intersection LOS: D |  |  |  |  |  |  |
| Intersection Capacity Utilization 90.7\% |  |  |  | ICU Level of Service E |  |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |



[^47]Synchro 10 Report

4: Thorold Townline Road \& Thorold Stone Road

| 4: Thorold Townline Road | \& Thorold Stone Road |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |

Uppers Quarry Traffic Impact Study
Synchro 10 Report

Timings
<2035 Total - Thorold Townline> AM Peak Hour
5: Thorold Townline Road \& Lundys Lane
$\square$


$\begin{array}{lrrrrrrrrrr}\text { Future Volume (vph) } & 205 & 607 & 107 & 38 & 422 & 77 & 140 & 45 & 85 & 84 \\ \text { Turn Type } & \text { Perm } & \text { NA } & \text { Perm } & \text { Perm } & \text { NA } & \text { Perm } & \text { NA } & \text { Perm } & \text { NA } & \text { Perm }\end{array}$
Protected Phase
Permitted Phase
Switch Phase
$\begin{array}{lllllllllll}\text { Minimum Initial (s) } & 20.0 & 20.0 & 20.0 & 20.0 & 20.0 & 100 & 100 & 10.0 & 10.0 & 10.0\end{array}$

| Minimum Initial (s) | 20.0 | 20.0 | 20.0 | 20.0 | 20.0 | 10.0 | 10.0 | 10.0 | 10.0 | 10.0 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Minimum Split (s) | 29.0 | 29.0 | 29.0 | 29.0 | 29.0 | 35.0 | 35.0 | 35.0 | 35.0 | 35.0 |
| Total Split (s) | 65.0 | 65.0 | 65.0 | 65.0 | 65.0 | 35.0 | 35.0 | 35.0 | 35.0 | 35.0 |

$\begin{array}{lrrrrrrrrrr}\text { Yellow Time (s) } & 5.0 & 5.0 & 5.0 & 5.0 & 5.0 & 4.0 & 4.0 & 4.0 & 4.0 & 4.0\end{array}$

| All-Red Time (s) | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |

$\begin{array}{lllllllllll}\text { Ost Time Adjust (s) } & 0.0 & 0.0 & 0.0 & 0.0 & 0.0 & 0.0 & 0.0 & 0.0 & 0.0 & 0.0 \\ \text { Total Lost Time (s) } & 7.0 & 7.0 & 7.0 & 7.0 & 7.0 & 6.0 & 6.0 & 6.0 & 6.0 & 6.0\end{array}$
Lead/La

| Lead-Lag Optimize? |  |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| R-Max | C-Max | C-Max | Max | Max | None | None | None | None | None |  |
| Recall Mode | 68.8 | 68.8 | 68.8 | 68.8 | 68.8 | 18.2 | 18.2 | 18.2 | 18.2 | 18.2 |
| Act Efct Green (s) | 0.69 | 0.69 | 0.69 | 0.69 | 0.69 | 0.18 | 0.18 | 0.18 | 0.18 | 0.18 |
| Actuated g/C Ratio | 0.46 | 0.52 | 0.11 | 0.09 | 0.44 | 0.39 | 0.63 | 0.30 | 0.31 | 0.30 |
| v/c Ratio | 12.1 | 10.4 | 4.0 | 7.1 | 8.9 | 39.8 | 43.8 | 38.3 | 36.6 | 9.6 |
| Control Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Queue Delay | 12.1 | 10.4 | 4.0 | 7.1 | 8.9 | 39.8 | 43.8 | 38.3 | 36.6 | 9.6 |
| Total Delay | B | B | A | A | A | D | D | D | D | A |
| LOS |  |  |  |  |  |  |  |  |  |  |

$\qquad$
Approach Delay
Approach LOS
Intersection Summary
Cycle Length: 100
Offset: 0 ( $0 \%$ ), Referenced to phase 2:EBTL, Start of Green
Natural Cycle: 80
$\begin{array}{ll}\text { Natural Cycle: } & \\ \text { Control Type: Actuated-Coordinated } & \\ \text { Maximum v/c Ratio: 0.63 } & \\ \begin{array}{ll}\text { Intersection Signal Delay: } 15.8 & \text { Intersection LOS: B } \\ \text { Intersection Capacity Utilization } 88.2 \% & \text { ICU Level of Service E }\end{array}\end{array}$
Analysis Period (min) 15


[^48]Synchro 10 Report

HCM Signalized Intersection Capacity Analysis<2035 Total - Thorold Townline> AM Peak Hour 5: Thorold Townline Road \& Lundys Lane


Timings
<2035 Total - Thorold Townline> AM Peak Hour 6: Thorold Townline Road \& Beaverdams Road 09-23-2021



[^49]Synchro 10 Report

HCM Signalized Intersection Capacity Analysis<2035 Total - Thorold Townline> AM Peak Hour 6: Thorold Townline Road \& Beaverdams Road 09-23-2021


HCM Unsignalized Intersection Capacity Analysi8035 Total - Thorold Townline> AM Peak Hour 7: Thorold Townline Road \& Uppers Lane 09-23-2021

<2035 Total - Thorold Townline> PM Peak Hour 1: Davis Road \& Thorold Stone Road


## Intersection Summar

Cycle Length: 120
ength: 120
Offset: 0 (0\%), Referenced to phase 2:EBTL and 6:WBTL, Start of Green
Natural Cycle: 115
Control Type: Actuated-Coordinated
$\begin{array}{ll}\text { Control Tyype: Actuated-Coordinated } & \\ \text { Maximum vcc Ratio: 0.04 } & \\ \text { Intersection Signal Delay: 39.3 } & \text { Intersection LOS: D } \\ \text { Intersection Capacity Utilization 93.1\% } & \text { ICU Level of Service F }\end{array}$
Analysis Period (min) 15


[^50]Synchro 10 Report

HCM Signalized Intersection Capacity Analysis<2035 Total - Thorold Townline> PM Peak Hour 1: Davis Road \& Thorold Stone Road

|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |

Timings 2: Davis Road \& Niagara Falls Road/Beaverdams Road

|  | $\rangle$ |  |  |  | 4 | 4 |  |  | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | WBL | WBT | NBL | NBT | SBL | SBT | SBR |
| Lane Configurations |  | $\dagger$ |  | ${ }_{\$}$ | ${ }^{*}$ | $\uparrow{ }^{\text {¢ }}$ | ${ }^{7}$ | 个 $\uparrow$ | F |
| Traffic Volume (vph) | 90 | 32 | 60 | 44 | 26 | 582 | 170 | 691 | 105 |
| Future Volume (vph) | 90 | 32 | 60 | 44 | 26 | 582 | 170 | 691 | 105 |
| Turn Type | Perm | NA | Perm | NA | Perm | NA | Perm | NA | Perm |
| Protected Phases |  | 2 |  | 6 |  | 4 |  | 8 |  |
| Permitted Phases | 2 |  | 6 |  | 4 |  | 8 |  | 8 |
| Detector Phase | 2 | 2 | 6 | 6 | 4 | 4 | 8 | 8 | 8 |
| Switch Phase |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 10.0 | 10.0 | 10.0 | 10.0 | 25.0 | 25.0 | 25.0 | 25.0 | 25.0 |
| Minimum Split (s) | 38.1 | 38.1 | 38.1 | 38.1 | 32.0 | 32.0 | 32.0 | 32.0 | 32.0 |
| Total Split (s) | 40.0 | 40.0 | 40.0 | 40.0 | 60.0 | 60.0 | 60.0 | 60.0 | 60.0 |
| Total Split (\%) | 40.0\% | 40.0\% | 40.0\% | 40.0\% | 60.0\% | 60.0\% | 60.0\% | 60.0\% | 60.0\% |
| Yellow Time (s) | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| All-Red Time (s) | 3.1 | 3.1 | 3.1 | 3.1 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |
| Lost Time Adjust (s) |  | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) |  | 8.1 |  | 8.1 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |
| Lead/Lag |  |  |  |  |  |  |  |  |  |
| Lead-Lag Optimize? |  |  |  |  |  |  |  |  |  |
| Recall Mode | C-Max | C-Max | Max | Max | None | None | None | None | None |
| Act Effict Green (s) |  | 46.8 |  | 46.8 | 38.1 | 38.1 | 38.1 | 38.1 | 38.1 |
| Actuated g/C Ratio |  | 0.47 |  | 0.47 | 0.38 | 0.38 | 0.38 | 0.38 | 0.38 |
| $\mathrm{v} / \mathrm{C}$ Ratio |  | 0.28 |  | 0.35 | 0.13 | 0.52 | 0.79 | 0.57 | 0.17 |
| Control Delay |  | 20.0 |  | 16.1 | 17.5 | 23.9 | 49.3 | 25.4 | 3.2 |
| Queue Delay |  | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay |  | 20.0 |  | 16.1 | 17.5 | 23.9 | 49.3 | 25.4 | 3.2 |
| LOS |  | B |  | B | B | C | D | C | A |
| Approach Delay |  | 20.0 |  | 16.1 |  | 23.7 |  | 27.2 |  |
| Approach LOS |  | B |  | B |  | C |  | C |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |
| Cycle Length: 100 |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 100 |  |  |  |  |  |  |  |  |  |
| Offset: 0 (0\%), Referenced to phase 2:EBTL, Start of Green |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 75 |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Coordinated |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.79 |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 24.1 |  |  |  |  | tersection | LOS: C |  |  |  |
| Intersection Capacity Utilization 78.5\% |  |  |  | ICU Level of Service D |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |



[^51]Synchro 10 Report

HCM Signalized Intersection Capacity Analysis<2035 Total - Thorold Townline> PM Peak Hour 2: Davis Road \& Niagara Falls Road/Beaverdams Road


[^52]Synchro 10 Report 3: Davis Road \& Lundys Lane 09-23-2021

| Lane Group | EBL | EBT | WBL | WBT | WBR | NBL | NBT | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \% | $\hat{\dagger}$ | \% | $\uparrow$ | 7 | 7 | F | ${ }^{7}$ | $\uparrow$ | F |
| Traffic Volume (vph) | 208 | 719 | 42 | 720 | 216 | 46 | 141 | 239 | 125 | 184 |
| Future Volume (vph) | 208 | 719 | 42 | 720 | 216 | 46 | 141 | 239 | 125 | 184 |
| Turn Type | pm+pt | NA | Perm | NA | Perm | Perm | NA | pm+pt | NA | Perm |
| Protected Phases | 5 | 2 |  | 6 |  |  | 4 | 3 | 8 |  |
| Permitted Phases | 2 |  | 6 |  | 6 | 4 |  | 8 |  | 8 |
| Detector Phase | 5 | 2 | 6 | 6 | 6 | 4 | 4 | 3 | 8 | 8 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 22.0 | 22.0 | 22.0 | 22.0 | 15.0 | 15.0 | 5.0 | 15.0 | 15.0 |
| Minimum Split (s) | 8.0 | 36.0 | 36.0 | 36.0 | 36.0 | 32.0 | 32.0 | 8.0 | 32.0 | 32.0 |
| Total Split (s) | 14.0 | 78.0 | 64.0 | 64.0 | 64.0 | 32.0 | 32.0 | 10.0 | 42.0 | 42.0 |
| Total Split (\%) | 11.7\% | 65.0\% | 53.3\% | 53.3\% | 53.3\% | 26.7\% | 26.7\% | 8.3\% | 35.0\% | 35.0\% |
| Yellow Time (s) | 3.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 3.0 | 5.0 | 5.0 |
| All-Red Time (s) | 0.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 0.0 | 2.0 | 2.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 3.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 3.0 | 7.0 | 7.0 |
| Lead/Lag | Lead |  | Lag | Lag | Lag | Lag | Lag | Lead |  |  |
| Lead-Lag Optimize? | Yes |  | Yes | Yes | Yes | Yes | Yes | Yes |  |  |
| Recall Mode | None | C-Max | Max | Max | Max | Max | Max | None | Max | Max |
| Act Effct Green (s) | 75.0 | 71.0 | 57.0 | 57.0 | 57.0 | 25.0 | 25.0 | 39.0 | 35.0 | 35.0 |
| Actuated g/C Ratio | 0.62 | 0.59 | 0.48 | 0.48 | 0.48 | 0.21 | 0.21 | 0.32 | 0.29 | 0.29 |
| V/c Ratio | 0.88 | 0.75 | 0.23 | 0.88 | 0.29 | 0.19 | 0.58 | 0.83 | 0.26 | 0.33 |
| Control Delay | 52.6 | 23.3 | 23.4 | 43.3 | 8.7 | 41.6 | 47.3 | 58.5 | 34.4 | 6.0 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 52.6 | 23.3 | 23.4 | 43.3 | 8.7 | 41.6 | 47.3 | 58.5 | 34.4 | 6.0 |
| LOS | D | C | C | D | A | D | D | E | C | A |
| Approach Delay |  | 29.7 |  | 34.8 |  |  | 46.2 |  | 35.3 |  |
| Approach LOS |  | C |  | C |  |  | D |  | D |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 120 |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 120 |  |  |  |  |  |  |  |  |  |  |
| Offset: $0(0 \%)$, Referenced to phase 2:EBTL, Start of Green |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 95 |  |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Coordinated |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.88 |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 34.1 |  |  |  |  | Intersection LOS: C |  |  |  |  |  |
| Intersection Capacity Utilization 112.8\% Analysis Period (min) 15 |  |  |  |  | ICU Level of Service H |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |



[^53]Synchro 10 Report

HCM Signalized Intersection Capacity Analysis<2035 Total - Thorold Townline> PM Peak Hour 3: Davis Road \& Lundys Lane

|  | $y$ |  |  | $\checkmark$ |  |  | 4 | $\dagger$ | P |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | $\hat{\square}$ |  | ${ }^{7}$ | $\uparrow$ | F' | \% | F |  | 7 | $\uparrow$ | r |
| Traffic Volume (vph) | 208 | 719 | 28 | 42 | 720 | 216 | 46 | 141 | 51 | 239 | 125 | 184 |
| Future Volume (vph) | 208 | 719 | 28 | 42 | 720 | 216 | 46 | 141 | 51 | 239 | 125 | 184 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 3.0 | 7.0 |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  | 3.0 | 7.0 | 7.0 |
| Lane Util. Factor | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 |
| Frpb, ped/bikes | 1.00 | 1.00 |  | 1.00 | 1.00 | 0.98 | 1.00 | 0.99 |  | 1.00 | 1.00 | 1.00 |
| Flpb, ped/bikes | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 |
| Frt | 1.00 | 0.99 |  | 1.00 | 1.00 | 0.85 | 1.00 | 0.96 |  | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 |  | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |  | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1719 | 1818 |  | 1611 | 1863 | 1473 | 1736 | 1652 |  | 1702 | 1743 | 1553 |
| Flt Permitted | 0.10 | 1.00 |  | 0.24 | 1.00 | 1.00 | 0.67 | 1.00 |  | 0.44 | 1.00 | 1.00 |
| Satd. Flow (perm) | 185 | 1818 |  | 415 | 1863 | 1473 | 1226 | 1652 |  | 790 | 1743 | 1553 |
| Peak-hour factor, PHF | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 |
| Adj. Flow (vph) | 224 | 773 | 30 | 45 | 774 | 232 | 49 | 152 | 55 | 257 | 134 | 198 |
| RTOR Reduction (vph) | 0 | 1 | 0 | 0 | 0 | 99 | 0 | 11 | 0 | 0 |  | 140 |
| Lane Group Flow (vph) | 224 | 802 | 0 | 45 | 774 | 133 | 49 | 196 | 0 | 257 | 134 | 58 |
| Confl. Peds. (\#\#hr) | 2 |  | 1 | 1 |  | 2 |  |  | 1 | 1 |  |  |
| Heavy Vehicles (\%) | 5\% | 3\% | 26\% | 12\% | 2\% | 7\% | 4\% | 9\% | 12\% | 6\% | 9\% | 4\% |
| Turn Type | pm+pt | NA |  | Perm | NA | Perm | Perm | NA |  | pm+pt | NA | Perm |
| Protected Phases | 5 | 2 |  |  | 6 |  |  | 4 |  | 3 | 8 |  |
| Permitted Phases | 2 |  |  | 6 |  | 6 | 4 |  |  | 8 |  | 8 |
| Actuated Green, G (s) | 71.0 | 71.0 |  | 57.0 | 57.0 | 57.0 | 25.0 | 25.0 |  | 35.0 | 35.0 | 35.0 |
| Effective Green, g (s) | 71.0 | 71.0 |  | 57.0 | 57.0 | 57.0 | 25.0 | 25.0 |  | 35.0 | 35.0 | 35.0 |
| Actuated g/C Ratio | 0.59 | 0.59 |  | 0.48 | 0.48 | 0.48 | 0.21 | 0.21 |  | 0.29 | 0.29 | 0.29 |
| Clearance Time (s) | 3.0 | 7.0 |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  | 3.0 | 7.0 | 7.0 |
| Vehicle Extension (s) | 3.0 | 4.0 |  | 4.0 | 4.0 | 4.0 | 2.0 | 2.0 |  | 3.0 | 2.0 | 2.0 |
| Lane Grp Cap (vph) | 250 | 1075 |  | 197 | 884 | 699 | 255 | 344 |  | 283 | 508 | 452 |
| v/s Ratio Prot | c0.08 | 0.44 |  |  | 0.42 |  |  | 0.12 |  | c0.05 | 0.08 |  |
| $\mathrm{v} / \mathrm{s}$ Ratio Perm | c0.45 |  |  | 0.11 |  | 0.09 | 0.04 |  |  | c0.21 |  | 0.04 |
| v/c Ratio | 0.90 | 0.75 |  | 0.23 | 0.88 | 0.19 | 0.19 | 0.57 |  | 0.91 | 0.26 | 0.13 |
| Uniform Delay, d1 | 28.1 | 17.9 |  | 18.6 | 28.3 | 18.2 | 39.2 | 42.7 |  | 41.0 | 32.6 | 31.3 |
| Progression Factor | 1.00 | 1.00 |  | 1.07 | 1.15 | 1.80 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 30.8 | 4.7 |  | 2.2 | 9.9 | 0.5 | 1.7 | 6.7 |  | 30.4 | 1.3 | 0.6 |
| Delay (s) | 58.9 | 22.6 |  | 22.0 | 42.5 | 33.2 | 40.8 | 49.4 |  | 71.4 | 33.9 | 31.9 |
| Level of Service | E | C |  | C | D | C | D | D |  | E | C |  |
| Approach Delay (s) |  | 30.5 |  |  | 39.6 |  |  | 47.7 |  |  | 49.6 |  |
| Approach LOS |  | C |  |  | D |  |  | D |  |  | D |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 2000 Control Delay |  |  | 39.1 |  | HCM 2000 | Level of S | ervice |  | D |  |  |  |
| HCM 2000 Volume to Capacity ratio |  |  | 0.95 |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length (s) |  |  | 120.0 |  | Sum of los | time (s) |  |  | 20.0 |  |  |  |
| Intersection Capacity Utilization |  |  | 112.8\% |  | CU Level | Service |  |  | H |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |
| c Critical Lane Group |  |  |  |  |  |  |  |  |  |  |  |  |

Uppers Quarry Traffic Impact Study
Synchro 10 Report

Timings
<2035 Total - Thorold Townline> PM Peak Hour 4: Thorold Townline Road \& Thorold Stone Road 09-23-2021



[^54]Synchro 10 Report
Snor

4: Thorold Townline Road \& Thorold Stone Road

|  | $\Rightarrow$ | $\rightarrow$ |  | 7 |  |  | 4 | $\dagger$ | 1 |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \% | ¢ $\uparrow$ | 7 | 7 | 个 $\uparrow$ | F | \% | $\hat{\dagger}$ |  | \% | F |  |
| Traffic Volume (vph) | 231 | 1128 | 97 | 111 | 954 | 35 | 203 | 211 | 201 | 48 | 211 | 27 |
| Future Volume (vph) | 231 | 1128 | 97 | 111 | 954 | 35 | 203 | 211 | 201 | 48 | 211 | 27 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 190 |
| Total Lost time (s) | 3.0 | 6.1 | 6.1 | 3.0 | 6.1 | 6.1 | 3.0 | 6.4 |  | 3.0 | 6.4 |  |
| Lane Util. Factor | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 |  |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 0.93 |  | 1.00 | 0.92 |  |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |  | 0.95 | 1.00 |  |
| Satd. Flow (prot) | 1671 | 3574 | 1357 | 1543 | 3539 | 1538 | 1626 | 1506 |  | 1671 | 1630 |  |
| Flt Permitted | 0.10 | 1.00 | 1.00 | 0.11 | 1.00 | 1.00 | 0.12 | 1.00 |  | 0.40 | 1.00 |  |
| Satd. Flow (perm) | 178 | 3574 | 1357 | 178 | 3539 | 1538 | 211 | 1506 |  | 702 | 1630 |  |
| Peak-hour factor, PHF | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 |
| Adj. Flow (vph) | 241 | 1175 | 101 | 116 | 994 | 36 | 211 | 220 | 209 | 50 | 220 | 28 |
| RTOR Reduction (vph) | 0 | 0 | 64 | 0 | 0 | 25 | 0 | 28 | 0 | 0 | 39 |  |
| Lane Group Flow (vph) | 241 | 1175 | 37 | 116 | 994 | 11 | 211 | 401 | 0 | 50 | 464 |  |
| Heavy Vehicles (\%) | 8\% | 1\% | 19\% | 17\% | 2\% | 5\% | 11\% | 15\% | 19\% | 8\% | 9\% | 5\% |
| Turn Type | pm+pt | NA | Perm | pm+pt | NA | Perm | pm+pt | NA |  | pm+pt | NA |  |
| Protected Phases | 5 | 2 |  | 1 | 6 |  | 7 | 4 |  | 3 | 8 |  |
| Permitted Phases | 2 |  | 2 | 6 |  | 6 | 4 |  |  | 8 |  |  |
| Actuated Green, G (s) | 54.5 | 44.3 | 44.3 | 43.7 | 36.5 | 36.5 | 53.0 | 45.2 |  | 41.0 | 36.2 |  |
| Effective Green, $\mathrm{g}(\mathrm{s}$ ) | 54.5 | 44.3 | 44.3 | 43.7 | 36.5 | 36.5 | 53.0 | 45.2 |  | 41.0 | 36.2 |  |
| Actuated g/C Ratio | 0.45 | 0.37 | 0.37 | 0.36 | 0.30 | 0.30 | 0.44 | 0.38 |  | 0.34 | 0.30 |  |
| Clearance Time (s) | 3.0 | 6.1 | 6.1 | 3.0 | 6.1 | 6.1 | 3.0 | 6.4 |  | 3.0 | 6.4 |  |
| Vehicle Extension (s) | 2.5 | 6.0 | 6.0 | 3.0 | 6.0 | 6.0 | 3.0 | 2.3 |  | 3.0 | 2.3 |  |
| Lane Grp Cap (vph) | 267 | 1319 | 500 | 146 | 1076 | 467 | 255 | 567 |  | 278 | 491 |  |
| v/s Ratio Prot | c0.11 | 0.33 |  | 0.05 | 0.28 |  | c0.09 | 0.27 |  | 0.01 | c0.28 |  |
| v/s Ratio Perm | c0.30 |  | 0.03 | 0.24 |  | 0.01 | 0.27 |  |  | 0.05 |  |  |
| $\mathrm{v} / \mathrm{C}$ Ratio | 0.90 | 0.89 | 0.07 | 0.79 | 0.92 | 0.02 | 0.83 | 0.71 |  | 0.18 | 0.94 |  |
| Uniform Delay, d1 | 33.0 | 35.6 | 24.6 | 29.6 | 40.4 | 29.3 | 26.2 | 31.8 |  | 27.1 | 40.9 |  |
| Progression Factor | 1.70 | 1.75 | 6.38 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 |  |
| Incremental Delay, d2 | 19.7 | 5.5 | 0.2 | 25.0 | 14.3 | 0.1 | 19.3 | 3.6 |  | 0.3 | 27.0 |  |
| Delay (s) | 76.0 | 67.7 | 156.8 | 54.6 | 54.7 | 29.4 | 45.5 | 35.3 |  | 27.4 | 67.9 |  |
| Level of Service | E | E | F | D | D | C | D | D |  | C | E |  |
| Approach Delay (s) |  | 75.0 |  |  | 53.9 |  |  | 38.7 |  |  | 64.3 |  |
| Approach LOS |  | E |  |  | D |  |  | D |  |  | E |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 61.2 |  | HCM 2000 | Level of S | Service |  | E |  |  |  |
| HCM 2000 Control Delay HCM 2000 Volume to Capacity ratio |  |  | 0.93 |  |  |  |  |  |  |  |  |  |
|  |  |  | 120.0 |  | Sum of los | time (s) |  |  | 18.5 |  |  |  |
| Actuated Cycle Length (s) Intersection Capacity Utilization |  |  | 95.3\% |  | CU Level | of Service |  |  | F |  |  |  |
|  |  |  | 15 |  |  |  |  |  |  |  |  |  |
| Analysis Period (min) c Critical Lane Group |  |  |  |  |  |  |  |  |  |  |  |  |

Uppers Quarry Traffic Impact Study

Timings
<2035 Total - Thorold Townline> PM Peak Hour
5: Thorold Townline Road \& Lundys Lane
<2035 Total - Thorold Townline> PM Peak Hour
$\square$

$\begin{array}{lrrrrrrrrrr}\text { Future Volume (vph) } & 116 & 673 & 117 & 44 & 711 & 117 & 142 & 96 & 118 & 185 \\ \text { Turn Type } & \text { Perm } & \text { NA } & \text { Perm } & \text { Perm } & \text { NA } & \text { Perm } & \text { NA } & \text { Perm } & \text { NA } & \text { Perm }\end{array}$
Protected Phase
Permitted Phases
Switch Phase
Minimum Initial
$\begin{array}{lllllllllll}\text { Minimum Initial (s) } & 20.0 & 20.0 & 20.0 & 20.0 & 20.0 & 10.0 & 10.0 & 10.0 & 10.0 & 10.0\end{array}$

| Minimum Split (s) | 29.0 | 29.0 | 29.0 | 29.0 | 29.0 | 35.0 | 35.0 | 35.0 | 35.0 | 35.0 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Total Split (s) | 85.0 | 85.0 | 85.0 | 85.0 | 85.0 | 35.0 | 35.0 | 35.0 | 35.0 | 35.0 | $\begin{array}{lllllllllll}\text { total Split (\%) } & 70.8 \% & 70.8 \% & 70.8 \% & 70.8 \% & 70.8 \% & 29.2 \% & 29.2 \% & 29.2 \% & 29.2 \% & 29.2 \%\end{array}$


| Yellow Time (s) | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


| All-Red Time (s) | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Total Lost Time (s) | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 |

Total Lost Time (s)
-ead/Lag

|  |  |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Lead-Lag Optimize? |  |  |  |  |  |  |  |  |  |  |
| R-Max | C-Max | C-Max | C-Max | C-Max | None | None | None | None | None |  |
| Recall Mode | 85.6 | 85.6 | 85.6 | 85.6 | 85.6 | 21.4 | 21.4 | 21.4 | 21.4 | 21.4 |
| Act ffct Green (s) | 051.11 | 0.71 | 0.71 | 0.71 | 0.71 | 0.18 | 0.18 | 0.18 | 0.18 | 0.18 |
| Actuated g/C Ratio | 0.42 | 0.57 | 0.11 | 0.12 | 0.66 | 0.66 | 0.65 | 0.77 | 0.41 | 0.46 |
| V/c Ratio | 14.2 | 13.6 | 4.5 | 7.7 | 13.3 | 60.7 | 51.5 | 80.1 | 46.2 | 8.7 |
| Control Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Queue Delay | 14.2 | 13.6 | 4.5 | 7.7 | 13.3 | 60.7 | 51.5 | 80.1 | 46.2 | 8.7 |
| Total Delay | B | B | A | A | B | E | D | F | D | A |
| LOS |  |  |  |  |  |  |  |  |  |  |

Approach Delay
Approach LOS

## Intersection Summary

ycle Lengin: 120
Offset: $0(0 \%)$, Referenced to phase 2:EBTL and $6: W B T L$, Start of Green
Control Typee: Actuated-Coordinated
$\begin{array}{ll}\text { Control Type: Actuated-Coordinated } & \\ \text { Maximum v/c Ratio: 0.77 } & \\ \begin{array}{ll}\text { Intersection Signal Delay: } 22.1 & \text { Intersection LOS: } C \\ \text { Intersection Capacity Utiization } 98.5 \% & \text { ICU Level of Service F }\end{array}\end{array}$
Analysis Period (min) 15


HCM Signalized Intersection Capacity Analysis<2035 Total - Thorold Townline> PM Peak Hour 5: Thorold Townline Road \& Lundys Lane


Timings
<2035 Total - Thorold Townline> PM Peak Hour 6: Thorold Townline Road \& Beaverdams Road 09-23-2021



[^55]Synchro 10 Report

HCM Signalized Intersection Capacity Analysis<2035 Total - Thorold Townline> PM Peak Hour 6: Thorold Townline Road \& Beaverdams Road 09-23-2021

|  | $\stackrel{ }{ }$ |  |  | $\dagger$ |  |  |  | $\uparrow$ | P |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | ${ }_{\text {¢ }}$ |  |  | $\dagger$ |  |  | $\dagger$ |  |  | ${ }_{4}$ |  |
| Traffic Volume (vph) | 27 | 205 | 16 | 124 | 178 | 21 | 32 | 584 | 94 | 20 | 363 | 41 |
| Future Volume (vph) | 27 | 205 | 16 | 124 | 178 | 21 | 32 | 584 | 94 | 20 | 363 | 41 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) |  | 6.0 |  |  | 6.0 |  |  | 6.0 |  |  | 6.0 |  |
| Lane Util. Factor |  | 1.00 |  |  | 1.00 |  |  | 1.00 |  |  | 1.00 |  |
| Frpb, ped/bikes |  | 1.00 |  |  | 1.00 |  |  | 1.00 |  |  | 1.00 |  |
| Flpb, ped/bikes |  | 1.00 |  |  | 1.00 |  |  | 1.00 |  |  | 1.00 |  |
| Frt |  | 0.99 |  |  | 0.99 |  |  | 0.98 |  |  | 0.99 |  |
| Flt Protected |  | 0.99 |  |  | 0.98 |  |  | 1.00 |  |  | 1.00 |  |
| Satd. Flow (prot) |  | 1830 |  |  | 1803 |  |  | 1636 |  |  | 1630 |  |
| Flt Permitted |  | 0.94 |  |  | 0.71 |  |  | 0.97 |  |  | 0.95 |  |
| Satd. Flow (perm) |  | 1727 |  |  | 1296 |  |  | 1585 |  |  | 1553 |  |
| Peak-hour factor, PHF | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 |
| Adj. Flow (vph) | 29 | 220 | 17 | 133 | 191 | 23 | 34 | 628 | 101 | 22 | 390 | 44 |
| RTOR Reduction (vph) | 0 | 3 | 0 | 0 | 3 | 0 | 0 | 7 | 0 | 0 | 5 |  |
| Lane Group Flow (vph) | 0 | 263 | 0 | 0 | 344 | 0 | 0 | 756 | 0 | 0 | 451 |  |
| Confl. Peds. (\#lhr) | 1 |  | 5 | 5 |  | 1 | 8 |  | 3 | 3 |  |  |
| Heavy Vehicles (\%) | 10\% | 1\% | 4\% | 4\% | 1\% | 0\% | 4\% | 16\% | 0\% | 2\% | 16\% | 6\% |
| Turn Type | Perm | NA |  | Perm | NA |  | Perm | NA |  | Perm | NA |  |
| Protected Phases |  | 2 |  |  | 6 |  |  | , |  |  | 8 |  |
| Permitted Phases | 2 |  |  | 6 |  |  | 4 |  |  | 8 |  |  |
| Actuated Green, G (s) |  | 30.2 |  |  | 30.2 |  |  | 47.8 |  |  | 47.8 |  |
| Effective Green, g(s) |  | 30.2 |  |  | 30.2 |  |  | 47.8 |  |  | 47.8 |  |
| Actuated g/C Ratio |  | 0.34 |  |  | 0.34 |  |  | 0.53 |  |  | 0.53 |  |
| Clearance Time (s) |  | 6.0 |  |  | 6.0 |  |  | 6.0 |  |  | 6.0 |  |
| Vehicle Extension (s) |  | 5.0 |  |  | 5.0 |  |  | 5.0 |  |  | 5.0 |  |
| Lane Grp Cap (vph) |  | 579 |  |  | 434 |  |  | 841 |  |  | 824 |  |
| v/s Ratio Prot |  |  |  |  |  |  |  |  |  |  |  |  |
| v/s Ratio Perm |  | 0.15 |  |  | c0.27 |  |  | c0.48 |  |  | 0.29 |  |
| v/c Ratio |  | 0.45 |  |  | 0.79 |  |  | 0.90 |  |  | 0.55 |  |
| Uniform Delay, d1 |  | 23.4 |  |  | 27.1 |  |  | 18.9 |  |  | 14.0 |  |
| Progression Factor |  | 1.00 |  |  | 1.00 |  |  | 1.00 |  |  | 1.00 |  |
| Incremental Delay, d2 |  | 2.6 |  |  | 13.9 |  |  | 13.2 |  |  | 1.3 |  |
| Delay (s) |  | 26.0 |  |  | 40.9 |  |  | 32.1 |  |  | 15.3 |  |
| Level of Service |  | C |  |  | D |  |  | C |  |  | B |  |
| Approach Delay (s) |  | 26.0 |  |  | 40.9 |  |  | 32.1 |  |  | 15.3 |  |
| Approach LOS |  | C |  |  | D |  |  | C |  |  | B |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 2000 Control Delay |  |  | 28.7 |  | HCM 2000 | Level of S | ervice |  | C |  |  |  |
| HCM 2000 Volume to Capacity ratio |  |  | 0.86 |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length (s) |  |  | 90.0 |  | Sum of los | time (s) |  |  | 12.0 |  |  |  |
| Intersection Capacity Utilization |  |  | 99.4\% |  | CU Level | f Service |  |  | F |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |
| c Critical Lane Group |  |  |  |  |  |  |  |  |  |  |  |  |

HCM Unsignalized Intersection Capacity Analysi8035 Total - Thorold Townline> PM Peak Hour 7: Thorold Townline Road \& Uppers Lane 09-23-2021


## APPENDIX D

Queueing Analysis

Intersection: 1: Davis Road \& Thorold Stone Road

| Movement | EB | EB | EB | WB | WB | WB | NB | NB | NB | SB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Directions Served | L | T | T | L | T | TR | L | LT | R | T |
| Maximum Queue (m) | 20.2 | 77.9 | 71.5 | 39.1 | 101.0 | 105.9 | 57.3 | 65.4 | 9.1 | 6.2 |
| Average Queue (m) | 3.5 | 35.6 | 19.8 | 13.7 | 35.5 | 39.9 | 34.2 | 37.1 | 0.3 | 0.4 |
| 95th Queue (m) | 12.0 | 62.1 | 49.6 | 29.6 | 73.1 | 81.6 | 54.6 | 58.1 | 6.4 | 3.3 |
| Link Distance ( m ) |  | 367.0 | 367.0 |  | 315.3 | 315.3 | 1000.6 | 1000.6 |  | 265.6 |
| Upstream Blk Time (\%) |  |  |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |  |  |  |
| Storage Bay Dist ( m ) | 105.0 |  |  | 70.0 |  |  |  |  | 80.0 |  |
| Storage Blk Time (\%) |  |  | 0 |  | 1 |  |  | 0 |  |  |
| Queuing Penalty (veh) |  |  | 0 |  | 1 |  |  | 0 |  |  |

ntersection: 2: Davis Road \& Niagara Falls Road/Beaverdams Road

| Movement | EB | WB | NB | NB | NB | SB | SB | SB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Directions Served | LTR | LTR | L | T | TR | L | T | T |
| Maximum Queue (m) | 34.2 | 35.7 | 8.5 | 46.7 | 61.4 | 32.3 | 55.3 | 41.7 |
| Average Queue (m) | 13.1 | 12.0 | 0.8 | 21.4 | 25.1 | 13.5 | 23.0 | 7.3 |
| 95 th Queue (m) | 27.2 | 24.8 | 4.6 | 40.3 | 47.3 | 26.5 | 43.1 | 25.7 |
| Link Distance ( m ) | 244.6 | 305.1 |  | 296.6 | 296.6 |  | 1000.6 | 1000.6 |
| Upstream B1k Time (\%) |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |  |
| Storage Bay Dist (m) |  |  | 80.0 |  |  | 140.0 |  |  |
| Storage BIk Time (\%) |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |  |

Intersection: 3: Davis Road \& Lundys Lane

|  |  |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Movement | EB | EB | WB | WB | WB | NB | NB | SB | SB | SB |
| Directions Served | L | TR | L | T | R | L | TR | L | T | R |
| Maximum Queue $(m)$ | 31.8 | 46.1 | 22.2 | 58.4 | 15.5 | 26.7 | 69.2 | 41.0 | 57.0 | 31.6 |
| Average Queue $(m)$ | 12.8 | 20.6 | 6.0 | 19.5 | 3.1 | 6.1 | 32.2 | 15.8 | 19.0 | 8.3 |
| 95th Queue $(\mathrm{m})$ | 26.6 | 39.4 | 17.4 | 44.6 | 10.6 | 18.5 | 57.7 | 32.9 | 42.6 | 21.4 |
| Link Distance $(\mathrm{m})$ |  | 266.3 |  | 1923.8 |  |  | 458.7 |  | 610.8 |  |
| Upstream BIk Time $(\%)$ |  |  |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  | 65.0 |  | 80.0 | 55.0 |  | 90.0 |  | 100.0 |
| Storage Bay Dist $(m)$ | 85.0 |  |  | 0 |  |  | 2 |  | 0 |  |
| Storage Bl Time $(\%)$ |  |  |  | 0 |  |  | 0 |  | 0 |  |

Intersection: 4: Thorold Townline Road \& Thorold Stone Road

| Movement | EB | EB | EB | EB | WB | WB | WB | WB | NB | NB | SB | SB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Directions Served | L | T | T | R | L | T | T | R | L | TR | L | TR |
| Maximum Queue (m) | 97.9 | 57.2 | 58.9 | 19.9 | 19.2 | 91.7 | 81.7 | 20.9 | 40.5 | 74.9 | 32.7 | 97.7 |
| Average Queue (m) | 49.6 | 18.2 | 23.2 | 2.8 | 4.6 | 55.6 | 45.3 | 7.5 | 14.7 | 26.4 | 10.8 | 47.3 |
| 95th Queue (m) | 81.8 | 42.4 | 47.2 | 11.7 | 14.7 | 82.7 | 74.6 | 17.7 | 33.7 | 52.7 | 26.1 | 86.5 |
| Link Distance ( m ) |  | 279.0 | 279.0 |  |  | 338.6 | 338.6 |  |  | 1028.0 |  | 311.8 |
| Upstream Blk Time (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Storage Bay Dist (m) | 100.0 |  |  | 50.0 | 85.0 |  |  | 90.0 | 80.0 |  | 75.0 |  |
| Storage Blk Time (\%) | 0 |  | 1 |  |  | 0 | 0 |  |  | 0 |  |  |
| Queuing Penalty (veh) | 1 |  | 0 |  |  | 0 | 0 |  |  | 0 |  |  |

Intersection: 5: Thorold Townline Road \& Lundys Lane


Intersection: 6: Thorold Townline Road \& Beaverdams Road

| Movement | EB | WB | NB | SB |
| :---: | :---: | :---: | :---: | :---: |
| Directions Served | LTR | LTR | LTR | LTR |
| Maximum Queue (m) | 25.4 | 17.6 | 45.1 | 29.7 |
| Average Queue (m) | 12.2 | 9.8 | 20.8 | 14.7 |
| 95th Queue (m) | 20.6 | 16.3 | 35.5 | 24.9 |
| Link Distance ( m ) | 192.4 | 256.5 | 1091.4 | 1028.0 |
| Upstream Blk Time (\%) |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |
| Storage Bay Dist ( m ) |  |  |  |  |
| Storage Blk Time (\%) |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |

## Uppers Quarry Traffic Impact Study

TMIG

Intersection: 7: Thorold Townline Road \& Uppers Lane

| Movement | WB |
| :--- | ---: |
| Directions Served | LR |
| Maximum Queue $(\mathrm{m})$ | 1.4 |
| Average Queueue $(\mathrm{m})$ | 0.1 |
| 95th Queue $(\mathrm{m})$ | 1.6 |
| Link Distance $(\mathrm{m})$ | 1027.2 |
| Upstream Blk Time $(\%)$ |  |
| Queuing Penalty (veh) |  |
| Storage Bay Dist $(\mathrm{m})$ |  |
| Storage Blk Time $(\%)$ |  |
| Queuing Penalty (veh) |  |
| Network Summary |  |
| Network wide Queuing Penalty: 39 |  |

Intersection: 1: Davis Road \& Thorold Stone Road

| Movement | EB | EB | EB | EB | WB | WB | WB | NB | NB | SB | SB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Directions Served | L | T | T | R | L | T | TR | L | LT | L | T |
| Maximum Queue ( m ) | 26.4 | 111.1 | 100.0 | 36.5 | 54.0 | 89.4 | 94.7 | 59.4 | 65.0 | 8.1 | 9.3 |
| Average Queue (m) | 5.0 | 55.4 | 42.3 | 1.2 | 21.1 | 39.7 | 42.5 | 34.6 | 37.6 | 0.8 | 1.8 |
| 95th Queue (m) | 16.4 | 93.4 | 82.9 | 18.3 | 45.6 | 75.5 | 80.1 | 54.1 | 59.3 | 4.4 | 7.1 |
| Link Distance ( m ) |  | 367.0 | 367.0 |  |  | 315.3 | 315.3 | 1000.6 | 1000.6 |  | 265.6 |
| Upstream BIk Time (\%) |  |  |  |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |  |  |  |  |
| Storage Bay Dist (m) | 105.0 |  |  | 50.0 | 70.0 |  |  |  |  | 30.0 |  |
| Storage Blk Time (\%) |  | 0 | 4 |  | 0 | 2 |  |  |  |  |  |
| Queuing Penalty (veh) |  | 0 | 18 |  | 1 | 1 |  |  |  |  |  |

ntersection: 2: Davis Road \& Niagara Falls Road/Beaverdams Road

| Movement | EB | WB | NB | NB | NB | SB | SB | SB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Directions Served | LTR | LTR | L | T | TR | L | T | T |
| Maximum Queue (m) | 28.3 | 50.6 | 8.6 | 41.1 | 53.2 | 58.1 | 51.4 | 34.1 |
| Average Queue (m) | 13.0 | 17.5 | 0.9 | 19.2 | 24.3 | 28.2 | 26.5 | 12.0 |
| 95 th Queue (m) | 25.0 | 35.4 | 4.9 | 35.4 | 44.0 | 47.0 | 45.6 | 30.2 |
| Link Distance ( m ) | 244.6 | 305.1 |  | 296.6 | 296.6 |  | 1000.6 | 1000.6 |
| Upstream BIk Time (\%) |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |  |
| $\begin{array}{lll}\text { Storage Bay Dist ( } \mathrm{m} \text { ) } & 80.0 & 140.0\end{array}$ |  |  |  |  |  |  |  |  |
| Storage Blk Time (\%) |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |  |

Intersection: 3: Davis Road \& Lundys Lane

| Movement | EB | EB | WB | WB | WB | NB | NB | SB | SB | SB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Directions Served | L | TR | L | T | R | L | TR | L | T | R |
| Maximum Queue (m) | 41.0 | 88.8 | 21.4 | 92.8 | 20.0 | 26.1 | 43.8 | 28.7 | 45.0 | 31.2 |
| Average Queue (m) | 17.6 | 43.0 | 6.1 | 44.1 | 5.8 | 7.9 | 18.7 | 10.8 | 12.6 | 6.8 |
| 95 th Queue (m) | 33.9 | 73.7 | 16.8 | 77.5 | 14.1 | 19.8 | 36.4 | 23.3 | 30.8 | 19.0 |
| Link Distance (m) |  | 266.3 |  | 1923.8 |  |  | 458.7 |  | 610.8 |  |
| Upstream B1k Time (\%) |  |  |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |  |  |  |
| Storage Bay Dist (m) | 85.0 |  | 65.0 |  | 80.0 | 55.0 |  | 90.0 |  | 100.0 |
| Storage BIk Time (\%) |  | 0 |  | 2 |  |  | 0 |  |  |  |
| Queuing Penalty (veh) |  | 0 |  | 2 |  |  | 0 |  |  |  |

Queuing and Blocking Report
<2018 Existing> PM Peak Hour

Intersection: 4: Thorold Townline Road \& Thorold Stone Road

| Movement | EB | EB | EB | EB | B24 | WB | WB | WB | WB | NB | NB | SB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Directions Served | L | T | T | R | T | L | T | T | R | L | TR |  |
| Maximum Queue (m) | 87.1 | 83.3 | 90.0 | 9.2 | 66.2 | 19.4 | 88.4 | 78.1 | 14.4 | 30.0 | 51.3 | 35.6 |
| Average Queue (m) | 37.1 | 37.3 | 42.7 | 2.4 | 2.2 | 5.9 | 53.4 | 40.2 | 3.4 | 12.6 | 18.4 | 9.8 |
| 95th Queue (m) | 67.1 | 75.6 | 83.1 | 8.3 | 46.6 | 15.4 | 80.9 | 70.1 | 10.7 | 27.0 | 41.3 | 24.6 |
| Link Distance ( m ) |  | 279.0 | 279.0 |  | 315.3 |  | 338.6 | 338.6 |  |  | 1028.0 |  |
| Upstream Blk Time (\%) |  |  |  |  | 0 |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  | 1 |  |  |  |  |  |  |  |
| Storage Bay Dist (m) | 100.0 |  |  | 50.0 |  | 85.0 |  |  | 90.0 | 80.0 |  | 75 |
| Storage Blk Time (\%) | 0 | 0 | 5 |  |  |  | 0 | , |  |  |  |  |
| Queuing Penalty (veh) | 1 | 0 | 2 |  |  |  | 0 |  |  |  |  |  |

ntersection: 4: Thorold Townline Road \& Thorold Stone Road

| Movement | SB |
| :--- | ---: |
| Directions Served | TR |
| Maximum Queue $(m)$ | 142.5 |
| Average Queue $(m)$ | 68.0 |
| 95th Queue $(m)$ | 121.3 |
| Link Distance $(m)$ | 311.8 |
| Usstream Blk Time $(\%)$ |  |
| Queuing Penalty (veh) |  |
| Storage Bay Dist $(m)$ |  |
| Storage Blk Time $(\%)$ | 9 |
| Queuing Penalty $($ veh $)$ | 4 |

Intersection: 5: Thorold Townline Road \& Lundys Lane

| Movement | EB | EB | EB | WB | WB | NB | NB | SB | SB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Directions Served | L | T | R | L | TR | L | TR | L | TR |
| Maximum Queue (m) | 27.3 | 79.7 | 40.6 | 21.2 | 63.8 | 57.0 | 67.2 | 17.2 | 54.9 |
| Average Queue (m) | 7.3 | 31.3 | 7.2 | 6.2 | 26.6 | 19.6 | 28.0 | 4.9 | 22.1 |
| 95th Queue (m) | 19.8 | 65.8 | 22.9 | 15.7 | 49.5 | 42.3 | 52.5 | 13.7 | 44.6 |
| Link Distance ( m ) |  | 1923.8 |  |  | 479.5 |  | 741.7 |  | 1500.1 |
| Upstream BIk Time (\%) |  |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |  |  |
| Storage Bay Dist (m) | 90.0 |  | 20.0 | 55.0 |  | 25.0 |  | 25.0 |  |
| Storage Bik Time (\%) |  | 12 | 0 |  | 0 | 8 | 14 | 0 | 10 |
| Queuing Penalty (veh) |  | 16 | 1 |  | 0 | 15 | 14 | 0 | 2 |

Intersection: 6: Thorold Townline Road \& Beaverdams Road


Intersection: 1: Davis Road \& Thorold Stone Road

| Movement | EB | EB | EB | WB | WB | WB | NB | NB | NB | SB | SB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Directions Served | L | T | T | L | T | TR | L | LT | R | L | T |
| Maximum Queue (m) | 13.7 | 93.5 | 128.0 | 37.0 | 108.8 | 115.9 | 96.5 | 100.8 | 42.6 | 3.4 | 7.4 |
| Average Queue (m) | 2.8 | 52.7 | 42.4 | 15.8 | 62.4 | 64.1 | 53.9 | 58.9 | 1.7 | 0.2 | 0.8 |
| 95th Queue ( m ) | 9.7 | 84.7 | 92.0 | 29.8 | 101.3 | 104.0 | 85.2 | 90.5 | 17.1 | 1.6 | 4.6 |
| Link Distance ( m ) |  | 367.0 | 367.0 |  | 315.3 | 315.3 | 1000.6 | 1000.6 |  |  | 265.6 |
| Upstream Blk Time (\%) |  |  |  |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |  |  |  |  |
| Storage Bay Dist ( m ) | 105.0 |  |  | 70.0 |  |  |  |  | 80.0 | 30.0 |  |
| Storage Blk Time (\%) |  | 0 | 3 |  | 6 |  |  | 2 |  |  |  |
| Queuing Penalty (veh) |  | 0 | 7 |  | 5 |  |  | 4 |  |  |  |

ntersection: 2: Davis Road \& Niagara Falls Road/Beaverdams Road

| Movement | EB | WB | NB | NB | NB | SB | SB | SB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Directions Served | LTR | LTR | L | T | TR | L | T | T |
| Maximum Queue (m) | 45.6 | 38.0 | 21.7 | 69.8 | 79.9 | 31.4 | 61.0 | 43.7 |
| Average Queue (m) | 17.6 | 14.2 | 3.4 | 35.8 | 42.6 | 15.8 | 30.0 | 13.8 |
| 95th Queue (m) | 35.4 | 28.0 | 13.5 | 58.6 | 69.2 | 28.3 | 52.0 | 36.1 |
| Link Distance (m) | 244.6 | 305.1 |  | 296.6 | 296.6 |  | 1000.6 | 1000.6 |
| Upstream BIk Time (\%) |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |  |
| Storage Bay Dist (m) |  |  | 80.0 |  |  | 140.0 |  |  |
| Storage BIk Time (\%) |  |  |  | 0 |  |  |  |  |
| Queuing Penalty (veh) |  |  |  | 0 |  |  |  |  |

ntersection: 3: Davis Road \& Lundys Lane

| Movement | EB | EB | WB | WB | WB | NB | NB | SB | SB | SB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Directions Served | L | TR | L | T | R | L | TR | L | T | R |
| Maximum Queue (m) | 58.7 | 87.9 | 34.6 | 80.2 | 34.8 | 25.2 | 69.0 | 93.8 | 56.5 | 34.1 |
| Average Queue (m) | 24.1 | 40.3 | 9.7 | 35.9 | 15.1 | 4.4 | 28.7 | 40.8 | 17.1 | 12.8 |
| 95 th Queue (m) | 49.2 | 73.0 | 23.9 | 68.0 | 28.6 | 15.1 | 54.6 | 75.2 | 42.1 | 26.0 |
| Link Distance ( m ) |  | 266.3 |  | 1920.7 |  |  | 458.7 |  | 610.8 |  |
| Upstream B1k Time (\%) |  |  |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |  |  |  |
| Storage Bay Dist ( m ) | 85.0 |  | 65.0 |  | 80.0 | 55.0 |  | 90.0 |  | 100.0 |
| Storage Blk Time (\%) |  | 0 |  | 1 |  |  | 1 | 0 |  |  |
| Queuing Penalty (veh) |  | 0 |  | 3 |  |  | 0 | 1 |  |  |

Queuing and Blocking Report
<2025 Background> AM Peak Hour

Intersection: 4: Thorold Townline Road \& Thorold Stone Road

| Movement | EB | EB | EB | EB | B24 | WB | WB | WB | WB | NB | NB | SB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Directions Served | L | 1 | T | R | T | L | T | T | R | L | TR |  |
| Maximum Queue (m) | 101.8 | 84.4 | 86.3 | 38.6 | 64.0 | 38.9 | 106.9 | 96.9 | 25.2 | 51.1 | 73.2 | 31.8 |
| Average Queue (m) | 62.6 | 47.7 | 51.4 | 14.9 | 2.1 | 18.1 | 68.4 | 59.3 | 9.1 | 18.3 | 27.0 | 11.0 |
| 95th Queue (m) | 96.3 | 72.9 | 75.6 | 30.8 | 45.1 | 34.2 | 103.5 | 93.4 | 20.7 | 40.5 | 57.4 | 26.2 |
| Link Distance ( m ) |  | 279.0 | 279.0 |  | 315.3 |  | 338.6 | 338.6 |  |  | 1028.0 |  |
| Upstream Blk Time (\%) |  |  |  |  | 0 |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  | 0 |  |  |  |  |  |  |  |
| Storage Bay Dist (m) | 100.0 |  |  | 50.0 |  | 85.0 |  |  | 90.0 | 80.0 |  | 75.0 |
| Storage Blk Time (\%) | 1 |  | 12 | 0 |  |  | 4 | 1 |  |  | 0 |  |
| Queuing Penalty (veh) | 2 |  | 12 | 0 |  |  | 5 | 1 |  |  | 0 |  |

Intersection: 4: Thorold Townline Road \& Thorold Stone Road

| Movement | SB |
| :--- | ---: |
| Directions Served | TR |
| Maximum Queue $(m)$ | 142.4 |
| Average Queue $(m)$ | 78.7 |
| 95th Queue $(m)$ | 136.5 |
| Link Distance $(m)$ | 311.8 |
| Usstream Blk Time $(\%)$ |  |
| Queuing Penalty (veh) |  |
| Storage Bay Dist $(m)$ | 13 |
| Storage Blik Time $(\%)$ | 7 |
| Queuing Penalty $($ veh $)$ | 7 |

Intersection: 5: Thorold Townline Road \& Lundys Lane

| Movement | EB | EB | EB | WB | WB | NB | NB | SB | SB | SB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Directions Served | L | T | R | L | TR | L | TR | L | T | R |
| Maximum Queue (m) | 43.1 | 66.4 | 41.2 | 17.2 | 58.1 | 54.9 | 80.3 | 16.9 | 43.0 | 21.7 |
| Average Queue (m) | 19.5 | 29.3 | 6.2 | 5.6 | 21.9 | 15.5 | 31.0 | 4.7 | 16.2 | 7.6 |
| 95th Queue (m) | 35.9 | 58.6 | 21.9 | 14.5 | 44.9 | 36.6 | 60.9 | 13.3 | 34.9 | 18.8 |
| Link Distance ( m ) |  | 1920.7 |  |  | 479.5 |  | 741.7 |  | 1500.2 |  |
| Upstream BIk Time (\%) |  |  |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |  |  |  |
| Storage Bay Dist (m) | 90.0 |  | 20.0 | 55.0 |  | 25.0 |  | 25.0 |  | 30.0 |
| Storage BIk Time (\%) |  | 10 | 0 |  | 0 | 5 | 16 | 0 | 5 | 0 |
| Queuing Penalty (veh) |  | 26 | 1 |  | 0 | 9 | 11 | 0 | 4 | 0 |

Intersection: 6: Thorold Townline Road \& Beaverdams Road


Intersection: 7: Thorold Townline Road \& Uppers Lane

## Movement

Maximum Queue (m)
Average Queue (m)
55th Queue ( m )
Link Distance (m)
Upstream BIk Time (\%)
Queuing Penalty (veh)
tome Bk Tim
Queuing Penalty (ve

Network Summary Network wide Queuing Penalty: 99

## ppers Quarry Traffic Impact Study <br> TMIG

Intersection: 1: Davis Road \& Thorold Stone Road

| Movement | EB | EB | EB | EB | WB | WB | WB | NB | NB | SB | SB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Directions Served | L | T | T | R | L | T | TR | L | LT | L | T |
| Maximum Queue (m) | 22.7 | 121.4 | 118.5 | 66.4 | 67.1 | 104.2 | 112.2 | 92.6 | 89.2 | 7.6 | 14.8 |
| Average Queue (m) | 5.0 | 77.0 | 64.7 | 3.7 | 26.0 | 48.5 | 50.4 | 52.7 | 54.9 | 0.8 | 2.5 |
| 95th Queue (m) | 15.3 | 118.8 | 110.0 | 30.4 | 51.2 | 87.9 | 93.4 | 78.0 | 80.7 | 4.2 | 9.5 |
| Link Distance ( m ) |  | 367.0 | 367.0 |  |  | 315.3 | 315.3 | 1000.6 | 1000.6 |  | 265.6 |
| Upstream Blk Time (\%) |  |  |  |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |  |  |  |  |
| Storage Bay Dist (m) | 105.0 |  |  | 50.0 | 70.0 |  |  |  |  | 30.0 |  |
| Storage Blk Time (\%) |  | 2 | 11 | 0 | 1 | 3 |  |  | 1 |  |  |
| Queuing Penalty (veh) |  | 0 | 64 | 0 | 4 | 4 |  |  | 2 |  |  |

ntersection: 2: Davis Road \& Niagara Falls Road/Beaverdams Road

| Movement |  | EB | WB | NB | NB | NB | SB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| SB |  |  |  |  |  |  |  |  |  |
| Directions Served | LTR | LTR | L | T | TR | L | T | T | R |
| Maximum Queue $(m)$ | 41.9 | 59.9 | 13.6 | 55.7 | 61.5 | 64.0 | 79.1 | 257.8 | 7.8 |
| Average Queue $(m)$ | 16.1 | 24.1 | 3.1 | 26.5 | 33.2 | 29.6 | 42.6 | 32.9 | 0.3 |
| 95th Queue $(m)$ | 33.9 | 46.8 | 9.6 | 48.4 | 56.0 | 52.0 | 68.9 | 169.0 | 4.0 |
| Link Distance $(m)$ | 244.6 | 305.1 |  | 296.6 | 296.6 |  | 1000.6 | 1000.6 |  |
| Upstream Blk Time $(\%)$ |  |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  | 80.0 |  |  | 140.0 |  | 180.0 |  |
| Storage Bay Dist $(\mathrm{m})$ |  |  |  |  |  |  |  |  |  |

Intersection: 3: Davis Road \& Lundys Lane

| Movement | EB | EB | WB | WB | WB | NB | NB | SB | SB | SB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Directions Served | L | TR | L | T | R | L | TR | L | T | R |
| Maximum Queue (m) | 86.8 | 121.0 | 53.8 | 140.7 | 68.0 | 32.9 | 76.4 | 115.7 | 70.1 | 43.4 |
| Average Queue (m) | 37.0 | 61.0 | 8.1 | 86.2 | 20.9 | 11.9 | 37.0 | 57.8 | 24.1 | 16.9 |
| 95th Queue (m) | 72.7 | 103.7 | 32.6 | 129.5 | 51.5 | 25.7 | 64.9 | 94.4 | 52.4 | 36.7 |
| Link Distance ( m ) |  | 266.3 |  | 1920.7 |  |  | 458.7 |  | 610.8 |  |
| Upstream Blk Time (\%) |  |  |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |  |  |  |
| Storage Bay Dist ( $m$ ) | 85.0 |  | 65.0 |  | 80.0 | 55.0 |  | 90.0 |  | 100.0 |
| Storage Blk Time (\%) | 2 | 3 |  | 18 |  |  | 4 | 2 | 0 |  |
| Queuing Penalty (veh) | 14 | 5 |  | 48 |  |  | 2 | 5 | 0 |  |

Queuing and Blocking Report

Intersection: 4: Thorold Townline Road \& Thorold Stone Road

| Movement | EB | EB | EB | EB | B24 | B24 | WB | WB | WB | WB | NB | NB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Directions Served | L | T | T | R | T | T | L | T | T | R | L | TR |
| Maximum Queue ( m ) | 76.9 | 123.9 | 129.9 | 16.9 | 62.7 | 62.8 | 29.6 | 109.0 | 92.6 | 14.4 | 45.4 | 5.4 |
| Average Queue (m) | 38.8 | 55.4 | 59.1 | 5.4 | 2.1 | 2.1 | 11.8 | 65.5 | 55.0 | 3.5 | 19.8 | 8.6 |
| 95th Queue (m) | 64.6 | 108.6 | 111.8 | 13.5 | 44.2 | 44.3 | 24.9 | 95.8 | 85.6 | 10.4 | 38.8 | 4.3 |
| Link Distance ( m ) |  | 279.0 | 279.0 |  | 315.3 | 315.3 |  | 338.6 | 338.6 |  |  |  |
| Upstream BIk Time (\%) |  |  |  |  | 0 | 0 |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  | 0 | 0 |  |  |  |  |  |  |
| Storage Bay Dist ( $m$ ) | 100.0 |  |  | 50.0 |  |  | 85.0 |  |  | 90.0 | 80.0 |  |
| Storage Blk Time (\%) |  | 2 | 15 |  |  |  |  | 2 | 0 |  |  |  |
| Queuing Penalty (veh) |  | 4 | 8 |  |  |  |  | 1 | 0 |  |  |  |

ntersection: 4: Thorold Townline Road \& Thorold Stone Road

| Movement | SB | SB |
| :---: | :---: | :---: |
| Directions Served | L | TR |
| Maximum Queue (m) | 86.6 | 169.6 |
| Average Queue (m) | 10.4 | 90.4 |
| 95th Queue (m) | 44.6 | 153.0 |
| Link Distance ( m ) |  | 311.8 |
| Upstream Blk Time (\%) |  |  |
| Queuing Penalty (veh) |  |  |
| Storage Bay Dist (m) | 75.0 |  |
| Storage Blk Time (\%) |  | 19 |
| Queuing Penalty (veh) |  | 9 |

Intersection: 5: Thorold Townline Road \& Lundys Lane

| Movement | EB | EB | EB | WB | WB | NB | NB | SB | SB | SB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Directions Served | L | T | R | L | TR | L | TR | L | T | R |
| Maximum Queue (m) | 38.4 | 59.7 | 28.3 | 19.4 | 80.5 | 53.4 | 57.4 | 30.7 | 54.0 | 28.1 |
| Average Queue (m) | 13.4 | 25.9 | 4.2 | 5.6 | 36.7 | 25.1 | 31.4 | 14.7 | 24.4 | 14.6 |
| 95th Queue (m) | 30.5 | 50.5 | 16.0 | 15.2 | 67.1 | 43.9 | 54.1 | 27.3 | 43.1 | 24.2 |
| Link Distance ( m ) | 1920.7 |  |  | 479.5 |  |  | 741.7 | 1500.2 |  |  |
| Upstream Blk Time (\%) |  |  |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |  |  |  |
| Storage Bay Dist (m) | 90.0 |  | 20.0 | 55.0 |  | 25.0 |  | 25.0 |  | 30.0 |
| Storage Blk Time (\%) |  | 9 | 0 |  | 2 | 15 | 19 | 3 | 11 | 0 |
| Queuing Penalty (veh) |  | 16 | 0 |  | 1 | 27 | 21 | 7 | 20 | 0 |



Intersection: 1: Davis Road \& Thorold Stone Road

| Movement | EB | EB | EB | WB | WB | WB | NB | NB | NB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | T | T | L | T | TR | L | LT | R | L | T |
| Maximum Queue $(m)$ | 16.2 | 73.6 | 68.6 | 50.1 | 93.7 | 104.7 | 92.0 | 90.5 | 26.7 | 1.9 | 4.5 |
| Average Queue $(m)$ | 3.3 | 43.0 | 29.3 | 19.8 | 58.3 | 61.7 | 58.1 | 60.5 | 1.2 | 0.1 | 0.3 |
| 95th Queue $(m)$ | 10.6 | 69.2 | 59.4 | 40.6 | 93.0 | 95.2 | 83.4 | 85.7 | 14.0 | 1.0 | 2.4 |
| Link Distance $(\mathrm{m})$ |  | 367.0 | 367.0 |  | 315.3 | 315.3 | 1000.6 | 1000.6 |  |  | 265.6 |
| Upstream Blk Time $(\%)$ |  |  |  |  |  |  |  |  |  |  |  |
| Queuing Penalty $($ veh $)$ |  |  |  | 70.0 |  |  |  |  | 80.0 | 30.0 |  |
| Storage Bay Dist $(m)$ | 105.0 |  | 1 |  | 5 |  |  | 2 |  |  |  |
| Storage Blk Time $(\%)$ |  |  | 3 |  | 4 |  |  | 4 |  |  |  |

ntersection: 2: Davis Road \& Niagara Falls Road/Beaverdams Road

| Movement | EB | WB | NB | NB | NB | SB | SB | SB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Directions Served | LTR | LTR | L | T | TR | L | T | T |
| Maximum Queue (m) | 42.7 | 53.2 | 21.9 | 67.7 | 82.0 | 39.0 | 65.4 | 38.1 |
| Average Queue (m) | 16.5 | 19.2 | 4.0 | 37.4 | 44.5 | 16.3 | 27.3 | 11.7 |
| 95th Queue (m) | 34.3 | 40.2 | 14.3 | 63.3 | 73.5 | 32.4 | 48.6 | 31.1 |
| Link Distance (m) | 244.6 | 305.1 |  | 296.6 | 296.6 |  | 1000.6 | 1000.6 |
| Upstream BIk Time (\%) |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |  |
| Storage Bay Dist (m) |  |  | 80.0 |  |  | 140.0 |  |  |
| Storage Blk Time (\%) |  |  |  | 0 |  |  |  |  |
| Queuing Penalty (veh) |  |  |  | 0 |  |  |  |  |

Intersection: 3: Davis Road \& Lundys Lane

| Movement | EB | EB | WB | WB | WB | NB | NB | SB | SB | SB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Directions Served | L | TR | L | T | R | L | TR | L | T | R |
| Maximum Queue (m) | 58.0 | 89.4 | 30.1 | 80.2 | 33.4 | 24.7 | 63.7 | 102.6 | 78.3 | 36.2 |
| Average Queue (m) | 23.4 | 39.8 | 8.6 | 33.2 | 15.6 | 6.7 | 28.6 | 47.4 | 20.2 | 12.9 |
| 95th Queue (m) | 45.8 | 72.2 | 22.3 | 66.7 | 28.9 | 18.4 | 53.2 | 95.1 | 59.4 | 28.7 |
| Link Distance ( m ) | 266.3 |  | 1920.7 |  | 458.7 |  |  | 610.8 |  |  |
| Upstream Blk Time (\%) |  |  |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |  |  |  |
| Storage Bay Dist ( $m$ ) | 85.0 |  | 65.0 |  | 80.0 | 55.0 |  | 90.0 |  | 100.0 |
| Storage Blk Time (\%) |  | 0 |  | 1 |  |  | 1 | 4 |  |  |
| Queuing Penalty (veh) |  | 0 |  | 2 |  |  | 0 | 9 |  |  |

Queuing and Blocking Report
<2025 Total - Thorold Townline> AM Peak Hour

Intersection: 4: Thorold Townline Road \& Thorold Stone Road

| Movement | EB | EB | EB | EB | WB | WB | WB | WB | NB | NB | SB | SB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Directions Served | L | T | T | R | L | T | T | R | L | TR | L | TR |
| Maximum Queue (m) | 123.3 | 89.7 | 95.5 | 40.6 | 62.4 | 120.8 | 114.2 | 28.0 | 62.6 | 97.5 | 36.4 | 147.8 |
| Average Queue (m) | 65.8 | 52.4 | 57.5 | 16.9 | 26.1 | 76.9 | 67.8 | 8.9 | 24.2 | 35.6 | 11.0 | 80.0 |
| 95th Queue (m) | 101.6 | 80.8 | 86.0 | 32.1 | 51.0 | 113.0 | 104.4 | 20.1 | 50.2 | 72.1 | 27.4 | 134.4 |
| Link Distance ( m ) |  | 279.0 | 279.0 |  |  | 338.6 | 338.6 |  |  | 1028.0 |  | 311.8 |
| Upstream Blk Time (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Storage Bay Dist (m) | 100.0 |  |  | 50.0 | 85.0 |  |  | 90.0 | 80.0 |  | 75.0 |  |
| Storage Blk Time (\%) | 1 | 0 | 16 | 0 | 0 | 7 | 2 |  |  | 1 |  | 12 |
| Queuing Penalty (veh) | , | 0 | 19 | 0 | 1 | 9 | 2 |  |  | 1 |  |  |

ntersection: 5: Thorold Townline Road \& Lundys Lane

| Movement |  |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |

Intersection: 6: Thorold Townline Road \& Beaverdams Road

| Movement | EB | WB | NB | SB |
| :---: | :---: | :---: | :---: | :---: |
| Directions Served | LTR | LTR | LTR | LTR |
| Maximum Queue (m) | 52.9 | 54.4 | 84.8 | 80.1 |
| Average Queue (m) | 23.8 | 24.9 | 39.9 | 37.9 |
| 95th Queue (m) | 45.5 | 45.4 | 74.2 | 67.8 |
| Link Distance ( m ) | 192.4 | 256.5 | 1091.4 | 1028.0 |
| Upstream Blk Time (\%) |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |
| Storage Bay Dist ( m ) |  |  |  |  |
| Storage Blk Time (\%) |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |

## Uppers Quarry Traffic Impact Study

TMIG

## Intersection: 7: Thorold Townline Road \& Uppers Lane



Intersection: 1: Davis Road \& Thorold Stone Road

| Movement | EB | EB | EB | EB | WB | WB | WB | NB | NB | NB | SB | SB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Directions Served | L | T | T | R | L | T | TR | L | LT | R | L |  |
| Maximum Queue (m) | 19.9 | 138.6 | 131.1 | 79.5 | 47.0 | 106.2 | 112.4 | 76.4 | 79.7 | 14.7 | 6.0 | 13.2 |
| Average Queue (m) | 4.8 | 73.0 | 62.8 | 5.7 | 22.7 | 60.6 | 64.1 | 48.8 | 52.8 | 0.9 | 1.0 | 2.2 |
| 95th Queue (m) | 15.0 | 116.5 | 108.9 | 45.6 | 41.8 | 96.5 | 101.1 | 68.7 | 72.3 | 10.0 | 4.1 | 8.3 |
| Link Distance (m) |  | 367.0 | 367.0 |  |  | 315.3 | 315.3 | 1000.6 | 1000.6 |  |  | 65.6 |
| Upstream Blk Time (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Storage Bay Dist ( m ) | 105.0 |  |  | 50.0 | 70.0 |  |  |  |  | 80.0 | 30.0 |  |
| Storage Blk Time (\%) |  | 2 | 12 | 0 |  | 5 |  |  | 0 |  |  |  |
| Queuing Penalty (veh) |  | 0 | 70 | 0 |  | 7 |  |  | 0 |  |  |  |

ntersection: 2: Davis Road \& Niagara Falls Road/Beaverdams Road

| Movement |  | EB | WB | NB | NB | NB | SB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| MBB |  |  |  |  |  |  |  |  |  |
| Directions Served | LTR | LTR | L | T | TR | L | T | T | R |
| Maximum Queue $(m)$ | 33.3 | 61.1 | 13.8 | 51.4 | 59.5 | 55.2 | 74.9 | 55.5 | 6.7 |
| Average Queue $(m)$ | 15.8 | 23.2 | 2.7 | 25.0 | 31.4 | 27.1 | 43.1 | 25.0 | 0.2 |
| 95th Queue $(\mathrm{m})$ | 30.6 | 47.5 | 9.3 | 46.4 | 53.8 | 47.6 | 66.6 | 50.8 | 3.4 |
| Link Distance $(\mathrm{m})$ | 244.6 | 305.1 |  | 296.6 | 296.6 |  | 1000.6 | 1000.6 |  |
| Upstream BIk Time $(\%)$ |  |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  | 80.0 |  |  | 140.0 |  | 180.0 |  |
| Storage Bay Dist $(m)$ |  |  |  |  |  |  |  |  |  |

Intersection: 3: Davis Road \& Lundys Lane

| Movement | EB | EB | WB | WB | WB | NB | NB | SB | SB | SB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Directions Served | L | TR | L | T | R | L | TR | L | T | R |
| Maximum Queue (m) | 69.8 | 119.3 | 20.8 | 156.5 | 65.6 | 28.4 | 73.3 | 118.4 | 66.7 | 45.6 |
| Average Queue (m) | 30.0 | 63.4 | 6.0 | 85.6 | 19.2 | 11.3 | 36.2 | 64.9 | 22.3 | 15.7 |
| 95 th Queue (m) | 56.6 | 104.9 | 16.6 | 133.8 | 42.9 | 23.1 | 63.0 | 103.9 | 48.9 | 34.2 |
| Link Distance ( m ) |  | 266.3 |  | 1920.7 |  |  | 458.7 |  | 610.8 |  |
| Upstream BIk Time (\%) |  |  |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |  |  |  |
| Storage Bay Dist (m) | 85.0 |  | 65.0 |  | 80.0 | 55.0 |  | 90.0 |  | 100.0 |
| Storage Blk Time (\%) | 0 | 3 |  | 17 |  |  | 3 | 3 | 0 |  |
| Queuing Penalty (veh) | 2 | 5 |  | 45 |  |  | 1 | 9 | 0 |  |

Queuing and Blocking Report
<2025 Total - Thorold Townline> PM Peak Hour

Intersection: 4: Thorold Townline Road \& Thorold Stone Road

| Movement | EB | EB | EB | EB | B24 | B24 | WB | WB | WB | WB | NB | NB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Directions Served | L | T | T | R | T | T | L | T | T | R | L | TR |
| Maximum Queue (m) | 91.7 | 134.1 | 132.0 | 24.7 | 128.9 | 129.8 | 37.8 | 118.1 | 107.4 | 19.8 | 72.0 | 104.0 |
| Average Queue (m) | 45.9 | 87.5 | 90.0 | 11.1 | 6.4 | 4.3 | 15.3 | 69.2 | 59.0 | 5.4 | 27.8 | 46.9 |
| 95th Queue (m) | 79.3 | 125.7 | 126.2 | 23.5 | 80.6 | 65.8 | 31.0 | 103.7 | 93.8 | 14.0 | 56.7 | 90.1 |
| Link Distance ( m ) |  | 279.0 | 279.0 |  | 315.3 | 315.3 |  | 338.6 | 338.6 |  |  | 1028.0 |
| Upstream Blk Time (\%) |  |  |  |  | 0 | 0 |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  | 0 | 2 |  |  |  |  |  |  |
| Storage Bay Dist (m) | 100.0 |  |  | 50.0 |  |  | 85.0 |  |  | 90.0 | 80.0 |  |
| Storage Blk Time (\%) | 0 | 6 | 32 |  |  |  |  | 4 | 1 |  | 0 |  |
| Queuing Penalty (veh) | 2 | 13 | 23 |  |  |  |  | 3 | 0 |  | 1 |  |

Intersection: 4: Thorold Townline Road \& Thorold Stone Road

| Movement | SB | SB |
| :---: | :---: | :---: |
| Directions Served | L | TR |
| Maximum Queue (m) | 54.7 | 152.9 |
| Average Queue (m) | 8.5 | 94.7 |
| 95 th Queue (m) | 33.0 | 146.4 |
| Link Distance ( m ) |  | 311.8 |
| Upstream BIk Time (\%) |  |  |
| Queuing Penalty (veh) |  |  |
| Storage Bay Dist ( m ) | 75.0 |  |
| Storage Blk Time (\%) |  | 21 |
| Queuing Penalty (veh) |  | 10 |

Intersection: 5: Thorold Townline Road \& Lundys Lane

| Movement | EB | EB | EB | WB | WB | NB | NB | SB | SB | SB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Directions Served | L | T | R | L | TR | L | TR | L | T | R |
| Maximum Queue (m) | 42.6 | 71.4 | 51.6 | 21.7 | 92.9 | 55.8 | 71.0 | 40.1 | 56.4 | 37.0 |
| Average Queue (m) | 15.5 | 27.4 | 5.8 | 6.3 | 43.8 | 23.9 | 32.3 | 15.2 | 24.9 | 15.1 |
| 95th Queue (m) | 32.8 | 60.1 | 25.7 | 15.6 | 78.1 | 44.3 | 58.8 | 31.1 | 46.9 | 30.0 |
| Link Distance ( m ) | 1920.7 |  |  | 479.5 |  | 741.7 |  | 1500.2 |  |  |
| Upstream BIk Time (\%) |  |  |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |  |  |  |
| Storage Bay Dist (m) | 90.0 |  | 20.0 | 55.0 |  | 25.0 |  | 25.0 |  | 30.0 |
| Storage Blk Time (\%) |  | 10 | 0 |  | 4 | 14 | 17 | 4 | 10 | 1 |
| Queuing Penalty (veh) |  | 18 | 1 |  | 2 | 26 | 19 | 11 | 18 | 1 |

Intersection: 6: Thorold Townline Road \& Beaverdams Road


Intersection: 1: Davis Road \& Thorold Stone Road

| Movement | EB | EB | EB | EB | WB | WB | WB | NB | NB | NB | SB | SB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Directions Served | L | T | T | R | L | T | TR | L | LT | R | L |  |
| Maximum Queue (m) | 16.4 | 94.8 | 144.2 | 36.2 | 46.9 | 115.2 | 118.0 | 120.3 | 123.3 | 75.4 | 1.0 | 6.0 |
| Average Queue (m) | 4.1 | 59.6 | 51.6 | 1.2 | 21.1 | 75.5 | 79.6 | 71.2 | 76.0 | 5.9 | 0.0 | 0.7 |
| 95th Queue (m) | 11.8 | 87.3 | 118.8 | 19.1 | 38.8 | 106.8 | 109.5 | 112.7 | 116.9 | 42.6 | 0.8 | 4.1 |
| Link Distance (m) |  | 367.0 | 367.0 |  |  | 315.3 | 315.3 | 1000.6 | 1000.6 |  |  | 265.6 |
| Upstream Blk Time (\%) |  |  | 0 |  |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  | 0 |  |  |  |  |  |  |  |  |  |
| Storage Bay Dist ( m ) | 105.0 |  |  | 50.0 | 70.0 |  |  |  |  | 80.0 | 30.0 |  |
| Storage Blk Time (\%) |  | 0 | 5 | 0 |  | 9 |  |  | 8 |  |  |  |
| Queuing Penalty (veh) |  | 0 | 15 | 0 |  | 10 |  |  | 21 |  |  |  |

ntersection: 2: Davis Road \& Niagara Falls Road/Beaverdams Road

| Movement | EB | WB | NB | NB | NB | SB | SB | SB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Directions Served | LTR | LTR | L | T | TR | L | T | T |
| Maximum Queue (m) | 45.1 | 55.7 | 24.8 | 81.7 | 82.4 | 33.2 | 63.8 | 51.5 |
| Average Queue (m) | 19.3 | 21.1 | 6.5 | 43.9 | 47.6 | 15.8 | 32.3 | 17.6 |
| 95th Queue (m) | 38.5 | 44.4 | 18.2 | 72.4 | 75.3 | 29.6 | 54.1 | 42.1 |
| Link Distance (m) | 244.6 | 305.1 |  | 296.6 | 296.6 |  | 1000.6 | 1000.6 |
| Upstream BIk Time (\%) |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |  |
| Storage Bay Dist (m) |  |  | 80.0 |  |  | 140.0 |  |  |
| Storage BIk Time (\%) |  |  |  | 0 |  |  |  |  |
| Queuing Penalty (veh) |  |  |  | 0 |  |  |  |  |

Intersection: 3: Davis Road \& Lundys Lane


Queuing and Blocking Report

Intersection: 4: Thorold Townline Road \& Thorold Stone Road

|  |  |  |  |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Movement | EB | EB | EB | EB | B24 | B24 | WB | WB | WB | WB | NB | NB |
| Directions Served | L | T | T | R | T | T | L | T | T | R | L | TR |
| Maximum Queue $(m)$ | 125.9 | 105.8 | 109.0 | 45.6 | 65.6 | 325.7 | 113.2 | 154.1 | 144.6 | 26.6 | 61.6 | 86.1 |
| Average Queue $(m)$ | 72.8 | 62.0 | 64.8 | 20.9 | 2.2 | 12.9 | 51.5 | 81.1 | 70.8 | 9.3 | 23.4 | 32.2 |
| 95th Queue $(m)$ | 116.8 | 92.6 | 94.7 | 37.8 | 46.2 | 117.6 | 106.0 | 136.6 | 118.0 | 19.7 | 47.8 | 66.1 |
| Link Distance $(m)$ |  | 279.0 | 279.0 |  | 315.3 | 315.3 |  | 338.6 | 338.6 |  |  | 1028.0 |
| Upstream Blk Time $(\%)$ |  |  |  |  | 0 | 0 |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  | 0 | 2 |  |  |  |  |  |  |
| Storage Bay Dist $(m)$ | 100.0 |  |  | 50.0 |  |  | 85.0 |  |  | 90.0 | 80.0 |  |
| Storage Blk Time $(\%)$ | 4 | 1 | 26 | 0 |  |  | 5 | 6 | 1 |  | 0 | 0 |
| Queuing Penalty (veh) | 15 | 2 | 41 | 0 |  |  | 23 | 11 | 1 |  | 1 | 1 |

ntersection: 4: Thorold Townline Road \& Thorold Stone Road

| Movement | SB | SB |
| :---: | :---: | :---: |
| Directions Served | L | TR |
| Maximum Queue (m) | 89.2 | 197.2 |
| Average Queue (m) | 13.3 | 119.1 |
| 95th Queue (m) | 54.1 | 192.3 |
| Link Distance ( $m$ ) |  | 311.8 |
| Upstream BIk Time (\%) |  |  |
| Queuing Penalty (veh) |  |  |
| Storage Bay Dist (m) | 75.0 |  |
| Storage Blk Time (\%) |  | 33 |
| Queuing Penalty (veh) |  | 17 |

Intersection: 5: Thorold Townline Road \& Lundys Lane

| Movement | EB | EB | EB | WB | WB | NB | NB | SB | SB | SB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Directions Served | L | T | R | L | TR | L | TR | L | T | R |
| Maximum Queue (m) | 75.3 | 86.3 | 50.4 | 19.5 | 77.5 | 59.1 | 78.7 | 37.8 | 50.6 | 35.8 |
| Average Queue (m) | 31.6 | 37.8 | 6.6 | 5.4 | 34.8 | 16.6 | 25.9 | 10.9 | 17.9 | 11.4 |
| 95th Queue (m) | 59.6 | 72.4 | 24.2 | 14.0 | 66.1 | 36.5 | 54.1 | 26.6 | 37.6 | 27.4 |
| Link Distance (m) | 1920.7 |  |  | 479.5 |  |  | 741.7 | 1500.2 |  |  |
| Upstream BIk Time (\%) |  |  |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |  |  |  |
| Storage Bay Dist (m) | 90.0 |  | 20.0 | 55.0 |  | 25.0 |  | 25.0 |  | 30.0 |
| Storage BIk Time (\%) | 0 | 14 | 0 |  | 2 | 6 | 14 | 2 | 6 | 1 |
| Queuing Penalty (veh) | 0 | 43 | 1 |  | 1 | 10 | 11 | 4 | 7 | 1 |


| Movement | EB | WB | NB | SB |
| :---: | :---: | :---: | :---: | :---: |
| Directions Served | LTR | LTR | LTR | LTR |
| Maximum Queue ( m ) | 54.0 | 72.8 | 102.5 | 119.0 |
| Average Queue (m) | 24.5 | 34.3 | 43.5 | 56.4 |
| 95th Queue (m) | 44.8 | 59.6 | 84.6 | 99.1 |
| Link Distance ( m ) | 192.4 | 256.5 | 1091.4 | 1028.0 |
| Upstream Bik Time (\%) |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |
| Storage Bay Dist (m) |  |  |  |  |
| Storage B1k Time (\%) |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |
| Intersection: 7: | Id To | nline | Road | \& Upp |
| Movement |  |  |  |  |
| Directions Served |  |  |  |  |
| Maximum Queue ( m ) |  |  |  |  |
| Average Queue (m) |  |  |  |  |
| 95th Queue (m) |  |  |  |  |
| Link Distance ( m ) |  |  |  |  |
| Upstream Bik Time (\%) |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |
| Storage Bay Dist (m) |  |  |  |  |
| Storage Bik Time (\%) |  |  |  |  |
| Queuing Penalty (veh |  |  |  |  |
| Network Summ |  |  |  |  |
| Network wide Queuing | : 242 |  |  |  |

Intersection: 1: Davis Road \& Thorold Stone Road

| Movement | EB | EB | EB | EB | WB | WB | WB | NB | NB | NB | SB | SB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Directions Served | L | T | T | R | L | T | TR | L | LT | R | L | T |
| Maximum Queue (m) | 24.7 | 146.4 | 150.1 | 111.5 | 72.5 | 111.3 | 112.8 | 114.9 | 116.3 | 87.8 | 3.9 | 11.8 |
| Average Queue (m) | 4.8 | 85.3 | 75.6 | 17.7 | 34.7 | 70.6 | 73.8 | 78.0 | 80.3 | 5.9 | 0.5 | 2.3 |
| 95th Queue (m) | 15.3 | 130.8 | 128.5 | 72.7 | 60.8 | 98.6 | 101.3 | 109.9 | 112.3 | 39.9 | 2.8 | 8.2 |
| Link Distance (m) |  | 367.0 | 367.0 |  |  | 315.3 | 315.3 | 1000.6 | 1000.6 |  |  | 265.6 |
| Upstream Blk Time (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Storage Bay Dist (m) | 105.0 |  |  | 50.0 | 70.0 |  |  |  |  | 80.0 | 30.0 |  |
| Storage BIk Time (\%) |  | 4 | 17 | 1 | 0 | 7 |  |  | 12 |  |  |  |
| Queuing Penalty (veh) |  | 1 | 122 | 7 | 3 | 14 |  |  | 22 |  |  |  |

ntersection: 2: Davis Road \& Niagara Falls Road/Beaverdams Road

| Movement | EB | WB | NB | NB | NB | SB | SB | SB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Directions Served | LTR | LTR | L | T | TR | L | T | T |
| Maximum Queue (m) | 50.9 | 62.2 | 19.3 | 65.8 | 71.4 | 60.2 | 88.2 | 80.5 |
| Average Queue (m) | 19.1 | 29.5 | 6.0 | 31.0 | 36.2 | 26.7 | 52.0 | 35.9 |
| 95th Queue (m) | 38.5 | 55.6 | 15.4 | 56.8 | 62.9 | 47.7 | 79.1 | 69.7 |
| Link Distance ( $m$ ) | 244.6 | 305.1 |  | 296.6 | 296.6 |  | 1000.6 | 1000.6 |
| Upstream BIk Time (\%) |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |  |
| Storage Bay Dist (m) |  |  | 80.0 |  |  | 140.0 |  |  |
| Storage Blk Time (\%) |  |  |  | 0 |  |  |  |  |
| Queuing Penalty (veh) |  |  |  | 0 |  |  |  |  |

Intersection: 3: Davis Road \& Lundys Lane

| Movement | EB | EB | WB | WB | WB | NB | NB | SB | SB | SB | B9 | B27 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Directions Served | L | TR | L | T | R | L | TR | L | T | R | T | T |
| Maximum Queue (m) | 119.8 | 170.0 | 113.5 | 239.1 | 107.4 | 37.0 | 84.6 | 169.3 | 301.6 | 127.4 | 30.4 | 54.3 |
| Average Queue (m) | 66.9 | 81.2 | 20.1 | 121.2 | 33.4 | 12.2 | 41.5 | 131.7 | 136.3 | 32.7 | 10.8 | 10.2 |
| 95th Queue (m) | 140.2 | 143.4 | 78.6 | 219.8 | 111.5 | 26.9 | 71.5 | 211.1 | 438.3 | 80.7 | 72.3 | 80.2 |
| Link Distance ( m ) |  | 266.3 |  | 1920.7 |  |  | 458.7 |  | 610.8 |  | 119.0 | 466.3 |
| Upstream BIk Time (\%) |  |  |  |  |  |  |  |  | 5 |  | 4 |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |  | 42 |  | 34 |  |
| Storage Bay Dist (m) | 85.0 |  | 65.0 |  | 80.0 | 55.0 |  | 90.0 |  | 100.0 |  |  |
| Storage Blk Time (\%) | 25 | 5 |  | 26 |  | 0 | 5 | 60 |  | 0 |  |  |
| Queuing Penalty (veh) | 187 | 10 |  | 67 |  | 0 | 2 | 186 |  | 0 |  |  |

Queuing and Blocking Report
<2035 Background> PM Peak Hour

Intersection: 4: Thorold Townline Road \& Thorold Stone Road

| Movement | EB | EB | EB | EB | B24 | B24 | WB | WB | WB | WB | NB | NB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Directions Served | L | T | T | R | T | T | L | T | T | R | L | TR |
| Maximum Queue (m) | 83.9 | 144.4 | 147.4 | 50.2 | 187.9 | 261.7 | 42.2 | 131.8 | 125.5 | 18.0 | . 9 | 142.3 |
| Average Queue (m) | 46.8 | 105.5 | 109.2 | 11.2 | 8.3 | 13.1 | 19.8 | 89.0 | 79.7 | 4.8 | 35.6 | 72.4 |
| 95th Queue (m) | 78.6 | 139.6 | 143.1 | 32.3 | 91.4 | 118.7 | 36.0 | 126.2 | 117.5 | 13.3 | 75. | 130.0 |
| Link Distance ( m ) |  | 279.0 | 279.0 |  | 315.3 | 315.3 |  | 338.6 | 338.6 |  |  | 1028.0 |
| Upstream Blk Time (\%) |  |  |  |  | 0 | 0 |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  | 0 | 3 |  |  |  |  |  |  |
| Storage Bay Dist ( $m$ ) | 100.0 |  |  | 50.0 |  |  | 85.0 |  |  | 90.0 | 80.0 |  |
| Storage Bik Time (\%) | 0 | 13 | 38 |  |  |  |  | 13 | 4 |  | 0 |  |
| Queuing Penalty (veh) | 0 | 30 | 30 |  |  |  |  | 13 | 2 |  | 1 |  |

ntersection: 4: Thorold Townline Road \& Thorold Stone Road


Intersection: 5: Thorold Townline Road \& Lundys Lane

| Movement | EB | EB | EB | WB | WB | NB | NB | SB | SB | SB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Directions Served | L | T | R | L | TR | L | TR | L | T | R |
| Maximum Queue (m) | 73.4 | 87.0 | 49.6 | 24.7 | 110.3 | 61.2 | 93.1 | 59.0 | 67.8 | 57.2 |
| Average Queue (m) | 29.5 | 43.2 | 5.9 | 6.7 | 60.3 | 29.8 | 39.2 | 24.4 | 26.2 | 27.3 |
| 95th Queue (m) | 60.3 | 73.8 | 23.4 | 17.3 | 101.3 | 52.3 | 67.9 | 46.4 | 53.1 | 50.1 |
| Link Distance ( m ) | 1920.7 |  |  | 479.5 |  |  | 741.7 | 1500.2 |  |  |
| Upstream B1k Time (\%) |  |  |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |  |  |  |
| Storage Bay Dist (m) | 90.0 |  | 20.0 | 55.0 |  | 25.0 |  | 25.0 |  | 30.0 |
| Storage BIk Time (\%) | 0 | 15 | 0 |  | 9 | 29 | 24 | 16 | 10 | 8 |
| Queuing Penalty (veh) | 2 | 35 | 0 |  | 4 | 56 | 28 | 49 | 26 | 17 |



Intersection: 1: Davis Road \& Thorold Stone Road

| Movement | EB | EB | EB | WB | WB | WB | NB | NB | NB | SB | SB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Directions Served | L | T | T | L | T | TR | L | LT | R | L | T |
| Maximum Queue (m) | 18.4 | 84.8 | 73.3 | 89.9 | 122.7 | 107.3 | 101.0 | 106.7 | 49.8 | 1.9 | 7.6 |
| Average Queue (m) | 3.7 | 47.1 | 33.0 | 43.9 | 74.0 | 74.8 | 67.8 | 70.9 | 3.6 | 0.1 | 0.6 |
| 95th Queue (m) | 12.5 | 75.9 | 63.6 | 103.5 | 104.7 | 102.0 | 95.5 | 97.6 | 23.8 | 1.3 | 4.4 |
| Link Distance ( m ) |  | 367.0 | 367.0 |  | 315.3 | 315.3 | 1000.6 | 1000.6 |  |  | 265.6 |
| Upstream BIk Time (\%) |  |  |  |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |  |  |  |  |
| Storage Bay Dist (m) | 105.0 |  |  | 70.0 |  |  |  |  | 80.0 | 30.0 |  |
| Storage Blk Time (\%) |  |  | 2 | 13 | 9 |  |  | 3 |  |  |  |
| Queuing Penalty (veh) |  |  | 6 | 75 | 11 |  |  | 9 |  |  |  |

ntersection: 2: Davis Road \& Niagara Falls Road/Beaverdams Road

| Movement | EB | WB | NB | NB | NB | SB | SB | SB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Directions Served | LTR | LTR | L | T | TR | L | T | T |
| Maximum Queue (m) | 41.9 | 54.6 | 30.4 | 78.2 | 85.3 | 36.7 | 82.0 | 66.4 |
| Average Queue (m) | 19.5 | 19.5 | 7.0 | 43.7 | 47.1 | 16.0 | 36.9 | 19.8 |
| 95th Queue (m) | 36.6 | 41.8 | 21.4 | 68.7 | 75.7 | 31.3 | 65.4 | 47.6 |
| Link Distance (m) | 244.6 | 305.1 |  | 296.6 | 296.6 |  | 1000.6 | 1000.6 |
| Upstream BIk Time (\%) |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |  |
| Storage Bay Dist (m) |  |  | 80.0 |  |  | 140.0 |  |  |
| Storage BIk Time (\%) |  |  |  | 0 |  |  |  |  |
| Queuing Penalty (veh) |  |  |  | 0 |  |  |  |  |

Intersection: 3: Davis Road \& Lundys Lane

| Movement | EB | EB | WB | WB | WB | NB | NB | SB | SB | SB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Directions Served | L | TR | L | T | R | L | TR | L | T | R |
| Maximum Queue (m) | 50.4 | 86.7 | 33.7 | 79.4 | 25.0 | 26.2 | 65.6 | 84.2 | 69.5 | 62.4 |
| Average Queue (m) | 23.1 | 40.3 | 11.4 | 38.2 | 9.6 | 5.8 | 28.6 | 36.3 | 20.4 | 18.3 |
| 95th Queue (m) | 42.3 | 74.5 | 26.1 | 71.1 | 20.8 | 17.7 | 54.3 | 69.7 | 49.5 | 41.4 |
| Link Distance ( m ) |  | 266.3 |  | 1920.7 |  |  | 458.7 |  | 610.8 |  |
| Upstream Blk Time (\%) |  |  |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |  |  |  |
| Storage Bay Dist ( $m$ ) | 85.0 |  | 65.0 |  | 80.0 | 55.0 |  | 90.0 |  | 100.0 |
| Storage Blk Time (\%) |  | 0 |  | 1 |  |  | 2 | 1 | 0 |  |
| Queuing Penalty (veh) |  | 0 |  | 2 |  |  | 0 | 2 | 0 |  |

Queuing and Blocking Report
<2035 Total - Thorold Townline> AM Peak Hour

Intersection: 4: Thorold Townline Road \& Thorold Stone Road

| Movement | EB | EB | EB | EB | B24 | B24 | WB | WB | WB | WB | NB | NB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Directions Served | L | T | T | R | T | T | L | T | T | R | L | TR |
| Maximum Queue (m) | 149.6 | 110.0 | 110.2 | 76.5 | 62.4 | 64.6 | 126.0 | 151.1 | 140.4 | 20.8 | 76.6 | 101.2 |
| Average Queue (m) | 73.8 | 67.8 | 70.9 | 27.2 | 2.1 | 2.2 | 56.8 | 102.1 | 95.3 | 8.6 | 33.0 | 44.7 |
| 95th Queue (m) | 116.7 | 98.3 | 100.9 | 53.6 | 44.0 | 45.5 | 103.8 | 145.3 | 138.0 | 17.9 | 66.1 | 88.7 |
| Link Distance ( m ) |  | 279.0 | 279.0 |  | 315.3 | 315.3 |  | 338.6 | 338.6 |  |  | 1028.0 |
| Upstream Blk Time (\%) |  |  |  |  |  | 0 |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  | 1 |  |  |  |  |  |  |
| Storage Bay Dist ( m ) | 100.0 |  |  | 50.0 |  |  | 85.0 |  |  | 90.0 | 80.0 |  |
| Storage Bik Time (\%) | 3 | 1 | 31 | 1 |  |  | 5 | 27 | 16 |  | 0 |  |
| Queuing Penalty (veh) | 13 | 2 | 55 | 5 |  |  | 20 | 58 | 11 |  |  |  |

ntersection: 4: Thorold Townline Road \& Thorold Stone Road

| Movement | SB | SB |
| :---: | :---: | :---: |
| Directions Served | L | TR |
| Maximum Queue ( m ) | 146.5 | 276.7 |
| Average Queue (m) | 32.7 | 147.4 |
| 95th Queue (m) | 123.0 | 270.7 |
| Link Distance ( $m$ ) |  | 311.8 |
| Upstream Blk Time (\%) |  | 2 |
| Queuing Penalty (veh) |  | 0 |
| Storage Bay Dist ( $m$ ) | 75.0 |  |
| Storage BIk Time (\%) |  | 43 |
| Queuing Penalty (veh) |  | 22 |

Intersection: 5: Thorold Townline Road \& Lundys Lane

| Movement | EB | EB | EB | WB | WB | NB | NB | SB | SB | SB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Directions Served | L | T | R | L | TR | L | TR | L | T | R |
| Maximum Queue (m) | 68.9 | 98.4 | 51.3 | 21.6 | 77.7 | 51.2 | 60.1 | 26.6 | 39.3 | 36.5 |
| Average Queue (m) | 33.6 | 36.0 | 8.7 | 6.3 | 36.3 | 14.7 | 28.6 | 10.0 | 16.4 | 12.8 |
| 95th Queue (m) | 61.1 | 73.1 | 34.1 | 16.0 | 65.8 | 34.2 | 50.7 | 21.8 | 35.5 | 27.3 |
| Link Distance ( $m$ ) | 1920.7 |  |  | 479.5 |  |  | 741.7 | 1500.2 |  |  |
| Upstream Blk Time (\%) |  |  |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |  |  |  |
| Storage Bay Dist (m) | 90.0 |  | 20.0 | 55.0 |  | 25.0 |  | 25.0 |  | 30.0 |
| Storage Blk Time (\%) | 0 | 14 | 0 |  | 1 | 4 | 16 | 1 | 5 | 1 |
| Queuing Penalty (veh) | 0 | 44 | 1 |  | 1 | 7 | 12 | 2 | 6 | 1 |

Intersection: 6: Thorold Townline Road \& Beaverdams Road


Intersection: 1: Davis Road \& Thorold Stone Road

| Movement | EB | EB | EB | EB | WB | WB | WB | NB | NB | NB | SB | SB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Directions Served | L | T | T | R | L | T | TR | L | LT | R | L | T |
| Maximum Queue (m) | 19.4 | 194.8 | 191.0 | 103.4 | 68.8 | 116.8 | 115.4 | 157.8 | 168.8 | 122.0 | 10.0 | 10.3 |
| Average Queue (m) | 4.7 | 92.0 | 80.5 | 16.4 | 36.2 | 75.7 | 77.7 | 94.7 | 97.9 | 18.3 | 1.2 | 2.0 |
| 95th Queue (m) | 14.5 | 161.4 | 143.6 | 71.5 | 61.6 | 102.2 | 103.8 | 141.5 | 146.4 | 86.4 | 5.9 | 7.3 |
| Link Distance (m) |  | 367.0 | 367.0 |  |  | 315.3 | 315.3 | 1000.6 | 1000.6 |  |  | 265.6 |
| Upstream BIk Time (\%) |  | 0 | 0 |  |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  | 0 | 0 |  |  |  |  |  |  |  |  |  |
| Storage Bay Dist (m) | 105.0 |  |  | 50.0 | 70.0 |  |  |  |  | 80.0 | 30.0 |  |
| Storage BIk Time (\%) |  | 5 | 20 | 1 | 0 | 9 |  |  | 28 |  |  |  |
| Queuing Penalty (veh) |  | 1 | 146 | 7 | 3 | 19 |  |  | 51 |  |  |  |

ntersection: 2: Davis Road \& Niagara Falls Road/Beaverdams Road

| Movement | EB | WB | NB | NB | NB | SB | SB | SB | SB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Directions Served | LTR | LTR | L | T | TR | L | T | T | R |
| Maximum Queue (m) | 52.2 | 67.3 | 18.7 | 66.7 | 76.4 | 62.4 | 93.7 | 83.5 | 6.7 |
| Average Queue (m) | 20.3 | 28.9 | 6.1 | 32.6 | 38.2 | 29.9 | 51.3 | 33.8 | 0.2 |
| 95 th Queue (m) | 40.2 | 57.6 | 15.0 | 58.1 | 65.1 | 53.2 | 79.2 | 66.8 | 3.4 |
| Link Distance ( m ) | 244.6 | 305.1 |  | 296.6 | 296.6 |  | 1000.6 | 1000.6 |  |
| Upstream B1k Time (\%) |  |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |  |  |
| Storage Bay Dist (m) |  |  | 80.0 |  |  | 140.0 |  |  | 180.0 |
| Storage BIk Time (\%) |  |  |  | 0 |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  | 0 |  |  |  |  |  |

Intersection: 3: Davis Road \& Lundys Lane

| Movement | EB | EB | WB | WB | WB | NB | NB | SB | SB | SB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Directions Served | L | TR | L | T | R | L | TR | L | T | R |
| Maximum Queue (m) | 82.6 | 143.3 | 82.6 | 191.2 | 86.9 | 27.8 | 81.9 | 173.1 | 248.3 | 81.8 |
| Average Queue (m) | 40.8 | 67.8 | 13.4 | 109.6 | 27.0 | 12.1 | 39.5 | 108.8 | 75.5 | 28.7 |
| 95th Queue (m) | 71.9 | 115.4 | 51.7 | 196.5 | 90.1 | 23.2 | 69.2 | 190.9 | 265.3 | 60.5 |
| Link Distance ( m ) |  | 266.3 |  | 1920.7 |  |  | 458.7 |  | 610.8 |  |
| Upstream BIk Time (\%) |  |  |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |  |  |  |
| Storage Bay Dist (m) | 85.0 |  | 65.0 |  | 80.0 | 55.0 |  | 90.0 |  | 100.0 |
| Storage BIk Time (\%) | 1 | 4 |  | 23 |  |  | 4 | 45 | 0 |  |
| Queuing Penalty (veh) | 7 | 8 |  | 59 |  |  | 2 | 138 | 0 |  |

Queuing and Blocking Report
<2035 Total - Thorold Townline> PM Peak Hour

Intersection: 4: Thorold Townline Road \& Thorold Stone Road

| Movement | EB | EB | EB | EB | B24 | B24 | WB | WB | WB | WB | NB | NB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Directions Served | L | T | T | R | T | T | L | , | T | R | L | TR |
| Maximum Queue (m) | 93.2 | 147.9 | 158.6 | 125.3 | 63.9 | 64.2 | 92.1 | 157.7 | 148.1 | 20.6 | 69.2 | 119.9 |
| Average Queue (m) | 51.7 | 113.6 | 116.7 | 21.1 | 4.2 | 6.3 | 26.9 | 100.5 | 91.3 | 4.9 | 35.1 | 68.9 |
| 95th Queue (m) | 83.2 | 146.9 | 150.0 | 72.3 | 63.7 | 79.0 | 60.1 | 143.8 | 135.1 | 13.9 | 62.4 | 113.2 |
| Link Distance ( m ) |  | 279.0 | 279.0 |  | 315.3 | 315.3 |  | 338.6 | 338.6 |  |  | 1028.0 |
| Upstream Blk Time (\%) |  |  |  |  | 0 | 0 |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  | 0 | 0 |  |  |  |  |  |  |
| Storage Bay Dist (m) | 100.0 |  |  | 50.0 |  |  | 85.0 |  |  | 90.0 | 80.0 |  |
| Storage Blk Time (\%) | 0 | 20 | 43 |  |  |  | 0 | 21 | 10 |  | 0 |  |
| Queuing Penalty (veh) | 0 | 47 | 42 |  |  |  | 0 | 24 | 4 |  | 0 |  |

ntersection: 4: Thorold Townline Road \& Thorold Stone Road

| Movement | SB | SB |
| :---: | :---: | :---: |
| Directions Served | L | TR |
| Maximum Queue ( m ) | 174.9 | 304.0 |
| Average Queue (m) | 56.7 | 202.6 |
| 95th Queue (m) | 182.7 | 346.1 |
| Link Distance ( m ) |  | 311.8 |
| Upstream Blk Time (\%) |  | 13 |
| Queuing Penalty (veh) |  | 0 |
| Storage Bay Dist ( $m$ ) | 75.0 |  |
| Storage BIk Time (\%) |  | 61 |
| Queuing Penalty (veh) |  | 29 |

Intersection: 5: Thorold Townline Road \& Lundys Lane

| Movement | EB | EB | EB | WB | WB | NB | NB | SB | SB | SB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Directions Served | L | T | R | L | TR | L | TR | L | T | R |
| Maximum Queue (m) | 90.0 | 86.4 | 40.5 | 23.0 | 125.6 | 60.9 | 82.2 | 66.0 | 80.4 | 61.0 |
| Average Queue (m) | 36.2 | 46.5 | 6.9 | 7.0 | 66.8 | 31.0 | 36.8 | 24.3 | 29.1 | 25.9 |
| 95th Queue (m) | 76.0 | 79.6 | 27.4 | 17.4 | 109.9 | 55.0 | 66.4 | 48.1 | 61.9 | 51.6 |
| Link Distance ( $m$ ) |  | 1920.7 |  |  | 479.5 |  | 741.7 |  | 500.2 |  |
| Upstream BIk Time (\%) |  |  |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |  |  |  |
| Storage Bay Dist (m) | 90.0 |  | 20.0 | 55.0 |  | 25.0 |  | 25.0 |  | 30.0 |
| Storage BIk Time (\%) | 2 | 16 | 0 |  | 11 | 29 | 23 | 16 | 11 | 7 |
| Queuing Penalty (veh) | 13 | 38 | 1 |  | 5 | 56 | 26 | 49 | 30 | 15 |

Intersection: 6: Thorold Townline Road \& Beaverdams Road


## APPENDIX E

Conceptual Site Access Design and Operations


PAVEMENT MARKING LEGEND

| PAVEMENT MARKING LEGEND |  |  |  |
| :---: | :---: | :---: | :---: |
| IDENTIFICATION | TYPE | COLOUR | WIDTH (cm) |
| 1 | SOLID | WHITE | 10 |
| 2 | $3-3-3$ BROKEN | WHITE | 10 |

PAVEMENT MARKING DENOTATION:
© PERMANENT

NOTES:

1) MEASUREMENTS IN METRES AND/OR MILLIMETRES UNLESS OTHERWISE SHOWN.
2) THIS DRAWING REPRESENTS A CONCEPTUAL DESIGN ONLY AND DOES NOT CONSIDER DETALLED TOPOGRAPHIC INFORMATION INCLUDING GRADING AND UTLITY LOCATIONS
3) LANE DIMENSIONS AS SHOWN REPRESENT THE MINIMUM CRITERIA AS PER THE 2017 TANASPRTATION OF CANADA TTACC GEOMETRIC DEEIIGN GUIDELING GR CANADII
TOADS. FINAL DIMENSIONS AND LAYOUT/ LOCATION OF AUXIIIRY LANES TO BE DETERMINED THROUGH DETALLED DESIGN AND CONSULTATION WITH MUNICIPAL STAFF

PROJECT No:
16137
16137
DATE:
SEPT. 2021


INBOUND LEFT TURN - OUTBOUND RIGHT TURN


INBOUND LEFT TURN - OUTBOUND RIGHT TURN


NOTES:

1) MEASUREMENTS IN METRES AND/OR MILLIMETRES UNLESS OTHERWISE SHOWN.
2) THIS DRAWING REPRESENTS A CONCEPTUAL DESIGN ONLY AND DOES NOT CONSIDER DETAILED TOPOGRAPHIC INFORMATION INCLUDING GRADING AND UTHITY LOCATIONS
3) WHILE THE PREFERRED AGGREGATE HAUL ROUTE IS TO THE NORTH VIA THOROLD TOWNLINE (THUS THE PROVISION OF A NORTHBOUND ACCELERATION LANE AND SOUTHBOUND LEFT-TURN LANE IN THE CONCEPTUAL DESIGN), OTHER FORMS OF SITE TRAFFIC MAY ACCESS THE QUARRY FROM THE SOUTH. A DEDICATED NORTHBOUND RIGHT TURN LANE HAS BEEN INCLUDED IN THE CONCEPTUAL DESIGN TO ACCOMMODATE NON-AGGRE

UPPERS QUARRY - THOROLD TOWNLINE ROAD
UPPERS LANE VEHICLE MOVEMENT DIAGRAM QUARRY TRUCK INBOUND AND OUTBOUND MANOEUVRES
${ }_{16137}^{\text {Project No: }}$
DATE:
SCALE:
1.500
VMD1

## APPENDIX F

## Sightline Assessment

Stopping sight distance is the sum of the distance travelled during the perception and reaction time and the braking distance.

$$
\begin{equation*}
\mathrm{SSD}=0.278 \mathrm{Vt}+0.039 \frac{\mathrm{~V}^{2}}{\mathrm{a}} \tag{2.5.2}
\end{equation*}
$$

Where:

$$
\begin{aligned}
\mathrm{SSD} & =\text { Stopping sight distance }(\mathrm{m}) \\
\mathrm{t} & =\text { Brake reaction time, } 2.5 \mathrm{~s} \\
\mathrm{~V} & =\text { Design speed }(\mathrm{km} / \mathrm{h}) \\
\mathrm{a} & =\text { Deceleration rate }\left(\mathrm{m} / \mathrm{s}^{2}\right)
\end{aligned}
$$

Table 2.5.2 gives the minimum stopping sight distances on level grade, on wet pavement, for a range of design speeds. These values are used for vertical curve design, intersection geometry and the placement of traffic control devices. The stopping sight distances quoted in Table 2.5.2 may need to be increased for a variety of reasons related to grade and vehicle type as noted below.

Table 2.5.2: Stopping Sight Distance on level roadways for Automobiles ${ }^{54}$

| $\begin{aligned} & \text { Design speed } \\ & (k m / h) \end{aligned}$ | Brake reaction distance ( $m$ ) | Braking distance on level (m) | Stopping sight distance |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  |  | Calculated (m) | Design (m) |
| 20 | 13.9 | 4.6 | 18.5 | 20 |
| 30 | 20.9 | 10.3 | 31.2 | 35 |
| 40 | 27.8 | 18.4 | 46.2 | 50 |
| 50 | 34.8 | 28.7 | 63.5 | 65 |
| 60 | 41.7 | 41.3 | 83.0 | 85 |
| 70 | 48.7 | 56.2 | 104.9 | 105 |
| 80 | 55.6 | 73.4 | 129.0 | 130 |
| 90 | 62.6 | 92.9 | 155.5 | 160 |
| 100 | 69.5 | 114.7 | 184.2 | 185 |
| 110 | 76.5 | 138.8 | 215.3 | 220 |
| 120 | 83.4 | 165.2 | 248.6 | 250 |
| 130 | 90.4 | 193.8 | 284.2 | 285 |

Note: Brake reaction distance predicated on a time of 2.5 s ; deceleration rate of $3.4 \mathrm{~m} / \mathrm{s}^{2}$ used to determine calculated sight distance.

## The Effect of Grade

Braking distances will increase on downgrades and decrease on upgrades. When the roadway is on a grade, formula 2.5.1 for braking distance is modified as follows:

$$
\begin{equation*}
d_{b}=\frac{V^{2}}{254[(a / 9.81)+G]} \tag{2.5.3}
\end{equation*}
$$

Where:

$$
\begin{aligned}
d_{b} & =\text { Braking distance }(\mathrm{m}) \\
\mathrm{V} & =\text { Design speed }(\mathrm{km} / \mathrm{h}) \\
\mathrm{a} & =\text { Deceleration rate }\left(\mathrm{m} / \mathrm{s}^{2}\right) \\
G & =G \text { rade }(\mathrm{m} / \mathrm{m})(G \text { is positive if vehicles uphill and negative if downhill })
\end{aligned}
$$

It has been noted that many drivers, particularly those in automobiles, do not compensate completely (i.e., by acceleration or deceleration) for the changes in speed caused by grade. It should also be noted that in many cases the sight distance available on downgrades is greater than on upgrades, which can help to provide the necessary corrections for grade. The following Table 2.5.3 summarizes the stopping sight distances on grades for a variety of design speeds.

Table 2.5.3: Stopping Sight Distance on Grades ${ }^{55}$

| Design Speed (km/h) | Stopping Sight Distance (m) |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Downgrades (\%) |  |  | Upgrades (\%) |  |  |
|  | 3 | 6 | 9 | 3 | 6 | 9 |
| 20 | 20 | 20 | 20 | 19 | 18 | 18 |
| 30 | 32 | 35 | 35 | 31 | 30 | 29 |
| 40 | 50 | 50 | 53 | 45 | 44 | 43 |
| 50 | 66 | 70 | 74 | 61 | 59 | 58 |
| 60 | 87 | 92 | 97 | 80 | 77 | 75 |
| 70 | 110 | 116 | 124 | 100 | 97 | 93 |
| 80 | 136 | 144 | 154 | 123 | 118 | 114 |
| 90 | 164 | 174 | 187 | 148 | 141 | 136 |
| 100 | 194 | 207 | 223 | 174 | 167 | 160 |
| 110 | 227 | 243 | 262 | 203 | 194 | 186 |
| 120 | 263 | 281 | 304 | 234 | 223 | 214 |
| 130 | 302 | 323 | 350 | 267 | 254 | 243 |

Limiting the sight distance to the stopping sight distance may preclude drivers from performing unusual, evasive maneuvers. Similarly, stopping sight distance may not provide drivers with enough visibility to allow them to piece together warning signals and decide on a course of action. Because decision sight distance allows drivers to maneuver their vehicles or vary their operating speed rather than stop, decision sight distance is much greater than stopping sight distance for a given design speed.

Designers should use decision sight distance wherever information may be perceived incorrectly, decisions are required, or control actions are required. Examples of situations where it could be desirable to provide decision sight distance include:

- Complex interchanges and intersections
- Locations where unusual or unexpected maneuvers occur
- Locations where significant changes to the roadway cross section are made
- Areas where there afe multiple demands on the driver's decision-making capabilities from road elements, traffic control devices, advertising, traffic, etc.
- Construction zones

Table 2.5.6 shows the range of values for decision sight distance. The decision sight distance increases with the complexity of the evasive action that is taken by the driver and with the complexity of the surroundings. The values for decision sight distance given in the table were developed from empirical data. When using these sight distances, the designer should consider eye and object heights appropriate for specific applications. Refer to Section 2.4.3.3 Driver Eye Height and Section 2.5.2.1 Object Height for additional information.

Table 2.5.6: Decision Sight Distance ${ }^{68}$

|  | Decision Sight Distance for Avoidance Maneuver (m) |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | A | B | C | D | E |
| 50 | 75 | 160 | 145 | 160 | 200 |
| 60 | 95 | 205 | 175 | 205 | 235 |
| 70 | 125 | 250 | 200 | 240 | 275 |
| 80 | 155 | 300 | 230 | 275 | 315 |
| 90 | 185 | 360 | 275 | 320 | 360 |
| 100 | 225 | 415 | 315 | 365 | 405 |
| 110 | 265 | 455 | 335 | 390 | 435 |
| $120+$ | 305 | 505 | 375 | 415 | 470 |


[^0]:    ppers Quarry Traffic Impact Study

[^1]:    ppers Quarry Traffic Impact Study

[^2]:    ppers Quarry Traffic Impact Study

[^3]:    ppers Quarry Traffic Impact Study

[^4]:    ppers Quarry Traffic Impact Study

[^5]:    ppers Quarry Traffic Impact Study
    tMIG

[^6]:    ppers Quarry Traffic Impact Study

[^7]:    ppers Quarry Traffic Impact Study

[^8]:    ppers Quarry Traffic Impact Study

[^9]:    ppers Quarry Traffic Impact Study

[^10]:    ppers Quarry Traffic Impact Study

[^11]:    Uppers Quarry Traffic Impact Study
    tMIG

[^12]:    Uppers Quarry Traffic Impact Study

[^13]:    ppers Quarry Traffic Impact Study

[^14]:    ppers Quarry Traffic Impact Study

[^15]:    ppers Quarry Traffic Impact Study

[^16]:    Uppers Quarry Traffic Impact Study
    tMIG

[^17]:    ppers Quarry Traffic Impact Study

[^18]:    ppers Quarry Traffic Impact Study

[^19]:    ppers Quarry Traffic Impact Study

[^20]:    Uppers Quarry Traffic Impact Study
    tMIG

[^21]:    Uppers Quarry Traffic Impact Study

[^22]:    ppers Quarry Traffic Impact Study

[^23]:    ppers Quarry Traffic Impact Study

[^24]:    ppers Quarry Traffic Impact Study

[^25]:    ppers Quarry Traffic Impact Study

[^26]:    ppers Quarry Traffic Impact Study

[^27]:    ppers Quarry Traffic Impact Study

[^28]:    Uppers Quarry Traffic Impact Study

[^29]:    Ippers Quarry Traffic Impact Study

[^30]:    ppers Quarry Traffic Impact Study

[^31]:    ppers Quarry Traffic Impact Study

[^32]:    ppers Quarry Traffic Impact Study

[^33]:    ppers Quarry Traffic Impact Study

[^34]:    ppers Quarry Traffic Impact Study

[^35]:    ppers Quarry Traffic Impact Study

[^36]:    ppers Quarry Traffic Impact Study

[^37]:    ppers Quarry Traffic Impact Study

[^38]:    Uppers Quarry Traffic Impact Study

[^39]:    ppers Quarry Traffic Impact Study

[^40]:    ppers Quarry Traffic Impact Study

[^41]:    ppers Quarry Traffic Impact Study

[^42]:    ppers Quarry Traffic Impact Study

[^43]:    Uppers Quarry Traffic Impact Study

[^44]:    ppers Quarry Traffic Impact Study

[^45]:    ppers Quarry Traffic Impact Study

[^46]:    ppers Quarry Traffic Impact Study

[^47]:    ppers Quarry Traffic Impact Study

[^48]:    ppers Quarry Traffic Impact Study

[^49]:    ppers Quarry Traffic Impact Study

[^50]:    Uppers Quarry Traffic Impact Study

[^51]:    ppers Quarry Traffic Impact Study

[^52]:    ppers Quarry Traffic Impact Study

[^53]:    ppers Quarry Traffic Impact Study

[^54]:    ppers Quarry Traffic Impact Study

[^55]:    ppers Quarry Traffic Impact Study

