TRAFFIC IMPACT STUDY

UPPER'S QUARRY

FINAL • OCTOBER 2021

REPORT PREPARED FOR

WALKER AGGREGATES INC. 1206 ROSEWARNE DRIVE THOROLD, ON L2V 3Y8

REPORT PREPARED BY



THE MUNICIPAL **TMIG** INFRASTRUCTURE GROUP LTD. 8800 DUFFERIN STREET, SUITE 200 VAUGHAN, ON L4K 0C5 (905) 738-5700

TMIG PROJECT NUMBER 16137





EXECUTIVE SUMMARY

The Municipal Infrastructure Group Ltd. (TMIG) was retained by Walker Aggregates Inc., to prepare a Traffic Impact Study (TIS) for the proposed Upper's Quarry. The proposed Upper's Quarry is located generally on lands situated south of Beaverdams Road, north of Lundy's Lane, west of Beechwood Road, and east of Thorold Townline Road, in the City of Niagara Falls, Region of Niagara, adjacent to City of Thorold.

The proposed Upper's Quarry has an approximate area of 106.3 hectares (262.7 acres) and an extraction area of 96.8 hectares (239.2 acres). The quarry is anticipated to have an annual extraction limit of 1.8 million tonnes of aggregate and a maximum annual production of 400,000 tonnes of asphalt from a portable asphalt plant to be located on-site.

The proposed Upper's Quarry access is proposed to be located at the Upper's Lane and Thorold Townline Road intersection. This proposed access is not dependent upon the sale of the Upper's Lane road allowance, as quarry traffic will either enter the site directly from this location on Thorold Townline Road, or travel to the same location via Upper's Lane. The proposed haul route will **not** make use of Beechwood Road to the east of Upper's Lane.

Two possible routes have been considered as appropriate 'haul routes' for material that will be shipped from the proposed Upper's Quarry to serve local and broader markets.

Haul Route Option 1

The first option of a haul route for trucks to / from Upper's Quarry would utilize Thorold Townline Road to the north of the site, as it is a regional road and provides the most direct route to / from the quarry. The haul route includes the following roads:

- Thorold Townline Road north of the site access to Thorold Stone Road
- Highway 406 via Thorold Stone Road westbound
- Queen Elizabeth Way (QEW) via Taylor Rd northbound
- Queen Elizabeth Way (QEW) via Thorold Stone Road eastbound

Haul Route Option 2

Davis Road is designated as a provincial highway and is a major boundary road in close proximity to the site. Accordingly, it can also be considered an appropriate roadway to accommodate truck traffic to / from the quarry. The use of Davis Road as a second option for a haul route would result in a more circuitous haul route, as access to Davis Road would require quarry trucks to first travel south on Thorold Townline Road to Lundy's Lane, and then proceed west to Davis Road. The second haul route option includes the following roadways:

- Thorold Townline Road south of the site access to Lundy's Lane
- Lundy's Lane west to Davis Road
- Davis Road north to Thorold Stone Road
- Highway 406 via Thorold Stone Road westbound
- Queen Elizabeth Way (QEW) via Thorold Stone Road (eastbound) and Taylor Road northbound
- Queen Elizabeth Way (QEW) via Thorold Stone Road eastbound

Based on analysis results for both haul routes and the future transportation network, TMIG recommends that Haul Route Option 1 be chosen as the preferred Haul Route, subject to approval by the Town and an appraisal of the cost of any road improvements potentially required to accommodate truck traffic.

Haul Route Option 1 will also be seen as a preferable route by current and future residents within the vicinity of the proposed Upper's Quarry, as the Rolling Meadows Secondary Plan area represents a large amount of future residential traffic that will travel along Davis Road and Lundy's Lane. As such, it would be ideal to have truck traffic travel north directly on Thorold Townline Road (Haul Route Option 1), compared to the more circuitous route around the boundary of the future Rolling Meadows area (Haul Route Option 2).



The traffic analysis considers traffic conditions at planning horizon years of 2025 and 2035. It is assumed that the proposed Upper's Quarry will be fully operational by the 2025 study horizon year. There are no planned changes to the existing local road network in the immediate vicinity of the proposed Upper's Quarry.

Two background developments were identified that are expected to be built-out by the 2035 planning horizon, and have been included in traffic analysis efforts. Approximately 100 acres of employment lands are owned by Walker on the west side of Thorold Townline Road, opposite Upper's Lane. These employment lands fall within The Neighbourhoods of Rolling Meadows Secondary Plan area.

The Rolling Meadows Development will consist of a mix of residential and employment land uses, is proposed to be built in five phases, and is planned to be fully built-out by 2030. Combined, the Thorold Townline Road Employment Lands and the Rolling Meadows Development are expected to generate a total of 2,254 trips during the a.m. peak hour, and 2,880 trips during the p.m. peak hour. Due to the significant amount of growth represented by the background developments (the equivalent of an annual growth rate of 5.14% in the a.m. peak hour and 4.51% in the p.m. peak), no additional background growth has been applied to the study area road network to avoid an over conservative analysis of future traffic conditions.

Based on the proposed annual extraction limit of aggregate and operation hours, hourly truck traffic of up to 47 inbound and 31 outbound trucks during the a.m. peak hour and 31 inbound and 31 outbound trucks during the p.m. peak hour were predicted. It was assumed that 7 aggregate-related employees would travel inbound and outbound during each peak hour.

Based on the proposed annual production limit of asphalt and operation hours, hourly truck traffic of up to 11 inbound and 7 outbound trucks during the a.m. peak hour and 7 inbound and 7 outbound trucks during the p.m. peak hour was predicted. It was assumed that 4 asphalt-related employees would travel inbound and outbound during each peak hour.

Walker Aggregates Inc. supplied TMIG with historical shipping data upon which to base the distribution of truck traffic to the broader transportation network outside of the proposed Upper's Quarry study area.

Overall, the study area intersections operate well or at acceptable levels under all planning horizons. Some individual movements are approaching capacity, particularly under 2035 conditions, but still operate with acceptable delays of 80 seconds or less, indicating a Level of Service (LOS) 'E' or better. Some geometric changes and modifications to signal timing plans are recommended in order to address any capacity or queuing issues in order to allow for efficient movement of traffic through the study area.

Haul Route Option 1 via Thorold Townline to the north was identified as the preferred haul route, and accordingly future total traffic operations were analyzed for Haul Route Option 1 only. A summary of recommendations and timing of the improvements are provided below.

Background Conditions (2025 & 2035)

- With adjustments to existing signal timing plans, all study intersections operate at acceptable levels under 2025 and 2035 background conditions. Some individual movements are approaching capacity but operate at acceptable levels of service.
- A signal warrant was conducted for the intersection of Thorold Townline Road and Beaverdams Road under 2025 Background conditions to confirm if the combined existing and 2025 background traffic would justify the installation of a traffic signal. Based on Justification 7 of Book 12 of the Ontario Traffic Manual (OTM), the estimated 2025 background traffic volumes fulfill Justification 1A and 1B at 97% and 100% respectively. Although not warranted under 2025 Background conditions, based on the 120% threshold applied to Justification 7 and the near 100% justification fulfillment it is TMIG's opinion signals should be considered at this intersection under 2025 Background conditions.
- Construction of an auxiliary southbound right turn lane at the intersection of Thorold Townline Road and Lundy's Lane by the 2035 background planning horizon was found to provide better overall operations at the intersection. Interim adjustments to signal timings and introduction of protected phases could potentially negate the need for a southbound right turn lane, however, high volumes of southbound right-turning vehicles are predicted in 2035 that would benefit from a dedicated lane compared to the existing shared through/right turn lane. Given that the proposed Upper's Quarry is assumed to be active by 2025,



quarry related traffic is not the primary cause of the high volume of right-turning vehicles predicted in 2035, particularly based on preferred Haul Route Option 1 (via Thorold Townline Road), as minimal staff site traffic travels through the intersection, and heavy vehicle site traffic will **not** travel through the Thorold Townline Road and Lundy's Lane intersection. The operational impact of Haul Route Option 1 site-related traffic at this intersection is negligible and will not trigger the aforementioned road improvements.

- There is opportunity to widen the existing 24 metre ROW at the Thorold Townline Road and Lundy's Lane intersection to the designated 26.2 metre road allowance to accommodate a southbound right turn lane. Furthermore, the Region may require road widening dedications in addition to the designated road allowances without the need for amendments to the Official Plan for purposes such as turning lanes at intersections.
- It is recommended the Thorold Townline Road and Lundy's Lane intersection be monitored in the future to determine whether constructing the dedicated southbound right turn lane would be the most appropriate solution to accommodate background development traffic volumes within the vicinity of the intersection.

Total Conditions (2025 & 2035)

- With adjustments to existing signal timing plans, all study intersections operate acceptably under 2025 and 2035 total conditions. Some intersections/movements are approaching, or are at capacity, but operate at acceptable levels of service.
- The proposed access design will be constructed in 2025 prior to the quarry becoming active. The proposed access design provides deceleration and accelerations lanes northbound at the site access (via Upper's Lane). A slip around lane is provided southbound, thus accommodating left-turning vehicles into the site and preventing blockage of through traffic at the site access.
- The southbound queue at Thorold Stone Road and Thorold Townline Road should be monitored in 2035 to determine if any upgrades to the intersection are needed to address the potential for long queues to build up (southbound left experiences a queue up to 160m according to simulations). The long southbound left queue buildup does not occur under 2025 total conditions when Upper's Quarry is active, as such, quarry related traffic is **not** the cause of the long queues predicted in 2035.
- In general, it is suggested that the Thorold Townline Road and Beaverdams Road intersection be monitored for signalization in 2025, and that signals be installed prior to the 2035 planning horizon (i.e. prior to the combined full build-out of the Rolling Meadows development, Thorold Townline Road Employment Lands, and the proposed Upper's Lane Quarry).

Preferred Haul Route

TMIG recommends that Haul Route Option 1 be chosen as the preferred Haul Route, subject to approval by the Town and an appraisal of the cost of any road improvements required to accommodate truck traffic.

Haul Route Option 1 will also be seen as a preferable route by current and future residents within the vicinity of Upper's Quarry, as the Rolling Meadows Secondary Plan area represents a large amount of future residential traffic that will travel along Davis Road and Lundy's Lane. As such, it would be ideal to have truck traffic travel north directly on Thorold Townline Road (Haul Route Option 1), compared to the more circuitous route around the boundary of the future Rolling Meadows area (Haul Route Option 2).

Of note, Haul Route Option 1 will direct trucks northbound on Thorold Townline Road through a non-residential area, however, a causeway has been constructed along Thorold Townline Road to cross a waterway immediately south of Beaverdams Road. Depending on the structural properties of the causeway, improvements may need to be made in order to sustain the regular truck traffic associated with the proposed Upper's Quarry. Before the choice of haul route is finalized, it is recommended that Walker Aggregates Inc. and the Town perform a review of the existing load capacity of Thorold Townline Road in order to determine if any upgrades are required, and if so, what cost would be associated with the upgrades. If it is found that upgrades are required, it should be determined if the upgrades would be needed to service the future Rolling Meadows development regardless of any Upper's Quarry operations. The cost of the roadway upgrades should be assigned proportionately to the parties that will derive direct benefits from the upgrades.

Additionally, the City of Thorold Official Plan (Section B1.8.12.3) Aggregate Resource Protection Policy states the following:



"It shall also be recognized that Thorold Townline Road is a Regional arterial road and is the likely aggregate haul route required to serve any future aggregate extraction operation to the east. Accordingly, all studies required by any policy of this Plan shall recognize that Thorold Townline Road is a future aggregate haul route. The haul route shall be restricted from the future extraction operation entrance southerly to Highway 20, a major arterial."

Based on our interpretation of the policy above the City prefers the proposed Haul Route Option 1.



THE MUNICIPAL INFRASTRUCTURE GROUP LTD. A T.Y. LIN INTERNATIONAL COMPANY

Kyla Zijlstra, B.A.Sc., E.I.T. Technical Lead | <u>kzijlstra@tmig.ca</u>

Wichus Dourball

Michael Dowdall, C.E.T., MITE Project Manager, Traffic Director | <u>mdowdall@tmig.ca</u>



This page left intentionally blank



This page left intentionally blank



CONTENTS

1	INTRODUCTION1			
	1.1	Retainer and Objective1		
2	BASEL	INE TRAFFIC CONDITIONS		
	2.1	Site Environs3		
	2.2	Phasing Plan5		
	2.3	Existing Road Network6		
	2.4	Thorold Townline Road Right-of-Way6		
	2.5	Proposed Haul Routes7		
	2.6	Study Area Intersections9		
	2.7	Baseline Traffic Volumes11		
	2.8 Upper's Lane Quarry Access Considerations			
	2.9	Existing Quarry Operations11		
3	FUTUF	RE BACKGROUND CONDITIONS		
	3.1	Study Horizon Years13		
	3.2	Study Area Road Network Improvements13		
	3.3	Future Background Developments13		
		3.3.1 Rolling Meadows Development		
		3.3.2 Thorold Townline Road Employment Lands		
	3.4	Future Background Growth21		
	3.5	Background Traffic Volumes21		
4	SITE G	ENERATED TRAFFIC		
	4.1	Site Trip Generation24		
	4.2	Traffic Distribution and Assignment26		
5	FUTUF	RE TOTAL TRAFFIC		
6	CAPAC	CITY ANALYSIS		
	6.1	Davis Road at Thorold Stone Road35		
	6.2	Davis Road at Niagara Falls Road/Beaverdams Road37		
	6.3	Davis Road at Lundy's Lane		
	6.4	Thorold Townline Road at Thorold Stone Road41		
	6.5	Thorold Townline Road at Lundy's Lane43		
	6.6	Thorold Townline Road at Beaverdams Road45		
	6.7	Thorold Townline Road at Proposed Upper's Quarry Access		
7	QUEU	EING ANALYSIS 48		
8		RY ACCESS 52		
Ŭ	8 1	Location 52		
	8.2	Access Design 52		
	8.3	Site Access Operation 52		
	8.4	Sightline Assessment		
9	CONCI			
	9.1	Haul Route Ontions 54		
	3.1	nuu noule options		



9.2	Preferred Haul Route	54
9.3	Capacity Analysis Results and Recommendations	55
9.4	Conceptual Site Access Design	56

APPENDICES

APPENDIX A	PREMINARY SITE PLAN
APPENDIX B	TRAFFIC DATA
APPENDIX C	CAPACITY ANALYSIS
APPENDIX D	QUEUEING ANALYSIS
APPENDIX E	CONCEPTUAL SITE ACCESS DESIGN AND OPERATIONS
APPENDIX F	SIGHTLINE ASSESSMENT

FIGURES

Figure 1-1	Upper's Quarry Location Map2
Figure 2-1	Surrounding Land Uses4
Figure 2-2	Simplified Operation Schematics5
Figure 2-3	Proposed Haul Route Options8
Figure 2-4	Study Area Existing Lane Configurations10
Figure 2-5	Existing Traffic Volumes12
Figure 3-1	Rolling Meadows Secondary Plan Land Uses15
Figure 3-2	2025 Background Traffic Volumes – Rolling Meadows16
Figure 3-3	2035 Background Traffic Volumes – Rolling Meadows17
Figure 3-4	2025 Background Traffic Volumes – Thorold Townline Road Employment Lands
Figure 3-5	2035 Background Traffic Volumes – Thorold Townline Road Employment Lands
Figure 3-6	2025 Background Total Traffic Volumes
Figure 3-7	2035 Background Total Traffic Volumes23
Figure 4-1	Upper's Quarry Site Traffic Volumes – Haul Route Option 1 Truck Trips
Figure 4-2	Upper's Quarry Site Traffic Volumes – Employee Automobile Trips
Figure 4-3	Upper's Quarry Site Traffic Volumes – Haul Route Option 1 Total Trips
Figure 5-1	2025 Total Traffic Volumes – Haul Route Option 132
Figure 5-2	2035 Total Traffic Volumes - Haul Route Option 1



TABLES

Table 3-1	Future Thorold Townline Road Employment Lands Site
	Trip Generation18
Table 4-1	Monthly Material Shipping Estimates25
Table 4-2	Directional Distribution of Upper's Quarry Truck Trips26
Table 6-1	Study Area Peak Hour Factors
Table 6-2	Capacity Analysis of Davis Road at Thorold Stone Road35
Table 6-3	Capacity Analysis of Davis Road at Niagara Falls Road/Beaverdams Road
Table 6-4	Capacity Analysis of Davis Road at Lundy's Lane
Table 6-5	Capacity Analysis of Thorold Townline Road and Thorold Stone Road41
Table 6-6	Capacity Analysis of Thorold Townline Road at Lundy's Lane43
Table 6-7	Capacity Analysis of Thorold Townline Road at Beaverdams Road46
Table 6-8	Capacity Analysis of Thorold Townline Road at Proposed Upper's Quarry Access47
Table 7-1	Existing (2018) and Future Total Background (2025 & 2035) Queuing Analysis48
Table 7-2	Future Total (2025 & 2035) Haul Route Option 1 Queuing Analysis



1 INTRODUCTION

The Municipal Infrastructure Group Ltd. (TMIG), a T.Y. Lin International Company, was retained by Walker Aggregates Inc., to prepare a Traffic Impact Study (TIS) for the proposed Upper's Quarry. The proposed Upper's Quarry is located generally on lands situated south of Beaverdams Road, north of Lundy's Lane, west of Beechwood Road, and east of Thorold Townline Road, in the City of Niagara Falls, Region of Niagara, adjacent to City of Thorold.

This TIS has been prepared in support of a Class A Licence (Quarry Below Groundwater) under the Aggregate Resources Act (ARA) application, Regional Official Plan Amendment (ROPA), City Official Plan Amendment (OPA), and City Zoning By-Law Amendment (ZBA). The proposed Upper's Quarry has an approximate licence area of 106.3 hectares (262.7 acres) and an extraction area of 96.8 hectares (239.2 acres). The site will incorporate setbacks of 15m along the north and south boundaries. Setbacks of 30m will be provided along the western boundary, and setbacks of 15m and 30m will be provided along the east boundary. A preliminary Existing Features and Cross Sections Plan is provided in **Appendix A**.

The proposed Upper's Quarry access is proposed to be located at the Upper's Lane and Thorold Townline Road intersection. This proposed access is not dependent upon the sale of the Upper's Lane road allowance, as quarry traffic will either enter the site directly from this location on Thorold Townline Road, or travel to the same location via Upper's Lane. The proposed haul route will **not** make use of Beechwood Road to the east of Upper's Lane.

The quarry is anticipated to have an annual extraction limit of 1.8 million tonnes of aggregate and a maximum annual production of 400,000 tonnes of asphalt from a portable asphalt plant to be located on-site. As per the proposed Upper's Quarry Operational Plan, the proposed quarry will have the following hours of operation:

- Drilling, extraction: Monday to Saturday 7:00 am 7:00 pm
- Processing: Monday to Saturday 7:00 am 7:00 pm
- Blasting: Monday to Friday 8:00 am 6:00 pm
- Shipping: 24 hours (7 days/week)

It is noted that a response to emergencies is not limited by the hours of operation. A preliminary Operational Plan is provided in **Appendix A**.

1.1 Retainer and Objective

The Traffic Impact Study will assess the extent of traffic-related impacts on the abutting roadway system generated by the proposed quarry. The objectives of this study are to:

- Establish baseline traffic conditions for the study area and update the existing traffic conditions,
- Derive the future background operating conditions for the study intersections at a future 2025 and 2035 planning horizon,
- Analyze future operating conditions for the study intersections at a future 2025 and 2035 planning horizon,
- Determine what, if any, traffic impacts there are on the study area haul route from the proposed quarry,
- Recommend road network improvements to address any future traffic impacts within the study area.

The proposed Upper's Quarry location is illustrated in **Figure 1-1**.





2 BASELINE TRAFFIC CONDITIONS

This section summarizes the surrounding road network, the data collection program, presents the existing traffic volume conditions on the proximate study area roadways and assesses the current operating conditions at the intersections examined in this study. These 'baseline conditions' form the foundation for future background traffic projections and the incremental site-impact analyses investigated later herein.

2.1 Site Environs

The proposed quarry is generally located on the east side of Thorold Townline Road, west of Beechwood Road, south of Beaverdams Road, and north of Lundy's Lane. A solitary quarry access is proposed via the Upper's Lane and Thorold Townline Road intersection.

The site is located on lands designated as "Good General Agriculture Area" by the Region's and City's Official Plans, as are the surrounding lands to the north, south and east of the site, whilst lands to the west are designated as an urban area. The lands immediately west of Thorold Townline Road have been identified in the Rolling Meadows Secondary Plan as a future employment area, and the lands further west are designated as a residential area.

The site and surrounding lands are largely undeveloped with a few residential farms which will be demolished. An existing church is situated immediately east of the proposed quarry and has direct access to Beechwood Road. The existing Fernwood subdivision is located southeast of the proposed quarry, to the east of Beechwood Road.

The existing watercourse which currently runs through the site is to be realigned and enhanced as part of the future quarry operations. Upon completion, the realigned watercourse will be referred to as Upper's Creek and run along the east side of Thorold Townline Road. The proposed quarry and adjacent land uses are illustrated in **Figure 2-1**.





2.2 Phasing Plan

The phasing plan for the proposed quarry has been designed to identify the sequence of operation throughout the life of the quarry and maximize progressive rehabilitation of the site. Overall, the proposed quarry includes three (3) phases which have been illustrated in **Figure 2-2**.







2.3 Existing Road Network

Based on road network connectivity and proposed access to the quarry, the abutting Thorold Townline Road will be an integral part of the quarry's haul route. Boundary roadways that make up the haul route(s) to the quarry include:

- Thorold Townline Road/Taylor Road (Regional Road 70) is a two-lane regional road generally oriented in a north-south direction, with a posted speed limit of 80 km/h in the study area and is under the jurisdiction of Niagara Region. Thorold Townline Road provides a connection to Thorold Stone Road Road to north and Lundy's Lane to the south.
- Thorold Stone Road (Regional Road 57 / Highway 58) is generally oriented in an east-west direction and has a four-lane cross section with a posted speed limit of 80 km/h in the study area. It is under the jurisdiction of Niagara Region east of Davis Road. Thorold Stone Road provides a connection to Highway 406 to the west via the Thorold Tunnel, and a connection to the Queen Elizabeth Way (QEW) to the east. Within the study area, Thorold Stone Road is under the jurisdiction of the Ministry of Transportation (MTO) west of Davis Road, and is known as Highway 58.
- Davis Road (Highway 58) is a north-south highway under the jurisdiction of the MTO, and has a posted speed limit of 80 km/h. Davis Road provides a connection between Lundy's Lane to the south and Thorold Stone Road to the north. Davis Road has a 2-lane cross-section between Lundy's Lane and a point approximately 300 metres south of Beaverdams Road where it transitions to a 4-lane cross-section northward to Thorold Stone Road.
- Lundy's Lane (Regional Road 20 / Highway 20) is generally oriented in an east-west direction within the study area and has a two-lane cross section with a posted speed limit of 80 km/h. Lundy's Lane is under the jurisdiction of Niagara Region, with the exception of the portion between Davis Road and Thorold Townline Road, which is under the jurisdiction of the MTO. Lundy's Lane provides a connection to Highway 406 in the west, and Highway 420 and the QEW in the east.

2.4 Thorold Townline Road Right-of-Way

Thorold Townline Road currently provides a right-of-way (ROW) width of 20 metres, within proximity of the proposed site access, between Thorold Stone Road and a distance approximately 320 metres north of Lundy's Lane at which point the ROW width increases to approximately 24 metres.

Niagara Region OP Chapter 9 - Transportation (adopted as Amendment 13 to the OP) has policies set in place to ensure the Region will:

- Ensure that corridors are identified and protected to meet current and projected needs for various modes of travel including active transportation.
- Support opportunities for multi-modal use where feasible, in particular prioritizing transit and goods movement needs over those of single occupant automobiles.
- For goods movement corridors, provide for linkages to planned or existing intermodal opportunities where feasible.

Moreover, the Region's OP (Policy 9.C.7) states:

'The widths for Regional Road allowances are designated in the Table titled "Road Allowance Widths". Each Regional Road allowance which is not presently at its designated width is a highway to be widened.'

Region OP Table 9-1 (Road Allowance Widths) identifies a designated 26.2 metre road Thorold Townline Road allowance width between Thorold Stone Road and Chippawa Creek Road, inclusive of the proposed site access (via Upper's Lane) and its intersection with Lundy's Lane. Road widening requirements will be confirmed with the Region as part of the application review process, and, as necessary, the Site Plans will be modified to reflect those requirements at that time.

Region OP Policy 9.C.12 states:



'Land for Regional Road widening normally will be required equally from both sides of the centreline of the designated Regional Road unless existing land uses, topographic features or other physical or environmental constraints necessitate taking greater widening on one side than the other'

Additionally, Region OP Policy 9.C.13 states:

'The Region may require road widening dedications in addition to the designated road allowances indicated in the Table titled "Road Allowance Widths" without the need for amendments to this Plan for purposes such as <u>turning lanes</u> at intersections or to provide suitable access to major traffic generator developments.'

Therefore, as discussed in **Section 6.5**, there is opportunity to widen the existing 24 metre ROW at the Thorold Townline Road and Lundy's Lane intersection to the designated 26.2 metre road allowance and/or provide a road widening dedications in addition to the designated road allowance to accommodate a southbound right turn lane.

2.5 **Proposed Haul Routes**

Two possible routes have been considered as appropriate 'haul routes' for material that will be shipped from the proposed Upper's Quarry to serve local and broader markets. Haul Route Option 1 and Option 2 are illustrated in **Figure 2-3**.

Haul Route Option 1

The first option of a haul route for trucks to / from the proposed Upper's Quarry would utilize Thorold Townline Road to the north of the site, as it is a regional road and provides the most direct route to / from the quarry. The haul route includes the following roads:

- Thorold Townline Road north of the site access to Thorold Stone Road
- Highway 406 via Thorold Stone Road westbound
- Queen Elizabeth Way (QEW) via Taylor Rd northbound
- Queen Elizabeth Way (QEW) via Thorold Stone Road eastbound

Haul Route Option 2

Davis Road is designated as a provincial highway and is a major boundary road in close proximity to the site. Accordingly, it can also be considered an appropriate roadway to accommodate truck traffic to / from the quarry. The use of Davis Road as a second option for a haul route would result in a more circuitous haul route, as access to Davis Road would require quarry trucks to first travel south on Thorold Townline Road to Lundy's Lane, and then proceed west to Davis Road. The second haul route option includes the following roadways:

- Thorold Townline Road south of the site access to Lundy's Lane
- Lundy's Lane west to Davis Road
- Davis Road north to Thorold Stone Road
- Highway 406 via Thorold Stone Road westbound
- Queen Elizabeth Way (QEW) via Thorold Stone Road (eastbound) and Taylor Road northbound
- Queen Elizabeth Way (QEW) via Thorold Stone Road eastbound

HWY 58

LEGEND

Haul Route-Option 1 via Thorold Townline Road

Haul Route-Option 2 via Davis Road

Upper's Quarry Boundary

Rolling Meadows Secondary Plan Area

Provincial Road

Regional Road Local Road

NIAGARA FALLS ROAD

DAVIS ROAD (HNNY 58)

诸和王帝子

LD TOWNLINE ROAD (R.R. 70)

TAYLOR ROAD

THOROLD STONE ROAD (R.R. 57)

BEAVERDAMS ROAD

PROPOSED UPPER'S QUARRY ACCESS





TMIG recommends that Haul Route Option 1 be chosen as the preferred Haul Route, subject to approval by the Town and an appraisal of the cost of any road improvements potentially required to accommodate truck traffic.

Haul Route Option 1 will also be seen as a preferable route by current and future residents within the vicinity of the proposed Upper's Quarry, as the Rolling Meadows Secondary Plan area represents a large amount of future residential traffic that will travel along Davis Road and Lundy's Lane. As such, it would be ideal to have truck traffic travel north directly on Thorold Townline Road (Haul Route Option 1), compared to the more circuitous route around the boundary of the future Rolling Meadows area (Haul Route Option 2).

Additionally, the City of Thorold Official Plan (Section B1.8.12.3) Aggregate Resource Protection Policy states the following:

"It shall also be recognized that Thorold Townline Road is a Regional arterial road and is the likely aggregate haul route required to serve any future aggregate extraction operation to the east. Accordingly, all studies required by any policy of this Plan shall recognize that Thorold Townline Road is a future aggregate haul route. The haul route shall be restricted from the future extraction operation entrance southerly to Highway 20, a major arterial."

Based on our interpretation of the policy above, the City prefers the proposed Haul Route Option 1.

Of note, Haul Route Option 1 will direct trucks northbound on Thorold Townline Road through a non-residential area, however, a causeway has been constructed along Thorold Townline Road to cross a waterway immediately south of Beaverdams Road. Depending on the structural properties of the causeway, improvements may need to be made in order to sustain the regular truck traffic associated with the proposed Upper's Quarry. Before the choice of haul route is finalized, it is recommended that Walker Aggregates Inc. and the Town perform a review of the existing load capacity of Thorold Townline Road in order to determine if any upgrades are required, and if so, what cost would be associated with the upgrades. If it is found that upgrades are required, it should be determined if the upgrades would be needed to service the future Rolling Meadows development regardless of any Upper's Quarry operations. The cost of the roadway upgrades should be assigned proportionately to the parties that will derive direct benefits from the upgrades.

As Haul Route Option 1 via Thorold Townline to the north has been identified as the preferred haul route, future total traffic operations were analyzed for Haul Route Option 1 only.

2.6 Study Area Intersections

The following study area intersections were analyzed:

- Thorold Townline Road at Thorold Stone Road
- Thorold Townline Road at Beaverdams Road
- Thorold Townline Road at Upper's Lane (proposed Upper's Quarry access via Upper's Lane)
- Thorold Townline Road at Lundy's Lane
- Davis Road at Thorold Stone Road
- Davis Road at Beaverdams Road
- Davis Road at Lundy's Lane

The existing lane configurations at each study area intersection and the extent of the study area can be seen in **Figure 2-4**.





2.7 Baseline Traffic Volumes

Turning movement counts were commissioned by TMIG for study intersections identified in **Section 2.6**. Weekday a.m. and p.m. peak period counts were collected twice for each study location over two days. Count data was collected on June 14 and June 19, 2018. Traffic volumes from the two surveys were then averaged to establish baseline volumes for existing conditions. Count data collected at study intersections over the two day period is provided in **Appendix B**.

Baseline existing weekday a.m. and p.m. peak hour volumes are shown in Figure 2-5.

2.8 Upper's Lane Quarry Access Considerations

Upper's Lane is a rural public road that operates in a general east-west direction and provides access between Thorold Townline Road and Beechwood Road. Upper's Lane bisects the land owned by Walker Aggregates Inc. that will form the proposed Upper's Quarry.

Although the road is open to the public, negligible existing traffic utilizes the road, as evidenced by the volumes recorded at the intersection of Thorold Townline and Upper's Lane. The a.m. peak hour records a total of 1 inbound and 1 outbound vehicle, and the p.m. peak hour records a total of 2 inbound and 1 outbound vehicles (refer to **Figure 2-5**). It is noted that these traffic counts were taken when Bible Baptist Church was still being accessed from Upper's Lane. The access to Bible Baptist Church was re-located and only has access points to Beechwood Road, resulting in minimal traffic expected to access the church property via Upper's Lane given the surrounding land uses and alternative routes to the church from populated areas.

Figure 2-5 identifies the intersection of Upper's Lane and Thorold Townline Road as the location of the "Proposed Upper's Quarry Access", as although Upper's Lane is a public road and is not considered to be the Quarry's physical entrance, this intersection represents the primary point at which the proposed quarry traffic will enter and exit the broader study area road network and interact with non-quarry traffic sources. In other words, regardless as to where the access to the proposed quarry is physically located along Upper's Lane, all property (and access points) along the Upper's Lane corridor is now owned by the applicant and minimal public traffic is expected to interact with proposed quarry traffic along Upper's Lane.

2.9 Existing Quarry Operations

Traffic generated by Walker Brothers Quarry (WBQ) located at 2800 Thorold Townline Road, north of Thorold Stone Road, was captured by the weekday a.m. and p.m. peak period turning movement counts collected at the study area intersections.

It is expected the WBQ will be depleted in +/-10 years. Ideally Walker Aggregates would prefer to have +/-5 years to transition between the WBQ and Uppers Quarry so production at Uppers Quarry can begin lower than maximum permitted (when operations are at the surface) and scale up when operations are deeper into the quarry.

As result, the forecasted total truck volumes on the road network contained herein provides a more conservative analysis and is expected to have less of an impact on the operations of the study intersections than reported.



3 FUTURE BACKGROUND CONDITIONS

3.1 Study Horizon Years

The analysis considers future background traffic conditions at planning horizon years of 2025 and 2035. For analysis purposes, it is assumed that the proposed Upper's Quarry will be fully operational by the 2025 study horizon year.

3.2 Study Area Road Network Improvements

There are no planned changes to the existing local road network in the immediate vicinity of the proposed Upper's Quarry.

Niagara Region's 2017 Transportation Master Plan (TMP) identified capacity improvements to Highway 20 (Lundy's Lane) on the capital works list, however, these improvements to Highway 20 have not yet been placed in the capital budget. The type of capacity improvements were not detailed in the TMP, as the improvements are not planned until sometime between the years of 2032 and 2041. The improvements will occur between Kottmeier Rd (west of the Welland Canal) and Davis Road. Given that the improvements fall outside of the immediate study area and could potentially be completed beyond the 2035 study horizon year, no capacity improvements to Highway 20 were assumed as a conservative measure.

3.3 Future Background Developments

3.3.1 Rolling Meadows Development

The Neighbourhoods of Rolling Meadows Secondary Plan was first approved in 2000, was updated in 2007 to conform to the Provincial Growth Plan, and was later integrated into the City of Thorold's OP in 2015. The Rolling Meadows Secondary Plan Area is generally bounded by Thorold Townline Road to the east, Davis Road to the west, Lundy's Lane to the south, and a hydro corridor to the north (south of Beaverdams Road). Schedule A-3 of the City's OP outlines the planned Land Uses of the Rolling Meadows Secondary Plan area, and is provided in **Figure 3-1**.

According to the *Rolling Meadows Development Traffic Impact Study* dated October 31st, 2018, the Rolling Meadows development covers approximately 160 hectares of land within the City of Thorold and is,

"... a proposed multi-phase development consisting of primarily residential land uses, including singlefamily homes, townhouses, medium density units and high density units. A total of approximately 2,099 residential units are currently proposed. Commercial/Retail areas totaling a gross floor area (GFA) of approximately 240,800 ft² are proposed with the majority situated along the Highway 20 frontage with some located centrally within the neighbourhood. Two institutional blocks are also proposed; assumed to be Elementary Schools accommodating up to 300 students each."

Given the wide range of uses within the proposed Rolling Meadows development, TMIG did not generate the background traffic of the development from first principles in favour of adopting the site traffic volumes detailed in the 2018 Rolling Meadows traffic study to remain consistent with traffic modeling efforts that have already been undertaken.

The site traffic assignment developed for the Rolling Meadows traffic report was generally maintained, however, the intersections of Davis Road and Thorold Townline at Thorold Stone Road were not included within the Rolling Meadows study area. A significant percentage of Rolling Meadows site traffic, 49%, was assigned to/from the north via Davis Road, however, the distribution of the site traffic at the intersection of Davis Road and Thorold Stone Road is unknown. Due to the high delays observed under future background traffic conditions at the Davis Road and Thorold Townline at Thorold Stone Road intersection, TMIG reassigned some of this northbound traffic (14% of total traffic) to an alternate routing via Lundy's Lane to the



west, assuming that a large portion of the 49% of Rolling Meadows traffic that travels north on Davis Road is ultimately bound for Highway 406, which is also accessible via Lundy's Lane.

The Rolling Meadows development is proposed to be constructed in five phases. Phases 1 through 5 are proposed to be completed in 2019, 2021, 2023, 2028, and 2030, respectively. Accordingly, site traffic generated by Phases 1 through 3 was included as background traffic for the 2025 planning horizon, and the total site traffic generated by Phases 1 through 5 was included as background traffic for the 2035 planning horizon.

Figures 3-2 and **3-3** provide the weekday a.m. and p.m. peak hour site traffic volumes produced by the Rolling Meadows development by 2025 and 2035, respectively.









THORG ← 69 (44) ← 5 (3) ← 123 (226) (0) (0)0 0 0 (0) 44 (154) 0 (0) 186 (182) 214 (48) 72 Ļ (4) 7 (23) 35 -LUNDY'S LANE (R.R. 20) (74) 22 (93) 141 (80) 25 (13) 5 (0) 0 (0) 0 (7) 12 (0) 0 (7) 2 (7) 3 (0) 0 **2025 BACKGROUND TRAFFIC VOLUMES** TMIG **ROLLING MEADOWS FIGURE 3-2**



THORC 20 (38) 0 (0) 13 (17) (3) (165) × 85 (71) 3 (21) 118 (310) 0 (0) 5 78 85 (157) 215 159 (159) 16 (18) (35) 21 LUNDY'S LANE (R.R. 20) (103) 35 (239) 227 (211) 80 00 (21) 21 1 (0) 0 (7) 2 (21) 9 (0) 0 (11) (0) **2035 BACKGROUND TRAFFIC VOLUMES** TMIG **ROLLING MEADOWS FIGURE 3-3**



3.3.2 Thorold Townline Road Employment Lands

Approximately 100 acres of future employment lands are located west of Thorold Townline Road (within the Rolling Meadows Secondary Plan area) to the north and south of Upper's Lane. Walker Aggregates Inc. currently owns the majority of these employment lands in addition to the proposed Upper's Quarry.

The City of Thorold's OP (2015) has designated the Thorold Townline Road Employment Lands as a mix of Light Industrial and "Prestige Industrial" land uses. Descriptions of the types of permitted uses allowed on these lands are located in Section B1.8.8 of the Official Plan.

At the time of this report, a specific development timeline for the Thorold Townline Road Employment Lands was not available. For analysis purposes, it was assumed that half of the employment lands would be constructed by the 2025 study horizon year, and that full build-out would occur before the 2035 study horizon year.

Site traffic generated by the future employment lands during the weekday a.m. and p.m. peak hours was estimated by applying the fitted curve equations for Land Use Code (LUC) 130 Industrial Park and LUC 150 Warehousing in Trip Generation, 10th Edition, published by the Institute of Transportation Engineers (ITE). No reductions for transit or active transportation were applied to the base trips generated by the ITE fitted curve equations. **Table 3-1** summarizes the estimated trips generated by the future employment lands.

	Peak Hour Trip Generation					
Parameters	Weekday AM			Weekday PM		
	In	Out	Total	In	Out	Total
		ITE LU	JC 130 – Indus	strial Park (50	acres)	
ITE Equation	Ln(T)	= 0.78 Ln(X) +	- 2.82	ln(T)	= 0.72 Ln(X) +	3.06
Gross Trip Rate	5.90	1.20	7.10	1.50	5.64	7.14
Trip Ratio	83%	17%	-	21%	79%	-
Gross Trips	295	60	355	75	282	357
	ITE LUC 150 – Warehousing (50 acres)					
ITE Equation	T = 7.55(X) + 49.85			T = 6.74(X) + 49.08		
Gross Trip Rate	6.14	2.40	8.54	2.70	5.02	7.72
Trip Ratio	72%	28%	-	35%	65%	-
Gross Trips	307	120	427	135	251	386
Total (2035)	602	180	782	210	533	743

Table 3-1 Future Thorold Townline Road Employment Lands Site Trip Generation

The estimated 2025 and 2035 weekday a.m. and p.m. peak hour trips generated by the Thorold Townline Road Employment Lands were assigned to the study road network as shown in **Figure 3-4** and **Figure 3-5**.







3.4 Future Background Growth

A significant amount of growth is expected to occur within the study area due largely to the implementation of the Rolling Meadows Secondary Plan. By 2035, the Rolling Meadows residential and employment uses (including the Thorold Townline Road Employment Lands) are projected to generate a combined total of 2,254 trips during the weekday a.m. peak hour, and 2,880 trips during the weekday p.m. peak hour. This represents a substantial amount of growth that will occur across the study area road network.

For example, under existing conditions the northbound through movement at the intersection of Davis Road and Beaverdams Road is recorded to have a volume of 267 and 275 vehicles during the existing weekday a.m. and p.m. peak hour, respectively. By 2035, volumes of 626 and 582 vehicles during the weekday a.m. and p.m. peak hours are predicted under future background traffic conditions. This represents an increase of 359 and 307 vehicles from existing traffic conditions. This increase in traffic is equivalent to an annual growth rate of 5.14% in the weekday a.m. peak hour and 4.51% in the weekday p.m. peak hour, calculated based on growth over 17 years (from 2018 to 2035). Similar increases in traffic can be seen throughout the study area road network.

As the Rolling Meadows residential and employment uses (including the Thorold Townline Road Employment Lands) are the only projected developments within the area, and create a substantial growth on the road network (approximately 5% annual growth rate) it was deemed that no further growth on the road network should be applied. As the Rolling Meadows Secondary Plan area provides a large volume of residential and employment traffic, applying additional annual growth on the major roads would over-estimate the future traffic analysis. To ensure an accurate estimation of the future traffic volumes, the annual growth rate applied on the roadways only included the growth due to the substantial, confirmed background traffic.

3.5 Background Traffic Volumes

The 2018 baseline traffic and the background development site traffic were combined to produce the 2025 and 2035 background total weekday a.m. and p.m. peak hour traffic volumes.

The background total (2025 and 2035) traffic volumes are presented in Figures 3-6 and 3-7.



FIGURE 3-6



THORC (118) (95) (183) (125) (239) 159 (184) 82 85 44 94 136 78 (63) 132 (216) 422 (711) 38 (44) 214 500 (718) 45 (42) (114) 203 -LUNDY'S LANE (R.R. 20) (208) 153 (673) 607 (717) 633 77 140 37 (117) 107 22 139 30 (28) 18 (117) (142) (50) (46) 141) (51) **2035 BACKGROUND TOTAL TRAFFIC VOLUMES** TMIG

FIGURE 3-7



4 SITE GENERATED TRAFFIC

For analysis purposes, it is assumed that the proposed Upper's Quarry will be fully operational by the 2025 study horizon year (i.e. ship maximum annual amount of material allowed to be extracted). However, this is understood to be a conservative assumption, and operations will begin lower than the maximum annual limit when quarry operations start at the surface. Over time, once operations are deeper into the quarry, annual extraction levels will increase and approach the maximum annual extraction limit. Accordingly, truck traffic from the quarry will increase over time to eventually meet the maximum operations outlined in this report. In this sense, the 2025 analysis results in particular can be considered conservative in terms of the assumed volume of trucks assigned to the study area road network.

4.1 Site Trip Generation

In order to generate the estimated truck traffic associated with the proposed Upper's Quarry, the following assumptions and base data have been adopted:

- Aggregate Maximum Annual Shipping Limit (License application) = 1,800,000 tonnes
- Asphalt Maximum Annual Shipping Limit (License application) = 400,000 tonnes
- Quarry operations proposed as follows:
 - □ Shipping hours of 7:00 am to 7:00 pm (12.0 hours) from Monday to Saturday
 - D Total of 72 shipping hours a week or an average of 312 hours a month
 - Average truck capacity of 35 tonnes

The quarry is proposed to operate year-round from January to December with variable amounts of material extraction and shipping depending on the month. Based on historical shipping data records archived by TMIG, peak shipping generally occurs during the 'construction season' between the months of May and October. **Table 4-1** summarizes the average monthly breakdown of material extraction based on archived historical data from existing quarry operations in the area. The estimated percentage of total annual material shipped per month was applied to the 1,800,000-tonne annual shipping limit.



Table 4-1	Monthly	Material	Shipping	Estimates
			• · · · · · · · · · · · · · · · · · · ·	

Month	Material Volume Per Month (Percent of Total)
January	3%
February	4%
March	5%
April	7%
May	12%
June	13%
July	11%
August	10%
September	12%
October	10%
November	7%
December	6%
Total	100%

To account for the occasional periods of higher-volume trucking that is likely to occur during high-construction activity (typically between May and October), the trip generation used in the analysis of quarry-generated traffic impacts is based on the peak level of shipping / trucking activity during these busy summertime periods. Based on **Table 4-1**, June represents the peak month during the peak construction season, with approximately 13% of the total annual material shipped during that month. As a conservative measure, an additional 5% was added onto the peak month percentage to account for potential fluctuations in monthly material shipped due to variations in market demand from year to year. Approximately 18% was applied to the annual Upper's Quarry extraction limit, resulting in 330,000 tonnes of the annual aggregate material estimated to be extracted during the peak summer month. This equates to 1,058 tonnes of material per hour based on an average of 312 shipping hours per month. With a capacity of approximately 35 tonnes per truck, 1,058 tonnes of material extraction generate approximately 31 outbound loaded aggregate truck trips per hour (plus the same number of returning trucks).

31 aggregate trucks trips per hour is considered to be a highly conservative estimate of the number of trucks that will be able to leave the quarry each hour, given there is only one weighing scale planned to service all outbound loaded trucks. The quarry is capable of shipping outside of the peak demand period (7:00 a.m. to 7:00 p.m.), which will likely be required during the peak construction season to fulfill all aggregate orders.

During the peak month of demand, approximately 73,333 tonnes of the annual asphalt limit is estimated to be produced by the on-site portable asphalt plant. This equates to 235 tonnes of asphalt per hour based on an average of 312 shipping hours per month. With a capacity of approximately 35 tonnes per truck, 235 tonnes of asphalt generate approximately 7 outbound loaded truck trips per hour (plus the same number of returning trucks).

It has been TMIG's experience that additional peaking occurs during early morning shipping activity, to provide material to construction sites in the morning. As a result, additional outbound loaded trucks could occasionally occur, creating a short-lived 'peak within a peak' condition (generally occurring prior to the adjacent street peak).

To account for this peaking, the a.m. peak hour outbound truck volume was increased by an additional 50%, equating to 47 aggregate and 11 asphalt loaded truck trips per hour. We have adopted this peak trip


generation as the design-hour vehicle volume for our site-impact analysis that follows. As alluded to above, these 'peak within a peak' activities are predicted to occur largely outside of the adjacent street peak hours, so in this respect we are predicting an unlikely (and conservative) scenario of the quarry and adjacent street peaks coinciding.

Aggregate recycling will be part of the tonnage limit under the new Aggregate Resources Act. These loads are already accounted for in the analysis. Extracted aggregate and recycled aggregate will be limited to 1,800,000 tonnes per year.

With adoption of the various peaking factors described above and employed in the regular aggregate shipping activity estimates, we have portrayed a conservative (high) trucking activity level of site-related traffic flows, and therefore impacts on the abutting street system.

It is assumed that approximately 7 aggregate-related and 4 asphalt-related employees will be working at the quarry per shift. Therefore, as a conservative measure, a total of 11 inbound and outbound employee trips were generated during both the a.m. and p.m. peak hours (assuming a shift change occurs within the peak hour of the surrounding road network).

4.2 Traffic Distribution and Assignment

Walker Aggregates Inc. supplied TMIG with two years of historical shipping data from an existing quarry in Niagara Region which is similar in size to the proposed Upper's Quarry. The historical shipping data was used to base the distribution of truck traffic to the broader transportation network outside of the Upper's Quarry study area. The total tonnage shipped each year was separated into the geographical location of the customers, averaged, and the percent of the total aggregate shipped to each location was determined. A summary of the directional distribution of truck traffic for the proposed Upper's Quarry is provided in **Table 4-2**.

Of note, approximately 5% of all truck trips are expected to make use of either Highway 406 or the Queen Elizabeth Way (QEW) to travel south to make local deliveries. A load limit on Lundy's Lane was identified at the Allanburg Bridge that crosses the Welland Canal, and as such, no southbound truck traffic was assigned via Lundy's Lane/R.R. 20 to the west of the subject site.

Direction To / From	% Distribution
North via Taylor Road and QEW	30%
East via Thorold Stone Road and QEW	30%
West via Thorold Stone Road and Hwy 406	40%
Total	100%

Table 4-2 Directional Distribution of Upper's Quarry Truck Trips

As discussed in **Section 2.5**, two possible haul routes were identified, however, only the preferred haul route was used for analysis purposes. The preferred haul route (Haul Route Option 1 via Thorold Townline Road) is the most direct and would primarily make use of Thorold Townline Road to access the broader transportation network. The preferred haul route option is described in greater detail below (the inbound trucks will follow the reverse of the outbound route described).



Haul Route Option 1

Outbound aggregate and asphalt trucks were assigned to the road network as follows:

- Right turn out of quarry access to travel north on Thorold Townline Road to Thorold Stone Road
 - Trucks traveling west to Highway 406 turn left onto Thorold Stone Road
 - Trucks traveling north to the QEW via Taylor Road continue northbound at Thorold Stone Road
 - □ Trucks traveling east to the QEW turn right onto Thorold Stone Road

All of the above-mentioned roadways are either regional or provincial roads, and as such, have been assumed to be designed to road standards acceptable and appropriate for use as aggregate haul routes.

The trip distribution summarized in **Table 4-2** has been applied to the calculated estimates of the peak hourly truck trips as described in **Section 4.1**, and the resultant truck traffic volume assignments are shown in **Figure 4-1** for Haul Route Option 1.

Given the lack of current employment uses in direct vicinity of the subject site, it was determined that Transportation Tomorrow Survey (TTS) Data would not provide a correct representation of traffic patterns for employment trip assignment purposes. The distribution of quarry employee traffic was based on logical routing between the quarry and surrounding major towns and cities that are likely to house quarry employees. The estimated employee site trips in each of the study peak hours are shown in **Figure 4-2**.

The estimated truck and employee site trips were combined to produce the total site-related trips presented in **Figure 4-3**.



THORC (0) (0) 0) 0 0 0 (0) 0 (0) 0 (0) 214 0 (0) 0 (0) 2 0 (0) (0) 0 / (0) 0 / (0) 0 / LUNDY'S LANE (R.R. 20) (0) 0 (0) 0 (0) 0 0 0 0 (0) 0 0 0 0 (0) **UPPER'S QUARRY SITE TRAFFIC VOLUMES** TMIG HAUL ROUTE OPTION #1 TRUCK TRIPS **FIGURE 4-1**







5 FUTURE TOTAL TRAFFIC

The future total traffic conditions for the peak study hours in the 2025 and 2035 planning horizons were derived by combining the projected future background traffic with the corresponding estimate of the total site generated traffic (quarry trucks and employees).

Figure 5-1 summarizes the future total traffic volumes for Haul Route Option 1 for the 2025 planning horizon during the weekday a.m. and p.m. peak hours. **Figure 5-2** summarizes the future total traffic volumes for Haul Route Option 1 for the 2035 planning horizon during the weekday a.m. and p.m. peak hours.



THORC (118) (53) 58 (132) 85 (118) 23 (53) (125) (300) 143 (157) 94 181 40 (33) 233 (241) 348 (555) 214 397 (555) 38 (44) 36 (28) (83) 159 -LUNDY'S LANE (R.R. 20) (179) 140 1 (527) 521 (567) 520 (103) 98 71 140 37 22 139 24 (28) 18 (113) (131) (50) (46) 141) (37) **2025 TOTAL TRAFFIC VOLUMES** TMIG **HAUL ROUTE OPTION #1** FIGURE 5-1



THORC (118) (96) 84 (185) 85 (118) 45 (96) (125) (239) 159 (184) 94 136 79 (64) 132 (216) 422 (711) 38 (44) 214 502 (720) 45 (42) (116) 205 LUNDY'S LANE (R.R. 20) (208) 153 (673) 607 (719) 635 (117) 107 77 140 37 22 139 30 (28) 18 (117) (142) (50) (46) 141) (51) **2035 TOTAL TRAFFIC VOLUMES** TMIG **HAUL ROUTE OPTION #1** FIGURE 5-2



6 CAPACITY ANALYSIS

The capacity analysis identifies how well the intersections and driveways are operating under existing conditions and how they are expected to operate in the future. The analysis contained within this report utilized the Highway Capacity Manual (HCM) 2000 techniques within the Synchro Version 10 Software package. The reported intersection volume-to-capacity ratios (v/c) are a measure of the volume versus the capacity of each turning movement, while the levels-of-service (LOS) are a measure of the average delay for each turning movement. Queuing characteristics are reported as the predicted 95th percentile queue for each turning movement.

Synchro Calibration Volume and Lane Settings:

The ideal saturated flow (flow rate) used in the analysis follows the Synchro 10 recommended default of 1,900 vphpl.

The peak hour factor (PHF) of the flow rate has been calculated to provide the most accurate representation of the peak 15-minutes for the study times. The specific calculated peak hour factors used are provided in **Table 6-1**.

Intersection Name	AM PHF	PM PHF
Davis Road & Thorold Stone Road	0.96	0.95
Davis Rd & Niagara Falls Road /Beaverdams Road	0.95	0.95
Davis Road & Lundy's Lane	0.94	0.93
Thorold Townline Road /Taylor Road & Thorold Stone Road	0.96	0.96
Thorold Townline Road & Lundy's Lane	0.93	0.91
Thorold Townline Road & Beaverdams Road	0.92	0.93
Thorold Townline Road & Upper's Lane	0.93	0.91

Table 6-1 Study Area Peak Hour Factors

For the purpose of the future site impact analyses, the heavy vehicle percentages calculated from the existing turning movement counts and applied to the Synchro analysis were updated for the 2025 and 2035 future total scenarios. The heavy vehicle percentages were increased for movements throughout the study area network to which proposed Upper's Quarry aggregate and asphalt traffic will be added to, as per the preferred haul route. The increased percentages were calculated by estimating the volume of heavy vehicles performing a given movement under 2025 or 2035 future background conditions (existing heavy vehicle percentage assumed), adding the estimated volume of heavy vehicle site traffic, and finally dividing the 2025 or 2035 future total heavy vehicle volumes by the total mixed-traffic volume for each movement.

The analysis includes identification of all intersections and for all movements; v/c ratios, LOS indicators and 95th percentile queue lengths. Critical intersections and movements shall be highlighted (in bold). 'Critical' intersections and movements include:

- through, shared through, or right-turn movements with a v/c ratio greater than 0.85 at signalized intersections
- exclusive turning movements with a v/c ratio greater than 0.90 at signalized intersections
- queue length of an individual movement is projected to exceed available turning lane storage at 95th percentile volumes at signalized intersections
- movements at unsignalized intersections that are expected to operate at LOS 'D' or worse, and/or the estimated 95th percentile queue length exceeds the available storage space



The following tables summarize the Synchro/HCM capacity results for the study intersections during the weekday a.m. and p.m. peak hours under existing, future background, and future total traffic conditions (for both haul route options). Detailed Synchro intersection capacity sheets are provided in **Appendix C**.

6.1 Davis Road at Thorold Stone Road

Signalized capacity analyses during the weekday a.m. and p.m. peak hours are summarized in **Table 6-2** for the intersection of Davis Road at Thorold Stone Road.

Condition	Movement	AI	M Peak Ho	ur	PM Peak Hour			
Condition	wovement	v/c	Delay (s)	LOS	v/c	Delay (s)	LOS	
	Overall	0.59	22	С	0.62	23	С	
	EBL	0.13	13	В	0.19	16	В	
	EBT	0.49	16	В	0.67	20	С	
	EBR	0.20	13	В	0.40	16	В	
	WBL	0.31	17	В	0.66	42	D	
Existing	WBTR	0.60	18	В	0.62	19	В	
-	NBL	0.66	45	D	0.66	45	D	
	NBLT	0.66	45	D	0.65	45	D	
	NBR	0.11	34	С	0.06	35	С	
	SBL	0.02	50	D	0.04	48	D	
	SBT	0.03	50	D	0.06	48	D	
	SBR	0.01	50	D	0.02	48	D	
	Overall	0.66	35	D	0.72	33	С	
	EBL	0.13	21	С	0.18	23	С	
	EBT	0.64	28	С	0.76	32	С	
	EBR	0.29	22	С	0.62	30	С	
	WBL	0.36	32	С	0.69	31	С	
Future Background	WBTR	0.60	34	С	0.59	19	В	
(2025)	NBL	0.80	56	E	0.77	64	Е	
	NBLT	0.81	58	ш	0.79	65	E	
	NBR	0.15	37	D	0.09	45	D	
	SBL	0.02	56	E	0.05	65	E	
	SBT	0.04	57	E	0.08	65	E	
	SBR	0.01	56	E	0.02	64	E	

 Table 6-2
 Capacity Analysis of Davis Road at Thorold Stone Road



		A	M Peak Ho	ur	PM Peak Hour			
Condition	Movement	v/c	Delay (s)	LOS	v/c	Delay (s)	LOS	
	Overall	0.66	29	С	0.77	34	С	
	EBL	0.14	15	В	0.20	23	С	
	EBT	0.54	19	В	0.82	33	С	
	EBR	0.24	15	В	0.62	28	С	
Future Total	WBL	0.47	28	С	0.77	51	D	
(2025)	WBTR	0.63	25	С	0.63	24	С	
Haul Route Option 1	NBL	0.78	55	D	0.80	60	E	
(Thorold Townline Road)	NBLT	0.80	56	E	0.82	62	E	
	NBR	0.15	37	D	0.09	40	D	
	SBL	0.02	56	E	0.04	55	D	
	SBT	0.04	57	E	0.07	55	D	
	SBR	0.01	56	E	0.02	54	D	
	Overall	0.74	41	D	0.86	46	D	
	EBL	0.15	24	С	0.23	28	С	
	EBT	0.72	32	С	0.91	44	D	
	EBR	0.38	26	С	0.84	44	D	
	WBL	0.52	43	D	0.88	67	E	
Future Background	WBTR	0.64	41	D	0.66	29	С	
(2035)	NBL	0.88	64	E	0.92	76	E	
	NBLT	0.89	65	E	0.94	78	E	
	NBR	0.18	36	D	0.13	39	D	
	SBL	0.02	56	E	0.04	55	D	
	SBT	0.04	57	E	0.07	55	D	
	SBR	0.01	56	E	0.02	54	D	
	Overall	0.75	33	С	0.87	46	D	
	EBL	0.16	17	В	0.24	29	С	
	EBT	0.59	21	С	0.94	47	D	
	EBR	0.31	17	В	0.84	45	D	
Future Total	WBL	0.73	47	D	0.88	65	E	
(2035)	WBTR	0.67	29	С	0.68	30	С	
Haul Route Option 1	NBL	0.87	61	E	0.92	76	E	
(Thorold Townline Road)	NBLT	0.87	63	E	0.94	78	E	
	NBR	0.18	35	D	0.13	39	D	
	SBL	0.02	56	E	0.04	55	D	
	SBT	0.04	57	E	0.07	55	D	
	SBR	0.01	56	E	0.02	54	D	

Under existing conditions, the intersection operates well during the a.m. and p.m. peak hours with overall LOS 'C' and v/c ratios of 0.59 and 0.62 during the a.m. and p.m. peak hours, respectively, indicating reserve capacity. Individual movements operate with v/c ratios of 0.67 or less and LOS 'D' or better.

Under 2025 background conditions, the intersection is expected to continue operating at acceptable levels with overall v/c ratios of 0.66 and 0.72 with LOS 'D' and 'C' during the a.m. and p.m. peak hours, respectively. However, some individual movements are predicted to experience longer delays (LOS 'E'), during the a.m. and p.m. peak hours compared to existing conditions. Individual movements are predicted to operate with v/c ratios of 0.80 or less, indicating reserve capacity remains.



Based on 2025 future total traffic conditions for Haul Route Option 1, the intersection is expected to continue operating at acceptable levels with an overall LOS 'C' and v/c ratios of 0.66 and 0.77 during the a.m. and p.m. peak hours, respectively. Individual movements are predicted to experience LOS 'E' or better and v/c ratios of 0.82 or less.

The intersection is expected to operate at acceptable levels under 2035 background conditions with overall LOS 'D' and v/c ratios of 0.74 and 0.86 during the a.m. and p.m. peak hours, respectively. During the p.m. peak hour, the northbound left and shared left/through movements are approaching capacity (v/c of 0.92 and 0.94), however, both movements still operate with acceptable delays and LOS 'E'. The eastbound through movement is also approaching capacity during the p.m. peak hour, predicted to operate with a v/c ratio of 0.91, however, it is expected to operate with acceptable delay and LOS 'D'.

Under 2035 future total traffic conditions for Haul Route Option 1, the intersection is expected to operate at acceptable levels with overall LOS 'C' and 'D' and v/c ratios of 0.75 and 0.87 during the a.m. and p.m. peak hours, respectively. During the p.m. peak hour, the northbound left and shared left/through movements are approaching capacity (v/c of 0.92 and 0.94), however, both movements still operate with acceptable delays and LOS 'E'. The eastbound through movement continues to approach capacity during the p.m. peak hour, predicted to operate with a v/c ratio of 0.94, however, it is expected to continue operating with acceptable delay and LOS 'D'.

Overall, this intersection is expected to have acceptable future operations despite some movements approaching capacity in 2035, and there are no required geometric improvements to the intersection.

6.2 Davis Road at Niagara Falls Road/Beaverdams Road

Signalized capacity analyses during the weekday a.m. and p.m. peak hours are summarized in **Table 6-3** for the intersection of Davis Road at Niagara Falls Road/Beaverdams Road.

0		A	M Peak Ho	ur	PM Peak Hour			
Condition	wovement	v/c	Delay (s)	LOS	v/c	Delay (s)	LOS	
	Overall	0.28	22	С	0.35	23	С	
	EBLTR	0.24	11	В	0.20	12	В	
	WBLTR	0.16	10	А	0.23	12	В	
Eviating	NBL	0.02	26	С	0.02	24	С	
Existing	NBTR	0.37	29	С	0.32	26	С	
	SBL	0.31	30	С	0.58	33	С	
	SBT	0.23	28	С	0.26	26	С	
	SBR	0.03	26	С	0.07	24	С	
	Overall	0.37	26	С	0.47	25	С	
	EBLTR	0.24	11	В	0.23	14	В	
	WBLTR	0.17	11	В	0.32	15	В	
Future Background	NBL	0.07	27	С	0.05	23	С	
(2025)	NBTR	0.64	34	С	0.44	27	С	
	SBL	0.51	36	D	0.72	41	D	
	SBT	0.31	29	С	0.46	28	С	
	SBR	0.03	27	С	0.07	24	С	

 Table 6-3
 Capacity Analysis of Davis Road at Niagara Falls Road/Beaverdams Road



Condition	Meyomont	AM Peak Hour			PM Peak Hour			
Condition	wovement	v/c	Delay (s)	LOS	v/c	Delay (s)	LOS	
	Overall	0.37	26	С	0.47	25	С	
	EBLTR	0.24	11	В	0.23	14	В	
Future Total	WBLTR	0.17	11	В	0.32	15	В	
(2025)	NBL	0.07	27	С	0.05	23	С	
Haul Route Option 1	NBTR	0.64	34	С	0.44	27	С	
(Thorold Townline Road)	SBL	0.51	36	D	0.72	41	D	
	SBT	0.31	29	С	0.46	28	С	
	SBR	0.03	27	С	0.07	24	С	
	Overall	0.43	26	С	0.53	25	С	
	EBLTR	0.27	14	В	0.27	17	В	
	WBLTR	0.17	13	В	0.32	18	В	
Future Background	NBL	0.10	24	С	0.13	21	С	
(2035)	NBTR	0.70	32	С	0.51	25	С	
	SBL	0.56	35	D	0.79	46	D	
	SBT	0.36	27	С	0.57	26	С	
	SBR	0.03	23	С	0.07	20	В	
	Overall	0.43	27	С	0.53	25	С	
	EBLTR	0.27	14	В	0.27	17	В	
Future Total	WBLTR	0.19	13	В	0.32	18	В	
(2035)	NBL	0.11	25	С	0.13	21	С	
Haul Route Option 1	NBTR	0.71	33	С	0.51	25	С	
(Thorold Townline Road)	SBL	0.57	36	D	0.79	46	D	
	SBT	0.36	27	С	0.57	26	С	
	SBR	0.03	24	С	0.07	20	В	

Under existing conditions, the intersection operates very well during the a.m. and p.m. peak hours with overall LOS 'C' and v/c ratios of 0.28 and 0.35 during the a.m. and p.m. peak hours, respectively, indicating significant reserve capacity.

Under 2025 background conditions, the intersection is expected to continue operating at acceptable levels, maintaining an overall LOS 'C' during peak hours with predicted overall v/c ratios of 0.37 and 0.47 during the a.m. and p.m. peak hours, respectively. Individual movements are predicted to operate with v/c ratios of 0.72 or less and experience LOS 'D' or better during both peak hours.

Based on 2025 future total traffic conditions for Haul Route Option 1, the intersection is expected to continue operating at acceptable levels with an overall LOS 'C' and v/c ratios of 0.37 and 0.47 during the a.m. and p.m. peak hours, respectively. Individual movements are predicted to continue experiencing LOS 'D' or better and operate with v/c ratios of 0.72 or less.

The intersection is expected to operate at acceptable levels under 2035 background conditions with overall LOS 'C' and v/c ratios of 0.43 and 0.53 during the a.m. and p.m. peak hours, respectively, indicating reserve capacity remains. Individual movements are predicted to experience LOS 'D' or better and v/c ratios of 0.79 or less.

Under 2035 future total traffic conditions for Haul Route Option 1, the intersection is expected to operate at acceptable levels with overall LOS 'C' and v/c ratios of 0.43 and 0.53 during the a.m. and p.m. peak hours, respectively. Similar to 2035 background conditions, reserve capacity remains, and individual movements are predicted to experience LOS 'D' or better and operate with v/c ratios of 0.79 or less.



Overall, this intersection is expected to have acceptable future operations and there are no required geometric improvements to the intersection.

6.3 Davis Road at Lundy's Lane

Signalized capacity analyses during the weekday a.m. and p.m. peak hours are summarized in **Table 6-4** for the intersection of Davis Road at Lundy's Lane.

Condition	Marran	A	M Peak Ho	ur	PM Peak Hour			
Condition	Movement	v/c	Delay (s)	LOS	v/c	Delay (s)	LOS	
	Overall	0.43	15	В	0.46	20	С	
	EBL	0.19	6	А	0.36	19	В	
	EBTR	0.39	8	А	0.61	21	С	
	WBL	0.07	5	А	0.10	14	В	
	WBT	0.28	7	А	0.55	20	В	
Existing	WBR	0.03	5	А	0.04	13	В	
	NBL	0.12	33	С	0.11	20	В	
	NBTR	0.60	38	D	0.27	22	С	
	SBL	0.36	35	С	0.19	21	С	
	SBT	0.35	34	С	0.20	21	С	
	SBR	0.06	32	С	0.08	19	В	
	Overall	0.59	18	В	0.78	36	D	
	EBL	0.30	10	В	0.77	37	D	
	EBTR	0.52	12	В	0.72	29	С	
	WBL	0.11	9	А	0.15	28	С	
	WBT	0.40	11	В	0.82	44	D	
Future Background	WBR	0.17	9	А	0.20	45	D	
(2023)	NBL	0.09	26	С	0.18	40	D	
	NBTR	0.44	29	С	0.51	46	D	
	SBL	0.76	42	D	0.70	32	С	
	SBT	0.27	28	С	0.20	25	С	
	SBR	0.11	26	С	0.11	24	С	
	Overall	0.59	18	В	0.79	36	D	
	EBL	0.30	10	В	0.69	28	С	
	EBTR	0.52	12	В	0.68	26	С	
	WBL	0.11	8	А	0.14	26	С	
Future Total	WBT	0.40	11	В	0.78	41	D	
(2023)	WBR	0.17	8	А	0.19	52	D	
Haul Route Option 1 (Therold Townline Read)	NBL	0.09	27	С	0.19	41	D	
	NBTR	0.45	29	С	0.53	48	D	
	SBL	0.78	45	D	0.77	39	D	
	SBT	0.27	28	С	0.21	27	С	
	SBR	0.11	27	С	0.11	26	С	
	Overall	0.62	17	В	0.94	39	D	
Future Background	EBL	0.36	10	А	0.89	58	E	
(2033)	EBTR	0.59	12	В	0.74	23	С	

 Table 6-4
 Capacity Analysis of Davis Road at Lundy's Lane



	WBL	0.16	8	А	0.23	22	С
	WBT	0.48	10	А	0.87	42	D
	WBR	0.10	7	А	0.19	34	С
	NBL	0.11	29	С	0.19	41	D
	NBTR	0.54	33	С	0.57	49	D
	SBL	0.71	43	D	0.91	71	E
	SBT	0.32	31	С	0.26	34	С
	SBR	0.12	29	С	0.13	32	С
	Overall	0.62	17	В	0.95	39	D
	EBL	0.36	10	А	0.90	59	E
	EBTR	0.59	12	В	0.75	23	С
	WBL	0.16	8	А	0.23	22	С
Future Lotal (2035)	WBT	0.48	10	А	0.88	43	D
(2000)	WBR	0.10	7	А	0.19	33	С
Haul Route Option 1 (Thorold Townline Road)	NBL	0.11	29	С	0.19	41	D
	NBTR	0.55	33	С	0.57	49	D
	SBL	0.72	43	D	0.91	71	E
	SBT	0.32	31	С	0.26	34	С
	SBR	0.12	29	С	0.13	32	С

Under existing conditions, the intersection operates well during the a.m. and p.m. peak hours with overall LOS 'B' and 'C' and v/c ratios of 0.43 and 0.46 during the a.m. and p.m. peak hours, respectively, indicating significant reserve capacity. Individual movements operate with a v/c of 0.61 or less and LOS 'D' or better.

Under 2025 background conditions, the intersection is expected to continue operating at acceptable levels with overall LOS 'B' and 'D' and v/c ratios of 0.59 and 0.78 during the a.m. and p.m. peak hours, respectively. Individual movements are predicted to experience LOS 'D' or better and v/c ratios of 0.82.

Based on 2025 future total traffic conditions for Haul Route Option 1, the intersection is expected to continue operating at acceptable levels with overall LOS 'B' and 'D' and v/c ratios of 0.59 and 0.79 during the a.m. and p.m. peak hours, respectively. Individual movements are predicted to experience LOS 'D' or better and v/c ratios of 0.78 or less.

The intersection is expected to operate at acceptable levels under 2035 background conditions with overall LOS 'B' and 'D' and v/c ratios of 0.62 and 0.94 during the a.m. and p.m. peak hours, respectively. During the p.m. peak hour, the southbound left movement is approaching capacity (v/c of 0.91), however, the movement operates with acceptable delay and LOS 'E'. All other movements at the intersection experience LOS 'E' or better and v/c ratios of 0.89 or less during both peak hours.

Under 2035 future total traffic conditions for Haul Route Option 1, the intersection is expected to operate at acceptable levels with overall LOS 'B' and 'D' and v/c ratios of 0.62 and 0.95 during the a.m. and p.m. peak hours, respectively. During the p.m. peak hour, the eastbound left and southbound left movements are approaching capacity (v/c ratios of 0.90 and 0.91, respectively), however, the movements operate with acceptable delays and LOS 'E' or better. All other movements at the intersection experience LOS 'E' or better and v/c ratios of 0.88 or less during both peak hours.

Overall, this intersection is expected to have acceptable future operations despite some movements approaching capacity in 2035, and there are no required geometric improvements to the intersection.



6.4 Thorold Townline Road at Thorold Stone Road

Signalized capacity analyses during the weekday a.m. and p.m. peak hours are summarized in **Table 6-5** for the intersection of Thorold Townline Road at Thorold Stone Road.

Condition		A	M Peak Ho	ur	P	M Peak Ho	ur
Condition	Movement	v/c	Delay (s)	LOS	v/c	Delay (s)	LOS
	Overall	0.78	24	С	0.73	26	С
	EBL	0.69	12	В	0.59	13	В
	EBT	0.28	6	А	0.47	11	В
	EBR	0.03 <i>(0.04)</i>	5 (3)	A (A)	0.02 (0.03)	8 (4)	A (A)
	WBL	0.06	12	В	0.13	16	В
Existing	WBT	0.43	16	В	0.48	19	В
	WBR	0.05	12	В	0.02	14	В
	NBL	1.03	168	F	1.04	164	F
	NBTR	0.47	43	D	0.24	34	С
	SBL	0.29	41	D	0.17	34	С
	SBTR	0.79	59	E	0.88	59	E
	Overall	0.83	40	D	0.79	35	С
	EBL	0.80	52	D	0.74	28	С
	EBT	0.42	34	С	0.67	29	С
	EBR	0.08 <i>(0.14)</i>	68 (22)	E (C)	0.04 (0.07)	19 <i>(</i> 2 <i>)</i>	В <i>(А)</i>
Future Deckground	WBL	0.34	20	В	0.34	23	С
(2025)	WBT	0.65	34	С	0.65	34	С
	WBR	0.05	24	С	0.02	24	С
	NBL	0.50	33	С	0.59	32	С
	NBTR	0.35	31	С	0.46	34	С
	SBL	0.20	36	D	0.15	30	С
	SBTR	0.88	65	E	0.89	62	E
	Overall	0.87	45	D	0.82	47	D
	EBL	0.88	68	E	0.76	53	D
	EBT	0.48	39	D	0.69	50	D
Future Total	EBR	0.11 <i>(0.21)</i>	68 <i>(24)</i>	E <i>(C)</i>	0.06 <i>(0.12)</i>	122 (25)	F <i>(C)</i>
(2025)	WBL	0.42	23	С	0.48	26	С
Haul Route Ontion 1	WBT	0.74	40	D	0.68	36	D
(Thorold Townline Road)	WBR	0.05	28	С	0.02	25	С
	NBL	0.56	31	С	0.73	41	D
	NBTR	0.42	29	С	0.54	34	С
	SBL	0.20	35	D	0.15	28	С
	SBTR	0.88	64	Е	0.91	63	Е
	Overall	0.93	50	D	0.91	57	E
Future Background	EBL	0.93	79	Е	0.87	66	E
(2035)	EBT	0.60	43	D	0.79	59	E
	EBR	0.16 <i>(0.27)</i>	76 (24)	E (C)	0.05 (0.11)	245 (20)	F (B)

 Table 6-5
 Capacity Analysis of Thorold Townline Road and Thorold Stone Road



	WBL	0.74	33	С	0.63	34	С
	WBT	0.82	45	D	0.83	43	D
	WBR	0.05	29	С	0.02	26	С
	NBL	0.58	31	С	0.88	60	E
	NBTR	0.40	28	С	0.72	39	D
	SBL	0.18	32	С	0.20	29	С
	SBTR	0.94	70	E	0.93	67	E
	Overall	0.95	52	D	0.93	61	E
	EBL	0.94	79	E	0.90	76	E
	EBT	0.65	47	D	0.89	68	E
Euture Total	EBR	0.21 <i>(0.34)</i>	74 (26)	E (C)	0.07 <i>(0.17)</i>	157 <i>(</i> 25)	F (C)
(2035)	WBL	0.80	39	D	0.79	55	D
Haul Doute Option 1	WBT	0.86	49	D	0.92	55	D
(Thorold Townline Road)	WBR	0.05	31	С	0.02	29	С
````,	NBL	0.78	48	D	0.83	46	D
	NBTR	0.50	28	С	0.71	35	D
	SBL	0.18	31	С	0.18	27	С
	SBTR	0.94	69	Е	0.94	68	Е

Note: Italicized rows indicate values where the Highway Capacity Manual (HCM) 2000 result differed significantly from the Intersection Capacity Utilization (ICU) results, which have been provided in brackets. Based on the capacity and demand at these locations, the level of delay is not reasonable according to HCM.

Under existing conditions, the intersection operates at acceptable levels during the a.m. and p.m. peak hours with overall LOS 'C' and v/c ratios of 0.78 and 0.73 during the a.m. and p.m. peak hours, respectively. The northbound left movement is currently operating at capacity with LOS 'F' and v/c ratios of 1.03 and 1.04 during the a.m. and p.m. peak hours, respectively. Capacity issues at this intersection are addressed in future background and total conditions through adjustments to the existing signal timing plan.

Under 2025 background conditions, the intersection is expected to continue operating at acceptable levels with overall LOS 'D' and 'C' and v/c ratios of 0.87 and 0.82 during the a.m. and p.m. peak hours, respectively. Individual movements are predicted to experience LOS 'E' or better.

Based on 2025 future total traffic conditions for Haul Route Option 1, the intersection is expected to continue operating at acceptable levels with overall LOS 'D' and v/c ratios of 0.87 and 0.82 during the a.m. and p.m. peak hours, respectively. The southbound shared through/right movement is approaching capacity with v/c ratios of 0.88 and 0.91 during the a.m. and p.m. peak hours, respectively, however, the movement is still experiencing acceptable delays. The eastbound right movement is expected to operate with relatively high delay during both peak hours, however, given the relatively low turning volumes and the queueing results, it was determined that the HCM delay calculation for the movement was not reasonable and that lower delays would be experienced (closer to those predicted in the ICU results for the intersection).

The intersection is expected to operate at acceptable levels under 2035 background conditions with overall LOS 'D' and 'E' and v/c ratios of 0.93 and 0.91 during the a.m. and p.m. peak hours, respectively. The southbound shared through/right movement continues to approach capacity with v/c ratios of 0.94 and 0.93 during the a.m. and p.m. peak hours, respectively, and experiences acceptable delays of 70 seconds or less. The eastbound left movement is approaching capacity with a v/c ratio of 0.93 during the a.m. peak hour and continues to experience acceptable delay (LOS 'E'). As mentioned previously, while the eastbound right movement is predicted to experience high delays, this is likely due to an error in Synchro's HCM 2000 capacity analysis methodology. Based on ICU results, the movement is expected to operate with acceptable levels of delay.

Under 2035 future total traffic conditions for Haul Route Option 1, the intersection is predicted to approach capacity with overall LOS 'D' and 'E' and v/c ratios of 0.95 and 0.93 during the a.m. and p.m. peak hours, respectively. The southbound shared through/right movement continues to approach capacity with v/c ratios



of 0.94 during both the a.m. and p.m. peak hours. Overall, all movements at the intersection experience acceptable levels of delay (LOS 'E' or better) despite several movements approaching capacity. Based on ICU results, the eastbound right movement is expected to operate with acceptable levels of delay compared to the HCM results.

Overall, this intersection is expected to have acceptable future operations despite some movements approaching capacity in 2025 and 2035. There are no required geometric improvements to the intersection, however, the intersection could benefit from monitoring to determine if constructing a dedicated southbound right turn lane will improve overall operations of the intersection and address any potential queueing problems for the southbound left turn lane identified in **Section 7** of this report.

## 6.5 Thorold Townline Road at Lundy's Lane

In order to address significant delays and capacity issues experienced by the northbound left movement under 2035 future total conditions, a variety of signal timing plans were tested to determine if all intersection movements could operate under capacity with acceptable delays. It was found that the addition of a dedicated southbound right turn lane aided in improving not only southbound operations, but the northbound left operations as well.

This is due in part to the high volume of southbound right vehicles being blocked by southbound through movements in the existing shared lane that are stopped by a red light. By constructing a southbound right turn lane, more southbound right turning vehicles are able to move through the intersection on a red light, providing more gaps for northbound left turning traffic during the green phase.

The southbound right turn lane was applied to all 2025 and 2035 analysis scenarios to provide consistent signal timing plans and the associated benefits of the dedicated lane on the overall traffic operations at the intersection. It is suggested that the intersection be monitored in the future to determine whether constructing the dedicated right turn lane in 2025 or making adjustments to the signal timings in the interim condition, including the addition of protected phases, would be the most economical solution.

As discussed in **Section 2.4**, there is opportunity to widen the existing 24 metre ROW at the Thorold Townline Road and Lundy's Lane intersection to the designated 26.2 metre road allowance to accommodate a southbound right turn lane. Furthermore, the Region may require road widening dedications in addition to the designated road allowances without the need for amendments to the Official Plan for purposes such as turning lanes at intersections.

Signalized capacity analyses during the weekday a.m. and p.m. peak hours are summarized in **Table 6-6** for the intersection of Thorold Townline Road at Lundy's Lane.

Condition	Movement	A	M Peak Ho	ur	PM Peak Hour			
Condition	wovement	v/c	Delay (s)	LOS	v/c	Delay (s)	LOS	
	Overall	0.39	17	В	0.43	18	В	
	EBL	0.10	6	А	0.07	5	А	
	EBT	0.33	7	А	0.37	7	А	
	EBR	0.07	5	А	0.08	5	А	
Evicting	WBL	0.06	5	А	0.08	5	А	
Existing	WBTR	0.27	7	А	0.36	7	А	
	NBL	0.34	39	D	0.65	51	D	
	NBTR	0.62	44	D	0.59	44	D	
	SBL	0.09	36	D	0.18	37	D	
	SBTR	0.38	39	D	0.52	42	D	
Future Background	Overall	0.48	16	В	0.52	21	С	

#### Table 6-6 Capacity Analysis of Thorold Townline Road at Lundy's Lane



Condition	Maxamant	A	M Peak Ho	ur	PM Peak Hour			
Condition	Movement	v/c	Delay (s)	LOS	v/c	Delay (s)	LOS	
(2025)	EBL	0.29	7	А	0.20	7	А	
	EBT	0.45	8	А	0.44	10	А	
	EBR	0.09	5	А	0.09	6	А	
	WBL	0.08	5	А	0.09	5	А	
	WBTR	0.34	7	А	0.49	9	А	
	NBL	0.35	38	D	0.67	58	E	
	NBTR	0.62	43	D	0.63	52	D	
	SBL	0.15	35	D	0.43	49	D	
	SBT	0.31	37	D	0.43	47	D	
	SBR	0.05	34	С	0.09	42	D	
	Overall	0.48	16	В	0.52	21	С	
	EBL	0.30	8	А	0.20	6	А	
	EBT	0.45	8	А	0.44	8	А	
	EBR	0.09	5	А	0.09	4	А	
Future Total (2025)	WBL	0.08	5	А	0.09	5	А	
(2020)	WBTR	0.34	7	А	0.49	8	А	
Haul Route Option 1	NBL	0.35	38	D	0.67	59	E	
	NBTR	0.62	43	D	0.63	52	D	
	SBL	0.15	35	D	0.44	49	D	
	SBT	0.31	37	D	0.43	47	D	
	SBR	0.05	34	С	0.10	42	D	
	Overall	0.54	16	В	0.68	23	С	
	EBL	0.45	10	В	0.41	11	В	
	EBT	0.52	9	А	0.57	12	В	
	EBR	0.10	5	А	0.10	6	А	
	WBL	0.09	6	А	0.12	6	А	
Future Background	WBTR	0.44	8	А	0.65	12	В	
(2000)	NBL	0.39	38	D	0.66	57	E	
	NBTR	0.62	43	D	0.64	52	D	
	SBL	0.29	37	D	0.77	74	E	
	SBT	0.31	37	D	0.41	46	D	
	SBR	0.07	34	С	0.13	42	D	
	Overall	0.54	16	В	0.68	23	С	
	EBL	0.46	10	В	0.42	11	В	
	EBT	0.52	9	А	0.57	12	В	
	EBR	0.10	5	А	0.10	6	А	
Future Total	WBL	0.09	6	А	0.12	6	А	
(2000)	WBTR	0.44	8	А	0.65	12	В	
Haul Route Option 1 (Thorold Townline Road)	NBL	0.39	38	D	0.66	56	E	
	NBTR	0.62	43	D	0.64	52	D	
	SBL	0.30	38	D	0.77	74	E	
	SBT	0.31	37	D	0.41	46	D	
	SBR	0.07	34	С	0.13	42	D	



Under existing conditions, the intersection operates very well during the a.m. and p.m. peak hours with overall LOS 'B' and v/c ratios of 0.39 and 0.43 during the a.m. and p.m. peak hours, respectively, indicating reserve capacity. Individual movements experience LOS 'D' or better.

Under 2025 background conditions, the intersection is expected to continue operating at acceptable levels with overall LOS 'B' and 'C' and v/c ratios of 0.48 and 0.52 during the a.m. and p.m. peak hours, respectively. Individual movements are predicted to experience LOS 'D' or better with the exception of the northbound left movement that is predicted to experience LOS 'E' during the p.m. peak hour.

Based on 2025 future total traffic conditions for Haul Route Option 1, the intersection is expected to continue operating at acceptable levels with an overall LOS 'B' and 'C' and v/c ratios of 0.48 and 0.52 during the a.m. and p.m. peak hours, respectively. With the exception of the northbound left movement that is predicted to experience LOS 'E' during the p.m. peak hour, all other individual movements are predicted to experience LOS 'D' or better.

The intersection is expected to operate at acceptable levels under 2035 background conditions with overall LOS 'B' and 'C' and v/c ratios of 0.54 and 0.68 during the a.m. and p.m. peak hours, respectively, indicating reserve capacity remains. With the exception of the northbound left and southbound left movements that are predicted to experience LOS 'E' during the p.m. peak hour, all other individual movements are predicted to experience LOS 'D' or better.

Under 2035 future total traffic conditions for Haul Route Option 1, the intersection is expected to operate with overall LOS 'B' and 'C' and v/c ratios of 0.54 and 0.68 during the a.m. and p.m. peak hours, respectively. With the exception of the northbound left and southbound left movements that are predicted to experience LOS 'E' during the p.m. peak hour, all other individual movements are predicted to experience LOS 'D' or better during both peak hours.

Overall, this intersection is expected to have acceptable future operations upon the construction of a dedicated southbound right turn lane. It is suggested that the southbound right turn lane be constructed prior to the 2035 planning horizon to facilitate efficient movement of traffic at the intersection. It should be noted that under the preferred Haul Route Option 1 traffic scenario, the site attributes a nominal volume of traffic to the southbound right turn movement (4 two-way trips) during the peak hour, as result the impact of site-related traffic on the intersection is negligible. Therefore, as previously mentioned, it is suggested that the intersection be monitored in the future to determine whether constructing the dedicated southbound right turn lane or making adjustments to the signal timings in the interim condition, including the addition of protected phases, would be the most appropriate solution to accommodate background traffic volumes.

## 6.6 Thorold Townline Road at Beaverdams Road

A signal warrant was conducted for the intersection of Thorold Townline Road and Beaverdams Road under 2025 Background conditions to confirm if the combined existing and 2025 background traffic would justify the installation of a traffic signal. Based on Justification 7 of Book 12 of the Ontario Traffic Manual (OTM), the estimated 2025 background traffic volumes fulfill Justification 1A and 1B at 97% and 100% respectively. Although not warranted under 2025 Background conditions, based on the 120% threshold applied to Justification 7 and the near 100% justification fulfillment it is TMIG's opinion signals should be considered at this intersection under 2025 Background conditions.

In general, it is suggested that the intersection be monitored for signalization in 2025, and that signals be installed prior to the 2035 planning horizon (i.e. prior to the combined full build-out of the Rolling Meadows development, Thorold Townline Road Employment Lands, and the proposed Upper's Lane Quarry).

Unsignalized and Signalized capacity analyses during the weekday a.m. and p.m. peak hours are summarized in **Table 6-7** for the intersection of Thorold Townline Road at Beaverdams Road.



Table 6-7 Capacity Analysis of Thorold Townline Road at Beaverdams Road

Under existing conditions, the unsignalized intersection operates with excellent operational characteristics during the a.m. and p.m. peak hours with delays of 12 seconds or less.

Under 2025 background conditions, the unsignalized intersection is expected to continue operating at acceptable levels, however, northbound traffic is expected to experience LOS 'E', and a delay of 36 seconds during the p.m. peak hour.

Under 2025 future total traffic conditions for Haul Route Option 1, the signalized intersection is expected to operate well with LOS 'C' or better, and reserve capacity during both the weekday a.m. and p.m. peak hours.

The signalized intersection is expected to operate well under 2035 background conditions with LOS 'C' or better, and delays of 33 seconds or less during the a.m. and p.m. peak hours. In general, all movements have considerable reserve capacity with the exception of the shared northbound movement during the p.m. peak hour that experiences a v/c ratio of 0.87. The northbound shared left/through/right lane is approaching capacity, but still operates with acceptable levels of delay.

Under 2035 future total traffic conditions for Haul Route Option 1, the intersection continues to operate well with individual movements at LOS 'C' or better and delays of 33 seconds or less during the a.m. peak hour. During the p.m. peak hour, movements operate at LOS 'D' or better and delays of 41 seconds or less. The northbound shared left/through/right movement is approaching capacity with a v/c ratio of 0.90, but still operates with acceptable levels of delay. During the p.m. peak hour, the intersection is expected to operate with an overall v/c ratio of 0.86, however, it operates with an acceptable overall LOS 'C'.

Overall, this intersection should be monitored for signalization under 2025 background and total conditions, and is expected to have acceptable future operations upon signalization prior to 2035.



## 6.7 Thorold Townline Road at Proposed Upper's Quarry Access

It is proposed that the access to Upper's Quarry be located at the Upper's Lane intersection with Thorold Townline Road as, regardless of ownership of the road, Upper's Lane will primarily serve Quarry traffic, not public traffic.

Unsignalized capacity analyses during the weekday a.m. and p.m. peak hours are summarized in **Table 6-8** for the intersection of Thorold Townline Road at Upper's Lane.

Condition	Movement	А	M Peak Ho	ur	PM Peak Hour				
Condition	wovement	v/c	Delay (s)	LOS	v/c	Delay (s)	LOS		
Future Total (2025)	WBLR	0.14	13	В	0.10	13	В		
Haul Route Option 1 (Thorold Townline Road)	SBL	0.06	9	А	0.06	9	А		
Future Total (2035)	WBLR	0.18	15	С	0.14	16	С		
Haul Route Option 1 (Thorold Townline Road)	SBL	0.06	10	В	0.07	11	В		

 Table 6-8
 Capacity Analysis of Thorold Townline Road at Proposed Upper's Quarry Access

Under 2025 future total traffic conditions, the quarry access via Thorold Townline Road is expected to operate with excellent operational characteristics and substantial reserve capacity during both the weekday a.m. and p.m. peak hours. The delay to the westbound vehicles exiting the quarry is minimal, a mere 13 seconds during both the peak hours.

Under 2035 future total traffic conditions, Haul Route Option 1 (via Thorold Townline Road), continues to operate well with acceptable delay to westbound vehicles exiting the quarry.

Overall, the proposed Upper's Quarry access via Thorold Townline Road is expected to have acceptable future operations and there are no required improvements other than the conceptual access design discussed in **Section 8** of this report.



## 7 QUEUEING ANALYSIS

Queuing analysis of the study intersections and the proposed Upper's Quarry site access was undertaken, and detailed reports are provided in **Appendix D**. A summary of the predicted 95th percentile queues for the weekday a.m. and p.m. peak hours under existing, background, and future total traffic is provided in **Table 7-1** and **Table 7-2**. The queuing reports were prepared using SimTraffic microsimulation software using the following methodology: 30 minutes seeding time, one-hour recording, and 5 simulation runs.

Table 7-1	Existing (2018) and Future	Total Background (202	25 & 2035) Queuing Analysis
-----------	----------------------------	-----------------------	-----------------------------

			95 th Percentile Queue Length (m)							
Intersection	Movement	Available Storage (m)	2018 E	xisting	2025 Backg	Total round	2035 Backg	Total round		
			AM	РМ	АМ	РМ	АМ	PM		
	EBL	105	12	16	11	15	13	15		
Davis Road at	WBL	70	30	46	41	42	104	62		
Road	NBL	275	55	54	86	72	96	142		
	SBL	30	-	1 veh	1 veh	1 veh	1 veh	1 veh		
Davis Road at Niagara Falls	NBL	80	1 veh	1 veh	14	9	21	15		
Road / Beaverdams Road	SBL	140	27	47	32	48	31	53		
	EBL	85	27	34	46	57	42	72		
	WBL	65	17	17	22	17	26	52		
Davis Road at	WBR	80	11	14	29	43	21	90		
Lundy's Lane	NBL	55	19	20	18	23	18	23		
	SBL	90	33	23	95	104	70	191		
	SBR	100	21	19	29	34	41	61		
	EBL	100	82	67	102	79	117	83		
	EBR	50	12	8	32	24	54	72		
Thorold Townline	WBL	85	15	15	51	31	104	60		
Stone Road	WBR	90	18	11	20	14	18	14		
	NBL	80	34	27	50	57	66	62		
	SBL	75	26	25	27	33	123	183		
	EBL	90	19	20	41	33	61	76		
	EBR	20	18	23	16	26	34	27		
Thorold Townline	WBL	55	12	16	14	16	16	17		
Lane	NBL	25	30	42	34	44	34	55		
	SBL	25	12	14	20	31	22	48		
	SBR	30	-	-	20	30	27	52		
	EBLTR	-	21	35	46	58	44	65		
Thorold Townline	WBLTR	-	16	19	45	49	58	98		
Beaverdams Road	NBLTR	-	36	32	74	113	148	254		
	SBLTR	-	25	26	68	91	122	216		
Thorold Townline Road at Upper's Lane	WBLR	-	1 veh	1 veh	29	23	25	26		



#### **Existing Conditions**

Under existing conditions, the 95th percentile queue lengths of dedicated movements at study intersections are not predicted to exceed the available storage, with the exception of the intersection of Thorold Townline Road and Lundy's Lane. The northbound left turn queue exceeds its storage by 5 metres during the a.m. peak hour, and by 17 metres during the p.m. peak hour. The 5 and 17 metres that the queue exceeds the existing storage for these two movements is representative of approximately one and two vehicles, respectively, and is considered to be an acceptable level of queueing although the extra vehicles may not fully fit in the allotted storage area.

#### 2025 Background Conditions

Under 2025 background conditions, the 95th percentile queue lengths at study intersections are generally not predicted to exceed the available storage. The northbound left queue at Thorold Townline Road and Lundy's Lane continues to exceed available storage during both peak hours by up to 19 metres.

#### 2035 Background Conditions

Overall, the study intersections experience minimal 95th percentile queuing problems under 2035 background traffic conditions.

Under 2035 background conditions, the intersection of Davis Road and Lundy's Lane becomes congested with background traffic and it is predicted that several dedicated turn movements may have 95th percentile queues that will extend beyond existing storage (eastbound left, westbound left, westbound right, and southbound left). In particular, the southbound left turn at Davis Road and Lundy's Lane during the p.m. peak hour experiences a large increase in the 95th percentile queue length between 2025 and 2035 background conditions. The queue length is predicted to be 211 metres long, exceeding the 90 metres of available storage.

As seen in **Table 7-2**, this queue continues to exceed the available storage under 2025 and 2035 future total conditions. It is recommended the intersection be monitored as the Rolling Meadows development phases are constructed to determine if any adjustments to signal timings and/or physical improvements to the roadway, such as extending the storage, is required. A minimal amount of non-aggregate site traffic is expected to travel through this intersection and will not create any measurable impacts to operations.

The 95th percentile queue of eastbound left turn and westbound left turn movements at the intersection of Thorold Townline Road and Thorold Stone Road are predicted to exceed storage during the a.m. peak hour under 2035 background conditions. The eastbound left is predicted to exceed storage by 17 metres, equivalent to approximately two cars. The westbound left is predicted to exceed storage by 21 metres, which is equivalent to approximately three cars. During the p.m. peak hour, the 95th percentile queue of the southbound left movement is expected to exceed available storage by 61 metres.

As discussed in Section 6.4, the intersection could benefit from monitoring in the future to determine if further signal timing modification or geometric improvements (such as a dedicated southbound right turn lane) would improve overall operations of the intersection and aid in moving the southbound traffic through the intersection more efficiently. A dedicated right-turn lane could potentially assist in reducing the queue spillback of the southbound through and right-turn traffic that may block the southbound left-turn lane at times.

Under 2035 background traffic conditions, the northbound left and southbound left queues at Thorold Townline Road and Lundy's Lane continue to meet or exceed available storage during the a.m. and p.m. peak hours. It should be noted that a railway crossing is located approximately 80 metres south of the intersection and extending the northbound left turn lane will not be a viable option. It is recommended that queue lengths be monitored at this intersection, and that the adjustment of the signal timings and phases should be reviewed to address the 95th percentile queues given the geometric constraints.

As discussed in **Section 6.5**, the dedicated southbound right lane at Thorold Townline Road and Lundy's Lane is suggested to be constructed prior to 2035 to aid in the overall operation of the intersection and to reduce delays. It should be noted under the preferred Haul Route Option 1 traffic scenario, the site attributes a nominal volume of traffic to the southbound right turn movement (4 two-way trips) during the peak hour. As a result, the operational impact of site-related traffic at this intersection is negligible and will not trigger the aforementioned road improvements. As such, it is suggested that the intersection be monitored in the future



to determine whether constructing the dedicated southbound right turn lane would be the most appropriate solution to accommodate background development traffic volumes within the vicinity of the intersection.

Table 7-2	Future Total	(2025 & 2035)	Haul Route Option 1	Queuing Analysis
-----------	--------------	---------------	---------------------	------------------

	95 th Percentile Que					
Intersection	Movement	Available Storage (m)	2025 Total Option 1 Townli	Haul Route (Thorold ne Rd)	2035 Total Option 1 Townli	Haul Route (Thorold ne Rd)
			AM	РМ	AM	РМ
	EBL	105	11	16	12	16
Davis Road at	WBL	70	56	42	79	61
Road	NBL	275	88	75	101	112
	SBL	30	1 veh	1 veh	1 veh	1 veh
Davis Road at Niagara Falls	NBL	80	16	8	18	15
Beaverdams Road	SBL	140	29	47	28	48
	EBL	85	45	58	43	81
	WBL	65	23	18	23	24
Davis Road at	WBR	80	30	45	23	54
Lundy's Lane	NBL	55	21	22	20	24
	SBL	90	76	112	54	162
	SBR	100	31	30	38	48
	EBL	100	103	76	115	98
	EBR	50	34	35	46	96
Thorold Townline	WBL	85	42	31	94	82
Stone Road	WBR	90	34	13	21	39
	NBL	80	52	50	65	85
	SBL	75	40	33	67	159
	EBL	90	41	30	68	60
	EBR	20	21	20	27	27
Thorold Townline	WBL	55	12	18	15	19
Lane	NBL	25	35	42	32	58
	SBL	25	17	29	22	50
	SBR	30	22	31	24	53
Thorold Townling	EBLTR	-	45	54	45	59
Road at	WBLTR	-	47	46	55	102
Beaverdams	NBLTR	-	63	113	112	540
Road	SBLTR	-	69	81	109	225
Thorold Townline Road at Upper's	WBLR	-	24	26	29	27
Lane	SBL	15	19	16	21	19



#### 2025 Total Conditions

Under 2025 total traffic (Haul Route Option #1) conditions, study intersections experience minimal queueing problems with the exception of the following movements that experience 95th percentile queues that exceed the available storage length by 5 metres or more:

- Southbound Left at Davis Road and Lundy's Lane (p.m. peak hour)
- Northbound Left at Thorold Townline Road and Lundy's Lane (a.m. and p.m. peak hours)

The 95th percentile queue for the southbound left movement at the intersection of Thorold Townline Road and the proposed Upper's Quarry access is predicted to be 19 and 16 metres during the weekday a.m. and p.m. peak hours, respectively. Given the minor predicted exceedance, the southbound left turn storage of 30 metres, as proposed in the conceptual site access design, can adequately accommodate the predicted 95th percentile queues under 2025 total conditions. The westbound queues at the site access will be accommodated by internal site roadways.

#### **2035 Total Conditions**

Under 2035 total traffic (Haul Route Option #1) conditions, study intersections experience longer queues than under 2025 total conditions, however, only the following movements experience 95th percentile queues that exceed the available storage length by 5 metres or more:

- Westbound Left at Davis Road and Thorold Stone Road (a.m. peak hour)
- Southbound Left at Davis Road and Lundy's Lane (p.m. peak hour)
- Eastbound Left at Thorold Townline Road and Thorold Stone Road (a.m. peak hour)
- Westbound Left at Thorold Townline Road and Thorold Stone Road (a.m. peak hour)
- Southbound Left at Thorold Townline Road and Thorold Stone Road (p.m. peak hour)
- Eastbound Right at Thorold Townline Road and Lundy's Lane (a.m. and p.m. peak hours)
- Northbound Left at Thorold Townline Road and Lundy's Lane (a.m. and p.m. peak hours)
- Southbound Left at Thorold Townline Road and Lundy's Lane (p.m. peak hour)
- Southbound Right at Thorold Townline Road and Lundy's Lane (p.m. peak hour)

The 95th percentile queue lengths that exceed the available storage space under 2035 total conditions are generally longer than the 2025 total conditions because of the sizeable increase in background traffic volumes from 2025 to 2035, which is particularly true at intersections that are not included in the preferred haul route.

Under 2035 future total conditions, the 95th percentile queue for the southbound left movement at the intersection of Thorold Townline Road and the proposed Upper's Quarry access is predicted to be 21 and 19 metres during the weekday a.m. and p.m. peak hours, respectively. Given the minor predicted exceedance, the southbound left turn storage of 30 metres, as proposed in the conceptual site access design, can adequately accommodate the predicted 95th percentile queues under 2035 total conditions. The westbound queues at the site access will be accommodated by internal site roadways.



## 8 QUARRY ACCESS

## 8.1 Location

The intersection of Uppers Lane and Thorold Townline Road is to be modified to accommodate truck traffic and function as the future access to the proposed Upper's Quarry. Access to the proposed Upper's Quarry via Upper's Lane will be achieved regardless as to the ownership of the road allowance, as the location will serve either as a direct access to the quarry, or as a roadway to access the quarry. Aggregate and Asphalt traffic (heavy vehicles) will access Upper's Lane / the proposed Upper's Quarry via Thorold Townline Road to/from the north, and will **not** access the proposed quarry via Beechwood Road. The quarry access will thus be located approximately one kilometre south of the Beaverdams Road and Thorold Townline Road intersection.

## 8.2 Access Design

The proposed design for the access incorporates engineering design criteria as per the 2017 Transportation of Canada (TAC) geometric design guideline for Canadian roads and The Ontario Ministry of Transportation's (MTO) Commercial Site Access Policy and Standard Designs. The proposed access design provides deceleration and accelerations lanes northbound at the site access. A slip around lane is provided southbound, thus accommodating left-turning vehicles into the site and preventing blockage of through traffic at the site access.

Access design includes curb radii of 16m and 18m to accommodate future truck turning movements into and out of the site. The access design can accommodate site-related traffic for both Haul Route Options 1 and 2, although the preferred Haul Route Option 1 will only require heavy vehicle site traffic to be accommodated for the southbound left and westbound right movements.

Of note, while the preferred aggregate haul route is to the north via Thorold Townline (thus the provision of a northbound acceleration lane and southbound left-turn lane in the conceptual design), other forms of site traffic may access the quarry from the south. A dedicated northbound right turn lane has been included in the conceptual design to accommodate non-aggregate site traffic without impeding northbound through traffic.

The design of the site access is provided in Appendix E.

## 8.3 Site Access Operation

Site access operation was reviewed using a heavy single unit (HSU) truck to simulate turning movements of aggregate trucks accessing and departing the site. Turning movement simulations show that all required turning movement operations can be accommodated at the site access.

Truck turning movement simulations at the future site access are provided in Appendix E.

## 8.4 Sightline Assessment

Sight distances were examined in both directions on Thorold Townline Road at the proposed site access. Our examination is based on the criteria contained in the Transportation Association of Canada (TAC) Guideline, 2017 edition. Thorold Townline Road has a posted speed of 80 km/h in the vicinity of the subject site. As per industry standard, sight distance was examined a design speed of 100 km/h or 20 km/h over the posted speed.

The criteria in the TAC guideline is based on passenger car operations and does not explicitly consider a variation for truck movements. Section 2.5.3.1 in the TAC Guideline indicates that although trucks need longer



stopping sight distances than passenger cars, the additional lengths required by trucks is balanced by the fact that a truck driver can generally see further than a passenger car driver due to the eye height advantage. The TAC Guideline goes on to say that "As a result, separate stopping sight distances for trucks are not generally used in highway design".

Our research of the policies employed by other jurisdictions in this regard revealed that a variation for trucks is likewise not applied. According to Section 3-6 in 'A Policy on Geometric Design of Highways and Streets, 6th Edition, 2011, published by the American Association of State Highway and Transportation Officials (AASHTO), the additional lengths required by trucks is balanced by the fact that "the truck driver is able to see substantially farther beyond vertical sight obstructions because of the higher position of the seat in the vehicle." Likewise, passenger cars approaching the site access would have longer sight lines due to the height of the trucks entering and exiting the site. In addition, due to their training, the average truck driver is typically more adept than the average passenger car driver at recognizing potential risks and reacting to same.

Based on the foregoing, we have utilized the criteria as presented in the TAC guideline. However, we have based our analysis on the maximum values contained therein to ensure a conservative analysis.

#### Assessment Criteria

Based on Table 2.5.2: Stopping Sight Distance on level roadways for Automobiles contained in the Transportation Association of Canada (TAC) Guideline (see **Appendix F**) the maximum stopping sight distance for an 100 km/h design speed is 185 metres.

Based on Table 2.5.3: Stopping Sight Distance on Grades contained in the Transportation Association of Canada (TAC) Guideline (see **Appendix F**) the maximum stopping sight distance for an 100 km/h design speed on a downgrade of 9% is 223 metres.

Based on Table 2.5.6 Decision Sight Distance contained in the Transportation Association of Canada (TAC) Guideline (see **Appendix F**) the maximum decision sight distance for a 100 km/h design speed on a roadway is 415 metres for an avoidance manoeuvre.

#### **Analysis Results**

The proposed access is located approximately 1.5 km north of the intersection of Lundy's Lane and 1.1 km south of Beaverdams Road. Based on our online review of Google aerial mapping, Thorold Townline Road is straight roadway with no horizontal curvature and minor vertical deflection gradually sloping upward from south to north, south of the proposed site access via Upper's Lane. The slope does not create any obstacles to drivers approaching the intersection nor to trucks at the site access. The proposed site access via Upper's Lane is located such that drivers approaching on Thorold Townline Road have an unimpeded view in excess of 415 metres in both directions.

Based on our review, the sight lines on Thorold Townline Road at the site access via Upper's Lane exceed those recommended for stopping and decision sight distances as contained in the TAC guideline.



## 9 CONCLUSION

Overall, the traffic generated by the proposed Upper's Quarry can be accommodated by the existing study area road network for the preferred haul route with minimal changes or upgrades to study area intersections. Two possible routes have been considered as appropriate 'haul routes' for material that will be shipped from the proposed Upper's Quarry to serve local and broader markets, however, Haul Route Option 1 (via Thorold Townline Road) was identified as the preferred haul route.

## 9.1 Haul Route Options

### Haul Route Option 1

The first option of a haul route for trucks to / from the proposed Upper's Quarry would utilize Thorold Townline Road to the north of the site, as it is a regional road and provides the most direct route to / from the quarry. The haul route includes the following roads:

- Thorold Townline Road north of the site access to Thorold Stone Road
- Highway 406 via Thorold Stone Road westbound
- Queen Elizabeth Way (QEW) via Taylor Rd northbound
- Queen Elizabeth Way (QEW) via Thorold Stone Road eastbound

#### Haul Route Option 2

Davis Road is designated as a provincial highway and is a major boundary road in close proximity to the site. Accordingly, it can also be considered an appropriate roadway to accommodate truck traffic to / from the quarry. The use of Davis Road as a second option for a haul route would result in a more circuitous haul route, as access to Davis Road would require quarry trucks to first travel south on Thorold Townline Road to Lundy's Lane, and then proceed west to Davis Road. The second haul route option includes the following roadways:

- Thorold Townline Road south of the site access to Lundy's Lane
- Lundy's Lane west to Davis Road
- Davis Road north to Thorold Stone Road
- Highway 406 via Thorold Stone Road westbound
- Queen Elizabeth Way (QEW) via Thorold Stone Road (eastbound) and Taylor Road northbound
- Queen Elizabeth Way (QEW) via Thorold Stone Road eastbound

### 9.2 Preferred Haul Route

TMIG recommends that Haul Route Option 1 be chosen as the preferred Haul Route, subject to approval by the Town and an appraisal of the cost of any road improvements required to accommodate truck traffic.

Haul Route Option 1 will also be seen as a preferable route by current and future residents within the vicinity of the proposed Upper's Quarry, as the Rolling Meadows Secondary Plan area represents a large amount of future residential traffic that will travel along Davis Road and Lundy's Lane. As such, it would be ideal to have truck traffic travel north directly on Thorold Townline Road (Haul Route Option 1), compared to the more circuitous route around the boundary of the future Rolling Meadows area (Haul Route Option 2).

Of note, Haul Route Option 1 will direct trucks northbound on Thorold Townline Road through a non-residential area, however, a causeway has been constructed along Thorold Townline Road to cross a waterway immediately south of Beaverdams Road. Depending on the structural properties of the causeway, improvements may need to be made in order to sustain the regular truck traffic associated with the proposed Upper's Quarry. Before the choice of haul route is finalized, it is recommended that Walker Aggregates Inc. and the Town perform a review of the existing load capacity of Thorold Townline Road in order to determine if any upgrades are required, and if so, what cost would be associated with the upgrades. If it is found that



upgrades are required, it should be determined if the upgrades would be needed to service the future Rolling Meadows development regardless of any Upper's Quarry operations. The cost of the roadway upgrades should be assigned proportionately to the parties that will derive direct benefits from the upgrades.

## 9.3 Capacity Analysis Results and Recommendations

Overall, the study area intersections operate well or at acceptable levels under all planning horizons. Some individual movements are approaching capacity, particularly under 2035 conditions, but still operate with acceptable delays of 80 seconds or less, indicating a Level of Service (LOS) 'E' or better. Some geometric changes and modifications to signal timing plans are recommended in order to address any capacity or queuing issues in order to allow for efficient movement of traffic through the study area.

Haul Route Option 1 via Thorold Townline to the north was identified as the preferred haul route, and accordingly future total traffic operations were analyzed for Haul Route Option 1 only. A summary of recommendations and timing of the improvements are provided below.

#### Background Conditions (2025 & 2035)

- With adjustments to existing signal timing plans, all study intersections operate at acceptable levels under 2025 and 2035 background conditions. Some individual movements are approaching capacity, but operate at acceptable levels of service.
- In general, it is suggested that the Thorold Townline Road and Beaverdams Road intersection be monitored for signalization in 2025, and that signals be installed prior to the 2035 planning horizon (i.e. prior to the combined full build-out of the Rolling Meadows development, Thorold Townline Road Employment Lands, and the proposed Upper's Lane Quarry).
- Construction of an auxiliary southbound right turn lane at the intersection of Thorold Townline Road and Lundy's Lane by the 2035 background planning horizon was found to provide better overall operations at the intersection. Interim adjustments to signal timings and introduction of protected phases could potentially negate the need for a southbound right turn lane, however, high volumes of southbound right-turning vehicles are predicted in 2035 that would benefit from a dedicated lane compared to the existing shared through/right turn lane. Given that the proposed Upper's Quarry is assumed to be active by 2025, quarry related traffic is not the primary cause of the high volume of right-turning vehicles predicted in 2035, particularly based on preferred Haul Route Option 1 (via Thorold Townline Road), as minimal staff site traffic travels through the intersection, and heavy vehicle site traffic will **not** travel through the Thorold Townline Road and Lundy's Lane intersection. The operational impact of Haul Route Option 1 site-related traffic at this intersection is negligible and will not trigger the aforementioned road improvements.
- There is opportunity to widen the existing 24 metre ROW at the Thorold Townline Road and Lundy's Lane intersection to the designated 26.2 metre road allowance to accommodate a southbound right turn lane. Furthermore, the Region may require road widening dedications in addition to the designated road allowances without the need for amendments to the Official Plan for purposes such as turning lanes at intersections.
- It is recommended the Thorold Townline Road and Lundy's Lane intersection be monitored in the future to determine whether constructing the dedicated southbound right turn lane would be the most appropriate solution to accommodate background development traffic volumes within the vicinity of the intersection.

#### Total Conditions (2025 & 2035)

- With adjustments to existing signal timing plans, all study intersections operate acceptably under 2025 and 2035 total conditions. Some intersections/movements are approaching, or are at capacity, but operate at acceptable levels of service.
- The proposed access design will be constructed in 2025 prior to the quarry becoming active. The proposed access design provides deceleration and accelerations lanes northbound at the site access (via Upper's Lane). A slip around lane is provided southbound, thus accommodating left-turning vehicles into the site and preventing blockage of through traffic at the site access.



The southbound queue at Thorold Stone Road and Thorold Townline Road should be monitored in 2035 to determine if any upgrades to the intersection are needed to address the potential for long queues to build up (southbound left experiences a queue up to 160m according to simulations). The long southbound left queue buildup does not occur under 2025 total conditions when Upper's Quarry is active, as such, quarry related traffic is **not** the cause of the long queues predicted in 2035.

## 9.4 Conceptual Site Access Design

The intersection of Uppers Lane and Thorold Townline Road is to be modified to accommodate truck traffic and function as the future access to the proposed Upper's Quarry. Access to the proposed Upper's Quarry via Upper's Lane will be achieved regardless as to the ownership of the road allowance, as the location will serve either as a direct access to the quarry, or as a roadway to access the quarry. Aggregate and Asphalt traffic (heavy vehicles) will access Upper's Lane / the proposed Upper's Quarry via Thorold Townline Road to/from the north, and will **not** access the proposed quarry via Beechwood Road. The quarry access will thus be located approximately one kilometre south of the Beaverdams Road and Thorold Townline Road intersection.

The proposed design for the access incorporates engineering design criteria as per the 2017 Transportation of Canada (TAC) geometric design guideline for Canadian roads and The Ontario Ministry of Transportation's (MTO) Commercial Site Access Policy and Standard Designs. The proposed access design provides deceleration and accelerations lanes northbound at the site access. A slip around lane is provided southbound, thus accommodating left-turning vehicles into the site and preventing blockage of through traffic at the site access.

Access design includes curb radii of 16m and 18m to accommodate future truck turning movements into and out of the site.

Entrance improvements shall be implemented prior to the haulage of extracted material off-site:

- At the intersection of Upper's Lane and Thorold Townline Road: including the installation of a southbound slip-around lane consisting of a parallel lane with 30 metres of storage plus approach / departure tapers of 150 metres, along with a northbound right-turn lane with a taper of 85 metres and a parallel length of 170 metres.
- Along Upper's Lane: including a widening of approximately 1.0 to 1.5 metres west of any proposed entrance along Upper's Lane and installation of a culvert for the future watercourse realignment.



## **APPENDIX A**

**Preliminary Site Plan** 



## A. General

1. This Site Plan is prepared under the Aggregate Resources Act for a Class A Licence for a quarry below the ground water table.

2. Area to be licenced 103.6 ha. (±256.0 ac.)

## Area to be extracted 89.1 ha. (±220.2 ac.) B. References

- Contour information was obtained from a topographic survey prepared by TEC Engineering (formerly Renishaw (Canada) Limited) using October 2016 and February 2017 aerial photography and are displayed in one metre intervals. Elevations shown are in metres above sea level (masl).
- Topographic information was obtained from numerous sources including Ontario GeoHub (Land Information Ontario), Google Earth Pro aerial photography captured on July 18, 2018 and field investigations for technical reports.
   All topographic features and structures are shown to scale in Universal Transverse
- Mercator (UTM) with North American Datum 1983 (NAD83), Zone 17 (metre), Central Meridian 81 degrees west coordinate system.
  Property boundaries were obtained from a Plan of Survey prepared by Matthews, Cameron, Heywood-Kerry T. Howe Surveying Ltd. dated April 5, 2012. Other property
- boundaries were established using Municipal Property Assessment Corporation (MPAC) parcel fabric data.
  5. Zoning categories on or within 120 metres of the licence boundary are from the City of
- Niagara Falls Zoning By-law No. 79-200 (Schedules A3 and A4 Consolidation April 2015).
  Land use information on or within 120 metres of the licence boundary has been compiled from October 2016 ortho photography, site visits and water well survey data.
- C. Groundwater
- The maximum predicted water table is 184.9 masl and the contact aquifer potentiometric contours ranges between 176.0 and 184.9 masl (as per WSP's "Proposed Upper's Quarry - Maximum Predicted Water Table Report", dated October 2021.
   Drainage

## 1. Existing surface water drainage on and within 120 metres of the licence boundaries

- are by overland flow in the direction shown by arrows on the plan view. E. Site Access and Fencing
- 1. There are two (2) existing site accesses on Thorold Townline Road, six (6) existing site accesses on Upper's Lane, and three (3) existing site accesses on Beechwood
- Road.2. Post and wire fencing (unless otherwise noted) exists in the locations shown on the

## plan view.

F. Aggregate Related Site Features

## There are no existing aggregate operations or features within the licence boundaries such as stationary or portable equipment, stockpiles, recyclable materials, scrap, fuel storage, haul roads, berms or excavation faces.

- G. Technical Reports References
- Upper's Quarry: Acoustic Assessment Report, RWDI, October 2021.
   Agricultural Impact Assessment for Upper's Quarry, Colville Consulting Inc., October
- 2021.
- 3. Upper's Quarry: Air Quality Assessment, RWDI Air Inc., October 2021.
- Archaeological Assessments:
   a. Stage 1 Archeological Resource Assessment of Walker Aggregates Proposed South Niagara Quarry, Part of Lots 102, 119, 120, 136 & 137, Archeological Services Inc., December 2008.
- b. Stage 1-2 Archeological Assessment of Part 9764 Uppers Lane, Part of Lots 119 & 120, Archeological Assessments Ltd., November 3, 2005.
- c. Stage 2-3 Archeological Assessment, Part of Lots 102, 119, 120, 136 & 137, Archeological Assessments Ltd., November 21, 2012.
- d. Stage 1-2 Archeological Assessments, Upper's Quarry Additional Lands, Part of Lots 119& 120, Archaeological Research Associates Ltd., April 20, 2020.e. Stage 3 Mitigation of Development Impacts, Final Excavation Report, Walker XI
- (AgGT-411), Upper's Quarry, Archaeological Research Associates Ltd., May 26, 2021.f. Stage 4 Mitigation of Development Impacts, Final Excavation Report, Walker XI
- (AgGT-178), Upper's Quarry, Archeological Research Associates Ltd., July 22, 2021.
- 5. Blast Impact Analysis, Upper's Quarry, Explotech, October 2021.
- 6. Cultural Heritage Impact Assessment Report, Proposed Upper's Quarry, MHBC, October 2021.
- 7. Economic Benefits Analysis, Prism, October 2021.
- 8. Level 2 Water Study Report, WSP, October 2021.
- 9. Maximum Predicted Water Table Report, WSP, October 2021.
- Upper's Quarry, Niagara: Level 1 and Level 2 Natural Environment Technical Report and Environmental Impact Study, Stantec, October 2021.
   Planning Justification Report and Summary Statement, MHBC, October 2021.
- 12. Traffic Impact Study, Upper's Quarry, TMIG, October 2021.
- 13. Visual Impact Assessment, Proposed Upper's Quarry, MHBC, October 2021.

- r
- 6.
- 7. 8.
- 9. 10.
- 1[.]
- 12. II 13. V





## Site Plan Acronyms

- 1. ARA Aggregate Resources Act
- 2. MNDMNRF Ministry of Northern Development, Mines, Natural Resources and Forestry
- 3. MHSTCI Ministry of Heritage, Sport, Tourism and Culture Industries
- MECP Ministry of the Environment, Conservation and Parks
   MGCS Ministry of Government and Consumer Services
- 6. DFO Department of Fisheries and Oceans Canada
- 7. ECA Environmental Compliance Approval
- 8. BMPP Best Management Practices Plan
- 9. PTTW Permit to Take Water
- 10. MASL Metres above sea level
- ROW Right of way
   HMA Hot mix asphalt

Site P	lan Amendmen	ts				
No.	Date		Descript	ion		Ву
Site P	lan Revisions (I	Pre-Licencing)				
No.	Date		Descript	ion		Ву
MHBC	<b>Stamp</b> <b>Debra Wall</b> s authorized by the Northern Developm latural Resources bursuant to Section Aggregate Resou prepare and certify	<b>ker</b> Ministry of ment, Mines, and Forestry 2 (1) of the roces Act to y site plans.	ABBC Stamp Christophe Is authorized by a Northern Develor Natural Resource pursuant to Secti Aggregate Resource prepare and cert	PLAN URBAN & LAN ARCHI 3.0045 F: 705.728.2010		G PE RE N.COM
Applic	cant	walk	Walke 2800 P.O. E tes Thoro L2V 3	er Aggregates Inc. Thorold Townline I Box 100 Id, Ontario Y8	Road	
Projec	:t	Upp	er's Qu	arry		

MNDMNRF Licence Reference No.	Applicant's S	ignature	
Plan Scale: 1:3000 (Arch E)	Date	Oct	tober 2021
0 90 180	Drawn By	C.P.	File No.
Meters	Checked By	D.W.	9811V
File Name Exist	ing Fea	ature	S
Drawing No.	1 of 6	)	

File Path N:\Brian\9811V - Walker Uppers Quarry\Drawings\Site Plan\CAD\9811V - Site Plan - Proposed Scenario.dwg

- A. General
- 1. Area to be licenced Area to be extracted
  - 89.1 ha. (±220.2 ac.)

103.6 ha. (±256.0 ac.)

- 2. The maximum amount of aggregate to be removed from this site in any calendar year is 1,800,000 tonnes. 3. In the event that Walker obtains permission from the City of Niagara Falls to extract the road allowance(s), the licensee may apply to the MNDMNRF to amend the licence and site plan to expand the licence boundary to include the road allowance directly adjacent to the licence boundary (i.e. Upper's Lane and/or the road allowance
- between Lots 120 and 136). An expansion to the licence boundary for this purpose will not require a new licence under Section 7 of the Aggregate Resources Act (ARA).
- 4. All technical reports have taken into consideration the potential removal of the road allowance(s).
- 5. Table 1 on this drawing identifies the number of sensitive receptors within 500 metres of the licence boundary and the distance from the licence boundary to each receptor.
- B. Hours of Operation 1. The proposed quarry will have the following hours of operation:

Activity	Monday to Friday	Saturday	Sunday
Drilling, extraction (at working face)	7:00 am to 7:00 pm	7:00 am to 7:00 pm	N/A
Blasting	8:00 am to 6:00 pm	N/A	N/A
Aggregate processing at mobile crusher plant	7:00 am to 7:00 pm	7:00 am to 7:00 pm	N/A
Asphalt plant operations	24 hours per day	24 hours per day	24 hours per day
Internal hauling of aggregate and/or recycled material: - From working face (shot rock) to mobile crusher	7:00cm to 7:00cm	7:00cm to 7:00cm	N//A
plant		7.00am to 7.00pm	N/A
- From mobile crusher plant/stockpiles to asphalt plant	24 hours per day	24 hours per day	24 hours per day
Aggregate and recycling shipping to and/or from the quarry (including hot mix asphalt shipping from quarry and receiving recycled asphalt to quarry)	24 hours per day	24 hours per day	24 hours per day
Maintenance	24 hours per day	24 hours per day	24 hours per day

C. Proposed Entrances/Exits and Fencing

## 1. For the Mid Extraction Area:

- a. All traffic for operations will enter and exit the Mid Extraction Area from Upper's Lane using a main entrance/exit in the location generally shown on the plan view.
- b. If an entrance/exit off of Upper's Lane is not permitted, traffic for operations will enter and exit the Mid Extraction area from Thorold Townline Road. If approved, the site plan will be updated to accurately depict the location of the entrance/exit off of Thorold Townline Road.

## 2. For the South Extraction Area:

- a. Material will be transported to the Mid Extraction Area for processing via a conveyor over the unopened road allowance between Lots 120 and 136. Limited traffic required for operations will enter and exit the South Extraction Area via a crossing over the unopened road allowance between Lots 120 and 136, subject to approval from the City, in the location generally shown on the plan view.
- b. If permission to cross the unopened road allowance is not granted, traffic for operations will enter and exit the South Extraction area from Thorold Townline Road. If approved, the site plan will be updated to accurately depict the location of the entrance/exit off of Thorold Townline Road.
- 3. For the North Extraction Area:
- a. All traffic for operations will enter and exit the North Extraction Area from Upper's Lane using a main entrance/exit in the locations generally shown on the plan view. b. If an entrance/exit off of Upper's Lane is not permitted, traffic for operations will enter and exit the North Extraction area from Thorold Townline Road. If approved, the site plan will be updated to accurately depict
- the location of the entrance/exit off of Thorold Townline Road.
- 4. Only one operational entrance/exit will be utilized at any one time. 5. Once established, each operational entrance/exit shall be gated. All gates shall be kept closed during hours of L. Spills Plan
- non-operation and shall be maintained throughout the life of the licence.
- 6. The licence boundaries shall be fenced in the locations shown on the plan view (prior to the commencement of operations) and shall be maintained for the life of the licence with upkeep during periodic inspections (see Section N Variations from Control and Operation Standards on this drawing).

## D. Drainage and Siltation Control

1. Silt fencing/sediment control measures will be installed within the Watercourse Realignment Transition Area prior to extraction in each extraction area and along the easterly and northerly limits of Phase 1B after the watercourse realignment is completed.

## E. Site Preparation

- 1. All existing structures within the licence boundary shall be demolished or removed prior to extraction in each extraction area. 2. Timber resources (if any) will be salvaged for use as saw logs, fence posts and fuel wood where appropriate.
- Stumps and brush cleared will be burned (with applicable permits), used for shoreline habitat enhancement or mulched for use in progressive rehabilitation. 3. Areas of the site will be stripped of topsoil/overburden in stages in accordance with the phases. Topsoil and
- overburden will be stripped and stored in berms and/or stockpiles wherever feasible. 4. Topsoil and overburden shall be placed in perimeter acoustic/visual berms, pond construction, watercourse **M. Scrap and Recycling** realignment or used immediately for progressive rehabilitation in this licence or existing Licence Numbers 11175 and 4437 (see Section N Variations from Control and Operation Standards on this drawing).
- 5. Excess topsoil and overburden not required for immediate use in berms or rehabilitation may be temporarily stockpiled on the quarry floor. Topsoil and overburden stockpiles shall be located within the limit of extraction and remain a minimum of 30 metres from the licence boundary and 90 metres from a property with a residential use.
- 6. Temporary topsoil and overburden stockpiles which remain for more than one year shall have their slopes vegetated to control erosion. Seeding shall not be required if these stockpiles have vegetated naturally in the first

## F. Setbacks, Berms and Screening

- Setbacks are as shown on the plan view. Excavation will occur within the extraction setback area along the west and northwest area of the licensed boundary to accommodate grading required for the realignment of the existing watercourse. Furthermore, areas within the setbacks will be accessed as necessary to perform general site servicing, maintenance (berming, fencing etc.) and progressive rehabilitation. See Section N Variations from Control and Operation Standards on drawing 2 of 6.
- Locations and heights for all acoustic/visual berms are provided on the plan view. All proposed berms shall be constructed in accordance with the "Typical Acoustic Berm Detail" (on this drawing), "Typical Visual Berm Detail" (on drawing 4 of 6) and, more specifically, berms adjacent to Beechwood Road will be constructed in accordance with "Typical Berm - Adjacent to Beechwood Berm Detail" (on this drawing). Where the proposed berm transects the existing watercourse along the north perimeter, a culvert shall be installed in accordance with DFO requirements. Culverts will also be installed under berms, where necessary, to maintain existing drainage to and from off-site and to the existing watercourse. All proposed berms and will be vegetated and maintained to control erosion. Temporary erosion control will be implemented as required.
- Perimeter acoustic berms may be removed for final rehabilitation in the final Phase when they are no longer required for noise attenuation.
- 4. Any natural treed buffer areas in the setbacks will be maintained where feasible subject to berm requirements. G. Site Dewatering
- 1. Surface water will be discharged from the sump areas to the existing watercourse until the watercourse is realigned to the location of Phases 1B and 2B. Once the watercourse realignment has been completed, surface N. Variations from Control and Operation Standards water will be discharged from the sumps to the realigned watercourse in Phase 1B.
- Sump: During quarry development, a portable submersible pumps will be installed in each Initial Sinking Cut Area for the purpose of dewatering to maintain a dry working area and/or aggregate washing. Water will be pumped from the sumps to a pond where it is either used for aggregate washing or discharged to the existing watercourse. The sumps shall be relocated (as required) within each extraction area during the operational life of the quarry

## H. Extraction Details 1. The extraction sequence is outlined on drawing 3 of 6.

- 2. The proposed maximum depth of extraction is indicated by the spot elevations shown on the plan view. Extraction shall proceed to a maximum depth of approximately 42 m below ground surface (ranging in elevation from 141 masl in the southwest to 149 masl in the northeast portions of the site), corresponding to the geologic base of the Gasport dolostone of the Lockport Group.
- 3. For Phases 1B and 2B, the maximum depth of extraction is approximately 30 metres (down to an elevation of 155 masl) and may be extracted in 1-2 lifts. 4. For the "Watercourse Realignment Transition Area", the maximum depth of extraction is approximately 1 metre
- (down to an elevation of 174 masl) and any extraction in the "Watercourse Realignment Transition Area" shall be completed as part of site preparation (construction of compensatory ponds). No drilling or blasting shall be permitted in the "Watercourse Realignment Transition Area".
- 5. Internal haul road locations shall vary as extraction progresses and will be located on the quarry floor with the exception of at grade crossings.
- 6. Blasted aggregate will be transported back to the mobile crusher plant and processing area on the quarry floor for processing and shipping. 7. An office/scale house and weigh scale will be established on site. A maintenance shop and shed(s) may be
- constructed on site. Portable office/storage trailers and structures associated with fuel storage may be brought onto the site for temporary periods for uses associated with quarry activity. All structures shall remain 30 metres from the licence boundary / Trans Canada Pipelines easement or 90 metres from the licence boundary if the boundary abuts land that is used for residential purposes or is restricted to residential use by the Zoning By-law at the time the licence is issued.
- Aggregate stockpiles (including recyclable material) shall be located within the limits of extraction and remain a minimum of 30 metres from the licence boundaries (except where the licence boundaries abut Upper's Lane and the unopened road allowance - See Section N Variations from Control and Operation Standards on this drawing) and 90 metres from a property with a residential use.

**Typical Acoustic Berm Detail** 



## I. Equipment and Processing

- permitted within the North and Mid Extraction Areas inclusive.
- boundary and 90 metres from a property with a residential use. tertiary crushers, will remain close to the quarry entrance. The processing plant will be located at varying and then the final quarry floor as space becomes available.
- location shown on the plan view for the life of the quarry.
- drawing 4 of 6.
- processing plant, subject to permit approval from MECP.
- 7. Equipment to be used onsite may include, but shall not be limited to: a. Working Face - 1 silenced rock drill; 1 loader;
- stockpiles):
- motor, conveyor motor, oven motor, pug mill (door and motor);
- d. Conveyor(s); e. Generator(s) (diesel-fueled); and
- f. Rock trucks, haul trucks, shipment trucks and fuel trucks.
- Certificate of Approval will be obtained for processing equipment to be used on site.

- Frequency / Timing of Blasts
- drawing 4 of 6.
- requirements. K. Fuel Storage

# 217/01.

- volume.
- 3. Fuel trucks shall be used to transfer fuel to on-site equipment in accordance with the Liquid Fuels Handling Code, 2000

this plan.

- 1. In case of an accidental spill of petroleum products, the following contingency plan will be activated: a. The Ministry of Environment, Conservation and Parks (MECP) (see address and phone number below) and
  - surrounding landowners will be notified.
- c. The quarry operator shall commence recovery procedures by collecting the spilled substance into
- containers.
- by the MECP. Ministry of Environment, Conservation and Parks Niagara District Office Garden City Tower 9th Floor Suite 15 301 St. Paul Street St. Catharines, Ontario

## L2R 7R4 Spills Action Centre: 1-800-268-6060

- 1. Scrap may be stored on-site and shall be removed on an on-going basis.
- scrap metal, lumber, discarded machinery, equipment and motor vehicles.
- disposed of in accordance with the Environmental Protection Act.
- proximity to the main processing plant.
- 5. Recycling of asphalt, concrete, porcelain and glass shall be permitted on-site.
- Recyclable asphalt materials shall not be stockpiled within:

## 6.1. 30 metres of any waterbody or man-made pond; or

- 6.2. 2 metres of the ground water table.
- 7. Recyclable material shall be kept in close proximity to the main processing plant.
- placed in a designated scrap pile on-site which shall be removed on an o-going basis.
- 9. Recycled aggregate shall be removed on an on-going basis.
- 11. Once the site is depleted, no further importation of recyclable material shall be permitted.
- operations shall cease.
- 13. The site shall be kept in an orderly condition.

# Variations from Contr

- Extraction shall occur within 30 metres but no close allowance and the unopened road allowance betw In addition, as part of construction of any access watercourse realignment, extraction may occur: - Within the 15 metre setback from the Upper's L allowance between Lots 120 and 136 for access - Within the 15 metre setback from the north and construction and - Within the 30 metre setback from Thorold Town
- Overburden may be removed from the extraction - Extraction within 30 metres but no closer than 15 the unopened road allowance between Lots 120 a Overburden and aggregate may be removed from
- construction of any access or to implement the ex - Within the 15 metre setback from the Upper's La allowance between Lots 120 and 136 for access - Within the 15 metre setback from the north and s construction and - Within the 30 metre setback from Thorold Town

**Typical Berm - Adjace** — 6.0m_-Red Fescue, Perennial Rye & White Clover)

1. A portable processing plant (including primary, secondary and tertiary crushing and screening units) will be 2. Processing shall be located within the limit of extraction and remain a minimum of 30 metres from the licence

During the sinking cuts and early phases of operation, the primary crusher will be integrated into a single processing plant located near the working face. In later phases, the primary crusher will split from the single integrated plant and start to follow the working face. The processing plant, which contains the secondary and

elevations, beginning at the top of rock during the sinking cut portion of operations, and moving to the first bench

Once processing has progressed to Phase 2A, a hot mix asphalt (HMA) batch plant facility shall be established on the quarry floor (in the location shown on the plan view) in Phase 1A. The HMA batch plant shall remain in the

5. In Phase 4, the portable processing plant shall require additional shielding in accordance with note A.5 on

6. A wash plant and temporary wash ponds may be established and located to move together with the portable

b. Processing - 1 portable processing plant including crushers, screeners, and stackers; 2 loaders (at

c. Asphalt - 1 asphalt plant; 2 loaders, 1 compressor vent, 1 dust controller blower (motor and stack); elevator

8. All processing equipment is subject to applicable permitting under MECP Environmental Compliance Approvals and Ontario Water Resources Act where water use requires water taking and/or discharge. If required, a 9. Equipment used for construction of the perimeter berms/barriers, overburden stripping, rehabilitation, the new watercourse corridor, as well as other quarry related construction projects will be utilized on site.

Prior to blasting being permitted within the 100 m setback of the TransCanada Pipeline, identified as 'TransCanada Blasting Buffer Area' on this Plan, the licensee shall address the requirements of notes D.5 on

2. All blast monitoring reports shall be retained by the licensee for a period of seven years after each blast and made available upon request for audit purposes. See Section D on drawing 4 of 6 for detailed blasting

Fuel storage tanks will be located in close proximity to the main processing plant (or in an alternative location subject to approval by the MNDMNRF). Fuel storage tanks shall be installed and maintained in accordance with Technical Standards and Safety Act, 2000. Liquid Fuels Handling Code, 2000 and Liquid Fuels Regulation Reg.

2. All fuel tanks shall be doubled sided or placed in containment facilities large enough to hold the tanks maximum

4. A Spills Contingency Plan shall be prepared and implemented prior to site preparation. The Spills Contingency Plan shall be available on site and all employees and contractors shall be informed and required to comply with

b. For a leakage or spill, immediate action will be taken to stop it. At the same, measures will be taken to prevent spreading. These measures may include building or berm or construction of a ditch, for instance.

d. The soil in the area affected by the spill or leak shall be removed and disposed of at a location prescribed

2. Scrap shall only include material generated directly as a result of the aggregate operation such as refuse, debris, 3. All fluids shall be drained from any discarded equipment, machinery or motor vehicle prior to storage and

4. Scrap shall not be stored within 30 metres of any body of water or the licence boundary and shall be kept in close

8. Rebar or other structural metal shall be separated from recyclable aggregate material during processing and

10. Recycling activities shall not interfere with the operational phases of the site or with rehabilitation.

12. Once final rehabilitation has been completed and approved in accordance with the site plan, all recycling

Variations from Control and Operation Standards							
	Variation	Standaro (0.13)					
	<ul> <li>Extraction shall occur within 30 metres but no closer than 15 metres from the Upper's Lane road allowance and the unopened road allowance between Lots 120 and 136.</li> <li>In addition, as part of construction of any access shown on the Site Plan and the existing watercourse realignment, extraction may occur: <ul> <li>Within the 15 metre setback from the Upper's Lane road allowance and the unopened road allowance between Lots 120 and 136 for access purposes,</li> <li>Within the 15 metre setback from the north and south boundaries of the site for riparian corridor construction and</li> <li>Within the 30 metre setback from Thorold Townline Road for riparian corridor construction.</li> </ul> </li> </ul>	(1) 9 and 10					
	<ul> <li>Overburden may be removed from the extraction setback area to permit:</li> <li>Extraction within 30 metres but no closer than 15 metres from Upper's Lane road allowance and the unopened road allowance between Lots 120 and 136</li> <li>Overburden and aggregate may be removed from the excavation setback areas to permit the construction of any access or to implement the existing watercourse realignment as follows:</li> <li>Within the 15 metre setback from the Upper's Lane road allowance and the unopened road allowance between Lots 120 and 136 for access purposes,</li> <li>Within the 15 metre setback from the north and south boundaries of the site for riparian corridor construction and</li> <li>Within the 30 metre setback from Thorold Townline Road for riparian corridor construction.</li> </ul>	(1) 11					
	Topsoil and overburden may be moved between this Licence and Licence Numbers 11175 & 4437 to provide for effective rehabilitation of these licences.	(1) 18					
	A portion of the quarry face shall remain vertical. See Rehabilitation Plan, drawing 5 of 6.	(1) 19					
-	The licence boundary for the North Extraction Area shall not be fenced on or west of the Trans Canada Pipeline easement. Fencing shall be erected on the eastern extent of the easement.	(3)(a)					

nt to Beechwood Road Detail	
N.T.S.	

Note: Construct berm in close proximity to limit of extraction to provide additional vegetative screening along Beechwood Road.



							Table 1: Rece	ptors Within	500m of Lice	nce Boundary						
Receptor	Address	Distance	Receptor	Address	Distance	Receptor	Address	Distance	Receptor	Address	Distance	Receptor	Address	Distance	Receptor	Address
101	10148 Beaverdams Road	184 m	121	5695 Osprey Avenue	374 m	141	9349 Madison Crescent	415 m	161	9245 Shoveller Drive	489 m	181	9414 Shoveller Drive	416 m	201	9461 Eagle Ridge Drive
102	10138 Beaverdams Road	442 m	122	5687 Osprey Avenue	362 m	142	9337 Madison Crescent	423 m	162	9245 Shoveller Drive	495 m	182	9404 Shoveller Drive	423 m	202	9500 Eagle Ridge Drive
103	9722 Beaverdams Road	234 m	123	5679 Osprey Avenue	350 m	143	9325 Madison Crescent	434 m	163	9312 Madison Crescent	417 m	183	9394 Shoveller Drive	428 m	203	9494 Eagle Ridge Drive
104	9582 Beaverdams Road	151 m	124	5671 Osprey Avenue	339 m	144	9315 Madison Crescent	445 m	164	9324 Madison Crescent	404 m	184	9374 Shoveller Drive	443 m	204	9490 Eagle Ridge Drive
105	9417 Beaverdams Road	447 m	125	5663 Osprey Avenue	333 m	145	9245 Shoveller Drive	469 m	165	9336 Madison Crescent	390 m	185	9364 Shoveller Drive	450 m	205	9484 Eagle Ridge Drive
106	9337 Beaverdams Road	475 m	126	5655 Osprey Avenue	321 m	146	9245 Shoveller Drive	461 m	166	9352 Madison Crescent	370 m	186	9354 Shoveller Drive	460 m	206	9440 Eagle Ridge Drive
107	5584 Beaverdams Road	81 m	127	5647 Osprey Avenue	311 m	147	9245 Shoveller Drive	453 m	167	9366 Madison Crescent	354 m	187	9344 Shoveller Drive	467 m	207	9440 Eagle Ridge Drive
108	5769 Beaverdams Road	287 m	128	5639 Osprey Avenue	299 m	148	9245 Shoveller Drive	447 m	168	9380 Madison Crescent	338 m	188	9334 Shoveller Drive	478 m	208	5772 Osprey Avenue
109	5821 Beaverdams Road	360 m	129	5631 Osprey Avenue	290 m	149	9245 Shoveller Drive	440 m	169	5610 Osprey Avenue	311 m	189	9324 Shoveller Drive	488 m	209	9440 Eagle Ridge Drive
110	5783 Osprey Avenue	490 m	130	5623 Osprey Avenue	284 m	150	9245 Shoveller Drive	410 m	170	5622 Osprey Avenue	323 m	190	9314 Shoveller Drive	494 m		
111	5775 Osprey Avenue	480 m	131	5615 Osprey Avenue	271 m	151	9245 Shoveller Drive	425 m	171	5632 Osprey Avenue	331 m	191	9355 Eagle Ridge Drive	494 m		
112	5767 Osprey Avenue	470 m	132	5607 Osprey Avenue	259 m	152	9245 Shoveller Drive	435 m	172	5642 Osprey Avenue	341 m	192	9365 Eagle Ridge Drive	481 m		
113	5759 Osprey Avenue	459 m	133	9445 Madison Crescent	280 m	153	9245 Shoveller Drive	443 m	173	5652 Osprey Avenue	350 m	193	9375 Eagle Ridge Drive	469 m		
114	5751 Osprey Avenue	448 m	134	9433 Madison Crescent	299 m	154	9245 Shoveller Drive	457 m	174	5668 Osprey Avenue	362 m	194	9385 Eagle Ridge Drive	471 m		
115	5743 Osprey Avenue	438 m	135	9421 Madison Crescent	316 m	155	9245 Shoveller Drive	467 m	175	9405 Shoveller Drive	374 m	195	9395 Eagle Ridge Drive	464 m		
116	5735 Osprey Avenue	424 m	136	9409 Madison Crescent	334 m	156	9245 Shoveller Drive	476 m	176	9395 Shoveller Drive	383 m	196	9045 Eagle Ridge Drive	457 m		
117	5727 Osprey Avenue	415 m	137	9397 Madison Crescent	351 m	157	9245 Shoveller Drive	485 m	177	9385 Shoveller Drive	392 m	197	9415 Eagle Ridge Drive	448 m		
118	5719 Osprey Avenue	404 m	138	9385 Madison Crescent	371 m	158	9245 Shoveller Drive	498 m	178	9446 Shoveller Drive	400 m	198	9425 Eagle Ridge Drive	445 m		
119	5711 Osprey Avenue	393 m	139	9373 Madison Crescent	391 m	159	9245 Shoveller Drive	474 m	179	9434 Shoveller Drive	405 m	199	9435 Eagle Ridge Drive	443 m		
120	5703 Osprey Avenue	383 m	140	9361 Madison Crescent	407 m	160	9245 Shoveller Drive	482 m	180	9424 Shoveller Drive	412 m	200	9445 Eagle Ridge Drive	436 m		

Legal Des	cription		
Part of Lo City of N Regional	ots 119, 120, 136 & 137 iagara Falls (Geographic Towi Municipality of Niagara	nship of St	amford)
Legend			
/··/	Licence Boundary		120m Offset From Licence Boundary
. — .	Limit of Extraction		Trans Canada Blasting Buffer Area - See Note D.5 on drawing 4 of 6
a a a a a a a a a	Additional Lands Owned by Licensee		Parcel Fabric
	Municipal Boundary	GAS GAS	Trans Canada Pipeline Easement
149 150 151	Contours with Elevation Metres above sea level (MASL)	ОНОН	Hydro One Easement
	Public Road		Entrance / Exit
, x _ + _ + _ + _ + _ + _ + _ + _ + _ + _	Fence 1.2m post & wire farm fence unless otherwise noted	$\Leftrightarrow$	Limited Service Access For Phases 1A, 1B and 5 in South Extraction Area
	Watercourse Direction of flow indicated by arrows	X	Gate
	Surface Drainage Feature		Culvert
===;;==;;==	Watercourse - Realigned (Stantec, 2020)		General Direction of Excavation & Boundary
	Water Feature	<i>V777777</i> 3507324	Berm Top - Noise Attenuation Berm Bottom - Visual Berm
	Wooded Area		Building/Structure
		+ 180.0 143.0	Spot Elevation Metres above sea level (MA Top - Existing Bottom - Maximum Depth of Extraction
		$\frown$	Cross Sections

## Site Plan Acronyms

- 1. ARA Aggregate Resources Act
- 2. MNDMNRF Ministry of Northern Development, Mines, Natural Resources and Forestry

A1

- 3. MHSTCI Ministry of Heritage, Sport, Tourism and Culture Industries
- 4. MECP Ministry of the Environment, Conservation and Parks 5. MGCS - Ministry of Government and Consumer Services
- 6. DFO Department of Fisheries and Oceans Canada
- 7. ECA Environmental Compliance Approval
- 8. BMPP Best Management Practices Plan
- 9. PTTW Permit to Take Water
- 10. MASL Metres above sea level
- 11. ROW Right of way 12. HMA - Hot mix asphalt

Site Plan Amendments						
No	Data		Descrir	ation		By
Site D	Date					By
Site P	ian Revisions (I	Pre-Licencing)				
No.	Date	Description				Ву
	113 CC	DLLIER STREET, BARRIE,	<b>HBC</b> 0N, L4M 1H2   P: 705.7	PLAN URBAN & LAN ARCHI 28.0045 F: 705.728.2010	NIN DESIC DSCA ECTU	G GN PE RE
MHBC Stamp			MHBC Stamp			
Debra Walker			Christopher Poole		N	
Is authorized by the Ministry of Northern Development, Mines, Natural Resources and Forestry pursuant to Section 2 (1) of the Aggregate Resources Act to prepare and certify site plans.			Is authorized by the Ministry of Northern Development, Mines, Natural Resources and Forestry pursuant to Section 2 (1) of the Aggregate Resources Act to prepare and certify site plans.			E
Applio	cant					



Project

File Name

Drawing No.

MNDMNRF Licence Reference No.

Walker Aggregates Inc. 2800 Thorold Townline Road P.O. Box 100 Thorold, Ontario L2V 3Y8

	Distance
ē	427 m
j	474 m
j	477 m
è	478 m
j	480 m
j	484 m
5	495 m
	499 m
j	494 m

## Plan Scale: 1:3000 (Arch E) October 2021 CP File No. 9811V hecked By D.W **Operational Plan**

**Applicant's Signature** 

Upper's Quarry

2 of 6

 File Path
 N:\Brian\9811V - Walker Uppers Quarry\Drawings\Site Plan\CAD\9811V - Site Plan - Proposed Scenario.dwg

- A. General
- 1. This plan depicts a schematic operations sequence for the property based on the best information available at the
- time of preparation. 2. Phases do not represent any specific or equal time period.
- 3. The direction of extraction will generally be in accordance with the General Direction of Excavation (shown on the plan view). Notwithstanding the operational and rehabilitation notes, demand for certain products, blending of materials or Water Study Contingency measures may require minor deviations in the extraction and rehabilitation sequence.
- Progressive and final rehabilitation will be completed in direct correlation to the development of the quarry as the extraction limits are reached and enough area is available to ensure that rehabilitation activities will not interfere with the production, stockpiling and processing of aggregate materials.
- B. Initial Site Preparation
- 1. Generally, site preparation in Phases 1 and 2 to include but not limited to:
- a. Constructing the main entrance and cross over(s) in accordance with entrance permit approvals b. Establishing fencing around licenced boundary (see Section N Variations from Control and Operation Standards on drawing 2 of 6)
- c. Removal of trees and existing buildings (in accordance with all site plan requirements and applicable
- regulations) d. Proceed with stripping of overburden/topsoil from Phase 1 and, if necessary, Phase 2
- e. Construction of berms/acoustic barriers within the perimeter setback of the licence boundary (as shown on the plan view).
- Install water management and erosion and sediment control measures (silt fencing) in accordance with note D.1 on this drawing and note E.1.c on drawing 4 of 6.
- 3. Commence portable crushing/screening plant set up. The plant shall operate in accordance with Section A on drawing 4 of 6 for all Phases.
- C. Phase 1 (1A and 1B)
- 1. Commence extraction in the 'Initial Sinking Cut Area' identified in the Mid Extraction Area (see plan view for location).
- 2. Phase 1A shall be extracted in up to three (3) lifts to a depth ranging between 140 masl and 145 masl. 3. Phase 1B shall be extracted in one (1) to two (2) lifts to a depth of 155 masl.
- 4. A portable pump shall be utilized as necessary in the Mid Extraction Area and the South Extraction Area to discharge water to a man-made pond for aggregate washing or to a sediment forebay before being discharged to **F.** Phase 4 the existing watercourse. During heavy rainfall events (25 mm or more), the pump will be deactivated as necessary to prevent flooding along the watercourse downstream of the site. The discharge pond and forebay 1. Proceed with stripping of overburden/topsoil. locations will move with the quarry face until the final quarry depth is reached in each extraction area. At this point, a permanent sump shall be established in each extraction area.
- During Phase 1, a new watercourse channel shall be constructed along the east side of Thorold Townline Road (within Phase 1B) for the eventual realignment of the existing watercourse. As resource extraction is completed in Phase 1B, this area will be filled with clay overburden material from on-site to an elevation ranging between 173 to 178 masl. The new watercourse and riparian wetland channel shall be constructed, designed and vegetated in accordance with DFO's authorization and this Rehabilitation Plan (drawing 5 of 6).
- As extraction reaches the final quarry floor, and there is sufficient separation from the quarry floor working areas in Phase 1A, a 2:1 sideslope along the easterly and northerly limit of Phase 1B shall be backfilled with either: (i) overburden stockpiled on-site; (ii) overburden in Phase 2; or (iii) material imported from Licence Numbers 11175
- 7. Commence site preparation of Phase 2.

## D. Phase 2 (2A & 2B)

- 1. Commence extraction in the 'Initial Sinking Cut Area' identified in the North Extraction Area (see plan view for location).
- 2. Phase 2A shall be extracted in up to three (3) lifts to a depth ranging between 141 masl to 145 masl. 3. Phase 2B shall be extracted in one (1) to two (2) lifts to a depth of 155 masl.

- site. The discharge, pond and forebay locations will move with the quarry face until the final quarry depth is reached. At this point, a permanent sump will be established.
- and 4437.
- 7. Commence site preparation of Phase 3.
- E. Phase 3 (3A & 3B)
- 1. Proceed with stripping of overburden/topsoil.
- Phase 3A. proceed before extraction in Phase 3A.
- discharge water to a man-made pond for aggregate washing or to a sediment forebay before being discharged to will be established.
- 5. Phase 3A and 3B shall be extracted in up to three (3) lifts to a depth ranging between 145 masl to 149 masl.
- 6. Once the existing watercourse has been realigned, extraction in Phase 3A may proceed.
- there is sufficient separation from the quarry floor working areas.
- 8. Commence site preparation of Phase 4.

- 2. Commence Phase 4 extraction in an easterly direction, moving gradually from north to south.
- there is sufficient separation from the quarry floor working areas.
- G. Phase 5
- 1. Proceed with stripping of overburden/topsoil.

- there is sufficient separation from the quarry floor working areas.
- H. Final Phase
- ramp)
- scrap from the site.
- identified on drawing 5 of 6.











Undisturbed Site Preparation O Under Extraction Progressive and Final Rehabilitation



## 4. A portable pump shall be utilized as necessary to discharge water to a man-made pond for aggregate washing or to a sediment forebay before being discharged to the existing watercourse. During heavy rainfall events (25 mm or more), the pump will be deactivated as necessary to prevent flooding along the watercourse downstream of the

Similar to Phase 1, the new watercourse channel shall be constructed within Phase 2 running along the east side of Thorold Townline Road (Phase 2B) for the eventual realignment of the existing watercourse. As resource extraction is completed in Phase 2B, this area will be filled with clay overburden material from on-site to an elevation ranging between 173 to 178 masl. The new watercourse and riparian wetland channel will be constructed, designed and vegetated in accordance DFO authorization and Rehabilitation Plan (drawing 5 of 6). As extraction reaches the final quarry floor, and there is sufficient separation from the quarry floor working areas in Phase 2A, a 2:1 sideslope along the easterly and northerly limit of Phase 2B shall be backfilled with either: (i) overburden stockpiled on-site; (ii) overburden in Phase 3B; or (iii) material imported from Licence Numbers 11175

## 2. Prior to undertaking any works within Phase 3A that may result in any serious harm to fish, according to 35(1) of the Fisheries Act, the Licensee shall obtain a Fisheries Act Authorization from the Department of Fisheries and Oceans (DFO) and shall fulfill any other conditions required by the DFO as stated on its authorization. Once the watercourse has been realigned to the satisfaction of DFO, stripping of overburden and topsoil can proceed in

3. In the event that watercourse relocation has not been approved or completed, extraction in Phase 3B may 4. In the event that Phase 3B is extracted before Phase 3A, a portable pump shall be utilized as necessary to

the existing watercourse. During heavy rainfall events (25 mm or more), the pump will be deactivated as necessary to prevent flooding along the watercourse downstream of the site. The discharge, pond and forebay locations will move with the quarry face until the final quarry depth is reached. At this point, a permanent sump

Extraction will proceed in an easterly direction, moving gradually from north to south.

7. Continue progressive rehabilitation of the quarry perimeter where limits of extraction have been reached and

3. Phase 4 shall be extracted in up to three (3) lifts to a depth ranging between 142 masl in and 147 masl. 4. Continue progressive rehabilitation of the quarry perimeter where limits of extraction have been reached and

## 2. Commence Phase 5 extraction in an easterly direction, moving gradually from north to south. 3. Phase 5 shall be extracted in up to three (3) lifts to a depth ranging between 140 masl and 143 masl.

4. Continue progressive rehabilitation of the quarry perimeter where limits of extraction have been reached and

1. Complete extraction of any remaining resource in the extraction limit near the entrance in Phase 1A and 1B (e.g. 2. As part of the final operations of the site, remove office/scale house and scales and any other equipment and

3. Continue with final rehabilitation of the site. Complete quarry face backfilling on the remaining quarry faces as



Legend						
	Licence Boundary		120m Offset From Licence Boundary			
. — .	Limit of Extraction		Trans Canada Blasting Buffer Area - See Note D.5 on drawing 4 of 6			
, - , - , ^{, , ,}	Additional Lands Owned by Licensee		Parcel Fabric			
	Municipal Boundary	GAS GAS	Trans Canada Pipeline Easement			
149 150 151	Contours with Elevation Metres above sea level (MASL)	ОН	Hydro One Easement			
	Public Road		Entrance / Exit			
, x , t , t	Fence 1.2m post & wire farm fence unless otherwise noted	$\Leftrightarrow$	Limited Service Access For Phases 1A, 1B and 5 in South Extraction Area			
	Watercourse Direction of flow indicated by arrows	X	Gate			
	Surface Drainage Feature		Culvert			
===;;==;;==	Watercourse - Realigned (Stantec, 2020)		General Direction of Excavation & Boundary			
	Water Feature	(////// (5:07:5+)	Berm Top - Noise Attenuation Berm Bottom - Visual Berm			
	Wooded Area		Building/Structure			
		+ 180.0 143.0	Spot Elevation Metres above sea level (MAS Top - Existing Bottom - Maximum Depth of Extraction			
			Cross Sections			

## Site Plan Acronyms

- 1. ARA Aggregate Resources Act
- 2. MNDMNRF Ministry of Northern Development, Mines, Natural Resources and Forestry
- 3. MHSTCI Ministry of Heritage, Sport, Tourism and Culture Industries
- 4. MECP Ministry of the Environment, Conservation and Parks 5. MGCS - Ministry of Government and Consumer Services
- 6. DFO Department of Fisheries and Oceans Canada
- 7. ECA Environmental Compliance Approval
- 8. BMPP Best Management Practices Plan
- 9. PTTW Permit to Take Water
- 10. MASL Metres above sea level
- 11. ROW Right of way 12. HMA - Hot mix asphalt

Site P	Plan Amendmen	ts					
No.	Date			Description		Ву	
Site P	lan Revisions (	Pre-Licencing)					
No.	Date	Description			Ву		
P L A N N I N URBAN DESIG & LANDSCA & LANDSCA & LANDSCA & LANDSCA & LANDSCA ARCHITECTUMHBC StampDebra WalkerMHBC StampIs authorized by the Ministry of Northern Development, Mines, Natural Resources and Forestry pursuant to Section 2 (1) of the Aggregate Resources Act to prepare and certify site plans.MHBC StampMHBC StampLis authorized by the Ministry of Northern Development, Mines, Natural Resources and Forestry pursuant to Section 2 (1) of the Aggregate Resources Act to prepare and certify site plans.Image: Statual Resources and Forestry pursuant to Section 2 (1) of the Aggregate Resources Act to prepare and certify site plans.Image: Statual Resources and Forestry pursuant to Section 2 (1) of the Aggregate Resources Act to prepare and certify site plans.Image: Statual Resources and Forestry pursuant to Section 2 (1) of the Aggregate Resources Act to prepare and certify site plans.MAMAMAMMAMAMAMA							
Walker Aggregates Inc.         2800 Thorold Townline Road         Project         Walker Aggregates Inc.         2800 Thorold Townline Road         Project							
MNDMNRF Licence Reference No.       Applicant's Signature							

Plan Scale: 1:3000 (Arch E) October 2021 C.P. File No. 9811V checked By D.W. File Name **Extraction Sequence** Drawing No. 3 of 6

 File Path
 N:\Brian\9811V - Walker Uppers Quarry\Drawings\Site Plan\CAD\9811V - Site Plan - Proposed Scenario.dwg
#### A. Acoustic Assessment

- 1. Minimum 3 metre tall acoustic berms shall be constructed in the locations shown on the plan view.
- 2. The acoustic berms shall be constructed during site preparation and prior to extraction.
- 3. The primary crusher shall stay within 30 metres of the working face to maximize shielding effect of the quarry terrain.
- 4. Material extracted from the South Extraction Area shall be processed in the Mid Extraction Area.
- 5. While processing in Phase 4, the licensee shall maintain an 8 metre tall barrier at a radius of 40 metres to the southeast of the processing plant's secondary crushers (see plan view for location). The barrier can be material stockpiles, noise walls, or a combination of both. The barrier shall extend long enough to shield receptors R4 and R5 (see plan view) from the secondary crushers.
- 6. All construction equipment shall meet the sound emission standards defined in MECP Publication NPC-115.
- 7. The following best practice measures shall be undertaken to minimize the potential for construction noise impacts: a. Construction will be limited to time periods allowed by the City's applicable by-laws. If construction activities are required outside of these hours, the licensee will seek permits / exemptions directly from the City in advance.
- b. All internal combustion engines will be fitted with appropriate muffler systems.
- c. The licensee's operating procedures will contain a provision that any initial complaint will trigger verification that the general noise control measures agreed to on this Plan are in effect.
- d. In the presence of persistent noise complaints, all construction equipment will be verified to comply with MECP's NPC-115 guidelines.
- e. In the event of verified noise complaints, alternative noise control measures may be required where reasonably available. In selecting appropriate noise control and mitigation measures, consideration will be given to the technical, administrative and economic feasibility of the various alternatives.

#### B. Air Quality

- 1. The licensee shall apply water or another provincially approved dust suppressant to internal haul roads and processing areas, as necessary to mitigate dust.
- . Processing equipment shall be equipped with dust suppressing or collection devices, where the equipment creates dust and is operating within 300 metres of an air quality sensitive receptor (as set out in the Air Quality Impact Assessment).
- . The licensee shall obtain an environmental compliance approval under the Environmental Protection Act where required to carry out operations at the quarry.
- 4. The site will operate in accordance with the Best Management Practices Plan (BMPP) for Fugitive Dust Emissions. The BMPP may be amended from time to time, considering actual impacts and operational considerations. The recommendations in the BMPP are based on the maximum daily production rates. At lower production rates, the control measures specified in the BMPP can be reduced accordingly, provided dust remains mitigated on site.
- 5. The following mitigation measures shall be incorporated into the BMPP:
- a. Blasting operations occurring within 300 metres of a residential receptor shall have a smaller blast area, not exceeding 200 m² in area. b. Aggregate extraction, processing and shipping does not exceed 9,000 tonnes per day.

#### C. Archaeology

- 1. Areas identified as "Archaeological Site Protected Areas Requiring Further Archaeological Assessment" on this drawing reflect areas that require further archaeological assessment and are protected by a 20 to 30 metre protective buffer. A 50 metre monitoring buffer is also identified on this drawing.
- No ground alterations including overburden stripping and excavation, or development of any kind shall occur within areas identified as "Archaeological Site - Protected Areas Requiring Further Archaeological Assessment" and their respective protective buffers until:
- a. the required investigations are completed in accordance with the Stage 1 and 2 Archaeological Assessment prepared by Archaeological Research Associates Ltd. (April 2020). b. any recommendations that the respective site(s) has no further cultural heritage value or interest are made as a result of completing further investigations, and,
- c. the associated reports are entered into the Ontario Public Register of Archaeological Reports. . A temporary barrier shall be established around the perimeter of each 'Archaeological Site - Protected Areas Requiring
- Further Archeological Assessment" identified on this drawing as part of site preparation and in advance of extraction. 4. All soil disturbing activities within the 50 metres monitoring buffers shall be monitored by a licensed archaeologist to ensure the effectiveness of the avoidance strategy. The archaeologist shall ensure that the temporary barrier is in the appropriate location and shall be empowered to stop construction if there is a concern for impacts to an archaeological site. 'No go' instructions shall be issued to all work crews for the protected areas, and the locations of the protected areas shall be shown on all appropriate contract drawings. The protected areas shall be inspected by a licensed archaeologist once the strategy is no longer required, and the effectiveness of the strategy shall be reported to the MHSTCI.
- Immediately upon issuance of the Licence, and once the construction schedule has been finalized, a licensed archaeologist will be retained by the licensee so that monitoring can occur where required. The remaining F. archaeological fieldwork will be completed upon issuance of the licence by the MNDMNRF.
- 6. Should deeply buried archaeology remains be found during the course of site preparation and/or extraction related activities, the MHSTCI shall be notified. 7. In the event that human remains are encountered during construction or extraction activities, the licensee shall
- immediately contact both the MHSTCI and Registrar or Deputy Registrar of the Cemeteries Regulation Unit of the G. Ministry of Government and Consumer Services (MGCS).

### D. Blasting

- 1. An attenuation study shall be undertaken by an independent blasting consultant during the first 12 months of operation in order to obtain sufficient quarry data to confirm the initial guideline parameters and assist in refining future blast 2. All blasts shall be monitored for both ground vibration and overpressure at the closest privately owned sensitive
- receptors adjacent the site, or closer, with a minimum of two (2) instruments one installed in front of the blast and one installed behind the blast. Blasts shall be designed to maintain vibrations below 13mm/s at the location of the closest identified active spawning
- bed as per DFO guidelines. When blasting during active spawning season, a minimum of one supplemental vibration monitor shall be installed on the shoreline closest to the spawning bed to confirm the vibration levels. 4. The guideline limits for vibration and water overpressure shall adhere to standards as outlined in the Guidelines For the Use of Explosives In or Near Canadian Fisheries Waters (1998) or any such document, regulation or guideline
- which supersedes this standard. . All blasts shall be monitored for ground vibration at the adjacent Trans Canada Energy High Pressure Natural Gas Pipeline when blasting within 100m of the pipeline or when calculations suggest vibrations in excess of 35mm/s.
- 6. Blasts shall be designed to maintain vibrations at the transmission towers in the Hydro One Corridor below 50mm/s or any such document, regulation or corporate policy in effect at the time. When vibration calculations suggest vibrations
- at the towers may exceed 35mm/s, the towers shall be monitored for ground vibration. Blasts shall be designed to maintain vibrations at the 4832 Thorold Townline Road utility buildings below 50mm/s.
- When vibration calculations suggest vibrations at the utility buildings may exceed 35mm/s, the buildings shall be monitored for ground vibration. 3. The guideline limits for ground vibration and air overpressure shall adhere to standards as outlined in the Model
- Municipal Noise Control By-law publication NPC 119 (1978) or any such document, regulation or guideline which supersedes this standard. 9. Orientation of the aggregate extraction operation shall be designed and maintained so that the direction of the overpressure propagation will be away from structures as much as possible.
- 10. Blast designs shall be continually reviewed with respect to fragmentation, ground vibration and overpressure. Blast designs shall be modified as required to maintain compliance with current applicable guidelines and regulations.

11. Detailed blast records shall be maintained in accordance with current industry best practices.

#### E. Natural Heritage 1. <u>General</u>

- a. Existing vegetation within the setbacks shall be maintained except where berms, haul roads and conveyors are
- b. New vegetation shall be maintained in accordance with note G.5 on this drawing. c. Silt fencing shall be installed at the easterly limit of Phases 1A and 2A where field drainage enters the existing **H**.
- watercourse. Silt fencing will serve to demarcate the limit of protected area until the watercourse is diverted. d. Stockpiling of all excavated material shall be in accordance with note H.7 on drawing 2 of 6.
- e. Topsoil and overburden stockpiles shall be maintained in accordance with the Best Management Practices for the Protection, Creation and Maintenance of Bank Swallow Habitat in Ontario (MNRF 2017). Stripped overburden and topsoil for rehabilitation shall be utilized in accordance with notes E.4, E.5 and E.6 on drawing 2 of 6.
- f. Dust control will be implemented in accordance with Section B on this drawing.
- g. Fuel storage shall be in accordance with the notes under Section K on drawing 2 of 6. 2. Natural Channel Design
- a. The existing watercourse will remain open (not culverted) where it enters the south limit of the South Extraction Area. b. Where the watercourse exits the North Extraction Area, a culvert will be installed to maintain the watercourse
- while allowing an acoustic berm to be constructed. As part of final rehabilitation, the berm and culvert shall be removed to allow for the watercourse to be open. c. As part of site preparation, a compensation pond will be constructed in the Watercourse Realignment Transition
- Area within Phase 2B, in accordance with the Natural Channel Design Report (Stantec 2021). The compensation pond will be excavated to a maximum depth of 174 masl in this area and in accordance with DFO authorization. No drilling or blasting shall occur in this Transition Area.
- d. As extraction is completed in Phases 1B and 2B, these areas will be filled with clay overburden material to an elevation ranging between 173 to 178 masl. In accordance with the Natural Channel Design Report (Stantec 2021), a new watercourse channel will be constructed, vegetated and designed in these areas and will include the following design elements:
- d.1. Floodplain wetlands
- d.2. Fish habitat ponds, including new pike spawning habitat as well as foraging, spawning and rearing habitat for other fish species d.3. Creek sections
- d.4. Wood debris toe protection and wood reinforced banks
- d.5. Log sills
- d.6. Augmented riffle.
- e. Culverts will be installed under Upper's Lane and the unopened road allowance.
- f. 2:1 side slopes shall be established on the east side of the new watercourse channel down to the quarry floor. Once the realigned watercourse channel has been constructed in Phases 1B and 2B and adequate vegetation
- has been established (as confirmed by an ecologist), water from the existing watercourse will be diverted to the realigned watercourse in consultation with regulatory authorities.
- 3. <u>Woodland and Terrestrial Habitat Enhancement</u>
- a. The 2.0 ha woodland situated on the east side of Thorold Townline Road shall be removed during the advancement of operations in Phase 1A/1B. Tree clearing in the woodlot shall be undertaken outside of the breeding bird period and the active bat season from March 23 and August 26.
- b. The lands identified off-site as "Woodland Compensation Area" on this drawing, an area of 4.7 ha, shall be planted in accordance with the Rehabilitation Plan (drawing 5 of 6).

	C.	The lands identifie	d on-site as Deciduous W	loodland, Treed Deciduous Swamp and Swamp Thicket / Marsh
	d.	Meadow on drawin Planting for the of	g 5 of 6, an area of 4.0 ha, f-site woodland compensa	shall be planted in accordance with the Rehabilitation Plan. tion will commence in the appropriate planting season following
4.	<u>Signi</u>	licence approval. ficant Wildlife Habita	t and Wildlife	
	a.	Vegetation clearin (September 30 to A	g where milkweed plants April 1).	s are present will proceed when monarch larvae are absent
Ē	b.	The setbacks along coniferous trees an and local landscap	g Thorold Townline Road a ad shrubs with a range of s e shall be used (see Rehab	nd Beechwood Road shall be planted with a mix of deciduous and izes. Native plant materials that are complementary to the regional bilitation Plan, drawing 5 of 6).
5.	<u>vvood</u> a.	A woodland and w to: (i) allow practice Areas such as per achieve a net gain	ildlife habitat compensation Plan es and management to res st infestations, climatic con in the ecological functions o	n plan shall be prepared in consultation with regulatory authorities pond to changing forest dynamics in the Woodland Compensation nditions (e.g. species selection) and restoration ecology; and (ii) of the local and regional landscape through:
		a.1. Increasing a.2. Improving a	associated landscape funct	cover in the regional landscape; ions such as vegetative linkages and interior forest areas
		a.3. Improving f diversity, w the remova	forest ecological characteris while retaining native general al of the existing 2 ha wood	stics such as species diversity, age class distribution and structural tics through seed collection and replanting. For example, prior to land:
		a.3.1. Tre Co coi	ee seeds and nuts will be g mpensation Area to promo mposition to the removed v	athered from the woodland for direct planting in the Woodland te the continuity of local genetic stock and a similar community egetation community (FOD9)
		a.3.2. Lea est	af litter and sods containing ablishment of a healthy for	native understory vegetation will be transplanted to promote rapid est soil microbiome
		a.3.3. Tra pla	ansplanting of native saplin nting area, where feasible.	gs and small shrubs from the woodland to the compensation
		a.4. Incorporati structures producing t	ng specific wildlife habitat (bat boxes or condos), co trees;	features for bats, deer and other wildlife, such as bat roosting niferous tree clusters for cover, browse-tolerant shrubs and mast
		a.5. Incorporatii plantings t milkweed (.	ng specific planting in set hat provide habitat for mo Asclepias incarnata) and no	tbacks and the watercourse realignment channel. For example, onarch including common milkweed (Asclepias syriaca), swamp ectar producing plants.
6.	Fish a	and Fish Habitat	2 and D.4 on this drawing	
	b.	Water shall be dis watercourse realig discharged from th	charged from the sump ar nment channel. Once the he sump locations to the	rea to the existing watercourse until water flow is diverted to the watercourse realignment has been completed, water shall be realigned watercourse. Pumping and discharge shall occur as
	C.	Water collected from suspended solids pond treatment, w watercourse realig	fish habitat. om the sump area shall b and dissipation of other c vater will be discharged to inment channel. Once the e bolding pond to the reali	the directed to a holding pond for storage to allow for settling of onstituents such as hydrogen sulfide an alkalinity. Following this to the existing watercourse until water flow is diverted to the e watercourse realignment has been completed, water shall be
7.	Wetla	to support fish habi	itat.	
	a.	Wetlands along th watercourse realigi	e existing watercourse wi nment channel.	Il be maintained until the watercourse has been diverted to the
	b.	Once the watercou maintained.	rse has been diverted, the	created wetlands in the watercourse realignment channel shall be
8.	<u>Monit</u> a.	oring Program A monitoring plan s	shall be prepared in consul	Itation with regulatory authorities to assess the performance of the
	b.	dewatering. A monitoring progr	am of compensation plant	ing shall be prepared in consultation with regulatory authorities to
	C.	A trigger mechanis	ditions have been establishes m and contingency plan,	ed. as detailed in WSP's Water Study Report, shall be implemented
		upon licence appro habitat, wetland fe rehabilitation phase	val to proactively ensure had at at a downstream and at es.	atural heritage features and their functions are maintained (i.e. fish 5584 Beechwood Road, and woodlands) during operational and
<b>Tra</b> 1.	ffic Prior wider gene Move	to commencement nings (to Thorold To ral accordance with ement Diagram" prov	of extraction operations, th wnline Road) shall be com the figures titled "Uppers ided on this drawing.	ne required entrance improvements, road improvements and road apleted to the satisfaction of the applicable road authorities and in Lane Conceptual Intersection Design" and "Uppers Lane Vehicle
<b>Vis</b> 1.	ual Wher	e possible and to th	e extent to which it is pres	ent, existing vegetation located along the site perimeter within the
2.	3.0 m view. respe appe mowi	netre high acoustic b Berms shall be co ecting minimum hei arance. Berms shall ng and maintenance	ained. erms and 2.4 metre high vi nstructed in a smooth, rol ight requirements), and v be seeded with a naturalizi	sual berms shall be established in the locations shown on the plan ling manner with varying highpoints (where space permits while variations along the berm frontage to create a more natural ing mix of wildflowers and grasses to stabilize slopes and minimize
3.	Withi on ce up to from tolera	n the "Extended Platentre, depending on one third of its max the berm towards t ance and hardiness.	nting Areas" (as shown on species. Where possible, p imum height to appear mo he road where available s Native species that comple	this drawing), trees shall be planted at a spacing of 5 to 10 metres plantings shall be randomly spaced and staggered up on the berm re natural. Plantings shall also extend a minimum of 3 metres out space permits. All vegetation shall be selected for wind and salt ment the existing surroundings shall be utilized.
	Wher shall heigh	e "Large Planting S be planted with deo t, and shrub species	tock" is indicated (see plan ciduous trees of minimum s of minimum 40 centimetre	view and "Typical Visual Berm Detail" on this drawing), this area 40 millimetres caliper, coniferous trees of minimum 1.0 metre in s height.
	Wher shall heigh	e "Small Planting Si be planted with deci t, and shrub species	tock" is indicated (see plan iduous tree whips of minim s of minimum 20 centimetre	view and "Typical Visual Berm Detail" on this drawing), this area um 1.2 metres in height, coniferous trees of minimum 0.6 metre in s height (or bare root stock when in season).
	Plant Thoro shall	ing shall occur for 4 old Town Line Road. extend from the toe	0 metre stretches on eithe The large planting stock sl of the berm to 2 metres up	er side of Upper's Lane and the unopened road allowance facing hall be planted 3 metres beyond the berm and small planting stock the berm.
	Plant	species for berms m	nay include, but shall not be	e limited to the following:
	Tree: White	s e Pine	Common Hackberry	Chokecherry
	White Suga White	e Spruce r / Silver Maple e Pine	Paper Birch Trembling Aspen White Spruce	Pin Oak Basswood White Cedar
	Shru Stagł	bs norn Sumac	Nannyberry	Common Ninebark
4.	Amer To er	ican Elder	Dogwood	Highbush Cranberry etative screening shall be maintained as an effective visual screen
5.	over Durin years	time. Allowance of n g the first year, plan s, trees shall be insp	atural succession is encour ited trees shall be watered ected biannually (end of Y	aged. and monitored until established. After the first year and up to five ear 1, beginning of Year 3 and end of Year 4). Trees which are in
6.	poor A mo	condition at the time	shall be fertilized, watered 15% of all trees planted of	and monitored to improve their health and vigor.
Wa	Trees ter Stu	s that die exceeding Idy	this percentage shall be re	placed yearly, preferably in the spring or late summer.
1.	A lor stable	ng-term monitoring p e conditions are obse	program will be implement erved after quarry decomm	ed during the quarry operational and rehabilitation phases, until issioning.
2.	In the tthe le	e event a well interfe ocal groundwater us	erence claim is received, th ers.	ne licensee shall implement the following mitigation plan to proect
	a.	Prior to extraction, contact information wellshelpdesk@on	landowners shall be provi on for the licensee a tario.ca).	ded with a copy of the water well interference plan as well as the and MECP (Wells Help Desk 1-888-396-9355 or email
	b.	If a water well inter	ference claim is received by	y the licensee the following actions shall be taken:
		b.1. The license b.2. The license provided a	ee shall immediately notify ee shall contact a well co temporary water supply	MNDMNRF and MECP of the complaint. ntractor in the event of a well malfunction and residents will be within 24 hours, if the issue cannot be easily determined and
	C.	rectified. The well contracto possible. provided	r shall contact the resider	nt with the supply issue to rectify the problem as expediently as the work.
	d.	If the issue raised hydrogeologist / we number of factors,	by the landowner is related on the landowner is related to the landowner is related to the landowner is related to the landowner including pump failure (ow	ted to loss of water supply, the licensee shall have a qualified e likely causes of the loss of water supply, which can result from a wner's expense), extended overuse of the well (owner's expense),

- e. If it has been determined that the quarry caused the water supply interference (i.e., lowering of the water level),
- e.1. Adjust pump pressure;
- e.3. Deepening of the well to increase the available drawdown, if the well deepening changes the water
- quality a water treatment shall be provided;
- e.5. Relocation of the well to another area on the property; or
- e.6. Drilling multiple wells.
- responsible for the expense to restore the water quality.
- 3. A spill action plan shall be carried out in accordance with the notes in Section N Spills Plan on drawing 2 of 3.



#### Chokecherry Pin Oak Basswood White Cedar

ated to loss of water supply, the licensee shall have a qualified e likely causes of the loss of water supply, which can result from a wner's expense), extended overuse of the well (owner's expense), vner's expense) or lowering of the water level in the well from the s assessment process shall be carried out at the expense of the

the licensee shall continue to supply water at their expense until the problem is rectified. The following mitigation measures shall be considered, and the appropriate measure(s) implemented at the expense of the licensee:

e.2. Lowering of the pump to take advantage of existing water storage within the well;

e.4. Widening of the well to increase the available storage of water;

f. If the issue raised by the landowner is related to water quality, the licensee shall have a qualified hydrogeologist / well contractor determine the likely causes of the change in water quality, and review monitoring results at the quarry and background monitoring results from the baseline well survey to determine if there is any potential correlation with the quarry. If it has been determined that the quarry caused a water quality issue, the licensee shall continue to supply water at their expense until the problem is rectified. The licensee shall be responsible for restoring the water supply by replacing the well or providing a water treatment system. The licensee is

4. A trigger mechanism and contingency plan as set out in WSP's Level 2 Water Study Report shall be implemented.





# Site Plan Acronyms

- 1. ARA Aggregate Resources Act
- 2. MNDMNRF Ministry of Northern Development, Mines, Natural Resources and Forestry
- 3. MHSTCI Ministry of Heritage, Sport, Tourism and Culture Industries
- 4. MECP Ministry of the Environment, Conservation and Parks 5. MGCS - Ministry of Government and Consumer Services
- 6. DFO Department of Fisheries and Oceans Canada
- 7. ECA Environmental Compliance Approval
- 8. BMPP Best Management Practices Plan
- 9. PTTW Permit to Take Water
- 10. MASL Metres above sea level
- 11. ROW Right of way 12. HMA - Hot mix asphalt

Site P	lan Amendmen	ts						
No.	Date		Descrip	otion		Ву		
Site P	lan Revisions (I	Pre-Licencing)						
No.	Date		Descrip	otion		Ву		
	113 CC		HBC	PLAN URBAN & LAN ARCHI	NIN DESIC DSCA IECTU	G GN PE RE		
мнво	Stamp		MHBC Stamp					
	Debra Wal	ker	Christop	her Poole	ът			
	s authorized by the Northern Developm latural Resources a bursuant to Section Aggregate Resou prepare and certify	e Ministry of hent, Mines, and Forestry 2 (1) of the rces Act to v site plans.	Is authorized by Northern Devel Natural Resource pursuant to Sec Aggregate Re prepare and co	y the Ministry of copment, Mines, ces and Forestry ction 2 (1) of the sources Act to ertify site plans.	W S	E		
Applic	cant							
Walker Aggregates Inc. 2800 Thorold Townline Road P.O. Box 100								



Project

Thorold, Ontario L2V 3Y8

# **Upper's Quarry**

MNDMNRF Licence Reference No.		Applicant's Si	gnature			
Plan Scale: 1:3000 (Arch E)		Date October 2021				
0 90	180	Drawn By	C.P.	File No.	004414	
		Checked By	D.W.		9811V	
File Name Rep	ort Re	comm	enda	tions		
Drawing No.		4 of 6				

 File Path
 N:\Brian\9811V - Walker Uppers Quarry\Drawings\Site Plan\CAD\9811V - Site Plan - Proposed Scenario.dwg

#### **PROGRESSIVE REHABILITATION**

# A. General

1.	Area	calc	ulations:	
	a. Li	icenc	ed area	103.6 ha
	b. T	o be	extracted	89.1 ha
	c. F	inal r	ehabilitation within licence (total)	103.6 ha
	C	.a.	Lake	68.8 ha
	C	.b.	Shoreline wetland	1.3 ha
	C	.C.	Wetland/pond/stream	2.9 ha
	C	.d.	Terrestrial	22.7 ha
	C	.e.	Deciduous Woodland	1.2 ha
	C	.f.	Treed Deciduous Swamp	2.0 ha
	C	.g.	Swamp Thicket & Marsh Meadow	0.8 ha
	C	.h.	Undisturbed	3.9 ha
	d. T	o be	rehabilitated outside of licence:	4.7 ha
	d	.a.	Woodland Compensation Area	4.7 ha

2. The maximum predicted water table is 184.9 masl and the contact aquifer potentiometric contours ranges between 176.0 and 184.9 masl (as per WSP's "Proposed Upper's Quarry -Maximum Predicted Water Table Report", dated October 2021.

### B. Phasing

- 1. As excavation reaches the limit of extraction or maximum depth, progressive rehabilitation shall commence.
- Progressive rehabilitation shall follow the general direction and sequence of extraction identified on the plan view and described in the notes on drawing 3 of 6. Minor deviations in operational/rehabilitation sequence will be permitted in order to adjust for any variable resource and market conditions.
- 3. Prior to extraction commencing in Phases 3A and 3B, side sloping adjacent to Phases 1B and 2B shall be completed to allow for the existing watercourse realignment to be finalized.
- 4. Dewatering of the quarry will ultimately discharge to the watercourse (pre and post realignment). The quarry will continue dewatering operations to maintain a dry quarry floor. When the rock is fully extracted, it is proposed that dewatering operations will cease and the quarry will be permitted to fill naturally with surplus precipitation, surface water and any contribution from groundwater seepage to form a lake. As shown on the plan view, shallow shoreline wetland areas shall be created to provide aquatic habitat.
- 5. Watercourse Realignment Channel Area As portions of the watercourse realignment channel are constructed, the channel shall be planted according to the requirements of each respective planting zone: (i) riparian planting zone; (ii) upland planting zone; (iii) shoreline planting zone and (iv) life staking planting zone. Details relating to construction, planting and monitoring requirements for the watercourse realignment corridor are contained within the "Natural Channel Design Report" prepared by Stantec Consulting Ltd. (dated October 2021).
- 6. Reforestation Areas There are two main reforestation areas:
- 6.1. The Woodland Compensation Area (Off-site) to be no less than 4.3 ha in area. Plantings in this area are set out in Table 1 on this drawing. Planting for this Area (Off-site) will commence in the appropriate planting season following licence approval.
- 6.2. The on-site Woodland Compensation Area includes the areas identified as the Deciduous Woodland, Treed Deciduous Swamp and Swamp Thicket/Marsh Meadow, to be no less than 4.0 ha in total area. Plantings in these areas are set out in Tables 1 to 3 on this drawing respectively. In the Deciduous Woodlands (on-site), additional conifer species will be added to the species mix to provide additional screening. 7. A woodland and wildlife habitat compensation plan shall be prepared in consultation with
- regulatory authorities in accordance with Note E.5.a on drawing 4 of 6.

# C. Slopes and Grading

- 1. Progressive rehabilitation will utilize a variety of rehabilitation techniques including: a. backfilling extraction faces and quarry floors; or
- Leaving extraction faces vertical
- 2. Excess soil, as defined by Ontario Regulation 406/19 under the Environmental Protection Act, may be imported for the following rehabilitation purposes: 2.1. To establish the final elevations, slopes and grades depicted on the plan view
- 3. Excess soil imported for the rehabilitation purposes described above shall meet the soil quality, tracking and testing standards required by Ontario Regulation 406/19 or the applicable MECP standards at the time.
- 4. The final rehabilitated landforms established using the rehabilitation techniques will consist of a lake, shoreline wetlands, riparian corridor, woodlands, gradually sloping grades, 2:1 and 3:1 side slopes, and vertical faces as shown on the plan view.

# D. Seeding and Planting

- 1. Side slopes steeper than 3:1 shall be seeded with the Ministry of Transportation's (MTO) Ontario Roadside Seed Mix (Creeping Red Fescue, Kentucky Bluegrass, Perennial Ryegrass and White Clover) or equivalent.
- 2. The deciduous woodlands, treed deciduous swamp, swamp thicket/marsh meadow, shoreline wetland, and realigned watercourse channel (riparian corridor) shall be planted with species identified in Tables 1-5 on this drawing respectively.

# E. Drainage

- 1. Final surface drainage will follow the rehabilitated contours and directional arrows shown on the plan view. 2. Once the quarry is depleted, pumping will cease and portions of the site below the ground
- water table will fill with water. 3. The quarry dewatering discharge will be directed to the watercourse (pre and post alignment)
- and ultimately flow to Beaverdams Creek to support fish habitat and downstream wetlands. 4. The licensee shall operate in accordance with the conditions of the MECP, PTTW and ECA

#### for the ongoing dewatering of the site. F. Trigger Mechanism and Contingency Plan

1. During progressive rehabilitation, until surrendering the licence, the licensee is required to operate in accordance with the Trigger Mechanism and Contingency Plan, included in the Upper's Quarry Level 2 Water Study Report prepared by WSP, dated October 2021, as may be amended from time to time with approval from MNDMNRF.

# FINAL REHABILITATION

# A. General

- 1. All equipment shall be removed from the licenced area.
- 2. A field/property access entrance shall remain to access the watercourse (as realigned). 3. The long term average surface water and lake level elevation is estimated to be
- approximately 175.15 masl.
- 4. At final rehabilitation, outflow from the realigned watercourse and the quarry lake will continue to discharge from the licence area at the present location where the existing watercourse channel crosses the northern licence boundary.

#### Table 1: Deciduous Woodland Planting List Botanical Name % TREES Sugar Maple Acer saccharum 25 Carya ovata 15 Fagus grandifolia 15 Ostrya virginiana 20 Prunus serotina 5 Quercus rubra 15 Tilia Americana SHRUBS 15 Amelanchier arborea 20 Carpinus caroliniana 15 Hamamelis virginiana 15 Prunus virginiana 20 Rhus typhina 20 Cornus racemosa 15 Rubus odoratus GROUND COVER 20 Schizachyrium scoparium 15 Elymus histrix 15 Rudbeckia hirta 15 Carex granularis 8 Solidago canadensis 8 Oenothera biennis 5 Asclepias syriaca 5 Clematis virginiana Monarda fistulosa Anemone canadensis Euthamia graminifolia Symphyotrichum cordifolium 1 Aster novae-angliae Table 2: Treed Deciduous Swamp Planting List % Botanical Name Common Name







Table 5: Riparian Planting List

#### % Common Name Latin Name SHRUBS 14 Cornus amomum 12 Cornus foemina 12 Ilex verticillata 12 Rosa palustris 12 Salix bebbiana 14 Spirea alba 12 Viburnum lentago 12 Viburnum trilobum LIKES STAKES (Along Creek) 34 Cornus sericea 33 Salix discolor 33 Salix eriocephala RIPARIAN SEED MIX 20 Poa palustris 20 Carex granularis 10 Asclepias syriaca 10 Verbena hastata 10 Andropogon gerardii 10 Juncus tenuis 5 Rudbeckia hirta 4 Solidago canadensis 4 Clematis virginiana

4 Monarda fistulosa Anemone canadensis Symphyotrichum novae-angliae Symphyotrichum puniceum



Shagbark Hickory American Beech Ironwood Black Cherry Red Oak Basswood Juneberry Blue-beech Witch Hazel Chokecherry Staghorn Sumac Grey Dogwood Purple-flowering Raspberry Little Bluestern Bottlebrush grass Black Eyed Susan Meadow Sedge Canada Goldenrod Evening Primrose Common Milkweed Virgin's Bower Wild Bergamot Canada Anemone Grass Leaved Goldenrod Heart-leaved Aster New England Aster Freeman's Maple Eastern Cottonwood Bur Oak Eastern White Cedar Silky Dogwood Gray Dogwood Winterberry Swamp Rose Bebb's Willow Meadowsweet Vannyberry American Cranberry-bush Table 3: Swamp Thicket / Marsh Meadow Planting List Common Name

Common Name

Swamp Rose Bebb's Willow Meadowsweet Nannyberry American Cranberry-bush Red Osier Dogwood Pussy Willow Heartleaf Willow Fowl Bluegrass Fox Sedge Blue Vervain Meadow Sedge Grass Leaved Goldenrod Swamp Milkweed Dark Green Bulrush Soft Rush Boneset Stalk Grain Sedge Tall Manna Grass Woolgrass Spotted Joe Pye Weed Bebb's Sedge Blue Lobelia Purple Stemmed Aster Square Stemmed Monkey Flower Common Name

Water-plantain Swamp Milkweed Wild Calla Tussock Sedge Fox Sedge Turtlehead Blue Flag Iris Little Duckweed Water Smartweed Broad-leaved Arrowhead Wool-grass

Silky Dogwood Gray Dogwood Winterberry Swamp Rose Bebb's Willow Meadowsweet Nannyberry American Cranberry-bush Red Osier Dogwood Pussy Willow Heartleaf Willow Fowl Bluegrass Meadow Sedge Common Milkweed Blue Vervain Big Bluestem Path Rush Black Eyed Susan Canada Goldenrod Virgin's Bower Wild Bergamot Canada Anemone New England Aster

Purple Stemmed Aster

- 9. PTTW Permit to Take Water 10. MASL - Metres above sea level
- 11. ROW Right of way
- 12. HMA Hot mix asphalt

egal Description											
Part of Lots 119, 120, 136 & 137 Sity of Niagara Falls (Geographic Township of Stamford) Regional Municipality of Niagara											
_egend											
· - · ^	Licence Boundary		120m Offset From Licence Boundary								
. — .	Limit of Extraction		Parcel Fabric								
~~~~~	Additional Lands Owned by Licensee	149 150 151	Contours with Elevation Metres above sea level (MASL)								
	Municipal Boundary		Public Road								
	Watercourse Direction of flow indicated by arrows	GAS GAS	Trans Canada Pipeline Easement								
	Surface Drainage Feature Direction of flow indicated by arrows	он он	Hydro One Easement								
Z	Watercourse - Realigned (Stantec, 2020)	THALL	Extraction Face (Below water)								
	Waterbody		Entrance / Exit								
	Shoreline Wetland		Gate								
	Terrestrial Habitat		Culvert								
	Deciduous Woodland	×+	Fence 1.2m post & wire farm fence unless otherwise noted								
	Treed Deciduous Swamp		Building/Structure								
* * * *	Swamp Thicket and Marsh Meadow	\$ (75)	Proposed Floor Elevation Metres above sea level (MASL)								
	Woodland Compensation Area (Off-site)	20.1	Proposed Final Grade								
	Wooded Area		Cross Sections								

Legend - Cross Sections

Licence Boundary
Limit of Extraction
Existing Grade - Undisturbed
Existing Grade - Removed / Altered
(See note A.2 on this drawing)
Quarry Floor / Face
Backfilled
Lake or Pond





Project

2800 Thorold Townline Road P.O. Box 100 Thorold, Ontario L2V 3Y8

#### Upper's Quarry MNDMNRF Licence Reference No Applicant's Signature

WINDMINKF LICENCE Kelefence no.	Applicant's Si	gnature		
Plan Scale: 1:3000 (Arch E)	Date	Oct	ober 2021	
0 90 180	Drawn By	C.P.	File No.	
Meters	Checked By	D.W.	90110	
File Name Rehat	oilitatio	n Pla	an	
Drawing No.	5 of 6			

File Path N:\Brian\9811V - Walker Uppers Quarry\Drawings\Site Plan\CAD\9811V - Site Plan - Proposed Scenario.dwg





Å **Cross Section Key Map** Scale 1:4000

120 240 Meters



Site P	lan Amendmer	nts						
No.	Date			Description				Ву
Site P	lan Revisions (	(Pre-Licencing)						
No.	Date			Description				Ву
	113 C	OLLIER STREET, BARRIE,	<b>HB</b> ON, L4M 1H2	P C P:705.728.004	PLA JRBA LA LA RCI	N N N D N D S HITE( 010   WWW	IN ESIC CA CTU	G GN PE RE N.COM
мнвс	Stamp		MHBC Sta	amp				
	Debra Wa	alker		Christopher P	oole		$\mathbf{N}$	
N F	Northern Develop latural Resources pursuant to Sectio Aggregate Resou prepare and certif	and Forestry and Forestry n 2 (1) of the urces Act to fy site plans.	North Natur pursu Agg prep	al Resources ar Jant to Section 2 Jant to Section 2 Jaregate Resource Jare and certify s	ant, Mines, ad Forestry (1) of the es Act to site plans.	W-		E
Applic	cant			-				
		<b>walk</b>	er ates	Walker A 2800 Tho P.O. Box Thorold, 0 L2V 3Y8	ggregates orold Town 100 Ontario	Inc. line Road		
Projec	t	Upp	er's	Qua	rry			
MNDM	INRF Licence F	Reference No.		Applicant's S	ignature			
Plan S	Scale: (Arch E)			Date	Oct	tober 202	21	
	Horizo Vertica	ntal 1:2500 al 1:500		Drawn By Checked By	C.P.	File No.	981 [,]	1V
File Na	ame		Cros	s Sect	tions	1		
Drawi	na No.							

6 of 6 
 File Path
 N:\Brian\9811V - Walker Uppers Quarry\Drawings\Site Plan\CAD\9811V - Site Plan - Proposed Scenario.dwg



#### **APPENDIX B**

**Traffic Data** 

Ontario Traffic Inc.											
Morning Peak Diagram	Specified Period         One Hour Peak           From:         6:00:00         From:         7:45:00           To:         9:00:00         To:         8:45:00										
Municipality:ThoroldSite #:1822100007Intersection:Thorold Stone Rd - RR 58 (Davis RdTFR File #:9Count date:19-Jun-18	Weather conditions: Person(s) who counted:										
** Signalized Intersection **	Major Road: Thorold Stone Rd - RR 58 (Davis R										
North Leg Total: 59       Heavys       0       0       0         North Entering:       20       Trucks       2       0       0       2         North Peds:       0       Cars       16       1       1       18         Peds Cross:       Image: Construct of the section of	Heavys 0 Trucks 8 Cars 31 Totals 39 Heavys 0 East Leg Total: 2048 East Entering: 1064 East Peds: 0 Peds Cross: X										
Heavys Trucks Cars Totals	Avis Rd Cars Trucks Heavys Totals 5 1 0 6 921 54 10 985 60 13 0 73										
RR 58 W <	♥ 986 68 10										
Heavys Trucks Cars Totals 0 1 20 21 21 3 3 49 826 878 25 108 231	RR 57 (Thorold Stone Rd)										
8 23 198 231 11 75 1044 RR 58	924         55         5         984										
Peds Cross:       Image: Construction of the c	rs       416       6       97       519       Peds Cross:       ⋈         ks       28       6       6       40       South Peds:       0         ys       8       0       2       10       South Entering:       569         vls       452       12       105       South Leg Total:       874										
Comn	nents										





	Ontario Traffic Inc. Traffic Count Summarv												
Intersection:	Intersection: Thorold Stone Rd - RR 58 (Davis F ^{Count Date:} 19-Jun-18 Municipality: Thorold												
	Nort	h Appro	ach Tot	als				Sout	h Appro	ach To	als		
	Includ	es Cars, T	rucks, & H	eavys		North/South		Include	es Cars, T	rucks, & H	eavys		
Hour Ending	Left	Thru	Right	Grand Total	Total Peds	Total Approaches	Hour Ending	Left	Thru	Right	Grand Total	Total Peds	
6:00:00 7:00:00 8:00:00 9:00:00 16:00:00 17:00:00 18:00:00 19:00:00	0 1 3 0 0 5 2 2	0 2 0 2 0 8 5 4	0 14 20 18 0 28 29 12	0 17 23 20 0 41 36 18	0 0 0 0 0 0	0 284 417 593 0 550 466 344	6:00:00 7:00:00 8:00:00 9:00:00 16:00:00 17:00:00 18:00:00 19:00:00	0 187 295 452 0 436 380 269	0 9 6 11 0 6 5 11	0 71 93 110 0 67 45 46	0 267 394 573 0 509 430 326	0 0 0 0 0 0	
Totals:	_13	21	121	155	0	2654		2019	48	432	2499	0	
	Last Include	<u>t Approa</u> es Cars T	ach Iota				West Approach Totals						
Hour	l - fi			Grand	Total	East/West Total	Hour		The second secon		Grand	Total	
Ending 6:00:00 7:00:00 8:00:00 9:00:00 16:00:00 17:00:00 18:00:00 19:00:00	Left 0 42 68 71 2 94 70 66	Thru 283 679 977 16 1003 1119 746	Right 0 10 7 8 0 4 3 4	Total 2 335 754 1056 18 1101 1192 816	Peds 0 0 0 0 0 0	Approaches 4 954 1597 2167 34 2677 2711 1969	Ending 6:00:00 7:00:00 9:00:00 16:00:00 17:00:00 18:00:00 19:00:00	Left 0 48 28 26 0 19 20 10	Thru 2 407 621 880 15 1183 1114 858	Right 0 164 205 1 374 385 285	Total 2 619 843 1111 16 1576 1519 1153	Peds 0 0 0 0 0 0 0	
Totals:	413	4825	36	5274	0	12113		151	5080	1608	6839	0	
Hours En Crossing	ding: Values:	6:00 0	<b>Calc</b> 7:00 197	ulated \ 8:00 304	/alues f 9:00 463	or Traffic Cr	<b>ossing M</b> 16:00 0	ajor Stre 17:00 449	eet 18:00 387	19:00 282			

Ontario Traffic Inc.										
Morning Peak Diagram	Specified Period         One Hour Peak           From:         6:00:00         From:         7:45:00           To:         9:00:00         To:         8:45:00									
Municipality:ThoroldSite #:1822100013Intersection:Thorold Stone Rd - RR 58 (Davis RdTFR File #:10Count date:14-Jun-18	Weather conditions: Person(s) who counted:									
** Signalized Intersection **	Major Road: Thorold Stone Rd - RR 58 (Davis R									
North Leg Total:       64       Heavys       0       0       0       0         North Entering:       22       Trucks       5       1       1       7         North Peds:       1       Cars       13       2       0       15         Peds Cross:       IM       Totals       18       3       1	Heavys 0 Trucks 8 Cars 34 Totals 42 Heavys 0 East Leg Total: 2232 East Entering: 1186 East Peds: 1 Peds Cross: X									
Heavys Trucks Cars Totals	Avis Rd Cars Trucks Heavys Totals 1 4 0 5 1059 53 9 1121 49 8 3 60									
RR 58 W	<ul> <li>✓ 1109 65 12</li> <li>✓ E</li> </ul>									
Heavys Trucks Cars Totals 0 3 17 20 5 5 50 798 853 7 7 15 199 221	Cars Trucks Heavys Totals									
12 68 1014 RR 58	974 65 7 1046									
Peds Cross:       I       Cars       250       Ca         West Peds:       1       Trucks       24       Truck         West Entering:       1094       Heavys       10       Heavy         West Leg Total:       2577       Totals       284       Totals	rs 305 16 176 497 Peds Cross: ▷ ks 28 1 14 43 South Peds: 0 ys <u>11 0 2</u> 13 South Entering: 553 south Leg Total: 837									
Comr	nents									





	Ontario Traffic Inc. Traffic Count Summarv											
Intersection:	Thorold	Stone R	d - RR 5	58 (Davis		^{Date:} 14-Jun-18	3 Muni	^{cipality:} Th	orold			
	Nort	h Appro	ach Tot	als				Sout	h Appro	ach To	als	
	Includ	es Cars, T	rucks, & H	eavys		North/South		Include	es Cars, T	rucks, & H	eavys	
Hour Ending	Left	Thru	Right	Grand Total	Total Peds	Total Approaches	Hour Ending	Left	Thru	Right	Grand Total	Total Peds
6:00:00 7:00:00 8:00:00 9:00:00 16:00:00 17:00:00 18:00:00 19:00:00	0 1 3 0 0 4 7 0	0 4 2 3 0 7 10 2	0 11 23 14 0 33 23 15	0 16 28 17 0 44 40 17	0 0 1 0 1 0 2	0 295 451 554 1 539 544 404	6:00:00 7:00:00 8:00:00 9:00:00 16:00:00 17:00:00 18:00:00 19:00:00	0 170 290 350 0 374 389 287	0 7 6 15 0 8 7 3	0 102 127 172 1 113 108 97	0 279 423 537 1 495 504 387	0 0 0 0 0 0
Totals:	_15	28	119	162	4	2788		1860	46	720	2626	0
	Last Include	<u>t Approa</u> es Cars T	ach Iota					West Approach Totals				
Hour				Grand	Total	East/West Total	_Hour				Grand	Total
Ending 6:00:00 7:00:00 8:00:00 9:00:00 16:00:00 17:00:00 18:00:00 19:00:00	Left 0 43 68 61 0 76 87 66	Thru 0 348 771 1065 1 1022 1061 813	Right 0 6 1 7 0 3 0 1	Total 0 397 840 1133 1 1101 1148 880	Peds 0 2 2 0 0 0 1	Approaches 0 1132 1788 2220 1 2744 2688 1957	Ending 6:00:00 7:00:00 9:00:00 16:00:00 17:00:00 18:00:00 19:00:00	Left 0 54 28 26 0 25 20 13	Thru 0 492 696 860 0 1189 1096 773	Right 0 189 224 201 0 429 424 291	Total 0 735 948 1087 0 1643 1540 1077	Peds 0 1 0 0 1 0 0
Totals:	401	5081	18	5500	5	12530		166	5106	1758	7030	2
Hours En Crossing	ding: Values:	6:00 0	<b>Calc</b> 7:00 178	ulated V 8:00 302	<b>/alues f</b> 9:00 367	or Traffic Cr	<b>ossing M</b> 16:00 0	ajor Stre 17:00 387	eet 18:00 406	19:00 291		

Ontario Traffic Inc.													
Morning Peak Diagram	Specified Period         One Hour Peak           From:         6:00:00         From:         7:45:00           To:         9:00:00         To:         8:45:00												
Municipality:ThoroldSite #:1822100004Intersection:Thorold Stone Rd & Thorold TownliTFR File #:14Count date:19-Jun-18	Weather conditions: Person(s) who counted:												
** Signalized Intersection **	Major Road: Thorold Stone Rd runs W/E												
North Leg Total:       827       Heavys       1       0       0       1         North Entering:       346       Trucks       34       14       4       52         North Peds:       4       Cars       175       65       53       29         Peds Cross:       Image: March Pedia structure       Totals       210       79       57	Heavys 1 Trucks 48 Cars 432 Totals 481 East Leg Total: 1500 East Entering: 798 East Peds: 0 Peds Cross: X												
Heavys Trucks Cars Totals 11 63 921 995	orold Townline Rd Cars Trucks Heavys Totals 51 4 0 55 700 16 9 725												
Thorold Stone Rd	$ \begin{array}{c}         14 & 4 & 0 \\         765 & 24 & 9 \end{array} $ 18												
Heavys Trucks Cars Totals 1 28 272 301 4 21 594 619	Thorold Stone Rd												
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	Cars Trucks Heavys Totals 666 31 5 702												
Peds Cross:Image: Carse of the c	s       46       109       19       174       Peds Cross:       ⋈         s       13       16       6       35       South Peds:       0         s       1       0       1       2       South Entering:       211         s       60       125       26       South Leg Total:       337												
Comn	nents												





	Ontario Traffic Inc. Traffic Count Summary														
Intersection: -	Thorold	Stone R	d & Tho	orold Tov		Date: 19-Jun-18	3 Muni	^{icipality:} Th	orold						
	Nort	h Appro	ach Tot	als				Sout	th Approach Totals						
	Includ	es Cars, T	rucks, & H	eavys		North/South		Includ	Includes Cars, Trucks, & Heavys						
Hour Ending	Left	Thru	Right	Grand Total	Total Peds	Total Approaches	Hour Ending	Left	Thru	Right	Grand Total	Total Peds			
6:00:00 7:00:00 8:00:00 9:00:00 16:00:00 17:00:00 18:00:00 19:00:00	0 25 38 51 0 55 36 20	0 36 83 70 0 127 97 52	0 54 141 200 0 258 250 164	0 115 262 321 0 440 383 236	0 1 0 4 0 0 1 0	0 207 422 527 0 631 506 365	6:00:00 7:00:00 8:00:00 9:00:00 16:00:00 17:00:00 18:00:00 19:00:00	0 15 38 61 0 61 56 55	0 69 105 124 0 104 46 56	0 8 17 21 0 26 21 18	0 92 160 206 0 191 123 129	0 2 0 0 0 0 0			
Totals:	225	465	1067	1757	6	2658		286	504	111	901	2			
	East	t Approa	ach Tota					Wes	t Appro	ach Tot					
Hour	menuu	55 Cars, 1		Grand	Total	East/West Total	Hour	meidu	55 Gars, 1		Grand	Total			
Ending	Left	Thru	Right	Total	Peds	Approaches	Ending	Left	Thru	Right	Total	Peds			
6:00:00 7:00:00 8:00:00 9:00:00 16:00:00 17:00:00 18:00:00 19:00:00	0 11 25 12 0 34 21 19	0 241 530 727 0 721 821 560	0 53 45 47 0 45 25 27	0 305 600 786 0 800 867 606	0 0 0 0 0 0 0	0 789 1295 1750 1 2027 1994 1488	6:00:00 7:00:00 8:00:00 9:00:00 16:00:00 17:00:00 18:00:00	0 195 252 292 1 245 173 127	0 269 423 648 0 955 939 730	0 20 24 0 27 15 25	0 484 695 964 1 1227 1127 882	0 0 0 0 0 0 0			
Totals:	122	3600	242	3964	0	9344		1285	3964	131	5380	0			
			Calc	ulated V	/alues f	or Traffic Cr	ossing M	ajor Stre	et						
Hours En Crossing	ding: Values:	6:00 0	7:00 109	8:00 181	9:00 236		16:00 0	17:00 243	18:00 189	19:00 131					

Ontario Traffic Inc.													
Morning Peak Diagram	Specified Period         One Hour Peak           From:         6:00:00         From:         7:45:00           To:         9:00:00         To:         8:45:00												
Municipality:ThoroldSite #:1822100010Intersection:Thorold Stone Rd & Thorold TownliTFR File #:9Count date:14-Jun-18	Weather conditions: Person(s) who counted:												
** Signalized Intersection **	Major Road: Thorold Stone Rd runs W/E												
North Leg Total:         858         Heavys         1         0         0         1           North Entering:         329         Trucks         32         16         6         54           North Peds:         0         Cars         167         67         40         27           Peds Cross:         Image: March 100         Totals         200         83         46	Heavys 1 Trucks 54 Cars 474 Totals 529 Heavys 1 East Leg Total: 1760 East Entering: 1000 East Peds: 0 Peds Cross: X												
Heavys Trucks Cars Totals 12 65 1079 1156	Cars Trucks Heavys Totals 83 7 0 90 857 21 10 888												
Thorold Stone Rd	$E = \frac{16}{956} = \frac{10}{34} = \frac{10}{10} = \frac{10}{22}$												
Heavys Trucks Cars Totals 1 32 307 340 6 21 665 692	Thorold Stone Rd												
0 10 29 39 7 63 1001 Thorold Townline Rd	Cars Trucks Heavys Totals 722 31 7 760												
Peds Cross:Image: XCars112CarsWest Peds:0Trucks32TruckWest Entering:1071Heavys0HeavyWest Leg Total:2227Totals144Totals	rs       55       84       17       156       Peds Cross:       ⋈         rs       12       15       4       31       South Peds:       0         rs       1       0       1       2       South Entering:       189         rs       68       99       22       South Leg Total:       333												
Comr	nents												





	Ontario Traffic Inc. Traffic Count Summary														
Intersection:	Thorold	Stone R	d & Tho	orold Tov		^{Date:} 14-Jun-18	з м	lunic	^{ipality:} Th	orold					
	Nortl	h Appro	ach Tot	als				South Approach Totals							
-	Include	es Cars, T	rucks, & H	eavys		North/South			Include	eavys					
Hour Ending	Left	Thru	Right	Grand Total	Total Peds	Total Approaches	Hour Ending	3	Left	Thru	Right	Grand Total	Total Peds		
6:00:00 7:00:00 8:00:00 9:00:00 16:00:00 17:00:00 18:00:00 19:00:00	0 23 31 50 0 47 37 25	0 44 80 74 6 159 136 71	0 58 165 207 1 250 268 175	0 125 276 331 7 456 441 271	0 0 0 0 2 0 0	0 234 432 508 19 632 611 385	6:00:0 7:00:0 8:00:0 16:00:0 17:00:0 18:00:0 19:00:0	00 00 00 00 00 00 00 00 00	0 24 49 59 4 67 71 46	0 76 97 97 8 79 76 50	0 9 10 21 0 30 23 18	0 109 156 177 12 176 170 114	0 0 0 0 2 0 0		
Totals:	213	570	1124	1907	2	2821			320	483	111	914	2		
	East	<b>Appro</b> a S Cars T	ach Tota	als eavys					West Include	t Appro	ach Tota rucks & H	als eavys			
Hour				Grand	Total	East/West Total	_Hour	F				Grand	Total		
Ending 6:00:00 7:00:00 8:00:00 9:00:00 16:00:00 17:00:00 18:00:00 19:00:00	Left 0 12 24 16 0 35 30 23	Thru 4 301 601 838 35 787 817 643	Right 0 43 69 77 1 38 23 13	Total 4 356 694 931 36 860 870 679	Peds 0 0 0 0 2 0 0	Approaches 6 962 1540 1988 82 2173 2067 1551	Ending 6:00:0 7:00:0 8:00:0 9:00:0 16:00:0 17:00:0 18:00:0	3 00 00 00 00 00 00 00 00 00 00	Left 0 235 293 316 13 249 200 132	Thru 2 335 514 702 30 1038 958 705	Right 0 36 39 39 39 39 35	Total 2 606 846 1057 46 1313 1197 872	Peds 0 0 0 0 2 0 0		
Totals:	140	4026	264	4430	2	10369			1438	4284	217	5939	2		
Hours En Crossing	ding: Values:	6:00 0	<b>Calc</b> 7:00 123	ulated \ 8:00 177	/alues f 9:00 206	or Traffic Cr	<b>ossing</b> 16:( 1	<b>Ma</b> 00 12	ajor Stre 17:00 277	eet 18:00 244	19:00 142				

Ontario T	Ontario Traffic Inc.														
Morning Peak Diagram	Specified Period         One Hour Peak           From:         6:00:00         From:         7:30:00           To:         9:00:00         To:         8:30:00														
Municipality:ThoroldSite #:1822100006Intersection:RR 58 (Davis Rd) & Beaverdams RTFR File #:9Count date:19-Jun-18	Weather conditions: Person(s) who counted:														
** Signalized Intersection **       Major Road:       RR 58 (Davis Rd) runs N/S															
North Leg Total:       832       Heavys       2       8       0       10         North Entering:       308       Trucks       5       38       1       44         North Peds:       0       Cars       34       137       83       25         Peds Cross:       Image: March Pedia Construction of the second consecond consecond construction of the second construction	Heavys 9 Heavys 9 Trucks 41 Cars 474 Totals 524 Heavys 9 East Leg Total: 341 East Entering: 188 East Peds: 0 Peds Cross: X														
Heavys Trucks Cars Totals	R 58 (Davis Rd) Cars Trucks Heavys Totals 140 2 1   143 16 2 0   18														
Beaverdams Rd-Niagara Falls Rd	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$														
Heavys Trucks Cars         Totals           1         10         95         106         10         5           0         2         35         37         10         5	Beaverdams Rd-Niagara Falls Rd														
0 0 6 6 1 12 136 RR 58 (Davis Rd)	Cars Trucks Heavys Totals 148 5 0 153														
Peds Cross:Image: Carse and Car	Irs       2       239       30       271       Peds Cross:       Image: mail with the state withe state withe state with the state withe state with the state wi														
Comr	nents														
West Leg Total: 211 Totals 216 Tota	als 3 275 32 South Leg Total: 526														

	raffic Inc.									
Afternoon Peak Diagram	Specified Period         One Hour Peak           From:         16:00:00         From:         16:00:00           To:         19:00:00         To:         17:00:00									
Municipality:ThoroldSite #:1822100006Intersection:RR 58 (Davis Rd) & Beaverdams RTFR File #:9Count date:19-Jun-18	Weather conditions: Person(s) who counted:									
** Signalized Intersection **	Major Road: RR 58 (Davis Rd) runs N/S									
North Leg Total: 959       Heavys 0       2       1       3         North Entering: 484       Trucks 3       23       3       2         North Peds: 0       Cars 89       198       165       4         Peds Cross:       Image: March Pede Pede Pede Pede Pede Pede Pede Ped	Heavys 5 Trucks 21 52 Totals 437 East Leg Total: 437 East Entering: 211 East Peds: 0 Peds Cross: X									
Heavys Trucks Cars Totals	R 58 (Davis Rd) Cars Trucks Heavys Totals 134 2 2 138 37 0 0 37									
Beaverdams Rd-Niagara Falls Rd	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$									
Heavys Trucks       Cars       Totals         1       1       87       89         0       0       32       32         0       1       32       1	Beaverdams Rd-Niagara Falls Rd									
0 1 3 4 1 2 122 RR 58 (Davis Rd)	1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1									
Peds Cross:Image: Carse 236Carse 236West Peds:0Trucks 25TruckWest Entering:125Heavys 2HeavyWest Leg Total:259Totals 263Totals	ars       5       228       23       256       Peds Cross:       Image: style="text-align: center;">Image: style="text-align: center;"/>Image: style="text-align: center;"/>Ima									
Com	nents									

Ontario T	Ontario Traffic Inc.													
Total Count Diagram														
Municipality:ThoroldSite #:1822100006Intersection:RR 58 (Davis Rd) & Beaverdams RTFR File #:9Count date:19-Jun-18	Weather conditions: Person(s) who counted:													
** Signalized Intersection **     Major Road:     RR 58 (Davis Rd) runs N/S														
North Leg Total: 4390       Heavys 3       14       1       18         North Entering: 1996       Trucks 19       111       13       14         North Peds: 0       Cars 375       935       525       18         Peds Cross:       Image: Construction of the second seco	Heavys 20 Heavys 20 Trucks 132 Cars 2242 Totals 2394 East Leg Total: 1868 East Entering: 964 East Peds: 0 Peds Cross: X													
Heavys Trucks Cars Totals	R 58 (Davis Rd) Cars Trucks Heavys Totals 618 11 3 632 179 6 0 185													
N Beaverdams Rd-Niagara Falls Rd W 🕌	$F = \frac{142}{939} \frac{3}{22} \frac{3}{3} = 147$													
Heavys Trucks Cars Totals 3 17 510 530 0 9 202 211	Beaverdams Rd-Niagara Falls Rd													
0 1 29 30 3 27 741 RR 58 (Davis Rd)	Cars Trucks Heavys Totals 874 28 2 904													
Peds Cross:     Image: Carse in the sector of	rs       19       1114       147       1280       Peds Cross:       ⋈         ks       2       104       6       112       South Peds:       0         ys       0       14       1       15       South Entering:       1407         xls       21       1232       154       South Leg Total:       2644													
Comr	nents													

	Ontario Traffic Inc. Traffic Count Summary															
Intersection:	RR 58 (I	Davis Ro	d) & Bea	averdam	S   Count D	Date: 19-Jun-18	3 N	Munic	^{ipality:} Th	orold						
	Nort	h Appro	ach Tot	als			South Approac					Totals				
Hour Ending	Left	Thru	Right	Grand Total	Total Peds	North/South Total Approaches	Hour	a	Left	Thru	Right	Grand Total	Total Peds			
6:00:00 7:00:00 8:00:00 9:00:00 16:00:00 17:00:00 18:00:00 19:00:00	0 32 60 85 0 169 126 67	0 148 171 151 4 223 203 158	0 38 35 45 1 92 86 100	0 218 266 281 5 484 415 325		0 379 510 593 10 762 640 507	6:00:0 7:00:0 8:00:0 9:00:0 16:00:0 17:00:0 18:00:0 19:00:0	00 00 00 00 00 00 00 00 00	0 1 1 4 0 5 7 3	0 140 203 280 5 248 197 159	0 20 40 28 0 25 21 20	0 161 244 312 5 278 225 182				
Totals:	539	1058	397	1994	0	3401			21	1232	154	1407	0			
	Include	es Cars, T	rucks, & H	als eavys		East/Mast			Include	es Cars, T	rucks, & H	ais eavys				
Hour Ending	Left	Thru	Right	Grand Total	Total Peds	Total Approaches	Hour Ending	g	Left	Thru	Right	Grand Total	Total Peds			
6:00:00 7:00:00 8:00:00 9:00:00 16:00:00 17:00:00 18:00:00 19:00:00	0 13 24 20 0 36 33 21	0 19 30 11 1 37 39 48	0 48 101 146 5 138 113 81	0 80 155 177 6 211 185 150	0 0 0 0 0 0	0 188 293 327 8 336 319 264	6:00:( 7:00:( 8:00:( 9:00:( 16:00:( 17:00:( 18:00:( 19:00:(	00 00 00 00 00 00 00 00	0 78 92 113 2 89 85 71	0 27 39 34 0 32 43 36	0 3 7 3 0 4 6 7	0 108 138 150 2 125 134 114	0 0 0 0 0 0 0			
Totals: Hours En Crossing	147 ding: Values:	<u>185</u> 6:00 0	632 <b>Calc</b> 7:00 118	964 ulated V 8:00 155	0 <b>/alues f</b> 9:00 167	1735 or Traffic Cr	<b>ossing</b> 16:0	<b>Ma</b> 00 3	530 ajor Stre 17:00 162	<u>211</u> eet 18:00 161	<u>30</u> 19:00 140	771	0			

Count Date: 19-Jun-18

Site #: 1822100006

**Passenger Cars - North Approach Trucks - North Approach** Heavys - North Approach Pedestrians Interval Left Thru Right Left Thru Right Left Thru Right North Cross Time Cum Incr 5:45:00 6:00:00 6:15:00 6:30:00 6:45:00 7:00:00 7:15:00 7:30:00 7:45:00 8:00:00 8:15:00 8:30:00 8:45:00 9:00:00 9:01:13 15:30:00 15:45:00 16:00:00 16:15:00 16:30:00 16:45:00 17:00:00 17:15:00 17:30:00 17:45:00 18:00:00 18:15:00 18:30:00 18:45:00 19:00:00 19:00:17 

Count Date: 19-Jun-18

Site #: 1822100006

**Passenger Cars - East Approach Trucks - East Approach** Heavys - East Approach Pedestrians Interval Left Thru Right Left Thru Right Left Thru Right East Cross Time Incr Cum Incr Cum Incr Cum Cum Incr 5:45:00 6:00:00 6:15:00 6:30:00 6:45:00 7:00:00 7:15:00 7:30:00 7:45:00 8:00:00 8:15:00 8:30:00 8:45:00 9:00:00 9:01:13 15:30:00 15:45:00 16:00:00 16:15:00 16:30:00 16:45:00 17:00:00 17:15:00 17:30:00 17:45:00 18:00:00 18:15:00 18:30:00 18:45:00 19:00:00 19:00:17 

Count Date: 19-Jun-18

Site #: 1822100006

Heavys - South Approach **Passenger Cars - South Approach Trucks - South Approach** Pedestrians Interval Left Thru Right Left Thru Right Left Thru Right South Cross Time Cum Incr Cum Incr Incr Cum Cum Incr 5:45:00 6:00:00 6:15:00 6:30:00 6:45:00 7:00:00 7:15:00 7:30:00 7:45:00 8:00:00 8:15:00 8:30:00 8:45:00 9:00:00 9:01:13 15:30:00 15:45:00 16:00:00 16:15:00 16:30:00 16:45:00 17:00:00 17:15:00 17:30:00 17:45:00 18:00:00 18:15:00 18:30:00 18:45:00 19:00:00 19:00:17 

Count Date: 19-Jun-18

Site #: 1822100006

Heavys - West Approach **Passenger Cars - West Approach Trucks - West Approach** Pedestrians Left Interval Left Thru Right Thru Right Left Thru Right West Cross Time Incr Cum Incr Cum Incr Cum Cum Incr 5:45:00 6:00:00 6:15:00 6:30:00 6:45:00 7:00:00 7:15:00 7:30:00 7:45:00 8:00:00 8:15:00 8:30:00 8:45:00 9:00:00 9:01:13 15:30:00 15:45:00 16:00:00 16:15:00 16:30:00 16:45:00 17:00:00 17:15:00 17:30:00 17:45:00 18:00:00 18:15:00 18:30:00 18:45:00 19:00:00 19:00:17 

Ontario T	raffic Inc.									
Morning Peak Diagram	Specified Period         One Hour Peak           From:         6:00:00         From:         7:45:00           To:         9:00:00         To:         8:45:00									
Municipality:ThoroldSite #:1822100012Intersection:RR 58 (Davis Rd) & Beaverdams RTFR File #:13Count date:14-Jun-18	Weather conditions: Person(s) who counted:									
** Signalized Intersection **	Major Road: RR 58 (Davis Rd) runs N/S									
North Leg Total:       848       Heavys       3       6       1       10         North Entering:       287       Trucks       4       22       0       26         North Peds:       0       Cars       40       133       78       25         Peds Cross:       Image: Construct on the second se	Heavys 13 Trucks 43 Cars 505 Totals 561 Heavys 13 East Leg Total: 356 East Entering: 224 East Peds: 0 Peds Cross: X									
Heavys Trucks Cars Totals	Cars         Trucks         Heavys         Totals           185         2         1         188           14         2         0         16									
Niagara Falls Rd	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$									
Heavys Trucks Cars         Totals           3         7         104         114         5           1         1         23         25         5	Beaverdams Rd									
0 1 6 7 4 9 133 RR 58 (Davis Rd)	Cars Trucks Heavys Totals 127 3 2 132									
Peds Cross:Image: Carse 157Carse 157West Peds:0Trucks 25TruckWest Entering:146Heavys 6HeavyWest Leg Total:214Totals 188Totals	rs       3       216       26       245       Peds Cross:       ⋈         rs       2       34       2       38       South Peds:       0         rs       0       9       0       9       South Entering:       292         rs       5       259       28       South Leg Total:       480									
Comn	nents									
Com	nents									

Ontario 7	raffic Inc.									
Afternoon Peak Diagram	Specified Period           From:         16:00:00           To:         19:00:00	One Hour Peak From: 16:30:00 To: 17:30:00								
Municipality:ThoroldSite #:1822100012Intersection:RR 58 (Davis Rd) & Beaverdams FTFR File #:13Count date:14-Jun-18	Weather conditions: Person(s) who counted:									
** Signalized Intersection **	Major Road: RR 58 (D	Davis Rd) runs N/S								
North Leg Total: 1100       Heavys 1       0       1       2         North Entering: 552       Trucks 0       13       2       1         North Peds: 0       Cars       116       251       168       1         Peds Cross:       Image: 100       Totals       117       264       171	Heavys 2 Trucks 23 Cars 523 Totals 548	East Leg Total: 492 East Entering: 253 East Peds: 0 Peds Cross: ∑								
Heavys Trucks Cars Totals	R 58 (Davis Rd)	Cars         Trucks         Heavys         Totals           154         1         156         156           49         1         0         50           40         1         0         17								
Niagara Falls Rd	F	249 3 1 249 3								
Heavys Trucks Cars Totals 0 1 90 91 0 1 31 32	Beav S	erdams Rd								
$\frac{1}{1}$ $\frac{1}{3}$ $\frac{2}{123}$ $\frac{4}{123}$ RR 58 (Davis Rd)		CarsFrucksHeavysFotals23441239								
Peds Cross:Image: Carse and Car	ars427935318ks021122ys0101als430136	Peds Cross:Image: MailSouth Peds:0South Entering:341South Leg Total:656								
	nents									



	Ontario Traffic Inc. Traffic Count Summary															
Intersection:	RR 58 (I	Davis Ro	d) & Bea	averdam	S   Count D	^{pate:} 14-Jun-18	3 N	Munic	^{ipality:} Th	orold						
	Nort	h Appro	ach Tot	als			South				h Approach Totals					
Hour Ending	Left	Thru	Right	Grand Total	Total Peds	North/South Total Approaches	Hour	a	Left	Thru	Right	Grand	Total Peds			
6:00:00 7:00:00 8:00:00 9:00:00 16:00:00 17:00:00 18:00:00 19:00:00	0 32 57 74 0 172 133 92	0 166 188 148 0 235 280 184	0 37 47 46 0 113 113 82	0 235 292 268 0 520 526 358	0 0 0 0 0 0 0 0	0 412 550 546 1 813 841 576	6:00:0 7:00:0 8:00:0 9:00:0 16:00:0 17:00:0 18:00:0 19:00:0	00 00 00 00 00 00 00 00	0 2 6 4 0 4 4 12	0 159 228 249 1 261 282 200	0 16 24 25 0 28 29 6	0 177 258 278 1 293 315 218	0 0 0 0 0 0 0 0			
Totals:	<u>560</u>	1201	438	2199	0	3739			32 West	1380	128 ach Tot	1540 als	0			
	Includ	es Cars, T	rucks, & H	eavys		Fast/West			Include	es Cars, T	rucks, & H	leavys				
Hour Ending	Left	Thru	Right	Grand Total	Total Peds	Total Approaches	Hour Ending	g	Left	Thru	Right	Grand Total	Total Peds			
6:00:00 7:00:00 8:00:00 9:00:00 16:00:00 17:00:00 18:00:00 19:00:00	0 14 11 26 0 30 40 20	0 13 43 14 0 56 58 23	0 52 100 177 0 142 141 102	0 79 154 217 0 228 239 145	0 0 0 0 0	0 175 302 375 0 363 355 241	6:00: 7:00: 8:00: 9:00: 16:00: 17:00: 18:00: 19:00:	00 00 00 00 00 00 00	0 76 107 124 0 92 92 80	0 16 33 25 0 39 20 12	0 4 8 9 0 4 4 4	0 96 148 158 0 135 116 96	0 0 1 0 0 0 1			
Totals	141	207	714	1062	0	1811			571	145	33	749	2			
10(013.	171	201	Calc	ulated V	alues f	or Traffic Cr	ossing	) Ma	ajor Stre	et	00	1-10	Z			
Hours En Crossing	ding: Values:	6:00 0	7:00 106	8:00 161	9:00 175		16:	00 0	17:00 178	18:00 190	19:00 123					

Count Date: 14-Jun-18 Site #: 1822100012

		Passeng	ger Cars -	North Ap	oproach			Tru	cks - Nor	th Appro	ach		Heavys - North Approach					Pede	Pedestrians		
Interval	Le	ft	Thi	u	Rig	Jht	Le	ft	Th	ru	Rig	ht	Le	eft	Thr	ru	Rig	ht	North	Cross	
Time	Cum	Incr	Cum	Incr	Cum	Incr	Cum	Incr	Cum	Incr	Cum	Incr	Cum	Incr	Cum	Incr	Cum	Incr	Cum	Incr	
6:00:00	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	(	) 0	
6:15:00	3	3	17	17	4	4	0	0	2	2	0	0	0	0	0	0	0	0	(	) 0	
6:30:00	7	4	56	39	10	6	0	0	4	2	0	0	0	0	0	0	0	0	(	) 0	
6:45:00	22	15	106	50	19	9	0	0	6	2	1	1	0	0	0	0	0	0	(	) 0	
7:00:00	32	10	157	51	36	17	0	0	8	2	1	0	0	0	1	1	0	0	(	) 0	
7:15:00	40	8	193	36	42	6	0	0	12	4	2	1	0	0	1	0	0	0	(	) 0	
7:30:00	48	8	234	41	56	14	1	1	20	8	3	1	1	1	4	3	1	1	(	) 0	
7:45:00	64	16	270	36	64	8	2	1	29	9	3	0	1	0	6	2	1	0	(	) 0	
8:00:00	86	22	308	38	77	13	2	0	38	9	4	1	1	0	8	2	3	2	(	) 0	
8:15:00	102	16	341	33	83	6	2	0	40	2	5	1	2	1	10	2	3	0	(	) 0	
8:30:00	126	24	369	28	92	9	2	0	44	4	6	1	2	0	11	1	4	1	(	) 0	
8:45:00	142	16	403	34	104	12	2	0	51	7	7	1	2	0	12	1	4	0	(	) 0	
9:00:00	157	15	435	32	118	14	4	2	54	3	8	1	2	0	13	1	4	0	(	) 0	
9:00:08	157	0	435	0	118	0	4	0	54	0	8	0	2	0	13	0	4	0	(	) 0	
16:00:00	157	0	435	0	118	0	4	0	54	0	8	0	2	0	13	0	4	0	(	) 0	
16:15:00	200	43	479	44	139	21	4	0	57	3	11	3	2	0	14	1	4	0	0		
16:30:00	236	36	532	53	175	36	4	0	65	8	12	1	2	0	15	1	5	1	(	) 0	
16:45:00	280	44	589	57	194	19	4	0	69	4	12	0	3	1	15	0	5	0	0		
17:00:00	327	47	651	62	226	32	5	1	71	2	12	0	3	0	15	0	5	0	(	) 0	
17:15:00	370	43	720	69	254	28	6	1	72	1	12	0	3	0	15	0	5	0	(	) 0	
17:30:00	404	34	783	63	291	37	6	0	78	6	12	0	3	0	15	0	6	1	(	) 0	
17:45:00	433	29	860	77	317	26	6	0	79	1	12	0	3	0	15	0	6	0	(	) 0	
18:00:00	459	26	921	61	338	21	6	0	81	2	12	0	3	0	15	0	6	0	(	) 0	
18:15:00	494	35	974	53	356	18	6	0	83	2	13	1	3	0	15	0	6	0	(	) 0	
18:30:00	517	23	1018	44	377	21	6	0	85	2	13	0	3	0	15	0	7	1	(	) 0	
18:45:00	534	17	1057	39	402	25	6	0	86	1	13	0	3	0	15	0	7	0	(	) 0	
19:00:00	551	17	1096	39	418	16	6	0	90	4	13	0	3	0	15	0	7	0	(	) 0	
19:00:04	551	0	1096	0	418	0	6	0	90	0	13	0	3	0	15	0	7	0	(	) 0	

Count Date: 14-Jun-18 Site #: 1822100012

		ger Cars	proach		Trucks - East Approach							Heavys - East Approach Pedestrians								
Interval	Left		Thru		Right		Left		Thru		Right		Left		Thru		Right		East Cross	
Time	Cum	Incr	Cum	Incr	Cum	Incr	Cum	Incr	Cum	Incr	Cum	Incr	Cum	Incr	Cum	Incr	Cum	Incr	Cum	Incr
6:00:00	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6:15:00	2	2	3	3	7	7	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6:30:00	9	7	5	2	17	10	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6:45:00	11	2	7	2	37	20	0	0	0	0	1	1	0	0	0	0	0	0	0	0
7:00:00	12	1	13	6	51	14	2	2	0	0	1	0	0	0	0	0	0	0	0	0
7:15:00	13	1	23	10	62	11	2	0	0	0	1	0	0	0	0	0	0	0	0	0
7:30:00	15	2	46	23	75	13	2	0	0	0	2	1	0	0	1	1	0	0	0	0
7:45:00	18	3	50	4	102	27	4	2	0	0	2	0	0	0	1	0	0	0	0	0
8:00:00	20	2	55	5	150	48	5	1	0	0	2	0	0	0	1	0	0	0	0	0
8:15:00	24	4	57	2	205	55	6	1	1	1	3	1	0	0	1	0	0	0	0	0
8:30:00	34	10	62	5	241	36	6	0	2	1	3	0	0	0	1	0	0	0	0	0
8:45:00	36	2	64	2	287	46	6	0	2	0	4	1	0	0	1	0	1	1	0	0
9:00:00	45	9	67	3	322	35	6	0	2	0	6	2	0	0	1	0	1	0	0	0
9:00:08	45	0	67	0	322	0	6	0	2	0	6	0	0	0	1	0	1	0	0	0
16:00:00	45	0	67	0	322	0	6	0	2	0	6	0	0	0	1	0	1	0	0	0
16:15:00	51	6	86	19	353	31	6	0	3	1	6	0	0	0	2	1	1	0	0	0
16:30:00	59	8	98	12	388	35	6	0	3	0	6	0	0	0	2	0	1	0	0	0
16:45:00	63	4	108	10	424	36	7	1	4	1	6	0	0	0	2	0	2	1	0	0
17:00:00	74	11	120	12	462	38	7	0	4	0	7	1	0	0	2	0	2	0	0	0
17:15:00	93	19	131	11	505	43	7	0	4	0	7	0	0	0	2	0	2	0	0	0
17:30:00	105	12	147	16	542	37	7	0	4	0	7	0	0	0	2	0	2	0	0	0
17:45:00	112	7	159	12	573	31	7	0	4	0	7	0	0	0	2	0	2	0	0	0
18:00:00	114	2	1//	18	603	30	/	0	5	1	/	0	0	0	2	0	2	0	0	0
18:15:00	120	6	187	10	634	31	/	0	5	0	1	0	0	0	2	0	2	0	0	0
18:30:00	128	8	190	3	664	30	/	0	5	0	8	1	0	0	2	0	2	0	0	0
18:45:00	130	2	195	5	680	16	/	0	5	0	8	0	0	0	2	0	2	0	0	0
19:00:00	134	4	200	5	704	24	/	0	5	0	8	0	0	0	2	0	2	0	0	0
19:00:04	134	0	200	0	704	0	7	0	5	0	8	0	0	0	2	0	2	0	0	C

Count Date: 14-Jun-18 Site #: 1822100012

		ger Cars -	South A	pproach	Trucks - South Approach							Heavys - South Approach								
Interval	Left		Thru		Right		Left		Thru		Right		Left		Thru		Right		South Cross	
Time	Cum	Incr	Cum	Incr	Cum	Incr	Cum	Incr	Cum	Incr	Cum	Incr	Cum	Incr	Cum	Incr	Cum	Incr	Cum	Incr
6:00:00	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6:15:00	0	0	18	18	0	0	0	0	3	3	0	0	0	0	0	0	0	0	0	0
6:30:00	0	0	59	41	4	4	0	0	6	3	0	0	0	0	0	0	0	0	0	0
6:45:00	1	1	100	41	9	5	0	0	14	8	1	1	0	0	0	0	0	0	0	0
7:00:00	2	1	138	38	15	6	0	0	20	6	1	0	0	0	1	1	0	0	0	0
7:15:00	2	0	177	39	20	5	0	0	29	9	2	1	0	0	2	1	0	0	0	0
7:30:00	4	2	225	48	23	3	0	0	38	9	2	0	0	0	2	0	0	0	0	0
7:45:00	5	1	268	43	31	8	0	0	43	5	2	0	1	1	6	4	1	1	0	0
8:00:00	6	1	327	59	37	6	1	1	52	9	2	0	1	0	8	2	1	0	0	0
8:15:00	6	0	368	41	42	5	2	1	61	9	2	0	1	0	11	3	1	0	0	0
8:30:00	6	0	438	70	53	11	2	0	68	7	3	1	1	0	13	2	1	0	0	0
8:45:00	8	2	484	46	57	4	2	0	77	9	4	1	1	0	15	2	1	0	0	0
9:00:00	9	1	534	50	60	3	2	0	86	9	4	0	1	0	16	1	1	0	0	0
9:00:08	9	0	535	1	60	0	2	0	86	0	4	0	1	0	16	0	1	0	0	0
16:00:00	9	0	535	0	60	0	2	0	86	0	4	0	1	0	16	0	1	0	0	0
16:15:00	9	0	590	55	70	10	2	0	94	8	4	0	1	0	17	1	1	0	0	0
16:30:00	10	1	641	51	73	3	2	0	97	3	6	2	1	0	18	1	1	0	0	0
16:45:00	11	1	702	61	80	7	2	0	104	7	6	0	1	0	19	1	1	0	0	0
17:00:00	13	2	770	68	86	6	2	0	109	5	6	0	1	0	19	0	1	0	0	0
17:15:00	13	0	840	70	105	19	2	0	113	4	6	0	1	0	19	0	1	0	0	0
17:30:00	14	1	920	80	108	3	2	0	118	5	7	1	1	0	19	0	1	0	0	0
17:45:00	16	2	980	60	109	1	2	0	121	3	7	0	1	0	20	1	1	0	0	0
18:00:00	17	1	1036	56	114	5	2	0	124	3	7	0	1	0	20	0	1	0	0	0
18:15:00	26	9	1103	67	117	3	2	0	126	2	7	0	1	0	20	0	1	0	0	0
18:30:00	28	2	1162	59	117	0	2	0	128	2	7	0	1	0	20	0	1	0	0	0
18:45:00	28	0	1200	38	119	2	2	0	130	2	/	0	1	0	21	1	1	0	0	0
19:00:00	29	1	1229	29	120	1	2	0	130	0	/	0	1	0	21	0	1	0	0	0
19:00:04	29	0	1229	0	120	0	2	0	130	U	1	0		U	21	0	1	0	0	0
## **Ontario Traffic Inc.**

Count Date: 14-Jun-18 Site #: 1822100012

	Passenger Cars - West Approach							Tru	cks - Wes	t Approa	ach		Heavys - West Approach					Pede	strians	
Interval	Le	ft	Th	ru	Rig	ht	Le	ft	Thr	ru	Rig	lht	Le	eft	Th	ru	Rig	ght	West	Cross
Time	Cum	Incr	Cum	Incr	Cum	Incr	Cum	Incr	Cum	Incr	Cum	Incr	Cum	Incr	Cum	Incr	Cum	Incr	Cum	Incr
6:00:00	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	C	0
6:15:00	13	13	3	3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6:30:00	35	22	5	2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	<i>)</i> 0
6:45:00	60	25	11	6	3	3	0	0	0	0	0	0	0	0	0	0	0	0	C	0
7:00:00	76	16	16	5	4	1	0	0	0	0	0	0	0	0	0	0	0	0	0	<u> </u>
7:15:00	105	29	23	7	5	1	1	1	0	0	0	0	0	0	0	0	0	0	0	0
7:30:00	121	16	33	10	5	0	4	3	2	2	0	0	1	1	0	0	0	0	1	1
7:45:00	157	36	40	7	8	3	5	1	2	0	1	1	1	0	2	2	0	0	1	0
8:00:00	176	19	44	4	11	3	5	0	2	0	1	0	2	1	3	1	0	0	1	0
8:15:00	205	29	48	4	11	0	7	2	2	0	1	0	3	1	3	0	0	0	1	0
8:30:00	236	31	54	6	14	3	10	3	2	0	2	1	3	0	3	0	0	0	1	0
8:45:00	261	25	63	9	14	0	12	2	3	1	2	0	4	1	3	0	0	0	1	0
9:00:00	287	26	68	5	19	5	14	2	3	0	2	0	6	2	3	0	0	0	1	0
9:00:08	287	0	68	0	19	0	14	0	3	0	2	0	6	0	3	0	0	0	1	0
16:00:00	287	0	68	0	19	0	14	0	3	0	2	0	6	0	3	0	0	0	1	0
16:15:00	310	23	74	6	20	1	14	0	4	1	2	0	7	1	3	0	0	0	1	0
16:30:00	335	25	87	13	21	1	15	1	4	0	2	0	/	0	3	0	0	0	1	0
16:45:00	361	26	96	9	21	0	15	0	5	1	3	1	/	0	3	0		1	1	0
17:00:00	376	15	105	9	21	0	16	1	5	0	3	0	1	0	3	0		0	1	0
17:15:00	401	25	111	6	22	1	16	0	5	0	3	0	1	0	3	0		0	1	0
17:30:00	425	24	118	(	23	1	16	0	5	0	3	0	1	0	3	0		0	1	0
17:45:00	444	19	122	4	24	1	16	0	5	0	3	0	7	0	3	0		0	1	0
18:00:00	407	23	120	3	20	1	10	1	5	0	3	0	7	0	<u> </u>	0		0		0
18:15:00	494	27	128	3	27		18	1	5	0	3	0	7	0	3	0		0	2	1
18:30:00	521	20	132	4	20	1	10	0	5	0	3	0	7	0		0		0	2	0
10.45.00	531	20	104	2	20	1	10	0	5	0	3	0	7	0	ు స	0		0	2	0
19.00.00	540	10	107	3	29	1	10	0	5	0	3	0	7	0	ు స	0		0	2	. 0
19.00.04	540	0	137	0	29	0	10	0	Э	0	3	0	1	0	3	0		0		0

Ontario Traffic Inc.										
Morning Peak Diagram	Specified Period         One Hour Peak           From:         6:00:00         From:         7:30:00           To:         9:00:00         To:         8:30:00									
Municipality:ThoroldSite #:1822100003Intersection:Beaverdams Rd & Thorold TownlinTFR File #:9Count date:19-Jun-18	Weather conditions: Person(s) who counted:									
** Non-Signalized Intersection **	Major Road: Beaverdams Rd runs W/E									
North Leg Total:       317       Heavys       0       0       0       0         North Entering:       126       Trucks       1       18       0       19         North Peds:       0       Cars       16       87       4       10         Peds Cross:       Image: Construct on the second secon	Heavys1East Leg Total:317Trucks27East Entering:167Cars163East Peds:0Totals191Peds Cross:X									
Heavys Trucks Cars Totals	CarsTrucksHeavysTotals12001214320145100010									
Beaverdams Rd	► E									
Heavys Trucks Cars Totals 0 0 6 6 0 0 138 138 0 1 6 7	Cars Trucks Heavys Totals									
$\frac{1}{0}$ $\frac{1}{150}$ Thorold Townline Rd										
Peds Cross:     Image: Carse in the sector of	rs       23       145       8       176       Peds Cross:       ⋈         rs       0       27       0       27       South Peds:       5         rs       0       1       0       1       South Entering:       204         rs       23       173       8       South Leg Total:       326									
Com	pents									
Com										





				<i>On</i> Traf	<i>itari</i> fic C	o <i>Traf</i> count S	fic In umm	C. ary				
Intersection:	Beaverd	lams Rd	& Thor	old Towr		Date: 19-Jun-18	3 Muni	^{cipality:} Th	orold			
	Nort	h Appro	ach Tot	als				Sout	h Appro	oach To	tals	
	Includ	es Cars, T	rucks, & H	eavys		North/South		Include	es Cars, T	rucks, & H	leavys	
Hour Ending	Left	Thru	Right	Grand Total	Total Peds	Total Approaches	Hour Ending	Left	Thru	Right	Grand Total	Total Peds
6:00:00 7:00:00 8:00:00 9:00:00 16:00:00 17:00:00 18:00:00 19:00:00	0 1 3 4 0 10 12 9	0 57 106 83 0 139 70 45	0 8 17 17 0 35 53 41	0 66 126 104 0 184 135 95	0 0 0 0 1 2 1	0 159 300 296 0 374 272 208	6:00:00 7:00:00 8:00:00 9:00:00 16:00:00 17:00:00 18:00:00	0 13 16 20 0 21 63 45	0 78 147 165 0 159 56 68	0 2 11 7 0 10 18 0	0 93 174 192 0 190 137 113	0 2 8 4 0 5 15 13
Totals:	39	500	171	710	4	1609		178	673	48	899	47
	East	t Approa	ach Tota	als				Wes	t Appro	ach Tot	als	
Hour	menuu			Grand	Total	East/West Total	Hour	moluuk			Grand	Total
Ending	Left	Thru	Right	Total	Peds	Approaches	Ending	Left	Thru	Right	Total	Peds
6:00:00 7:00:00 8:00:00 9:00:00 16:00:00 17:00:00 18:00:00 19:00:00	0 2 5 9 0 13 9 29	0 62 127 130 0 153 64 64	0 7 4 16 0 17 11 26	0 71 136 155 0 183 84 119	0 0 1 0 3 0 1	0 148 277 300 0 415 277 241	6:00:00 7:00:00 8:00:00 9:00:00 16:00:00 17:00:00 18:00:00 19:00:00	0 5 7 6 0 15 56 38	0 69 124 129 0 204 81 44	0 3 10 10 0 13 56 40	0 77 141 145 0 232 193 122	0 2 4 8 0 8 6 8
Totals: Hours En	67 ding:	<u>600</u> 6:00	81 <b>Calc</b> 7:00	748 ulated V 8:00	5 <b>/alues f</b> 9:00	1658 or Traffic Cr	<b>ossing M</b> 16:00	127 ajor Stre 17:00	<u>651</u> eet 18:00	<u>132</u> 19:00	910	36
Crossing	Values:	0	94	170	198		0	201	151	131		

Ontario Traffic Inc.									
Morning Peak Diagram	Specified Period         One Hour Peak           From:         6:00:00         From:         7:45:00           To:         9:00:00         To:         8:45:00								
Municipality:ThoroldSite #:1822100009Intersection:Beaverdams Rd & Thorold TownlinTFR File #:25Count date:14-Jun-18	Weather conditions: Person(s) who counted:								
** Non-Signalized Intersection **	Major Road: Beaverdams Rd runs W/E								
North Leg Total:       326       Heavys       0       0       0         North Entering:       136       Trucks       2       26       3       31         North Peds:       0       Cars       15       76       14       10         Peds Cross:       Image: March Peds       Totals       17       102       17	Heavys2East Leg Total:336Trucks28East Entering:226Cars160East Peds:0Totals190Peds Cross:X								
Heavys Trucks Cars Totals	orold Townline Rd Cars Trucks Heavys Totals 31 1 0 32 186 2 0 188								
Beaverdams Rd	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$								
Heavys Trucks Cars Totals 1 1 1 19 21 1 2 88 91 0 1 24 25	Beaverdams Rd								
2 4 131 Thorold Townline Rd									
Peds Cross:Image: Carsent and	rs       14       110       2       126       Peds Cross:       ⊠         rs       0       26       0       26       South Peds:       0         rs       0       1       0       1       South Entering:       153         rs       14       137       2       South Leg Total:       286								
Comr	nents								





				<i>On</i> Traf	<i>itari</i> fic C	o <i>Traf</i> count S	fic In umm	ic. ary				
Intersection:	Beaverd	ams Rd	& Thor	old Towr		Date: 14-Jun-18	3 Mun	^{icipality:} Th	orold			
	Nort	h Appro	ach Tot	als				Sout	h Appro	oach To	tals	
	Includ	es Cars, T	rucks, & H	eavys		North/South		Include	es Cars, T	rucks, & H	eavys	
Hour Ending	Left	Thru	Right	Grand Total	Total Peds	Total Approaches	Hour Ending	Left	Thru	Right	Grand Total	Total Peds
6:00:00 7:00:00 8:00:00 9:00:00 16:00:00 17:00:00 18:00:00 19:00:00	0 9 17 15 3 28 26 8	2 74 99 95 1 156 157 93	0 7 27 10 2 39 25 27	2 90 143 120 6 223 208 128	0 0 1 0 1 0 1	7 186 282 265 13 375 365 236	6:00:00 7:00:00 8:00:00 9:00:00 16:00:00 17:00:00 18:00:00	0 9 22 17 25 34 16	4 87 117 126 4 121 116 85	1 0 2 1 6 7 7	5 96 139 145 7 152 157 108	0 0 0 0 0 1 0
Totals:	106	677	137	920	3	1729		125	660	24	809	1
	Lasi Includ	es Cars. T	rucks & H	als eavys				West Approach Totals				
Hour	Loft	Thru	Pight	Grand	Total	East/West Total	Hour	Loft	Thru	Pight	Grand	Total
6:00:00 7:00:00 8:00:00 9:00:00 16:00:00 17:00:00 18:00:00 19:00:00	Leπ 0 3 7 1 7 6 4	107 0 66 109 187 2 164 171 109	Right 0 12 19 33 1 28 26 15	101a1 0 78 131 227 4 199 203 128	Peds 0 0 0 0 0 1 0	Approaches 0 129 240 354 9 429 380 238	Ending 6:00:00 7:00:00 8:00:00 9:00:00 16:00:00 17:00:00 18:00:00 19:00:00	Left 0 9 19 21 2 24 24 10	1nru 0 27 62 89 2 184 127 77	Right 0 15 28 17 1 22 26 23	101ai 0 51 109 127 5 230 177 110	Peds 0 1 0 0 0 0 0
Totals:	28	808	134	970	1	1779		109	568	132	809	1
Hours En Crossing	ding: Values:	6:00 4	Calc 7:00 106	ulated V 8:00 156	alues f 9:00 158	or Traffic Cr	ossing M 16:00 9	ajor Stre 17:00 209	eet 18:00 218	19:00 117		

Ontario T	raffic Inc.						
Morning Peak Diagram	Specified Period         One Hour Peak           From:         6:00:00         From:         7:30:00           To:         9:00:00         To:         8:30:00						
Municipality:ThoroldSite #:1822100005Intersection:Hwy 20 (Lundy's Lane) & RR 58 (DTFR File #:12Count date:19-Jun-18	Weather conditions: Person(s) who counted:						
** Signalized Intersection **	Major Road: Hwy 20 (Lundy's Lane) runs W/E						
North Leg Total:       541       Heavys       5       1       3       9         North Entering:       232       Trucks       7       27       10       44         North Peds:       0       Cars       70       71       38       17         Peds Cross:       Image: Cars of the second s	9 Heavys 8 East Leg Total: 860 Trucks 35 East Entering: 378 Cars 266 East Peds: 0 Totals 309 Peds Cross: X						
Heavys Trucks Cars Totals	Cars Trucks Heavys Totals 45 2 2 49 272 27 2 301						
Hwy 20 (Lundy's Lane)	$\begin{array}{c} 21 & 6 & 1 \\ \hline 338 & 35 & 5 \end{array} \begin{array}{c} 28 \\ \hline 28 \\ 28 \\$						
Heavys Trucks Cars Totals 3 7 116 126 5 0 10 399 409 5	Hwy 20 (Lundy's Lane)						
0 1 15 16 RR 58 (Davis Rd)	Cars Trucks Heavys Totals 450 29 3 482						
Peds Cross:Image: XCars107CarsWest Peds:0Trucks34TruckWest Entering:551Heavys2HeavyWest Leg Total:954Totals143Totals	rs       17       105       13       135       Peds Cross:       Image: second secon						
Comn	nents						
Comn	nents						

Ontario 1	Traffic Inc.						
Afternoon Peak Diagram	Specified Period         One Hour Peak           From:         16:00:00         From:         16:15:00           To:         19:00:00         To:         17:15:00						
Municipality:ThoroldSite #:1822100005Intersection:Hwy 20 (Lundy's Lane) & RR 58 (DTFR File #:12Count date:19-Jun-18	Weather conditions: Person(s) who counted:						
** Signalized Intersection **	Major Road: Hwy 20 (Lundy's Lane) runs W/E						
North Leg Total:         576         Heavys         1         0         0         1           North Entering:         304         Trucks         1         13         5         1           North Peds:         2         Cars         110         97         77         2           Peds Cross:         Image: March 112         110         82	Heavys 1 Frucks 18 Cars 253 Totals 272 Heavys 1 East Leg Total: 1053 East Entering: 502 East Peds: 1 Peds Cross: X						
Heavys Trucks Cars Totals	R 58 (Davis Rd) Cars Trucks Heavys Totals 46 3 0 49 428 7 0 435 N 15 3 0 18						
Hwy 20 (Lundy's Lane)							
Heavys Trucks Cars Totals 0 3 93 96 1 10 425 436	Hwy 20 (Lundy's Lane)						
0 7 24 31 1 20 542 RR 58 (Davis Rd)	Cars Trucks Heavys Totals 531 18 2 551						
Peds Cross:Image: Carse 136Carse 136West Peds:0Trucks 23Trucks 23West Entering:563Heavys 0HeavyWest Leg Total:1144Totals 159Totals	ars       33       114       29       176       Peds Cross:       ⋈         sks       1       12       3       16       South Peds:       1         rys       0       1       1       2       South Entering:       194         als       34       127       33       South Leg Total:       353						
Com	ments						

Ontario Traffic Inc.									
Total Count Diagram									
Municipality:ThoroldWeather conditions:Site #:1822100005Person(s) who counted:Intersection:Hwy 20 (Lundy's Lane) & RR 58 (DPerson(s) who counted:TFR File #:1212Count date:19-Jun-1819-Jun-18									
** Signalized Intersection **	Major Road: Hwy 20 (Lundy's Lane) runs W/E								
North Leg Total:         2837         Heavys         10         2         3         15           North Entering:         1364         Trucks         18         83         34         135           North Peds:         4         Cars         403         483         328         121           Peds Cross:         Image: Mathematical Science Scien	Heavys18East Leg Total:4655Trucks117East Entering:2150Cars1338East Peds:5Totals1473Peds Cross:X								
Heavys Trucks Cars       Totals       RR 58 (Davis Rd)         13       99       2185       2297         Image: Cars       Trucks       Heavys Totals         13       13       1630       65       3         13       128       21       1       150									
Heavys Trucks Cars Totals 9 20 515 544 S 2 44 1944 1990	E Hwy 20 (Lundy's Lane)								
0 17 106 123 11 81 2565 RR 58 (Davis Rd)	Cars Trucks Heavys Totals 2396 103 6 2505								
Peds Cross:Image: Carse of the c	152     544     124     820     Peds Cross:     ⋈       16     77     25     118     South Peds:     5       0     6     1     7     South Entering:     945       168     627     150     South Leg Total:     1786								
Comm	ents								

				<i>Or</i> Traf	<i>itari</i> fic C	o <i>Traf</i> count S	fic In umm	C. ary				
Intersection:	Hwy 20	(Lundy's	s Lane)	& RR 58	([ Count D	Date: 19-Jun-18	3 Muni	^{cipality:} Th	orold			
	Nort	h Appro	ach Tot	als				Sout	h Appro	oach To	tals	
	Includ	es Cars, T	rucks, & H	eavys		North/South		Includ	es Cars, T	rucks, & H	leavys	
Hour Ending	Left	Thru	Right	Grand Total	Total Peds	Total Approaches	Hour Ending	Left	Thru	Right	Grand Total	Total Peds
6:00:00 7:00:00 8:00:00 9:00:00 16:00:00 17:00:00 18:00:00 19:00:00	0 42 48 64 0 81 90 40	0 96 85 92 0 109 108 78	0 27 81 54 0 111 97 61	0 165 214 210 0 301 295 179	0 0 0 0 2 2 0	0 294 374 375 1 494 485 286	6:00:00 7:00:00 8:00:00 9:00:00 16:00:00 17:00:00 18:00:00 19:00:00	0 17 25 23 1 35 39 28	0 89 107 126 0 126 112 67	0 23 28 16 0 32 39 12	0 129 160 165 1 193 190 107	0 0 1 0 1 1 2
Totals:	365	568	431	1364	4	2309		168	627	150	945	5
		es Cars. T	rucks, & H	als eavys			West Approach Totals					
Hour	Loft	Thru	Pight	Grand	Total	Total	Hour	Loft	Thru	Pight	Grand	Total
Ending 6:00:00 7:00:00 8:00:00 9:00:00 16:00:00 17:00:00 18:00:00 19:00:00	Left 0 33 23 0 17 28 16	1hru 0 130 229 303 0 429 381 226	Right 0 43 54 47 0 50 71 37	10tal 0 206 316 373 0 496 480 279	Peds 0 1 0 1 2 1	Approaches 0 442 800 895 0 1052 951 667	Ending 6:00:00 7:00:00 9:00:00 16:00:00 17:00:00 18:00:00 19:00:00	Left 0 68 116 120 0 94 71 75	1hru 0 154 347 385 0 429 380 295	Right 0 14 21 17 0 33 20 18	10tal 0 236 484 522 0 556 471 388	Peds 0 0 0 0 0 0 0
Totals:	150	1698	302	2150	5	4807		544	1990	123	2657	0
Hours En Crossing	ding: Values:	6:00 0	<b>Calc</b> 7:00 155	ulated \ 8:00 181	/alues f 9:00 213	or Traffic Cr	<b>ossing M</b> 16:00 1	ajor Stro 17:00 243	eet 18:00 243	19:00 147		

Ontario Traffic Inc.										
Morning Peak Diagram	Specified Period         One Hour Peak           From:         6:00:00         From:         7:45:00           To:         9:00:00         To:         8:45:00									
Municipality:ThoroldSite #:1822100011Intersection:Hwy 20 (Lundy's Lane) & RR 58 (DTFR File #:7Count date:14-Jun-18	Weather conditions: Person(s) who counted:									
** Signalized Intersection **	Major Road: Hwy 20 (Lundy's Lane) runs W/E									
North Leg Total:       495       Heavys       5       1       1       7         North Entering:       201       Trucks       6       15       5       26         North Peds:       0       Cars       54       62       52       16         Peds Cross:       IM       Totals       65       78       58	Heavys8East Leg Total:905Trucks35East Entering:383Cars251East Peds:0Totals294Peds Cross:X									
Heavys Trucks Cars Totals	R 58 (Davis Rd) Cars Trucks Heavys Totals 38 5 2 45 285 23 0 308									
Hwy 20 (Lundy's Lane)	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$									
Heavys Trucks Cars         Totals           3         8         99         110         110         110         110         110         110         110         110         110         110         110         110         110         110         110         110         110         110         110         110         110         110         110         110         110         110         110         110         110         110         110         110         110         110         110         110         110         110         110         110         110         110         110         110         110         110         110         110         110         110         110         110         110         110         110         110         110         110         110         110         110         110         110         110         110         110         110         110         110         110         110         110         110         110         110         110         110         110         110         110         110         110         110         110         110         110         110         110         110         110	Hwy 20 (Lundy's Lane)									
0 6 13 19 5 29 542 RR 58 (Davis Rd)	Cars Trucks Heavys Totals 493 25 4 522									
Peds Cross:     X     Cars     99     Ca       West Peds:     0     Trucks     27     Truck       West Entering:     576     Heavys     1     Heavy       West Leg Total:     972     Totals     127     Totals	rs       15       114       11       140       Peds Cross:       ⋈         rs       8       22       5       35       South Peds:       0         rs       0       3       1       4       South Entering:       179         rs       23       139       17       South Leg Total:       306									
Comn	nents									

Ontario T	raffic Inc.						
Afternoon Peak Diagram	Specified Period         One Hour Peak           From:         16:00:00         From:         16:15:00           To:         19:00:00         To:         17:15:00						
Municipality:ThoroldSite #:1822100011Intersection:Hwy 20 (Lundy's Lane) & RR 58 (DTFR File #:7Count date:14-Jun-18	Weather conditions: Person(s) who counted:						
** Signalized Intersection **	Major Road: Hwy 20 (Lundy's Lane) runs W/E						
North Leg Total: 637       Heavys 1       0       1       2         North Entering: 314       Trucks 5       9       3       17         North Peds:       0       Cars       108       125       62       29         Peds Cross:       Image: Second Sec	Heavys2East Leg Total:1151Trucks22East Entering:5685Cars299East Peds:2Totals323Peds Cross:X						
Heavys Trucks Cars Totals	R 58 (Davis Rd) Cars Trucks Heavys Totals 64 4 1 69 454 15 0 469 28 2 0 30						
Hwy 20 (Lundy's Lane)	F						
Heavys Trucks Cars Totals 0 7 107 114 1 18 472 491	Hwy 20 (Lundy's Lane)						
$\frac{0}{1}$ $\frac{7}{32}$ $\frac{17}{596}$ $\frac{24}{58}$ RR 58 (Davis Rd)	Cars         Hucks         Heavys         Holais           557         23         3         583						
Peds Cross:     Image: Construction       West Peds:     0       West Entering:     629       West Leg Total:     1270	rs       55       128       23       206       Peds Cross:       ⋈         rs       3       11       2       16       South Peds:       0         rs       0       1       1       2       South Entering:       224         rs       58       140       26       South Leg Total:       412						
Com	nents						
Com							

Ontario Traffic Inc.								
Total Count Diagram								
Municipality:ThoroldSite #:1822100011Intersection:Hwy 20 (Lundy's Lane) & RR 58 (DTFR File #:7Count date:14-Jun-18	Weather conditions: Person(s) who counted:							
** Signalized Intersection **	Major Road: Hwy 20 (Lundy's Lane) runs W/E							
North Leg Total: 2987       Heavys 11       3       4       18         North Entering: 1403       Trucks 32       55       17       10         North Peds:       0       Cars       428       540       313       124         Peds Cross:       IM       Totals       471       598       334	Heavys 22 Trucks 137 Cars 1425 Totals 1584 Heavys 22 East Leg Total: 4896 East Entering: 2286 East Peds: 3 Peds Cross: X							
Heavys Trucks Cars Totals 14 122 2337 2473 Hwy 20 (Lundy's Lane) RR 58 (Davis Rd) RR 58 (Davis Rd) Cars Trucks Heavys Totals 280 21 4 131 26 0 2167 112 7								
Heavys Trucks Cars Totals 11 30 550 591 591 591 591 591 591 591 500 500 500 500 500 500 500 500 500 50	Hwy 20 (Lundy's Lane)							
0 24 112 136 15 125 2742 RR 58 (Davis Rd)	Cars Trucks Heavys Totals 2486 113 11 2610							
Peds Cross:     Image: Carse in the state in	s       153       595       93       841       Peds Cross:       ⋈         s       25       86       25       136       South Peds:       0         s       0       7       3       10       South Entering:       987         s       178       688       121       South Leg Total:       1878							
Comr	ients							

				<i>Or</i> Traf	<i>itari</i> fic C	o <i>Traf</i> count S	fic I umr	n na	c. ary				
Intersection:	Hwy 20	(Lundy's	s Lane)	& RR 58	([ Count D	Date: 14-Jun-18	3 M	lunici	^{ipality:} Th	orold			
	Nort	h Appro	ach Tot	als					Sout	h Appro	ach Tot	als	
	Includ	es Cars, T	rucks, & H	eavys	_	North/South		_	Includes Cars, Trucks, & Heavys				
Hour Ending	Left	Thru	Right	Grand Total	Total Peds	Total Approaches	Hour Ending	,	Left	Thru	Right	Grand Total	Total Peds
6:00:00 7:00:00 8:00:00 9:00:00 16:00:00 17:00:00 18:00:00 19:00:00	1 26 50 60 1 68 78 50	1 92 83 79 4 114 139 85	0 57 75 58 3 102 102 74	2 175 208 197 8 284 319 209	0 0 0 0 0 0	2 293 385 368 15 495 503 325	6:00:0 7:00:0 8:00:0 9:00:0 16:00:0 17:00:0 18:00:0 19:00:0	00 00 00 00 00 00 00 00	0 9 29 26 1 60 30 23	0 90 124 131 6 130 127 77	0 19 24 14 0 21 27 16	0 118 177 171 7 211 184 116	
Totals:	334	597	471	1402	0	2386			178	685	121	984	0
	East	t Approa	ach Tota							<u>t Appro</u>	ach Tot	als	
Hour	moldu	cs oars, 1		Grand	Total	East/West Total	Hour		monud			Grand	Total
Ending 6:00:00 7:00:00 8:00:00 9:00:00 16:00:00 17:00:00 18:00:00 19:00:00	Left 1 24 28 30 0 26 28 20	Thru 3 137 222 286 5 437 426 308	Right 0 32 34 55 0 71 70 43	Total 4 193 284 371 5 534 524 371	Peds 0 0 0 0 2 0 1	Approaches 10 435 784 886 16 1151 1026 860	Ending 6:00:0 7:00:0 8:00:0 9:00:0 16:00:0 17:00:0 18:00:0 19:00:0	) 00 00 00 00 00 00 00 00	Left 0 61 99 95 0 101 127 108	Thru 5 165 375 401 11 486 356 356	Right 1 16 26 19 0 30 19 25	Total 6 242 500 515 11 617 502 489	Peds 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
Totals:	157	1824	305	2286	3	5168			591	2155	136	2882	0
Hours En Crossing	ding: Values:	6:00 2	<b>Calc</b> 7:00 127	ulated \ 8:00 203	/alues f 9:00 217	or Traffic Cr	ossing 16:0	<b>Ma</b> 00 8	i <b>jor Stre</b> 17:00 260	eet 18:00 247	19:00 159		







				<i>Or</i> Traf	<i>itari</i> fic C	o <i>Traf</i> count S	fic In umm	C. ary				
Intersection:	_undy's	Ln & Th	norold To	ownline l		Date: 19-Jun-18	3 Muni	^{cipality:} Th	orold			
	Nort	h Appro	ach Tot	als				Sout	h Appro	oach To	<b>Fotals</b>	
	Includ	es Cars, T	rucks, & H	eavys		North/South		Includes Cars, Trucks, & Heavys				
Hour Ending	Left	Thru	Right	Grand Total	Total Peds	Total Approaches	Hour Ending	Left	Thru	Right	Grand Total	Total Peds
6:00:00 7:00:00 8:00:00 9:00:00 16:00:00 17:00:00 18:00:00 19:00:00	0 5 9 14 0 20 12 16	0 49 84 67 0 118 84 78	0 10 25 26 0 22 39 18	0 64 118 107 0 160 135 112	0 1 0 1 0 0	0 202 359 328 0 426 341 255	6:00:00 7:00:00 8:00:00 9:00:00 16:00:00 17:00:00 18:00:00 19:00:00	0 40 76 67 0 92 72 42	0 71 129 131 0 130 92 73	0 27 36 23 0 44 42 28	0 138 241 221 0 266 206 143	0 1 0 0 1 0
Totals:	_76	480	140	696	3	1911		389	626	200	1215	2
	East	t Approa	ach Tota	als				Wes	t Appro	ach Tot	als	
Hour	menuu			Grand	Total	East/West Total	Hour	monuu			Grand	Total
Ending 6:00:00 7:00:00 8:00:00 16:00:00 17:00:00 18:00:00 19:00:00	Left 0 35 34 25 0 41 42 16	Thru 0 148 208 293 1 373 360 220	Right 0 5 8 0 27 11 12	Total 0 188 247 326 1 441 413 248	Peds 0 0 0 0 0 0 0	Approaches 0 413 622 798 1 959 903 563	Ending 6:00:00 7:00:00 8:00:00 9:00:00 16:00:00 17:00:00 18:00:00 19:00:00	Left 0 18 38 53 0 31 30 25	Thru 0 159 257 345 0 379 403 253	Right 0 48 80 74 0 108 57 37	Total 0 225 375 472 0 518 490 315	Peds 0 0 0 0 0 0 0
Totals:	193	1603	68	1864	0	4259		195	1796	404	2395	0
Hours En Crossing	ding: Values:	6:00 0	<b>Calc</b> 7:00 116	ulated \ 8:00 214	/alues f 9:00 212	or Traffic Cr	<b>ossing M</b> 16:00 0	ajor Stre 17:00 242	eet 18:00 176	19:00 136		

Ontario T	raffic Inc.					
Morning Peak Diagram	Specified Period         One Hour Peak           From:         6:00:00         From:         7:45:00           To:         9:00:00         To:         8:45:00					
Municipality:ThoroldSite #:1822100008Intersection:Lundy's Ln & Thorold Townline RdTFR File #:7Count date:14-Jun-18	Weather conditions: Person(s) who counted:					
** Signalized Intersection **	Major Road: Lundy's Ln runs W/E					
North Leg Total: 285       Heavys 0       0       0       0         North Entering: 132       Trucks 5       22       0       27         North Peds: 0       Cars 18       74       13       10         Peds Cross:       Image: Core set of the set of	Heavys1East Leg Total:812Trucks25East Entering:361Cars127East Peds:0Totals153Peds Cross:X					
Heavys Trucks Cars Totals	orold Townline Rd       Cars       Trucks       Heavys Totals         8       0       0       8         291       17       1       309         41       2       1       44					
w -	E					
Heavys Trucks Cars       Totals         0       5       42         2       15       379 $\frac{1}{3}$ 28       494	Cars Trucks Heavys Totals 431 16 4 451					
Peds Cross:       Image: Construction of the state of th	rs       51       77       39       167       Peds Cross:       Image: second					
Comr	nents					
Comn	nents					





				<i>Or</i> Traf	<i>itari</i> fic C	o <i>Traf</i> count S	fic In umm	C. ary				
Intersection:	_undy's	Ln & Th	norold To	ownline l		Date: 14-Jun-18	3 Muni	^{cipality:} Th	orold			
	Nort	h Appro	ach Tot	als				Sout	h Appro	oach Tot	als	
	Includ	es Cars, T	rucks, & H	eavys		North/South		Includes Cars, Trucks, & Heavys				
Hour Ending	Left	Thru	Right	Grand Total	Total Peds	Total Approaches	Hour Ending	Left	Thru	Right	Grand Total	Total Peds
6:00:00 7:00:00 8:00:00 9:00:00 16:00:00 17:00:00 18:00:00 19:00:00	0 6 10 19 0 25 30 20	0 69 100 79 0 115 117 75	0 14 17 20 0 47 42 25	0 89 127 118 0 187 189 120	0 0 0 0 0 0	0 239 320 319 0 456 423 268	6:00:00 7:00:00 8:00:00 9:00:00 16:00:00 17:00:00 18:00:00 19:00:00	0 48 61 57 0 108 92 54	0 73 101 104 0 104 109 69	0 29 31 40 0 57 33 25	0 150 193 201 0 269 234 148	0 1 0 0 0 1 4 0
Totals:	110	555	165	830	0	2025		420	560	215	1195	6
	Last Include	t Approa	ach lota rucks & H						t Appro	ach Iot		
Hour		-		Grand	Total	East/West Total	_Hour		-		Grand	Total
Ending 6:00:00 7:00:00 8:00:00 9:00:00 16:00:00 17:00:00 18:00:00 19:00:00	Left 0 38 36 32 0 48 47 28	Thru 0 152 214 300 0 400 399 309	Right 0 5 11 0 15 15 19	Total 0 196 255 343 0 463 461 356	Peds 0 0 0 0 1 1	Approaches 0 381 684 812 0 1021 935 793	Ending 6:00:00 7:00:00 8:00:00 9:00:00 16:00:00 17:00:00 18:00:00 19:00:00	Left 0 15 37 31 0 32 32 19	Thru 0 136 297 364 0 428 367 349	Right 0 34 95 74 0 98 75 69	Total 0 185 429 469 0 558 474 437	Peds 0 0 0 0 0 1 0
Totals:	229	1774	71	2074	2	4626		166	1941	445	2552	1
Hours En Crossing	ding: Values:	6:00 0	<b>Calc</b> 7:00 127	ulated \ 8:00 172	/alues f 9:00 180	or Traffic Cr	<b>ossing M</b> 16:00 0	ajor Stre 17:00 248	eet 18:00 241	19:00 150		







	Ontario Traffic Inc. Traffic Count Summary												
Intersection:	Thorold	Townlin	eRd &	Upper's		Date: 19-Jun-18	3 N	Munic	^{ipality:} Th	orold			
	Nort Include	h Appro	ach Tot	als eavys		North (Occuth			Souti Include	h Appro	ach To	tals leavys	
Hour Ending	Left	Thru	Right	Grand Total	Total Peds	North/South Total Approaches	Hour Ending	g	Left	Thru	Right	Grand Total	Total Peds
6:00:00 7:00:00 8:00:00 9:00:00 16:00:00 17:00:00 18:00:00 19:00:00	0 0 1 0 1 1 1	2 63 118 105 2 162 133 112	0 0 0 0 0 0	2 63 119 105 2 163 134 113	0 0 0 0 0 0	5 156 293 303 7 353 267 223	6:00: 7:00: 8:00: 9:00: 16:00: 17:00: 18:00: 19:00:	00 00 00 00 00 00 00 00		3 93 173 198 5 189 132 109	0 0 1 0 1 1 1	3 93 174 198 5 190 133 110	0 0 0 0 0 0
Totals:	4	697	0	701	1	1607			0	902	4	906	0
	East Includ	t <b>Appro</b> a es Cars. T	ach Tota rucks. & H	als eavvs					West Include	t Appro es Cars. T	ach Tot rucks. & ⊢	als leavys	
Hour Ending	Left	Thru	Right	Grand Total	Total Peds	East/West Total Approaches	Hour Ending	g	Left	Thru	Right	Grand Total	Total Peds
6:00:00 7:00:00 8:00:00 9:00:00 16:00:00 17:00:00 18:00:00 19:00:00	0 0 1 1 0 0 1		0 0 0 1 1 2	0 0 1 1 1 3		0 0 1 1 1 3	6:00:0 7:00:0 8:00:0 9:00:0 16:00:0 17:00:0 18:00:0 19:00:0	00 00 00 00 00 00 00 00		0 0 0 0 0			
Totals:	3	0	4	7	0	7		. 87	0	0	0	0	0
Hours En Crossing	ding: Values:	6:00 0	7:00 0	8:00 0	9:00 9:00	or traffic Cr	<b>ussing</b> 16:	00 00	17:00 0	<b>יפנ</b> 18:00 0	19:00 2		

Signal Code: H58	ovs								
Intersection: HW	Intersection: HWY 58 & DAVIS RD./THOROLD STONE RD.								
<b>Municipality: thor</b>	old								
Owner: MTO	Owner: MTO								
Last Modified: 4/24/2019 10:46:51 AM									
Timing Parameters	EBD & WBD THOROLD STONE RD.	NBD HWY 58 (SPLIT)	SBD DAVIS RD. (SPLIT)	n/a	n/a	n/a			
Min Green	20	10	10	0	0	0			
Walk	15	15	15	0	0	0			
Ped Clearance	7	7	7	0	0	0			
Vehicle Ext.	4.5	3	3	0	0	0			
Max Green	32	38	15	0	0	0			
Yellow	5.7	5.4	5.4	0	0	0			
All Red	2	2	1.5	0	0	0			

		Offset
Minimum Cycle	45.1	0
Pedestrian Cycle	59.1	
Maximum Cycle	107	0
Operation	FA	

8/23/1999

Count Date:

--/--/

FA = Fully Actuated

SA = Semi Actuated

FT = Fixed Time

Signal Code: 0570	70								
Intersection: RR5	7 (THOROLD STO	NE RD,) & RR70	(THOROLD TOWN	ILINE RD.)					
<b>Municipality: thore</b>	bld								
Owner: MTO									
Last Modified: 12/10/2013 9:50:43 AM									
Timing Parameters	EBD ADVANCE THOROLD STONE RD.	EBD & WBD THRU THOROLD STONE RD.	NBD & SBD THRU THOROLD TOWNLINE RD.	n/a	n/a	n/a			
Min Green	8	10	10	0	0	0			
Walk	0	11	15	0	0	0			
Ped Clearance	0	18	25	0	0	0			
Vehicle Ext.	2.5	6	2.3	0	0	0			
Max Green	20	44	35	0	0	0			
Yellow	3	4.1	4.1	0	0	0			
All Red	0	2	2.3	0	0	0			

		Offset
Minimum Cycle	32.5	0
Pedestrian Cycle	81.5	
Maximum Cycle	114.5	0
Operation	FA	

6/12/2003

Count Date:

5/10/2012

FA = Fully Actuated

SA = Semi Actuated

FT = Fixed Time

Signal Code: H58	BVR								
Intersection: High	way 58 & Beaver	dams Rd.							
<b>Municipality: thor</b>	old								
Owner: mto	Owner: mto								
Last Modified: 5/2	Last Modified: 5/29/2015 8:46:42 AM								
Timing Parameters	NBD & SBD THRU HWY 58	EBD & WBD THRU BEAVERDAMS RD.	n/a	n/a	n/a	n/a			
Min Green	25	10	0	0	0	0			
Walk	10	11	0	0	0	0			
Ped Clearance	15	19	0	0	0	0			
Vehicle Ext.	5	3	0	0	0	0			
Max Green	45	35	0	0	0	0			
Yellow	5	5	0	0	0	0			
All Red	2	3.1	0	0	0	0			

		Offset
Minimum Cycle	50.1	0
Pedestrian Cycle	70.1	
Maximum Cycle	95.1	0
Operation	FA	

```
5/29/2015
```

Count Date:

--/--/

FA = Fully Actuated

SA = Semi Actuated

FT = Fixed Time

Signal Code: H20H	158								
Intersection: HWY	7. 20 & HWY. 58/	RR82 (ALLANPO	RT RD.)						
<b>Municipality: thor</b>	old								
Owner: MTO									
Last Modified: 5/1	Last Modified: 5/18/2017 2:36:50 PM								
Timing Parameters	EBD & WBD THRU HWY 20	NBD & SBD THRU ALLANPORT RD./HWY 58	n/a	n/a	n/a	n/a			
Min Green	22	15	0	0	0	0			
Walk	11	10	0	0	0	0			
Ped Clearance	18	15	0	0	0	0			
Vehicle Ext.	4	2	0	0	0	0			
Max Green	45	35	0	0	0	0			
Yellow	5	5	0	0	0	0			
All Red	2	2	0	0	0	0			

	Offset	
Minimum Cycle	51	0
Pedestrian Cycle	68	
Maximum Cycle	94	0
Operation	FA	

10/2/2000

Count Date:

--/--/

FA = Fully Actuated

SA = Semi Actuated

FT = Fixed Time

Signal Code: 070H20							
Intersection: RR70 (TOWNLINE RD.) & HWY 20 (LUNDYS LANE)							
Municipality: thorold							
Owner: MTO Last Modified: 3/28/2018 11:28:16 AM							
Min Green	20	10	0	0	0	0	
Walk	15	15	0	0	0	0	
Ped Clearance	7	14	0	0	0	0	
Vehicle Ext.	5	5	0	0	0	0	
Max Green	50	40	0	0	0	0	
Yellow	5	4	0	0	0	0	
All Red	2	2	0	0	0	0	

	Offset	
Minimum Cycle	43	0
Pedestrian Cycle	64	
Maximum Cycle	103	0
Operation	FA	

5/2/2001

**Count Date:** 

5/14/2008

FA = Fully Actuated

SA = Semi Actuated

FT = Fixed Time



## **APPENDIX C**

**Capacity Analysis**
Timings 1: Davis Road & Th		<2018 Existing> AM Peak Hour 09-14-2021										
	٦	-	$\mathbf{r}$	4	-	1	Ť	1	1	ţ	-	
Lane Group	EBL	EBT	EBR	WBL	WBT	NBL	NBT	NBR	SBL	SBT	SBR	
Lane Configurations	ሻ	- <b>†</b> †	1	<u>۲</u>	<b>↑</b> 1≽	<u>۲</u>	र्भ	1	<u>۳</u>	<b>↑</b>	1	
Traffic Volume (vph)	21	866	226	67	1053	398	15	149	1	2	18	
Future Volume (vph)	21	866	226	67	1053	398	15	149	1	2	18	
Turn Type	Perm	NA	Perm	Perm	NA	Split	NA	Perm	Split	NA	Perm	
Protected Phases		2			6	4	4		8	8		
Permitted Phases	2		2	6				4			8	
Detector Phase	2	2	2	6	6	4	4	4	8	8	8	
Switch Phase												
Minimum Initial (s)	20.0	20.0	20.0	20.0	20.0	10.0	10.0	10.0	10.0	10.0	10.0	
Minimum Split (s)	28.9	28.9	28.9	28.9	28.9	29.7	29.7	29.7	21.7	21.7	21.7	
Total Split (s)	39.7	39.7	39.7	39.7	39.7	45.4	45.4	45.4	21.9	21.9	21.9	
Total Split (%)	37.1%	37.1%	37.1%	37.1%	37.1%	42.4%	42.4%	42.4%	20.5%	20.5%	20.5%	
Yellow Time (s)	5.4	5.4	5.4	5.4	5.4	5.7	5.7	5.7	5.7	5.7	5.7	
All-Red Time (s)	1.5	1.5	1.5	1.5	1.5	2.0	2.0	2.0	2.0	2.0	2.0	
Lost Time Adjust (s)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Total Lost Time (s)	6.9	6.9	6.9	6.9	6.9	7.7	7.7	7.7	7.7	7.7	7.7	
Lead/Lag												
Lead-Lag Optimize?												
Recall Mode	C-Max	C-Max	C-Max	Max	Max	None	None	None	None	None	None	
Act Effct Green (s)	62.8	62.8	62.8	62.8	62.8	22.5	22.5	22.5	10.0	10.0	10.0	
Actuated g/C Ratio	0.59	0.59	0.59	0.59	0.59	0.21	0.21	0.21	0.09	0.09	0.09	
v/c Ratio	0.12	0.45	0.26	0.29	0.55	0.66	0.66	0.36	0.01	0.01	0.08	
Control Delay	18.8	16.4	6.0	21.4	18.2	47.5	47.7	7.3	44.0	44.5	0.7	
Queue Delay	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Total Delay	18.8	16.4	6.0	21.4	18.2	47.5	47.7	7.3	44.0	44.5	0.7	
LOS	В	В	A	С	В	D	D	A	D	D	А	
Approach Delay		14.4			18.4		36.9			6.6		
Approach LOS		В			В		D			A		
Intersection Summarv												
Cycle Length: 107												
Actuated Cycle Length: 107												
Offset: 0 (0%), Referenced to	o phase 2	EBTL St	art of Gre	en								
Natural Cycle: 85	- prideo 21	, 00										
Control Type: Actuated-Cool	rdinated											
Maximum v/c Ratio: 0.66												
Intersection Signal Delay: 20	).4			Ir	ntersectio	n LOS: C						
Intersection Capacity Utilizat	tion 82.0%				CU Level	of Service	e D					
Analysis Period (min) 15				IX.								

Splits and Phases: 1: Davis Road & Thorold Stone Road

Ø2 (R)	<b>▲</b> Ø4	<b>4</b> ►ø8
39.7 s	45.4 s	21.9 s
₹ø6		
39.7 s		

Uppers Quarry Traffic Impact Study TMIG

Synchro 10 Report

HCM Signalized Intersection Capacity Analysis 1: Davis Road & Thorold Stone Road <2018 Existing> AM Peak Hour _____09-14-2021

	٦	-	$\mathbf{\hat{z}}$	4	+	*	1	1	۲	1	ŧ	-
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	ň	44	1	۲.	<b>≜t</b> ≽		5	ę.	1	5	•	1
Traffic Volume (vph)	21	866	226	67	1053	6	398	15	149	1	2	18
Future Volume (vph)	21	866	226	67	1053	6	398	15	149	1	2	18
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Total Lost time (s)	6.9	6.9	6.9	6.9	6.9		7.7	7.7	7.7	7.7	7.7	7.7
Lane Util. Factor	1.00	0.95	1.00	1.00	0.95		0.95	0.95	1.00	1.00	1.00	1.00
Frpb, ped/bikes	1.00	1.00	1.00	1.00	1.00		1.00	1.00	0.99	1.00	1.00	0.99
Flpb, ped/bikes	1.00	1.00	1.00	1.00	1.00		1.00	1.00	1.00	1.00	1.00	1.00
Frt	1.00	1.00	0.85	1.00	1.00		1.00	1.00	0.85	1.00	1.00	0.85
Flt Protected	0.95	1.00	1.00	0.95	1.00		0.95	0.96	1.00	0.95	1.00	1.00
Satd. Flow (prot)	1640	3406	1442	1530	3398		1559	1549	1475	1388	1624	1338
Flt Permitted	0.19	1.00	1.00	0.26	1.00		0.95	0.96	1.00	0.95	1.00	1.00
Satd. Flow (perm)	321	3406	1442	416	3398		1559	1549	1475	1388	1624	1338
Peak-hour factor, PHF	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96
Adj. Flow (vph)	22	902	235	70	1097	6	415	16	155	1	2	19
RTOR Reduction (vph)	0	0	79	0	0	0	0	0	122	0	0	18
Lane Group Flow (vph)	22	902	156	70	1103	0	216	215	33	1	2	1
Confl. Peds. (#/hr)	1					1	1		1	1		1
Heavy Vehicles (%)	10%	6%	12%	18%	6%	30%	10%	28%	8%	30%	17%	19%
Turn Type	Perm	NA	Perm	Perm	NA		Split	NA	Perm	Split	NA	Perm
Protected Phases		2			6		. 4	4		. 8	8	
Permitted Phases	2		2	6					4			8
Actuated Green, G (s)	58.2	58.2	58.2	58.2	58.2		22.5	22.5	22.5	4.0	4.0	4.0
Effective Green, g (s)	58.2	58.2	58.2	58.2	58.2		22.5	22.5	22.5	4.0	4.0	4.0
Actuated g/C Ratio	0.54	0.54	0.54	0.54	0.54		0.21	0.21	0.21	0.04	0.04	0.04
Clearance Time (s)	6.9	6.9	6.9	6.9	6.9		7.7	7.7	7.7	7.7	7.7	7.7
Vehicle Extension (s)	3.0	3.0	3.0	3.0	3.0		4.5	4.5	4.5	4.5	4.5	4.5
Lane Grp Cap (vph)	174	1852	784	226	1848		327	325	310	51	60	50
v/s Ratio Prot		0.26			c0.32		0.14	c0.14		0.00	c0.00	
v/s Ratio Perm	0.07		0.11	0.17					0.02			0.00
v/c Ratio	0.13	0.49	0.20	0.31	0.60		0.66	0.66	0.11	0.02	0.03	0.01
Uniform Delay, d1	12.0	15.1	12.5	13.4	16.5		38.7	38.8	34.1	49.6	49.6	49.6
Progression Factor	1.00	1.00	1.00	1.00	1.00		1.00	1.00	1.00	1.00	1.00	1.00
Incremental Delay, d2	1.5	0.9	0.6	3.5	1.4		5.9	6.0	0.3	0.3	0.4	0.2
Delay (s)	13.4	16.1	13.0	16.9	17.9		44.6	44.7	34.4	49.9	50.0	49.8
Level of Service	В	В	В	В	В		D	D	С	D	D	D
Approach Delay (s)		15.4			17.8			42.0			49.8	
Approach LOS		В			В			D			D	
Intersection Summary												
HCM 2000 Control Delay			21.9	Н	CM 2000	Level of S	Service		С			
HCM 2000 Volume to Capa	icity ratio		0.59									
Actuated Cycle Length (s)			107.0	S	um of lost	time (s)			22.3			
Intersection Capacity Utiliza	ation		82.0%	IC	U Level o	of Service			D			
Analysis Period (min)			15									

c Critical Lane Group

Uppers Quarry Traffic Impact Study TMIG

	,				,					
	٠	-	1	+	1	T.	-	Ŧ	-	
Lane Group	EBL	EBT	WBL	WBT	NBL	NBT	SBL	SBT	SBR	
Lane Configurations		4		4	ሻ	A	<u>۲</u>	- <b>†</b> †	7	
Traffic Volume (vph)	110	31	24	17	4	267	82	172	44	
Future Volume (vph)	110	31	24	17	4	267	82	172	44	
Furn Type	Perm	NA	Perm	NA	Perm	NA	Perm	NA	Perm	
Protected Phases		2		6		4		8		
Permitted Phases	2		6		4		8		8	
Detector Phase	2	2	6	6	4	4	8	8	8	
Switch Phase										
Vinimum Initial (s)	10.0	10.0	10.0	10.0	25.0	25.0	25.0	25.0	25.0	
Minimum Split (s)	38.1	38.1	38.1	38.1	32.0	32.0	32.0	32.0	32.0	
i otal Split (s)	43.1	43.1	43.1	43.1	52.0	52.0	52.0	52.0	52.0	
rotai Split (%)	45.3%	45.3%	45.3%	45.3%	54.7%	54.7%	54.7%	54.7%	54.7%	
rellow Time (s)	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	
All-Red Time (S)	3.1	3.1	3.1	3.1	2.0	2.0	2.0	2.0	2.0	
LOST TIME Adjust (s)		0.0		0.0	0.0	0.0	0.0	0.0	0.0	
ood/Log		0.1		0.1	7.0	7.0	7.0	7.0	7.0	
ead Lag Optimize?										
	C Max	C Max	Max	Max	None	None	None	None	None	
Act Effet Green (s)	0-IVIUX	55.0	WIGA	55.0	25.0	25.0	25.0	25.0	25.0	
Actuated g/C Ratio		0.58		0.58	0.26	0.26	0.26	0.26	0.26	
//c Ratio		0.24		0.22	0.02	0.38	0.31	0.23	0.11	
Control Delay		10.8		3.0	26.5	28.6	32.0	28.5	6.0	
Queue Delav		0.0		0.0	0.0	0.0	0.0	0.0	0.0	
Total Delay		10.8		3.0	26.5	28.6	32.0	28.5	6.0	
_OS		В		A	C	С	С	C	А	
Approach Delay		10.8		3.0	-	28.6	_	26.1		
Approach LOS		В		Α		С		С		
ntersection Summary										
Cycle Length: 95.1										
Actuated Cycle Length: 9	5.1									
Offset: 0 (0%), Reference	d to phase 2:	EBTL, St	art of Gre	en						
latural Cycle: 75										
Control Type: Actuated-C	pordinated									
Maximum v/c Ratio: 0.38										
ntersection Signal Delay:	19.5			I	ntersectio	n LOS: B	_			
ntersection Capacity Utili	zation 87.6%			10	CU Level	ot Service	θÉ			

opina ana i nasos.	2. Davis Road & Niagara Fail	3 Road/Dear	Verdams read
[▲] ø2 (R)			<td< td=""></td<>
43.1 s			52 s
₹ø6			€ 08
43.1 s			52 s

Synchro 10 Report

HCM Signalized Intersection Capacity Analysis 2: Davis Road & Niagara Falls Road/Beaverdams Road <2018 Existing> AM Peak Hour 09-14-2021

	۶	-	$\mathbf{\hat{z}}$	4	+	×	1	Ť	۲	1	Ŧ	~
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		4			4		ሻ	<b>4</b> 12		5	44	1
Traffic Volume (vph)	110	31	7	24	17	166	4	267	30	82	172	44
Future Volume (vph)	110	31	7	24	17	166	4	267	30	82	172	44
deal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Total Lost time (s)		8.1			8.1		7.0	7.0		7.0	7.0	7.0
Lane Util. Factor		1.00			1.00		1.00	0.95		1.00	0.95	1.00
Frt		0.99			0.89		1.00	0.98		1.00	1.00	0.85
Flt Protected		0.96			0.99		0.95	1.00		0.95	1.00	1.00
Satd. Flow (prot)		1667			1629		1388	3113		1787	2983	1392
Flt Permitted		0.66			0.96		0.64	1.00		0.56	1.00	1.00
Satd. Flow (perm)		1138			1569		932	3113		1054	2983	1392
Peak-hour factor, PHF	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95
Adj. Flow (vph)	116	33	7	25	18	175	4	281	32	86	181	46
RTOR Reduction (vph)	0	1	0	0	74	0	0	13	0	0	0	34
Lane Group Flow (vph)	0	155	0	0	144	0	4	300	0	86	181	12
Heavy Vehicles (%)	10%	7%	7%	7%	12%	2%	30%	15%	7%	1%	21%	16%
Turn Type	Perm	NA		Perm	NA		Perm	NA		Perm	NA	Perm
Protected Phases		2			6			4			8	
Permitted Phases	2			6			4			8		8
Actuated Green, G (s)		55.0			55.0		25.0	25.0		25.0	25.0	25.0
Effective Green, g (s)		55.0			55.0		25.0	25.0		25.0	25.0	25.0
Actuated g/C Ratio		0.58			0.58		0.26	0.26		0.26	0.26	0.26
Clearance Time (s)		8.1			8.1		7.0	7.0		7.0	7.0	7.0
Vehicle Extension (s)		3.0			3.0		5.0	5.0		5.0	5.0	5.0
Lane Grp Cap (vph)		658			907		245	818		277	784	365
//s Ratio Prot								c0.10			0.06	
//s Ratio Perm		c0.14			0.09		0.00			0.08		0.01
//c Ratio		0.24			0.16		0.02	0.37		0.31	0.23	0.03
Uniform Delay, d1		9.8			9.3		25.9	28.6		28.1	27.5	26.1
Progression Factor		1.00			1.00		1.00	1.00		1.00	1.00	1.00
Incremental Delay, d2		0.8			0.4		0.1	0.6		1.3	0.3	0.1
Delay (s)		10.6			9.7		26.0	29.2		29.5	27.8	26.1
Level of Service		В			А		С	С		С	С	С
Approach Delay (s)		10.6			9.7			29.1			28.0	
Approach LOS		В			Α			С			С	
Intersection Summary												
HCM 2000 Control Delay			21.7	Н	CM 2000	Level of S	Service		С			
HCM 2000 Volume to Capacity	ratio		0.28									
Actuated Cycle Length (s)			95.1	S	um of los	t time (s)			15.1			
Intersection Capacity Utilization	ı		87.6%	IC	CU Level	of Service			E			
Analysis Period (min)			15									
c Critical Lane Group												

Uppers Quarry Traffic Impact Study TMIG

3: Davis Road & Lundys Lane 09-14-2021											
	٦	-	4	+	•	1	1	1	۰ŧ	~	
Lane Group	EBL	EBT	WBL	WBT	WBR	NBL	NBT	SBL	SBT	SBR	
Lane Configurations	ሻ	ĥ	ሻ	•	1	ሻ	ĥ	٦	•	1	
Traffic Volume (vph)	118	433	29	305	47	22	137	58	89	74	
Future Volume (vph)	118	433	29	305	47	22	137	58	89	74	
Turn Type	Perm	NA	Perm	NA	Perm	Perm	NA	Perm	NA	Perm	
Protected Phases		2		6			4		8		
Permitted Phases	2		6		6	4		8		8	
Detector Phase	2	2	6	6	6	4	4	8	8	8	
Switch Phase											
Vinimum Initial (s)	22.0	22.0	22.0	22.0	22.0	15.0	15.0	15.0	15.0	15.0	
Vinimum Split (s)	36.0	36.0	36.0	36.0	36.0	32.0	32.0	32.0	32.0	32.0	
Total Split (s)	52.0	52.0	52.0	52.0	52.0	42.0	42.0	42.0	42.0	42.0	
Total Split (%)	55.3%	55.3%	55.3%	55.3%	55.3%	44.7%	44.7%	44.7%	44.7%	44.7%	
Yellow Time (s)	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	
All-Red Time (s)	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	
ost Time Adjust (s)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Fotal Lost Time (s)	7.0	7.0	7.0	7.0	7.0	7.0	7.0	7.0	7.0	7.0	
ead/Lag	1.0										
ead-Lag Ontimize?											
Recall Mode	C-Max	C-Max	Max	Max	Max	None	None	None	None	None	
Act Effct Green (s)	63.5	63.5	63.5	63.5	63.5	16.5	16.5	16.5	16.5	16.5	
Actuated g/C Ratio	0.68	0.68	0.68	0.68	0.68	0.18	0.18	0.18	0.18	0.18	
v/c Ratio	0.00	0.39	0.06	0.28	0.05	0.10	0.10	0.36	0.35	0.10	
Control Delay	7.0	8.2	6.3	7.2	2.0	33.2	43.2	39.6	37.4	9.8	
	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Total Delay	7.0	8.2	6.3	7.2	2.0	33.2	43.2	39.6	37.4	0.0	
	7.0	0.2	0.0	1.2	2.0	00.2	40.2 D	00.0 D	л. Т	5.0	
LUG Approach Dolov	A	70	A	6 F	A	U	42.0	U	20.7	A	
Approach LOS		1.9		0.5			42.0 D		20.7		
Appidacii 203		A		A			U		U		
ntersection Summary											
Cycle Length: 94											
Actuated Cycle Length: 94											
Offset: 0 (0%), Referenced	to phase 2	EBTL, St	art of Gre	en							
Vatural Cycle: 70											
Control Type: Actuated-Coc	ordinated										
Maximum v/c Ratio: 0.61											
ntersection Signal Delay: 1	5.5			I	ntersectio	n LOS: B					
ntersection Capacity Utiliza	ition 90.8%			10	CU Level	of Service	εE				
Analysis Period (min) 15											
Colite and Phases 2: De	via Dood º	Lunduc	000								
Splits and Phases: 3: Day	vis Road &	Lundys L	ane								

✓ Ø2 (R)	Ø4	
52 s	42 s	
<b>∲</b> Ø6		
52 s	42 s	

Synchro 10 Report

HCM Signalized Intersection Capacity Analysis 3: Davis Road & Lundys Lane <2018 Existing> AM Peak Hour 09-14-2021

	٦	-	$\mathbf{i}$	1	+	×	1	t	۲	1	Ŧ	~
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	۲.	4Î		۲	•	1	۲	f,		ň	•	1
Traffic Volume (vph)	118	433	18	29	305	47	22	137	21	58	89	74
Future Volume (vph)	118	433	18	29	305	47	22	137	21	58	89	74
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Total Lost time (s)	7.0	7.0		7.0	7.0	7.0	7.0	7.0		7.0	7.0	7.0
Lane Util. Factor	1.00	1.00		1.00	1.00	1.00	1.00	1.00		1.00	1.00	1.00
Frpb, ped/bikes	1.00	1.00		1.00	1.00	1.00	1.00	1.00		1.00	1.00	1.00
Flpb, ped/bikes	1.00	1.00		1.00	1.00	1.00	1.00	1.00		1.00	1.00	1.00
Frt	1.00	0.99		1.00	1.00	0.85	1.00	0.98		1.00	1.00	0.85
Flt Protected	0.95	1.00		0.95	1.00	1.00	0.95	1.00		0.95	1.00	1.00
Satd. Flow (prot)	1656	1821		1466	1743	1442	1444	1535		1530	1532	1392
Flt Permitted	0.56	1.00		0.46	1.00	1.00	0.70	1.00		0.61	1.00	1.00
Satd. Flow (perm)	984	1821		706	1743	1442	1057	1535		986	1532	1392
Peak-hour factor, PHF	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94
Adj. Flow (vph)	126	461	19	31	324	50	23	146	22	62	95	79
RTOR Reduction (vph)	0	1	0	0	0	16	0	7	0	0	0	65
Lane Group Flow (vph)	126	479	0	31	324	34	23	161	0	62	95	14
Confl. Peds. (#/hr)			1	1								
Heavy Vehicles (%)	9%	3%	19%	23%	9%	12%	25%	20%	30%	18%	24%	16%
Turn Type	Perm	NA		Perm	NA	Perm	Perm	NA		Perm	NA	Perm
Protected Phases		2			6			4			8	
Permitted Phases	2			6		6	4			8		8
Actuated Green, G (s)	63.5	63.5		63.5	63.5	63.5	16.5	16.5		16.5	16.5	16.5
Effective Green, g (s)	63.5	63.5		63.5	63.5	63.5	16.5	16.5		16.5	16.5	16.5
Actuated g/C Ratio	0.68	0.68		0.68	0.68	0.68	0.18	0.18		0.18	0.18	0.18
Clearance Time (s)	7.0	7.0		7.0	7.0	7.0	7.0	7.0		7.0	7.0	7.0
Vehicle Extension (s)	4.0	4.0		4.0	4.0	4.0	2.0	2.0		2.0	2.0	2.0
Lane Grp Cap (vph)	664	1230		476	1177	974	185	269		173	268	244
v/s Ratio Prot		c0.26			0.19			c0.10			0.06	
v/s Ratio Perm	0.13			0.04		0.02	0.02			0.06		0.01
v/c Ratio	0.19	0.39		0.07	0.28	0.03	0.12	0.60		0.36	0.35	0.06
Uniform Delay, d1	5.7	6.7		5.2	6.1	5.1	32.7	35.7		34.1	34.1	32.3
Progression Factor	1.00	1.00		1.00	1.00	1.00	1.00	1.00		1.00	1.00	1.00
Incremental Delay, d2	0.6	0.9		0.3	0.6	0.1	0.1	2.4		0.5	0.3	0.0
Delay (s)	6.3	7.6		5.4	6.7	5.1	32.8	38.1		34.6	34.4	32.3
Level of Service	А	А		А	Α	А	С	D		С	С	С
Approach Delay (s)		7.4			6.4			37.4			33.7	
Approach LOS		А			А			D			С	
Intersection Summary												
HCM 2000 Control Delay			15.4	Н	CM 2000	Level of	Service		В			
HCM 2000 Volume to Capa	acity ratio		0.43									
Actuated Cycle Length (s)			94.0	S	um of los	t time (s)			14.0			
Intersection Capacity Utiliza	ation		90.8%	IC	U Level	of Service			E			
Analysis Period (min)			15									
- Oritical Lana Origin												

c Critical Lane Group

Uppers Quarry Traffic Impact Study TMIG

	≯	-	$\rightarrow$	4	+	•	1	<b>†</b>	1	Ŧ	
Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	SBL	SBT	
Lane Configurations	- N	- <b>†</b> †	1	<u>۲</u>	- <b>††</b>	1	<u>۲</u>	4Î	<u>۲</u>	4Î	
Traffic Volume (vph)	323	659	34	20	807	73	64	112	52	81	
Future Volume (vph)	323	659	34	20	807	73	64	112	52	81	
Turn Type	pm+pt	NA	Perm	Perm	NA	Perm	Perm	NA	Perm	NA	
Protected Phases	5	2			6			4		8	
Permitted Phases	2		2	6		6	4		8		
Detector Phase	5	2	2	6	6	6	4	4	8	8	
Switch Phase											
Minimum Initial (s)	8.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	
Minimum Split (s)	11.0	35.1	35.1	35.1	35.1	35.1	41.4	41.4	41.4	41.4	
Total Split (s)	23.0	73.1	73.1	50.1	50.1	50.1	41.4	41.4	41.4	41.4	
Total Split (%)	20.1%	63.8%	63.8%	43.8%	43.8%	43.8%	36.2%	36.2%	36.2%	36.2%	
Yellow Time (s)	3.0	4.1	4.1	4.1	4.1	4.1	4.1	4.1	4.1	4.1	
All-Red Time (s)	0.0	2.0	2.0	2.0	2.0	2.0	2.3	2.3	2.3	2.3	
Lost Time Adjust (s)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Total Lost Time (s)	3.0	6.1	6.1	6.1	6.1	6.1	6.4	6.4	6.4	6.4	
Lead/Lag	Lead			Lag	Lag	Lag					
_ead-Lag Optimize?	Yes			Yes	Yes	Yes					
Recall Mode	None	C-Max	C-Max	C-Max	C-Max	C-Max	None	None	None	None	
Act Effct Green (s)	84.6	81.5	81.5	63.2	63.2	63.2	20.5	20.5	20.5	20.5	
Actuated g/C Ratio	0.74	0.71	0.71	0.55	0.55	0.55	0.18	0.18	0.18	0.18	
v/c Ratio	0.68	0.28	0.04	0.06	0.43	0.09	1.03	0.48	0.29	0.84	
Control Delay	13.5	7.2	2.6	18.8	18.7	5.1	165.7	42.7	41.2	47.5	
Queue Delay	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Total Delay	13.5	7.2	2.6	18.8	18.7	5.1	165.7	42.7	41.2	47.5	
LOS	В	А	А	В	В	Α	F	D	D	D	
Approach Delay		9.0			17.6			82.1		46.6	
Approach LOS		А			В			F		D	
Intersection Summary											
Cycle Length: 114.5											
Actuated Cycle Length: 11	4.5										
Offset: 0 (0%), Referenced	I to phase 2	EBTL an	d 6:WBTL	., Start of	Green						
Natural Cycle: 90											
Control Type: Actuated-Co	ordinated										
Maximum v/c Ratio: 1.03											
ntersection Signal Delay:	23.3			Ir	ntersectio	n LOS: C					
Intersection Capacity Utiliz	ation 86.3%			IC	CU Level	of Service	ε				
Analysis Period (min) 15											

Splits and Phases: 4: Thorold Townline Road & Thorold Stone Road

	,	≪¶ø4
73.1s		41.4 s
	∮ ∮ Ø6 (R)	Ø8
23 s	50.1s	41.4 s

Uppers Quarry Traffic Impact Study TMIG

Synchro 10 Report

HCM Signalized Intersection Capacity Analysis <u>4</u>: Thorold Townline Road & Thorold Stone Road <2018 Existing> AM Peak Hour 09-14-2021

	٦	+	>	4	+	×.	•	Ť	1	1	Ŧ	1
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	٦	<u></u>	1	ľ	<u></u>	1	ľ	4Î		ľ	et e	
Traffic Volume (vph)	323	659	34	20	807	73	64	112	24	52	81	205
Future Volume (vph)	323	659	34	20	807	73	64	112	24	52	81	205
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Total Lost time (s)	3.0	6.1	6.1	6.1	6.1	6.1	6.4	6.4		6.4	6.4	
Lane Util. Factor	1.00	0.95	1.00	1.00	0.95	1.00	1.00	1.00		1.00	1.00	
Frpb, ped/bikes	1.00	1.00	1.00	1.00	1.00	0.97	1.00	1.00		1.00	1.00	
Flpb, ped/bikes	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00		1.00	1.00	
Frt	1.00	1.00	0.85	1.00	1.00	0.85	1.00	0.97		1.00	0.89	
Flt Protected	0.95	1.00	1.00	0.95	1.00	1.00	0.95	1.00		0.95	1.00	
Satd. Flow (prot)	1640	3471	1369	1444	3505	1454	1492	1596		1641	1446	
Flt Permitted	0.27	1.00	1.00	0.39	1.00	1.00	0.23	1.00		0.61	1.00	
Satd. Flow (perm)	460	3471	1369	594	3505	1454	365	1596		1058	1446	
Peak-hour factor, PHF	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96
Adj. Flow (vph)	336	686	35	21	841	76	67	117	25	54	84	214
RTOR Reduction (vph)	0	0	10	0	0	34	0	8	0	0	94	0
Lane Group Flow (vph)	336	686	25	21	841	42	67	134	0	54	204	0
Confl. Peds. (#/hr)	4					4						
Heavy Vehicles (%)	10%	4%	18%	25%	3%	8%	21%	14%	25%	10%	18%	17%
Turn Type	pm+pt	NA	Perm	Perm	NA	Perm	Perm	NA		Perm	NA	
Protected Phases	5	2			6			4			8	
Permitted Phases	2		2	6		6	4			8		
Actuated Green, G (s)	81.5	81.5	81.5	63.3	63.3	63.3	20.5	20.5		20.5	20.5	
Effective Green, g (s)	81.5	81.5	81.5	63.3	63.3	63.3	20.5	20.5		20.5	20.5	
Actuated g/C Ratio	0.71	0.71	0.71	0.55	0.55	0.55	0.18	0.18		0.18	0.18	
Clearance Time (s)	3.0	6.1	6.1	6.1	6.1	6.1	6.4	6.4		6.4	6.4	
Vehicle Extension (s)	2.5	6.0	6.0	6.0	6.0	6.0	2.3	2.3		2.3	2.3	
Lane Grp Cap (vph)	484	2470	974	328	1937	803	65	285		189	258	
v/s Ratio Prot	c0.09	0.20			0.24			0.08			0.14	
v/s Ratio Perm	c0.40		0.02	0.04		0.03	c0.18			0.05		
v/c Ratio	0.69	0.28	0.03	0.06	0.43	0.05	1.03	0.47		0.29	0.79	
Uniform Delay, d1	7.9	5.9	4.8	11.9	15.1	11.8	47.0	42.1		40.7	44.9	
Progression Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00		1.00	1.00	
Incremental Delay, d2	4.0	0.3	0.0	0.4	0.7	0.1	120.5	0.7		0.5	14.0	
Delay (s)	11.9	6.2	4.9	12.2	15.8	11.9	167.5	42.8		41.2	59.0	
Level of Service	В	А	А	В	В	В	F	D		D	E	
Approach Delay (s)		8.0			15.4			82.8			56.2	
Approach LOS		A			В			F			E	
Intersection Summary												
HCM 2000 Control Delay			23.5	Н	CM 2000	Level of	Service		С			
HCM 2000 Volume to Capa	city ratio		0.78									
Actuated Cycle Length (s)			114.5	S	um of los	t time (s)			15.5			
Intersection Capacity Utiliza	ition		86.3%	IC	CU Level of	of Service	)		E			
Analysis Period (min)			15									
0.111 0												

c Critical Lane Group

Uppers Quarry Traffic Impact Study TMIG

	٨	+	1	4	t	*	t	ŕ	Ļ	
Lane Group	FBI	FBT	FBR	WBI	WBT	NBI	NBT	SBI	SBT	
Lane Configurations	<u> </u>		1	*	1	*	1	3	1	
Traffic Volume (voh)	62	380	86	38	304	66	141	13	86	
Future Volume (vph)	62	380	86	38	304	66	141	13	86	
Turn Type	Perm	NA	Perm	Perm	NA	Perm	NA	Perm	NA	
Protected Phases		2			6		4		8	
Permitted Phases	2	-	2	6	Ű	4		8	Ű	
Detector Phase	2	2	2	6	6	4	4	8	8	
Switch Phase	_	-	-	, in the second s	Ű			, in the second se	Ű	
Minimum Initial (s)	20.0	20.0	20.0	20.0	20.0	10.0	10.0	10.0	10.0	
Minimum Split (s)	29.0	29.0	29.0	29.0	29.0	35.0	35.0	35.0	35.0	
Total Split (s)	57.0	57.0	57.0	57.0	57.0	46.0	46.0	46.0	46.0	
Total Split (%)	55.3%	55.3%	55.3%	55.3%	55.3%	44.7%	44.7%	44.7%	44.7%	
Yellow Time (s)	5.0	5.0	5.0	5.0	5.0	4.0	4.0	4.0	4.0	
All-Red Time (s)	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	
Lost Time Adjust (s)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Total Lost Time (s)	7.0	7.0	7.0	7.0	7.0	6.0	6.0	6.0	6.0	
Lead/Lag	1.0					0.0	0.0	0.0	0.0	
Lead-Lag Optimize?										
Recall Mode	C-Max	C-Max	C-Max	Max	Max	None	None	None	None	
Act Effct Green (s)	71.3	71.3	71.3	71.3	71.3	18.7	18.7	18.7	18.7	
Actuated g/C Ratio	0.69	0.69	0.69	0.69	0.69	0.18	0.18	0.18	0.18	
v/c Ratio	0.10	0.33	0.09	0.06	0.27	0.34	0.63	0.09	0.41	
Control Delay	6.9	7.9	3.5	6.7	7.4	39.5	44.5	33.4	34.7	
Queue Delav	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Total Delay	6.9	7.9	3.5	6.7	7.4	39.5	44.5	33.4	34.7	
LOS	A	A	A	A	А	D	D	С	С	
Approach Delay		7.1			7.3		43.2	-	34.6	
Approach LOS		A			A		D		C	
Internetion Cummon										
Cycle Length: 103	00									
Actuated Cycle Length: I	03		1 (0							
Uffset: 0 (0%), Reference	ed to phase 2	EBIL, St	art of Gre	en						
Natural Cycle: 65	a a sellar a fa al									
Jonitol Type: Actuated-C	ourdinated									
viaximum v/c Ratio: 0.63	17.0				atoro o oti -					
Intersection Signal Delay	. 17.U			li V		ILUS: B				
intersection Capacity Util	ization 04.1%			10	CO LEVEI	OI SELVICE	30			

≠ø2 (R)	≪¶ _{Ø4}						
57 s		46 s					
<b>₩</b> Ø6		₽ Ø8					
57 s		46 s					

Synchro 10 Report

										ι.		,
	×	-	$\mathbf{r}$	1	-		1	T	1	-	Ŧ	*
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SB
Lane Configurations	<u>۲</u>	•	1	٦	ĥ		٦	4		٦	4	
Traffic Volume (vph)	62	380	86	38	304	9	66	141	37	13	86	2
Future Volume (vph)	62	380	86	38	304	9	66	141	37	13	86	2
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	190
Total Lost time (s)	7.0	7.0	7.0	7.0	7.0		6.0	6.0		6.0	6.0	
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00		1.00	1.00		1.00	1.00	
Frpb, ped/bikes	1.00	1.00	1.00	1.00	1.00		1.00	1.00		1.00	1.00	
Flpb, ped/bikes	1.00	1.00	1.00	1.00	1.00		1.00	1.00		1.00	1.00	
Frt	1.00	1.00	0.85	1.00	1.00		1.00	0.97		1.00	0.96	
Flt Protected	0.95	1.00	1.00	0.95	1.00		0.95	1.00		0.95	1.00	
Satd. Flow (prot)	1581	1810	1495	1752	1786		1612	1608		1671	1540	
Flt Permitted	0.56	1.00	1.00	0.51	1.00		0.68	1.00		0.50	1.00	
Satd. Flow (perm)	924	1810	1495	932	1786		1152	1608		877	1540	
Peak-hour factor, PHF	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.9
Adj. Flow (vph)	67	409	92	41	327	10	71	152	40	14	92	2
RTOR Reduction (vph)	0	0	16	0	1	0	0	12	0	0	14	
Lane Group Flow (vph)	67	409	76	41	336	0	71	180	0	14	106	
Confl. Peds. (#/hr)	1					1						
Heavy Vehicles (%)	14%	5%	8%	3%	6%	0%	12%	17%	5%	8%	16%	29
Turn Type	Perm	NA	Perm	Perm	NA		Perm	NA		Perm	NA	
Protected Phases		2			6			4			8	
Permitted Phases	2		2	6			4			8		
Actuated Green, G (s)	71.3	71.3	71.3	71.3	71.3		18.7	18.7		18.7	18.7	
Effective Green, g (s)	71.3	71.3	71.3	71.3	71.3		18.7	18.7		18.7	18.7	
Actuated g/C Ratio	0.69	0.69	0.69	0.69	0.69		0.18	0.18		0.18	0.18	
Clearance Time (s)	7.0	7.0	7.0	7.0	7.0		6.0	6.0		6.0	6.0	
Vehicle Extension (s)	5.0	5.0	5.0	5.0	5.0		5.0	5.0		5.0	5.0	
Lane Grp Cap (vph)	639	1252	1034	645	1236		209	291		159	279	
v/s Ratio Prot		c0.23			0.19			c0.11			0.07	
v/s Ratio Perm	0.07		0.05	0.04			0.06			0.02		
v/c Ratio	0.10	0.33	0.07	0.06	0.27		0.34	0.62		0.09	0.38	
Uniform Delay, d1	5.3	6.3	5.1	5.1	6.0		36.8	38.9		35.1	37.1	
Progression Factor	1.00	1.00	1.00	1.00	1.00		1.00	1.00		1.00	1.00	
Incremental Delay, d2	0.3	0.7	0.1	0.2	0.5		2.0	5.5		0.5	1.8	
Delay (s)	5.6	7.0	5.3	5.3	6.6		38.8	44.4		35.6	38.9	
Level of Service	A	A	A	A	A		D	D		D	D	
Approach Delay (s)		6.6			6.4			42.9			38.5	
Approach LOS		А			А			D			D	
Intersection Summary												
HCM 2000 Control Delay			16.8	н	CM 2000	l evel of 9	Service		B			
HCM 2000 Volume to Canac	ity ratio		0.30	10	2000	20101010	501 1100		U			
Actuated Cycle Length (c)	ity ratio		103.0	C,	im of lost	time (s)			13.0			
Intersection Canacity I Itilizat	ion		64.1%	10		of Service			13.0			
Analysis Period (min)			15	10	C LOVEL				0			
			10									

Uppers Quarry Traffic Impact Study TMIG

HCM Unsignalized Intersection Capacity Analysis	
6 [.] Thorold Townline Road & Beaverdams Road	

	≯	-	$\mathbf{F}$	∢	←	•	•	Ť	۲	1	ŧ	4
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		\$			\$			\$			\$	
Sign Control		Stop			Stop			Stop			Stop	
Traffic Volume (vph)	14	115	16	8	167	22	24	175	5	11	104	17
Future Volume (vph)	14	115	16	8	167	22	24	175	5	11	104	17
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Hourly flow rate (vph)	15	125	17	9	182	24	26	190	5	12	113	18
Direction, Lane #	EB 1	WB 1	NB 1	SB 1								
Volume Total (vph)	157	215	221	143								
Volume Left (vph)	15	9	26	12								
Volume Right (vph)	17	24	5	18								
Hadj (s)	0.01	-0.04	0.27	0.26								
Departure Headway (s)	5.3	5.1	5.4	5.5								
Degree Utilization, x	0.23	0.31	0.33	0.22								
Capacity (veh/h)	625	650	623	597								
Control Delay (s)	9.8	10.4	11.1	10.1								
Approach Delay (s)	9.8	10.4	11.1	10.1								
Approach LOS	А	В	В	В								
Intersection Summary												
Delay			10.4									
Level of Service			В									
Intersection Capacity Utilization	n		35.3%	IC	U Level o	of Service			А			
Analysis Period (min)			15									

HCM Unsignalized Intersection Capacity Analysis 7: Thorold Townline Road & Uppers Lane

<2018 Existing> AM Peak Hour 09-14-2021

	4	•	Ť	1	1	ţ
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations	Y		ţ,			<del>د</del> ا
Traffic Volume (veh/h)	1	0	211	1	0	124
Future Volume (Veh/h)	1	0	211	1	0	124
Sign Control	Stop		Free			Free
Grade	0%		0%			0%
Peak Hour Factor	0.93	0.93	0.93	0.93	0.93	0.93
Hourly flow rate (vph)	1	0	227	1	0	133
Pedestrians						
Lane Width (m)						
Walking Speed (m/s)						
Percent Blockage						
Right turn flare (veh)						
Median type			None			None
Median storage veh)						
Upstream signal (m)						
pX_platoon unblocked						
vC. conflicting volume	360	228			228	
vC1, stage 1 conf vol						
vC2, stage 2 conf vol						
vCu, unblocked vol	360	228			228	
tC single (s)	6.4	6.2			4 1	
tC 2 stage (s)						
tF (s)	3.5	3.3			2.2	
p0 queue free %	100	100			100	
cM capacity (veh/h)	642	817			1352	
			07.4			
Direction, Lane #	WB 1	NB 1	SB 1			
Volume Total	1	228	133			
Volume Left	1	0	0			
Volume Right	0	1	0			
cSH	642	1700	1352			
Volume to Capacity	0.00	0.13	0.00			
Queue Length 95th (m)	0.0	0.0	0.0			
Control Delay (s)	10.6	0.0	0.0			
Lane LOS	В					
Approach Delay (s)	10.6	0.0	0.0			
Approach LOS	В					
Intersection Summary						
Average Delay			0.0			
Intersection Canacity Utiliz	zation		21.2%	IC	Ulevelo	of Service
Analysis Period (min)			15			

Uppers Quarry Traffic Impact Study TMIG

Synchro 10 Report

Uppers Quarry Traffic Impact Study TMIG

Timings 1: Davis Road & Th	norold S	Stone F	Road		<2018 Existing> PM Peak Hou 09-14-202							
	۶	-	$\mathbf{\hat{z}}$	4	+	•	Ť	1	1	ţ	4	
Lane Group	EBL	EBT	EBR	WBL	WBT	NBL	NBT	NBR	SBL	SBT	SBR	
Lane Configurations	ሻ		1	ሻ	A	ሻ	ę	1	٦	<b>↑</b>	1	
Traffic Volume (vph)	24	1209	427	78	1108	412	5	86	4	6	28	
Future Volume (vph)	24	1209	427	78	1108	412	5	86	4	6	28	
Turn Type	Perm	NA	Perm	Perm	NA	Split	NA	Perm	Split	NA	Perm	
Protected Phases		2			6	4	4		8	8		
Permitted Phases	2		2	6				4			8	
Detector Phase	2	2	2	6	6	4	4	4	8	8	8	
Switch Phase												
Minimum Initial (s)	20.0	20.0	20.0	20.0	20.0	10.0	10.0	10.0	10.0	10.0	10.0	
Minimum Split (s)	28.9	28.9	28.9	28.9	28.9	29.7	29.7	29.7	21.7	21.7	21.7	
Total Split (s)	39.7	39.7	39.7	39.7	39.7	45.4	45.4	45.4	21.9	21.9	21.9	
Total Split (%)	37.1%	37.1%	37.1%	37.1%	37.1%	42.4%	42.4%	42.4%	20.5%	20.5%	20.5%	
Yellow Time (s)	5.4	5.4	5.4	5.4	5.4	5.7	5.7	5.7	5.7	5.7	5.7	
All-Red Time (s)	1.5	1.5	1.5	1.5	1.5	2.0	2.0	2.0	2.0	2.0	2.0	
Lost Time Adjust (s)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Total Lost Time (s)	6.9	6.9	6.9	6.9	6.9	7.7	7.7	7.7	7.7	7.7	7.7	
Lead/Lag												
Lead-Lag Optimize?												
Recall Mode	C-Max	C-Max	C-Max	Max	Max	None	None	None	None	None	None	
Act Effct Green (s)	60.3	60.3	60.3	60.3	60.3	21.5	21.5	21.5	10.0	10.0	10.0	
Actuated g/C Ratio	0.56	0.56	0.56	0.56	0.56	0.20	0.20	0.20	0.09	0.09	0.09	
v/c Ratio	0.18	0.64	0.46	0.63	0.59	0.66	0.65	0.23	0.02	0.04	0.12	
Control Delay	22.1	21.0	9.9	48.7	19.8	48.0	47.6	4.3	44.5	44.8	0.9	
Queue Delay	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Total Delay	22.1	21.0	9.9	48.7	19.8	48.0	47.6	4.3	44.5	44.8	0.9	
LOS	С	С	Α	D	В	D	D	Α	D	D	Α	
Approach Delay		18.2			21.7		40.3			12.2		
Approach LOS		В			С		D			В		
Intersection Summary												
Cycle Length: 107												
Actuated Cycle Length: 107												
Offset: 0 (0%), Referenced t	to phase 2	EBTL, St	art of Gre	en								
Natural Cycle: 105												
Control Type: Actuated-Coo	rdinated											
Maximum v/c Ratio: 0.66												
Intersection Signal Delay: 22	2.6			Ir	ntersectio	n LOS: C						
Intersection Capacity Utiliza	tion 86.2%			IC	CU Level	of Service	ε					
Analysis Period (min) 15												

Splits and Phases: 1: Davis Road & Thorold Stone Road

Ø2 (R)	<b>★</b> Ø4	<b>↓</b> _{Ø8}
39.7 s	45.4 s	21.9 s
₹ø6		
39.7 s		

Uppers Quarry Traffic Impact Study TMIG

Synchro 10 Report

HCM Signalized Intersection Capacity Analysis 1: Davis Road & Thorold Stone Road <2018 Existing> PM Peak Hour _____09-14-2021

	٦	-	$\mathbf{F}$	4	+	×	٠	Ť	۲	1	Ŧ	~
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	۲.	<b>^</b>	1	۲	<b>≜1</b> ≱		۲	ર્શ	1	۲	•	1
Traffic Volume (vph)	24	1209	427	78	1108	1	412	5	86	4	6	28
Future Volume (vph)	24	1209	427	78	1108	1	412	5	86	4	6	28
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Total Lost time (s)	6.9	6.9	6.9	6.9	6.9		7.7	7.7	7.7	7.7	7.7	7.7
Lane Util. Factor	1.00	0.95	1.00	1.00	0.95		0.95	0.95	1.00	1.00	1.00	1.00
Frpb, ped/bikes	1.00	1.00	1.00	1.00	1.00		1.00	1.00	1.00	1.00	1.00	0.99
Flpb, ped/bikes	1.00	1.00	1.00	1.00	1.00		1.00	1.00	1.00	1.00	1.00	1.00
Frt	1.00	1.00	0.85	1.00	1.00		1.00	1.00	0.85	1.00	1.00	0.85
Fit Protected	0.95	1.00	1.00	0.95	1.00		0.95	0.95	1.00	0.95	1.00	1.00
Satd. Flow (prot)	1433	3539	1568	1671	3539		1681	1677	1482	1805	1810	1531
Flt Permitted	0.16	1.00	1.00	0.13	1.00		0.95	0.95	1.00	0.95	1.00	1.00
Satd. Flow (perm)	245	3539	1568	232	3539		1681	1677	1482	1805	1810	1531
Peak-hour factor, PHF	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95
Adj. Flow (vph)	25	1273	449	82	1166	1	434	5	91	4	6	29
RTOR Reduction (vph)	0	0	110	0	0	0	0	0	73	0	0	27
Lane Group Flow (vph)	25	1273	339	82	1167	0	221	218	18	4	6	2
Confl. Peds. (#/hr)							1					1
Heavy Vehicles (%)	26%	2%	3%	8%	2%	0%	2%	30%	9%	0%	5%	4%
Turn Type	Perm	NA	Perm	Perm	NA		Split	NA	Perm	Split	NA	Perm
Protected Phases		2			6		.4	4		. 8	8	
Permitted Phases	2		2	6					4			8
Actuated Green, G (s)	57.2	57.2	57.2	57.2	57.2		21.5	21.5	21.5	6.0	6.0	6.0
Effective Green, g (s)	57.2	57.2	57.2	57.2	57.2		21.5	21.5	21.5	6.0	6.0	6.0
Actuated g/C Ratio	0.53	0.53	0.53	0.53	0.53		0.20	0.20	0.20	0.06	0.06	0.06
Clearance Time (s)	6.9	6.9	6.9	6.9	6.9		7.7	7.7	7.7	7.7	7.7	7.7
Vehicle Extension (s)	3.0	3.0	3.0	3.0	3.0		4.5	4.5	4.5	4.5	4.5	4.5
Lane Grp Cap (vph)	130	1891	838	124	1891		337	336	297	101	101	85
v/s Ratio Prot		c0.36			0.33		c0.13	0.13		0.00	c0.00	
v/s Ratio Perm	0.10		0.22	0.35					0.01			0.00
v/c Ratio	0.19	0.67	0.40	0.66	0.62		0.66	0.65	0.06	0.04	0.06	0.02
Uniform Delay, d1	12.9	18.1	14.8	17.9	17.3		39.3	39.3	34.6	47.8	47.8	47.7
Progression Factor	1.00	1.00	1.00	1.00	1.00		1.00	1.00	1.00	1.00	1.00	1.00
Incremental Delay, d2	3.3	1.9	1.5	24.4	1.5		5.5	5.2	0.2	0.3	0.4	0.2
Delay (s)	16.2	20.0	16.2	42.4	18.8		44.8	44.5	34.7	48.1	48.3	47.9
Level of Service	В	С	В	D	В		D	D	С	D	D	D
Approach Delay (s)		19.0			20.4			43.0			48.0	
Approach LOS		В			С			D			D	
Intersection Summary												
HCM 2000 Control Delay			23.4	Н	CM 2000	Level of S	Service		С			
HCM 2000 Volume to Capa	city ratio		0.62									
Actuated Cycle Length (s)			107.0	S	um of lost	time (s)			22.3			
Intersection Capacity Utiliza	ation		86.2%	IC	CU Level o	of Service			E			
Analysis Period (min)			15									

c Critical Lane Group

Uppers Quarry Traffic Impact Study TMIG

									,	
	٠	-	1	-	1	T.	1	÷	-	
Lane Group	EBL	EBT	WBL	WBT	NBL	NBT	SBL	SBT	SBR	
Lane Configurations		4		4	ሻ	<b>↑</b> Ъ	ሻ	- <b>†</b> †	1	
Traffic Volume (vph)	90	32	42	44	5	275	170	244	105	
Future Volume (vph)	90	32	42	44	5	275	170	244	105	
Turn Type	Perm	NA	Perm	NA	Perm	NA	Perm	NA	Perm	
Protected Phases		2		6		4		8		
Permitted Phases	2		6		4		8		8	
Detector Phase	2	2	6	6	4	4	8	8	8	
Switch Phase										
Minimum Initial (s)	10.0	10.0	10.0	10.0	25.0	25.0	25.0	25.0	25.0	
Vinimum Split (s)	38.1	38.1	38.1	38.1	32.0	32.0	32.0	32.0	32.0	
Total Split (s)	43.1	43.1	43.1	43.1	52.0	52.0	52.0	52.0	52.0	
Total Split (%)	45.3%	45.3%	45.3%	45.3%	54.7%	54.7%	54.7%	54.7%	54.7%	
Yellow Time (s)	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	
All-Red Time (s)	3.1	3.1	3.1	3.1	2.0	2.0	2.0	2.0	2.0	
ost Time Adjust (s)		0.0		0.0	0.0	0.0	0.0	0.0	0.0	
Total Lost Time (s)		8.1		8.1	7.0	7.0	7.0	7.0	7.0	
_ead/Lag										
ead-Lag Optimize?										
Recall Mode	C-Max	C-Max	Max	Max	None	None	None	None	None	
Act Effct Green (s)		51.9		51.9	28.1	28.1	28.1	28.1	28.1	
Actuated g/C Ratio		0.55		0.55	0.30	0.30	0.30	0.30	0.30	
//c Ratio		0.20		0.27	0.02	0.33	0.58	0.26	0.20	
Control Delay		13.1		8.2	20.8	24.9	36.1	25.5	5.1	
Queue Delay		0.0		0.0	0.0	0.0	0.0	0.0	0.0	
Total Delay		13.1		8.2	20.8	24.9	36.1	25.5	5.1	
_OS		В		А	С	С	D	С	А	
Approach Delay		13.1		8.2		24.8		24.8		
Approach LOS		В		А		С		С		
Intersection Summary										
Cycle Length: 95.1										
Actuated Cycle Length: 95	5.1									
Offset: 0 (0%), Reference	d to phase 2	EBTL, St	art of Gre	en						
Vatural Cycle: 75										
Control Type: Actuated-Co	pordinated									
Maximum v/c Ratio: 0.58										
ntersection Signal Delay:	20.3			I	ntersectio	n LOS: C				
Intersection Capacity Utiliz	zation 81.2%			10	CU Level	of Service	e D			

43.1s	52 s	
₹ø6	\$ Ø8	
43.15	52 s	

Synchro 10 Report

HCM Signalized Intersection Capacity Analysis 2: Davis Road & Niagara Falls Road/Beaverdams Road <2018 Existing> PM Peak Hour 09-14-2021

	۶	-	$\mathbf{r}$	1	-	•	1	Ť	1	1	Ŧ	-
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		4			4		٦	¢β		<u> </u>	<b>^</b>	1
Traffic Volume (vph)	90	32	4	42	44	147	5	275	31	170	244	105
Future Volume (vph)	90	32	4	42	44	147	5	275	31	170	244	105
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Total Lost time (s)		8.1			8.1		7.0	7.0		7.0	7.0	7.0
Lane Util. Factor		1.00			1.00		1.00	0.95		1.00	0.95	1.00
Frt		1.00			0.91		1.00	0.98		1.00	1.00	0.85
Flt Protected		0.97			0.99		0.95	1.00		0.95	1.00	1.00
Satd. Flow (prot)		1777			1692		1805	3301		1770	3343	1583
Flt Permitted		0.66			0.93		0.59	1.00		0.56	1.00	1.00
Satd. Flow (perm)		1221			1582		1126	3301		1037	3343	1583
Peak-hour factor, PHF	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95
Adj. Flow (vph)	95	34	4	44	46	155	5	289	33	179	257	111
RTOR Reduction (vph)	0	1	0	0	47	0	0	12	0	0	0	78
Lane Group Flow (vph)	0	132	0	0	198	0	5	310	0	179	257	33
Heavy Vehicles (%)	2%	2%	30%	2%	1%	2%	0%	8%	5%	2%	8%	2%
	Perm	NA		Perm	NA		Perm	NA		Perm	NA	Perm
Protected Phases		2			6			4			8	
Permitted Phases	2			6			4			8	-	8
Actuated Green, G (s)		51.9			51.9		28.1	28.1		28.1	28.1	28.1
Effective Green, g (s)		51.9			51.9		28.1	28.1		28.1	28.1	28.1
Actuated g/C Ratio		0.55			0.55		0.30	0.30		0.30	0.30	0.30
Clearance Time (s)		8.1			8.1		7.0	7.0		7.0	7.0	7.0
Vehicle Extension (s)		3.0			3.0		5.0	5.0		5.0	5.0	5.0
Lane Grp Cap (vph)		666			863		332	975		306	987	467
v/s Ratio Prot								0.09			0.08	
v/s Ratio Perm		0.11			c0.13		0.00			c0.17		0.02
v/c Ratio		0.20			0.23		0.02	0.32		0.58	0.26	0.07
Uniform Delay, d1		11.0			11.2		23.7	26.0		28.5	25.6	24.1
Progression Factor		1.00			1.00		1.00	1.00		1.00	1.00	1.00
Incremental Delay, d2		0.7			0.6		0.0	0.4		4.4	0.3	0.1
Delay (s)		11.7			11.8		23.7	26.4		32.9	25.9	24.2
Level of Service		В			В		C	C		C	C	C
Approach Delay (s)		11.7			11.8			26.4			27.8	
Approach LOS		В			В			С			С	
Intersection Summary												
HCM 2000 Control Delay			22.6	Н	CM 2000	Level of	Service		С			
HCM 2000 Volume to Capacit	ty ratio		0.35									
Actuated Cycle Length (s)			95.1	S	um of lost	time (s)			15.1			
Intersection Capacity Utilization	on		81.2%	IC	CU Level o	of Service			D			
Analysis Period (min)			15									
c Critical Lane Group												

Uppers Quarry Traffic Impact Study TMIG

ane Group ane Configurations fraffic Volume (vph) uture Volume (vph) fum Type Protected Phases Permitted Phases Detector Phase witch Phase Minimum Initial (s)	EBL     105     105     Perm     2     2     2     2     2     2     2	EBT \$ 464 464 NA 2 2	WBL VBL 24 24 24 Perm	WBT 452 452 NA	WBR 7 59 59	NBL	↑ NBT	SBL	↓ SBT	<b>↓</b> SBR	
ane Group ane Configurations Traffic Volume (vph) ¹ uture Volume (vph) ¹ rotected Phases ² rotected Phases ² remited Phases Detector Phase Minimum Initial (s)	EBL 105 105 Perm 2 2	EBT 464 464 NA 2	WBL 24 24 Perm	WBT 452 452 NA	WBR 59 59	NBL	NBT	SBL	SBT	SBR	
ane Configurations fraffic Volume (vph) Future Volume (vph) ium Type Protected Phases Parmited Phases Detector Phase Minimum Initial (s)	105 105 Perm 2 2	464 464 NA 2	24 24 Perm	452 452 NA	7 59 59	1	<b>1</b> .				
Fraffic Volume (vph) Luture Volume (vph) Furn Type Protected Phases Permitted Phases Detector Phase Witch Phase Minimum Initial (s)	105 105 Perm 2 2	464 464 NA 2	24 24 Perm	452 452 NA	59 59	16	17	<u>່</u>	<b>↑</b>	1	
Future Volume (vph) furn Type Protected Phases Permitted Phases Detector Phase Switch Phase Minimum Initial (s)	105 Perm 2 2	464 NA 2	24 Perm	452 NA	59	40	134	74	122	113	
Furn Type Protected Phases Permitted Phases Detector Phase Witch Phase Jinimum Initial (s)	Perm 2 2 2	NA 2 2	Perm	NA		46	134	74	122	113	
Protected Phases Permitted Phases Detector Phase Switch Phase Ainimum Initial (s)	2 2	2	a		Perm	Perm	NA	Perm	NA	Perm	
Permitted Phases Detector Phase Switch Phase Minimum Initial (s)	2	2	6	6			4		8		
Detector Phase Switch Phase Ainimum Initial (s)	2	2	0		6	4		8		8	
Switch Phase Minimum Initial (s)	22.0	2	6	6	6	4	4	8	8	8	
Ainimum Initial (s)	22.0										
r : 0 m ( )	22.0	22.0	22.0	22.0	22.0	15.0	15.0	15.0	15.0	15.0	
Vinimum Split (s)	36.0	36.0	36.0	36.0	36.0	32.0	32.0	32.0	32.0	32.0	
Total Split (s)	52.0	52.0	52.0	52.0	52.0	42.0	42.0	42.0	42.0	42.0	
otal Split (%)	55.3%	55.3%	55.3%	55.3%	55.3%	44.7%	44.7%	44.7%	44.7%	44.7%	
(ellow Time (s)	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	
All-Red Time (s)	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	
ost Time Adjust (s)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Total Lost Time (s)	7.0	7.0	7.0	7.0	7.0	7.0	7.0	7.0	7.0	7.0	
ead/Lag											
ead-Lag Optimize?											
Recall Mode	C-Max	C-Max	Max	Max	Max	Max	Max	Max	Max	Max	
Act Effet Green (s)	45.0	45.0	45.0	45.0	45.0	35.0	35.0	35.0	35.0	35.0	
Actuated g/C Ratio	0.48	0.48	0.48	0.48	0.48	0.37	0.37	0.37	0.37	0.37	
Ic Ratio	0.40	0.40	0.40	0.55	0.40	0.01	0.37	0.07	0.07	0.07	
Control Delay	19.6	21.7	14.8	20.2	4.0	20.2	20.4	21.4	21.1	4.6	
	0.0	0.0	0.0	0.0	0.0	0.0	20.4	0.0	0.0	0.0	
Intal Delay	19.6	21.7	14.8	20.2	4.0	20.2	20.4	21.4	21.1	4.6	
	13.0 D	21.7	14.0 P	20.2	4.U	20.2	20.4	21.4	21.1	4.0	
John Dolov	D	21.2	D	10 1	A	U U	20.4	U	15.4	А	
Approach LOS		21.3		10.1			20.4		10.1		
uppidacii LUS		U		В			U		В		
ntersection Summary											
Cycle Length: 94											
Actuated Cycle Length: 94											
Offset: 0 (0%), Referenced	to phase 2:	EBTL, St	art of Gre	en							
Vatural Cycle: 70											
Control Type: Actuated-Co	ordinated										
Aaximum v/c Ratio: 0.61											
ntersection Signal Delay: 1	19.0			Ir	ntersectio	n LOS: B					
ntersection Capacity Utilization	ation 101.19	%		IC	CU Level	of Service	G				
Analysis Period (min) 15											
Solits and Phases: 3. Da	ivis Road &	Lundvs I	ane								
						4					

→ø2 (R)	Ø4	
52 s	42.5	
₹ Ø6	↓ øs	
50 -	40.0	

Synchro 10 Report

## HCM Signalized Intersection Capacity Analysis 3: Davis Road & Lundys Lane

<2018 Existing> PM Peak Hour 09-14-2021

	٦	-	$\mathbf{\hat{z}}$	4	+	×	1	t	۲	1	Ŧ	~
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	5	4Î		٦	<b>†</b>	1	۲	ĥ		<u> </u>	1	1
Traffic Volume (vph)	105	464	28	24	452	59	46	134	30	74	122	113
Future Volume (vph)	105	464	28	24	452	59	46	134	30	74	122	113
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Total Lost time (s)	7.0	7.0		7.0	7.0	7.0	7.0	7.0		7.0	7.0	7.0
Lane Util. Factor	1.00	1.00		1.00	1.00	1.00	1.00	1.00		1.00	1.00	1.00
Frpb, ped/bikes	1.00	1.00		1.00	1.00	0.98	1.00	1.00		1.00	1.00	1.00
Flpb, ped/bikes	1.00	1.00		1.00	1.00	1.00	1.00	1.00		1.00	1.00	1.00
Frt	1.00	0.99		1.00	1.00	0.85	1.00	0.97		1.00	1.00	0.85
Flt Protected	0.95	1.00		0.95	1.00	1.00	0.95	1.00		0.95	1.00	1.00
Satd. Flow (prot)	1717	1804		1611	1863	1474	1736	1680		1700	1743	1553
Flt Permitted	0.37	1.00		0.33	1.00	1.00	0.67	1.00		0.65	1.00	1.00
Satd. Flow (perm)	662	1804		557	1863	1474	1230	1680		1156	1743	1553
Peak-hour factor, PHF	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93
Adj. Flow (vph)	113	499	30	26	486	63	49	144	32	80	131	122
RTOR Reduction (vph)	0	2	0	0	0	33	0	9	0	0	0	77
Lane Group Flow (vph)	113	527	0	26	486	30	49	167	0	80	131	45
Confl. Peds. (#/hr)	2		1	1		2			1	1		
Heavy Vehicles (%)	5%	3%	26%	12%	2%	7%	4%	9%	12%	6%	9%	4%
Turn Type	Perm	NA		Perm	NA	Perm	Perm	NA		Perm	NA	Perm
Protected Phases		2			6			4			8	
Permitted Phases	2			6		6	4			8		8
Actuated Green, G (s)	45.0	45.0		45.0	45.0	45.0	35.0	35.0		35.0	35.0	35.0
Effective Green, g (s)	45.0	45.0		45.0	45.0	45.0	35.0	35.0		35.0	35.0	35.0
Actuated g/C Ratio	0.48	0.48		0.48	0.48	0.48	0.37	0.37		0.37	0.37	0.37
Clearance Time (s)	7.0	7.0		7.0	7.0	7.0	7.0	7.0		7.0	7.0	7.0
Vehicle Extension (s)	4.0	4.0		4.0	4.0	4.0	2.0	2.0		2.0	2.0	2.0
Lane Grp Cap (vph)	316	863		266	891	705	457	625		430	648	578
v/s Ratio Prot		c0.29			0.26			c0.10			0.08	
v/s Ratio Perm	0.17			0.05		0.02	0.04			0.07		0.03
v/c Ratio	0.36	0.61		0.10	0.55	0.04	0.11	0.27		0.19	0.20	0.08
Uniform Delay, d1	15.4	18.0		13.4	17.3	13.0	19.3	20.6		19.9	20.0	19.1
Progression Factor	1.00	1.00		1.00	1.00	1.00	1.00	1.00		1.00	1.00	1.00
Incremental Delay, d2	3.1	3.2		0.7	2.4	0.1	0.5	1.0		1.0	0.7	0.3
Delay (s)	18.5	21.3		14.1	19.7	13.2	19.8	21.6		20.8	20.7	19.3
Level of Service	В	С		В	В	В	В	С		С	С	В
Approach Delay (s)		20.8			18.7			21.2			20.2	
Approach LOS		С			В			С			С	
Intersection Summary												
HCM 2000 Control Delay			20.1	Н	CM 2000	Level of	Service		С			
HCM 2000 Volume to Capa	acity ratio		0.46									
Actuated Cycle Length (s)			94.0	S	um of losi	t time (s)			14.0			
Intersection Capacity Utiliza	ation		101.1%	IC	U Level	of Service	)		G			
Analysis Period (min)			15									

c Critical Lane Group

Uppers Quarry Traffic Impact Study TMIG

Lane Group         EBL         EBT         EBR         WBL         WBT         WBR         NBL         NBT         SBL         SBT           Lane Configurations         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1												
Lane Group         EBL         EBT         EBR         WBL         WBT         WBL         NBT         SBL         SBT           Lane Configurations         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1<		≯	-	$\rightarrow$	4	-	•	1	<b>†</b> _	1	Ŧ	
ane Configurations       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1	ane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	SBL	SBT	
Traffic Volume (vph) 231 1036 32 30 821 35 69 83 48 138 Future Volume (vph) 231 1036 32 30 821 35 69 83 48 138 Future Volume (vph) 231 1036 32 30 821 35 69 83 48 138 Turn Type pm-pt NA Perm Perm NA Perm NA Perm NA Protected Phases 5 2 6 6 4 8 Parmitted Phases 2 2 2 6 6 6 4 8 Switch Phase 5 2 2 6 6 6 4 4 8 Switch Phase 5 2 2 6 6 6 4 4 8 Switch Phase 5 2 2 6 6 6 4 4 8 Switch Phase 5 2 2 6 6 6 4 4 4 8 Switch Phase 5 2 2 6 6 6 4 4 4 8 Switch Phase 5 2 2 6 6 6 4 4 4 8 Switch Phase 5 2 2 6 6 6 4 4 4 8 Switch Phase 5 2 2 6 6 6 4 4 4 8 Switch Phase 5 2 2 6 6 6 4 4 4 8 Switch Phase 5 2 2 6 6 6 4 4 4 8 Switch Phase 5 2 2 6 6 6 4 4 4 8 Switch Phase 5 2 2 2 6 6 6 6 4 4 4 8 Switch Phase 5 2 2 2 6 6 6 6 4 4 4 8 Switch Phase 5 2 2 2 6 8 6 8 3 48 138 Switch Phase 5 2 2 2 6 6 6 6 4 4 4 8 Switch Phase 5 2 2 2 6 6 6 4 4 4 8 Switch Phase 5 2 2 2 6 6 6 4 4 4 8 Switch Phase 5 2 2 2 6 6 6 6 4 4 4 14 414 Total Split (s) 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.	ane Configurations	ሻ	- <b>†</b> †	1	ሻ		1	<u>۲</u>	1+	<u>۳</u>	1	
Future Volume (vph)       231       1036       32       30       821       35       69       83       48       138         funn Type       pm+pt       NA       Perm       Perm       NA       Perm       NA       Perm       Perm       NA       Perm	Traffic Volume (vph)	231	1036	32	30	821	35	69	83	48	138	
Turn Type         pm+pt         NA         Perm         Perm         NA         Perm         NA         Perm         Perm         NA         Perm         Perm         Perm         Permited Traine for the term in term in the term in term	Future Volume (vph)	231	1036	32	30	821	35	69	83	48	138	
Protected Phases         5         2         6         4         8           Permitted Phases         2         2         6         6         4         8           Detector Phase         5         2         2         6         6         4         8           Winimum Initial (s)         8.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0	Furn Type	pm+pt	NA	Perm	Perm	NA	Perm	Perm	NA	Perm	NA	
Deremitted Phases         2         2         6         6         4         8           Detector Phase         5         2         2         6         6         4         4         8         8           Switch Phase         Minimum Initial (s)         8.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0<	Protected Phases	5	2			6			4		8	
Detector Phase         5         2         2         6         6         6         4         4         8         8           Switch Phase         Simital (s)         8.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0 <td>Permitted Phases</td> <td>2</td> <td></td> <td>2</td> <td>6</td> <td></td> <td>6</td> <td>4</td> <td></td> <td>8</td> <td></td> <td></td>	Permitted Phases	2		2	6		6	4		8		
Switch Phase         Image of the transmission of transmission of the transmission of transmissin transmission of transmissinteriments of transmis	Detector Phase	5	2	2	6	6	6	4	4	8	8	
Minimum Initial (s)       8.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       1	Switch Phase		-	-	, in the second s							
Main Mark 14, 1         Main	Minimum Initial (s)	8.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	
Total Split (s)       23.0       73.1       73.1       50.1       50.1       50.1       50.1       41.4       41.4       41.4       41.4         Total Split (%)       20.1%       63.8%       63.8%       43.8%       43.8%       36.2%       36.2%       36.2%       36.2%       36.2%       36.2%       36.2%       36.2%       36.2%       36.2%       36.2%       36.2%       36.2%       36.2%       36.2%       36.2%       36.2%       36.2%       36.2%       36.2%       36.2%       36.2%       36.2%       36.2%       36.2%       36.2%       36.2%       36.2%       36.2%       36.2%       36.2%       36.2%       36.2%       36.2%       36.2%       36.2%       36.2%       36.2%       36.2%       36.2%       36.2%       36.2%       36.2%       36.2%       36.2%       36.2%       36.2%       36.2%       36.2%       36.2%       36.2%       36.2%       36.2%       36.2%       36.2%       36.2%       36.2%       36.2%       36.2%       36.2%       36.2%       36.2%       36.2%       36.2%       36.2%       36.2%       36.2%       36.2%       36.2%       36.2%       36.2%       36.2%       36.2%       36.2%       36.2%       36.2%       36.2%	Minimum Split (s)	11.0	35.1	35.1	35.1	35.1	35.1	41.4	41.4	41.4	41.4	
Dear Spin (y)       20.0       63.8%       63.8%       63.8%       43.8%       43.8%       36.2%       36.2%       36.2%         fellow Time (s)       3.0       4.1       4.1       4.1       4.1       4.1       4.1       4.1       4.1       4.1       4.1       4.1       4.1       4.1       4.1       4.1       4.1       4.1       4.1       4.1       4.1       4.1       4.1       4.1       4.1       4.1       4.1       4.1       4.1       4.1       4.1       4.1       4.1       4.1       4.1       4.1       4.1       4.1       4.1       4.1       4.1       4.1       4.1       4.1       4.1       4.1       4.1       4.1       4.1       4.1       4.1       4.1       4.1       4.1       4.1       4.1       4.1       4.1       4.1       4.1       4.1       4.1       4.1       4.1       4.1       4.1       4.1       4.1       4.1       4.1       4.1       4.1       4.1       4.1       4.1       4.1       4.1       4.1       4.1       4.1       4.1       4.1       4.1       4.1       4.1       4.1       4.1       4.1       4.1       4.1       4.1       4.1	Fotal Split (s)	23.0	73.1	73.1	50.1	50.1	50.1	41.4	41.4	41.4	41.4	
Call Delta (S)       Coloration (S)       No.57       Q.2       Q	Fotal Split (%)	20.1%	63.8%	63.8%	43.8%	43.8%	43.8%	36.2%	36.2%	36.2%	36.2%	
Church Linte (v)         O.0         T.1         T.1 <tht.1< th="">         T.1         <tht.1< th=""></tht.1<></tht.1<>	Yellow Time (s)	3.0	Δ 1	Δ 1	Δ 1	Δ 1	<u>4</u> 1	<u>4</u> 1	Δ 1	Δ 1	4 1	
Name         None         Z.0         Z.0 <thz.0< t<="" td=""><td>All Red Time (a)</td><td>0.0</td><td>2.0</td><td>2.0</td><td>2.0</td><td>2.0</td><td>2.0</td><td>2.1</td><td>2.1</td><td>2.1</td><td>2.1</td><td></td></thz.0<>	All Red Time (a)	0.0	2.0	2.0	2.0	2.0	2.0	2.1	2.1	2.1	2.1	
Lost nime Adjust (s)       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0	act Time Adjust (s)	0.0	2.0	2.0	2.0	2.0	2.0	2.5	2.5	2.5	2.5	
Utail Explore         Usan Dial         D.1         D.1 <thd.1< th="">         D.1         D.1</thd.1<>	Lost Time Aujust (s)	2.0	6.1	6.1	6.1	6.1	6.1	6.4	6.4	6.4	6.4	
Lead Lag         Lag <thlag< th="">         Lag         <thlag< th=""> <thlag< <="" td=""><td>rotal Lost Time (S)</td><td>U.C</td><td>0.1</td><td>0.1</td><td>0.1</td><td>0.1</td><td>0.1</td><td>0.4</td><td>0.4</td><td>0.4</td><td>0.4</td><td></td></thlag<></thlag<></thlag<>	rotal Lost Time (S)	U.C	0.1	0.1	0.1	0.1	0.1	0.4	0.4	0.4	0.4	
Lead-Lag Opinitizer         Tes	ead Lag Optimize?	Leau			Lag	Lag	Lag					
Vector         Notife         C-Max         Los         Z         S         C         C         C         C         C         C         C         C         C         C         C         C         C         D         C         C         D         C         D         C         D         C         D         C         D         C         D         C         D <td>Leau-Lag Optimize?</td> <td>Nene</td> <td>C May</td> <td>C Max</td> <td>C Mex</td> <td>C Mex</td> <td>C Mex</td> <td>None</td> <td>None</td> <td>None</td> <td>Mana</td> <td></td>	Leau-Lag Optimize?	Nene	C May	C Max	C Mex	C Mex	C Mex	None	None	None	Mana	
Val Entr Green (s)       70.3       73.2       73.2       73.2       58.0       58.0       58.0       58.8       28.8       28.8       28.8       28.8       28.8       28.8       28.8       28.8       28.8       28.8       28.8       28.8       28.8       28.8       28.8       28.8       28.8       28.8       28.8       28.8       28.8       28.8       28.8       28.8       28.8       28.8       28.8       28.8       28.8       28.8       28.8       28.8       28.8       28.8       28.8       28.8       28.8       28.8       28.8       28.8       28.8       28.8       28.8       28.8       28.8       28.8       28.8       28.8       28.8       28.8       28.8       28.8       28.8       28.8       28.8       28.8       28.8       28.8       28.8       28.8       28.8       28.8       28.8       28.8       28.8       28.8       28.8       28.8       28.8       28.8       28.8       28.8       28.8       28.8       28.8       28.8       28.4       28.4       28.4       28.4       28.4       28.4       28.4       28.4       28.4       28.4       28.4       28.4       28.4       28.4       28.4       2		None	C-Max	C-IVIAX	C-Max	C-IVIAX	C-Max	None	None	None	None	
Actuate g/C Ratio 0.67 0.64 0.64 0.61 0.51 0.51 0.25 0.25 0.25 0.25 0.25 0.25 0.25 0.25	Act Effect Green (s)	/6.3	73.2	73.2	58.0	58.0	58.0	28.8	28.8	28.8	28.8	
Vic Ratio       0.57       0.47       0.03       0.13       0.48       0.04       1.04       0.26       0.17       0.90         Control Delay       14.1       12.3       3.6       21.1       21.3       2.1       162.2       30.1       32.3       54.1         Duceu Delay       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0	Actuated g/C Ratio	0.67	0.64	0.64	0.51	0.51	0.51	0.25	0.25	0.25	0.25	
Control Delay         14.1         12.3         3.6         21.1         21.3         2.1         162.2         30.1         32.3         54.1           Queue Delay         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0	//c Ratio	0.57	0.47	0.03	0.13	0.48	0.04	1.04	0.26	0.17	0.90	
Jueue Delay         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0 <th< td=""><td>Control Delay</td><td>14.1</td><td>12.3</td><td>3.6</td><td>21.1</td><td>21.3</td><td>2.1</td><td>162.2</td><td>30.1</td><td>32.3</td><td>54.1</td><td></td></th<>	Control Delay	14.1	12.3	3.6	21.1	21.3	2.1	162.2	30.1	32.3	54.1	
Total Delay         14.1         12.3         3.6         21.1         21.3         2.1         162.2         30.1         32.3         54.1           LOS         B         B         A         C         C         A         F         C         D           Approach Delay         12.4         20.5         82.1         51.8         S1.8	Queue Delay	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
LOS     B     B     A     C     C     A     F     C     D       Approach Delay     12.4     20.5     82.1     51.8       Approach LOS     B     C     F     D   Intersection Summary  Cycle Length: 114.5  Cycle Length: 114.5  Cycle Length: 114.5  Cycle: 90  Control Type: Actuated-Coordinated  Maximum v/c Ratio: 1.04 Intersection LOS: C Intersection LOS: C Intersection LOS: C Intersection Gaacity Utilization 90.1% ICU Level of Service E	Total Delay	14.1	12.3	3.6	21.1	21.3	2.1	162.2	30.1	32.3	54.1	
Approach Delay     12.4     20.5     82.1     51.8       Approach LOS     B     C     F     D   Intersection Summary       Dycle Length:     114.5   Valuated Cycle Length: 114.5 Offset: 0 (0%), Referenced to phase 2:EBTL and 6:WBTL, Start of Green Vatural Cycle: 90 Control Type: Actuated-Coordinated Valural V Ratio: 1.04 Intersection LOS: C Intersection Signal Delay: 25.7 Intersection LOS: C Intersection Signal Delay: 25.7 ICU Level of Service E	_OS	В	В	A	С	С	A	F	С	С	D	
Approach LOS     B     C     F     D       Intersection Summary     Cycle Length: 114.5     Cycle Length: 114.5     Cycle Length: 114.5       Offset: 0 (0%), Referenced to phase 2:EBTL and 6:WBTL, Start of Green     Vatural Cycle: 90     Vatural Cycle: 90       Control Type: Actuated-Coordinated     Vaximum v/c Ratio: 1.04     Vaximum v/c Ratio: 1.04       Intersection Signal Delay: 25.7     Intersection LOS: C     Intersection Cost of Service E	Approach Delay		12.4			20.5			82.1		51.8	
Intersection Summary         Cycle Length: 114.5         Schulated Cycle Length: 114.5         Offset: 0 (0%), Referenced to phase 2:EBTL and 6:WBTL, Start of Green         Jatural Cycle: 90         Sontrol Type: Actuated-Coordinated         Jaximum v/c Ratio: 1.04         Intersection Signal Delay: 25.7         Intersection LOS: C         Intersection Capacity Utilization 90.1%	Approach LOS		В			С			F		D	
Cycle Length: 114.5         Actuated Cycle Length: 114.5         Diffset: 0 (0%), Referenced to phase 2:EBTL and 6:WBTL, Start of Green         Vatural Cycle: 90         Control Type: Actuated-Coordinated         Vaximum v/c Ratio: 1.04         Intersection Signal Delay: 25.7         Intersection LOS: C         Intersection Capacity Utilization 90.1%	ntersection Summary											
Actuated Cycle Length: 114.5 Diffset: 0 (0%), Referenced to phase 2:EBTL and 6:WBTL, Start of Green Vatural Cycle: 90 Control Type: Actuated-Coordinated Maximum v/c Ratio: 1.04 ntersection Signal Delay: 25.7 Intersection LOS: C ntersection LOS: C Intersection Capacity Utilization 90.1% ICU Level of Service E	Cycle Length: 114.5											
Offset: 0 (0%), Referenced to phase 2:EBTL and 6:WBTL, Start of Green         Vatural Cycle: 90         Control Type: Actuated-Coordinated         Maximum v/c Ratio: 1.04         Intersection Signal Delay: 25.7         Intersection LOS: C         Intersection Capacity Utilization 90.1%	Actuated Cycle Length: 114	.5										
Vatural Cycle: 90 Control Type: Actuated-Coordinated Vaximum v/c Ratio: 1.04 Intersection Signal Delay: 25.7 Intersection LOS: C Intersection Capacity Utilization 90.1% ICU Level of Service E	Offset: 0 (0%), Referenced t	o phase 2:	EBTL an	d 6:WBTL	, Start of	Green						
Control Type: Actuated-Coordinated       Jaximum v/c Ratio: 1.04       Intersection Signal Delay: 25.7       Intersection LOS: C       Intersection Capacity Utilization 90.1%       ICU Level of Service E	Vatural Cycle: 90											
Idaximum     Vic Ratio: 1.04       Intersection Signal Delay: 25.7     Intersection LOS: C       Intersection Capacity Utilization 90.1%     ICU Level of Service E	Control Type: Actuated-Coo	rdinated										
ntersection Signal Delay: 25.7 Intersection LOS: C ntersection Capacity Utilization 90.1% ICU Level of Service E	/laximum v/c Ratio: 1.04											
ntersection Capacity Utilization 90.1% ICU Level of Service E	ntersection Signal Delay: 25	5.7			Ir	ntersectio	n LOS: C					
	ntersection Capacity Utiliza	tion 90.1%			10	CU Level	of Service	Ε				

		¶ø4	
73.1.s		41,4 s	
≯ _{øs}	💗 🗲 ø6 (R)	Ø8	
23 s	50.1 s	41.4 s	

Synchro 10 Report

HCM Signalized Intersection Capacity Analysis 4: Thorold Townline Road & Thorold Stone Road

<2018 Existing> PM Peak Hour 09-14-2021

	≯	+	$\mathbf{F}$	4	+	*	•	Ť	1	1	ŧ	~
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	ľ	<u></u>	1	٢	<u></u>	1	ľ	¢Î		٢	ę	
Traffic Volume (vph)	231	1036	32	30	821	35	69	83	24	48	138	272
Future Volume (vph)	231	1036	32	30	821	35	69	83	24	48	138	272
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Total Lost time (s)	3.0	6.1	6.1	6.1	6.1	6.1	6.4	6.4		6.4	6.4	
Lane Util. Factor	1.00	0.95	1.00	1.00	0.95	1.00	1.00	1.00		1.00	1.00	
Frt	1.00	1.00	0.85	1.00	1.00	0.85	1.00	0.97		1.00	0.90	
Flt Protected	0.95	1.00	1.00	0.95	1.00	1.00	0.95	1.00		0.95	1.00	
Satd. Flow (prot)	1671	3574	1568	1671	3539	1538	1736	1652		1671	1635	
Flt Permitted	0.25	1.00	1.00	0.26	1.00	1.00	0.15	1.00		0.69	1.00	
Satd. Flow (perm)	432	3574	1568	466	3539	1538	278	1652		1206	1635	
Peak-hour factor, PHF	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96
Adj. Flow (vph)	241	1079	33	31	855	36	72	86	25	50	144	283
RTOR Reduction (vph)	0	0	12	0	0	18	0	10	0	0	67	0
Lane Group Flow (vph)	241	1079	21	31	855	18	72	101	0	50	360	0
Heavy Vehicles (%)	8%	1%	3%	8%	2%	5%	4%	10%	15%	8%	4%	5%
Turn Type	pm+pt	NA	Perm	Perm	NA	Perm	Perm	NA		Perm	NA	
Protected Phases	5	2			6			4			8	
Permitted Phases	2		2	6		6	4			8		
Actuated Green, G (s)	73.2	73.2	73.2	58.0	58.0	58.0	28.8	28.8		28.8	28.8	
Effective Green, g (s)	73.2	73.2	73.2	58.0	58.0	58.0	28.8	28.8		28.8	28.8	
Actuated g/C Ratio	0.64	0.64	0.64	0.51	0.51	0.51	0.25	0.25		0.25	0.25	
Clearance Time (s)	3.0	6.1	6.1	6.1	6.1	6.1	6.4	6.4		6.4	6.4	
Vehicle Extension (s)	2.5	6.0	6.0	6.0	6.0	6.0	2.3	2.3		2.3	2.3	
Lane Grp Cap (vph)	408	2284	1002	236	1792	779	69	415		303	411	
v/s Ratio Prot	c0.06	0.30			0.24			0.06			0.22	
v/s Ratio Perm	c0.31		0.01	0.07		0.01	c0.26			0.04		
v/c Ratio	0.59	0.47	0.02	0.13	0.48	0.02	1.04	0.24		0.17	0.88	
Uniform Delay, d1	10.5	10.7	7.6	14.9	18.4	14.1	42.9	34.2		33.5	41.1	
Progression Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00		1.00	1.00	
Incremental Delay, d2	1.9	0.7	0.0	1.1	0.9	0.1	120.9	0.2		0.2	18.3	
Delay (s)	12.5	11.4	7.6	16.1	19.3	14.2	163.7	34.3		33.6	59.4	
Level of Service	В	В	А	В	В	В	F	С		С	E	
Approach Delay (s)		11.5			19.0			85.3			56.7	
Approach LOS		В			В			F			Е	
Intersection Summary												
HCM 2000 Control Delay			25.8	H	CM 2000	Level of	Service		С			
HCM 2000 Volume to Capa	city ratio		0.73									
Actuated Cycle Length (s)			114.5	S	um of los	t time (s)			15.5			
Intersection Capacity Utiliza	ition		90.1%	IC	CU Level	of Service			E			
Analysis Period (min)			15									
c Critical Lane Group												

Uppers Quarry Traffic Impact Study TMIG

	٦	-+	$\mathbf{r}$	1	-	•	t	1	Ļ	
Lane Group	EBL	EBT	EBR	WBL	WBT	NBL	NBT	SBL	SBT	
Lane Configurations	<b>N</b>	•	1	3	1.	3	1.	5	1.	
Traffic Volume (vph)	37	434	96	44	401	100	132	25	118	
Future Volume (vph)	37	434	96	44	401	100	132	25	118	
Turn Type	Perm	NA	Perm	Perm	NA	Perm	NA	Perm	NA	
Protected Phases		2			6		4		8	
Permitted Phases	2		2	6		4		8		
Detector Phase	2	2	2	6	6	4	4	8	8	
Switch Phase										
Minimum Initial (s)	20.0	20.0	20.0	20.0	20.0	10.0	10.0	10.0	10.0	
Minimum Split (s)	29.0	29.0	29.0	29.0	29.0	35.0	35.0	35.0	35.0	
Total Split (s)	57.0	57.0	57.0	57.0	57.0	46.0	46.0	46.0	46.0	
Total Split (%)	55.3%	55.3%	55.3%	55.3%	55.3%	44.7%	44.7%	44.7%	44.7%	
Yellow Time (s)	5.0	5.0	5.0	5.0	5.0	4.0	4.0	4.0	4.0	
All-Red Time (s)	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	
Lost Time Adjust (s)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Total Lost Time (s)	7.0	7.0	7.0	7.0	7.0	6.0	6.0	6.0	6.0	
Lead/Lag										
Lead-Lag Optimize?										
Recall Mode	C-Max	C-Max	C-Max	Max	Max	None	None	None	None	
Act Effct Green (s)	71.9	71.9	71.9	71.9	71.9	18.1	18.1	18.1	18.1	
Actuated g/C Ratio	0.70	0.70	0.70	0.70	0.70	0.18	0.18	0.18	0.18	
v/c Ratio	0.07	0.37	0.10	0.08	0.36	0.65	0.62	0.18	0.55	
Control Delay	6.6	8.1	3.7	6.6	7.9	56.8	42.4	36.6	40.2	
Queue Delay	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Total Delay	6.6	8.1	3.7	6.6	7.9	56.8	42.4	36.6	40.2	
LOS	A	A	A	A	A	E	D	D	D	
Approach Delay		7.3			7.8		47.5		39.7	
Approach LOS		A			A		D		D	
Intersection Summary										
Cycle Length: 103										
Actuated Cycle Length: 10	03									
Offset: 0 (0%), Reference	d to phase 2:	EBTL, St	art of Gre	en						
Natural Cycle: 65										
Control Type: Actuated-C	oordinated									
Maximum v/c Ratio: 0.65										
ntersection Signal Delay:	18.9			li	ntersectio	n LOS: B				
Intersection Capacity Utili	zation 70.7%			10	CU Level	of Service	эC			

률 ø2 (R)	₫ Ø4	
57 s	46 s	
₹ø6	Ø8	
57 s	46.5	

Synchro 10 Report

5: Thoroid Townlin	e Road		луз ца									
	≯	-	$\mathbf{r}$	1	-	*	1	1	1	1	Ŧ	-
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SB
Lane Configurations	<u></u>	•	1	۲.	ĥ		۲	ĥ		ň	ĥ	
Traffic Volume (vph)	37	434	96	44	401	21	100	132	50	25	118	3
Future Volume (vph)	37	434	96	44	401	21	100	132	50	25	118	3
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	190
Total Lost time (s)	7.0	7.0	7.0	7.0	7.0		6.0	6.0		6.0	6.0	
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00		1.00	1.00		1.00	1.00	
Frpb, ped/bikes	1.00	1.00	1.00	1.00	1.00		1.00	1.00		1.00	1.00	
Flpb, ped/bikes	1.00	1.00	1.00	1.00	1.00		1.00	1.00		1.00	1.00	
Frt	1.00	1.00	0.85	1.00	0.99		1.00	0.96		1.00	0.96	
Fit Protected	0.95	1.00	1.00	0.95	1.00		0.95	1.00		0.95	1.00	
Satd. Flow (prot)	1624	1827	1553	1752	1835		1687	1746		1736	1715	
Flt Permitted	0.47	1.00	1.00	0.46	1.00		0.54	1.00		0.47	1.00	
Satd. Flow (perm)	804	1827	1553	852	1835		963	1746		861	1715	
Peak-hour factor, PHF	0.91	0.91	0.91	0.91	0.91	0.91	0.91	0.91	0.91	0.91	0.91	0.9
Adi, Flow (vph)	41	477	105	48	441	23	110	145	55	27	130	4
RTOR Reduction (vph)	0	0	16	0	1	0	0	18	0	0	15	
ane Group Flow (vph)	41	477	89	48	463	0	110	182	0	27	157	
Confl. Peds. (#/hr)	1			10	100	1			Ŭ			
Heavy Vehicles (%)	11%	4%	4%	3%	2%	15%	7%	6%	0%	4%	7%	6
	Perm	NA	Perm	Perm	NA		Perm	NA		Perm	NA	
Protected Phases	1 Cilli	2	1 GIIII	1 Cilli	6		1 CHI	4		1 CIIII	8	
Permitted Phases	2	2	2	6	0		4	-		8	0	
Actuated Green G (s)	71 9	71 9	71 9	71 9	71 9		18 1	18 1		18 1	18 1	
Effective Green, a (s)	71.0	71.9	71.0	71.0	71.9		18.1	18.1		18.1	18.1	
Actuated g/C Ratio	0 70	0 70	0.70	0 70	0 70		0.18	0.18		0.18	0.18	
Clearance Time (s)	7.0	7.0	7.0	7.0	7.0		6.0	6.0		6.0	6.0	
Vehicle Extension (s)	5.0	5.0	5.0	5.0	5.0		5.0	5.0		5.0	5.0	
ano Cro Con (unh)	5.0	1275	109/	504	1290		160	206		151	201	
ula Batia Brat	501	0.26	1004	094	0.25		109	0.10		101	0.00	
Vis Ratio Prot	0.05	CU.20	0.06	0.06	0.25		o0 11	0.10		0.02	0.09	
VIS Ralio Ferrir	0.05	0.27	0.00	0.00	0.26		0.65	0.50		0.03	0.62	
V/C Naliu	0.07	0.37	0.00	0.00	0.30		20.5	20.1		0.10	20.52	
Drinorni Deidy, ut	4.9	1.00	1.00	1.00	1.00		1.00	1 00		1.00	1.00	
Progression Factor	1.00	1.00	1.00	1.00	1.00		11.00	1.00		1.00	1.00	
Delev (e)	0.5	0.0	0.1	0.3	0.0		F1.0	4.0		1.2	3.1	
Delay (S)	5.2	1.2	5.1	5.2	7.1		51.0	43.7		37.3	41.0	
Approach Doloy (c)	A	6 7	A	A	A 6.0		U	46.2		U	41.0	
Approach Delay (S)		0.7			0.9			40.5			41.0	
Approach LOS		А			A			U			U	
Intersection Summary			10.1									
HCM 2000 Control Delay			18.4	H	CM 2000	Level of S	Service		В			
HCM 2000 Volume to Capa	acity ratio		0.43									
Actuated Cycle Length (s)			103.0	S	um of lost	time (s)			13.0			
Intersection Capacity Utiliza	ation		70.7%	IC	U Level o	of Service			С			
Analysis Period (min)			15									
c Critical Lane Group												

Uppers Quarry Traffic Impact Study TMIG

HCM Unsignalized Intersection Capacity Analysis	
6 [.] Thorold Townline Road & Beaverdams Road	

	۶	-	$\mathbf{\hat{v}}$	∢	-	×	1	Ť	1	1	Ŧ	~
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBF
Lane Configurations		\$			\$			÷			\$	
Sign Control		Stop			Stop			Stop			Stop	
Traffic Volume (vph)	24	197	16	11	166	21	32	148	7	20	150	35
Future Volume (vph)	24	197	16	11	166	21	32	148	7	20	150	35
Peak Hour Factor	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93
Hourly flow rate (vph)	26	212	17	12	178	23	34	159	8	22	161	38
Direction, Lane #	EB 1	WB 1	NB 1	SB 1								
Volume Total (vph)	255	213	201	221								
Volume Left (vph)	26	12	34	22								
Volume Right (vph)	17	23	8	38								
Hadj (s)	0.02	-0.04	0.16	0.01								
Departure Headway (s)	5.5	5.6	5.8	5.6								
Degree Utilization, x	0.39	0.33	0.32	0.34								
Capacity (veh/h)	601	592	562	585								
Control Delay (s)	12.0	11.2	11.5	11.5								
Approach Delay (s)	12.0	11.2	11.5	11.5								
Approach LOS	В	В	В	В								
Intersection Summary												
Delay			11.6									
Level of Service			В									
Intersection Capacity Utilizati	on		42.3%	IC	CU Level of	of Service			А			
Analysis Period (min)			15									

HCM Unsignalized Intersection Capacity Analysis 7: Thorold Townline Road & Uppers Lane

<2018 Existing> PM Peak Hour 09-14-2021

	✓	•	1	1	•	ŧ
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations	¥		î,			ų
Traffic Volume (veh/h)	0	1	189	1	1	179
Future Volume (Veh/h)	0	1	189	1	1	179
Sign Control	Stop		Free			Free
Grade	0%		0%			0%
Peak Hour Factor	0.91	0.91	0.91	0.91	0.91	0.91
Hourly flow rate (vph)	0	1	208	1	1	197
Pedestrians						
Lane Width (m)						
Walking Speed (m/s)						
Percent Blockage						
Right turn flare (veh)						
Median type			None			None
Median storage veh)						
Upstream signal (m)						
pX, platoon unblocked						
vC, conflicting volume	408	208			209	
vC1, stage 1 conf vol						
vC2, stage 2 conf vol						
vCu, unblocked vol	408	208			209	
tC, single (s)	6.4	6.2			4.1	
tC, 2 stage (s)						
tF (s)	3.5	3.3			2.2	
p0 queue free %	100	100			100	
cM capacity (veh/h)	603	837			1374	
Direction. Lane #	WB 1	NB 1	SB 1			
Volume Total	1	209	198			
Volume Left	0	0	1			
Volume Right	1	1	0			
cSH	837	1700	1374			
Volume to Capacity	0.00	0.12	0.00			
Queue Length 95th (m)	0.0	0.0	0.0			
Control Delay (s)	9.3	0.0	0.0			
Lane LOS	A		А			
Approach Delay (s)	9.3	0.0	0.0			
Approach LOS	А					
Intersection Summary						
Average Delay			0.0			
Intersection Capacity Utiliza	ation		20.2%	IC	U Level of	Service
Analysis Period (min)			15			

Uppers Quarry Traffic Impact Study TMIG

Synchro 10 Report

Uppers Quarry Traffic Impact Study TMIG

Timings 1: Davis Road & Th	orold S	Stone F	Road				<202	5 Bacl	kgroun	d> AM	l Peak l ⁰⁹⁻¹	Hour 4-2021
	۶	-	$\mathbf{\hat{z}}$	4	+	•	1	1	1	ţ	4	
Lane Group	EBL	EBT	EBR	WBL	WBT	NBL	NBT	NBR	SBL	SBT	SBR	
Lane Configurations	ሻ		1	ሻ	<b>≜</b> ⊅	ሻ	ę	1	٦	•	1	
Traffic Volume (vph)	21	929	274	87	1076	542	15	211	1	2	18	
Future Volume (vph)	21	929	274	87	1076	542	15	211	1	2	18	
Turn Type	Perm	NA	Perm	pm+pt	NA	Split	NA	Perm	Split	NA	Perm	
Protected Phases		2		1	6	4	4		8	8		
Permitted Phases	2		2	6				4			8	
Detector Phase	2	2	2	1	6	4	4	4	8	8	8	
Switch Phase												
Minimum Initial (s)	20.0	20.0	20.0	8.0	20.0	10.0	10.0	10.0	10.0	10.0	10.0	
Minimum Split (s)	28.9	28.9	28.9	12.5	28.9	29.7	29.7	29.7	21.7	21.7	21.7	
Total Split (s)	46.3	46.3	46.3	13.0	59.3	39.0	39.0	39.0	21.7	21.7	21.7	
Total Split (%)	38.6%	38.6%	38.6%	10.8%	49.4%	32.5%	32.5%	32.5%	18.1%	18.1%	18.1%	
Yellow Time (s)	5.4	5.4	5.4	3.0	5.4	5.7	5.7	5.7	5.7	5.7	5.7	
All-Red Time (s)	1.5	1.5	1.5	0.0	1.5	2.0	2.0	2.0	2.0	2.0	2.0	
Lost Time Adjust (s)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Total Lost Time (s)	6.9	6.9	6.9	3.0	6.9	7.7	7.7	7.7	7.7	7.7	7.7	
Lead/Lag	Lag	Lag	Lag	Lead								
Lead-Lag Optimize?	Yes	Yes	Yes	Yes								
Recall Mode	C-Max	C-Max	C-Max	None	Max	None	None	None	None	None	None	
Act Effct Green (s)	58.3	58.3	58.3	74.3	70.4	27.9	27.9	27.9	10.0	10.0	10.0	
Actuated g/C Ratio	0.49	0.49	0.49	0.62	0.59	0.23	0.23	0.23	0.08	0.08	0.08	
v/c Ratio	0.12	0.59	0.36	0.33	0.57	0.80	0.81	0.43	0.01	0.01	0.08	
Control Delay	26.1	27.0	10.6	27.4	32.6	59.5	61.1	7.3	51.0	51.0	0.7	
Queue Delay	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Total Delay	26.1	27.0	10.6	27.4	32.6	59.5	61.1	7.3	51.0	51.0	0.7	
LOS	С	С	В	С	С	E	E	A	D	D	A	
Approach Delay		23.3			32.2		45.7			7.5		
Approach LOS		С			С		D			A		
Intersection Summary												
Cycle Length: 120												
Actuated Cycle Length: 120												
Offset: 0 (0%). Referenced to	o phase 2	EBTL. St	art of Gre	en								
Natural Cycle: 95												
Control Type: Actuated-Coor	rdinated											
Maximum v/c Ratio: 0.81												
Intersection Signal Delay: 31	1.9			Ir	ntersectio	n LOS: C						
Intersection Capacity Utilizat	tion 86.6%			10	CU Level	of Service	εE					
Analysis Period (min) 15												
Splits and Phases: 1: Dav	is Road &	Thorold S	Stone Roa	ad								

Ø1	🚽 💠 🛛 🖉 2 (R)	<b>▲</b> Ø4
13 s	46.3 s	39 s

<b>√</b> Ø1	₩ Ø2 (R)	<b>₩</b> Ø4	<b>1</b> 208
13 s	46.3 s	39 s	21.7s
₹ø6			
59.3 s			

Synchro 10 Report

HCM Signalized Intersection Capacity Analysis 1: Davis Road & Thorold Stone Road

<2025 Background> AM Peak Hour

	٦	-	$\mathbf{r}$	4	←	•	•	Ť	۲	1	ŧ	~
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	۲.	44	1	٦	<b>≜t</b> ≽		5	ą	1	5	•	1
Traffic Volume (vph)	21	929	274	87	1076	6	542	15	211	1	2	18
Future Volume (vph)	21	929	274	87	1076	6	542	15	211	1	2	18
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Total Lost time (s)	6.9	6.9	6.9	3.0	6.9		7.7	7.7	7.7	7.7	7.7	7.7
Lane Util. Factor	1.00	0.95	1.00	1.00	0.95		0.95	0.95	1.00	1.00	1.00	1.00
Frpb, ped/bikes	1.00	1.00	1.00	1.00	1.00		1.00	1.00	0.99	1.00	1.00	0.99
Flpb, ped/bikes	1.00	1.00	1.00	1.00	1.00		1.00	1.00	1.00	1.00	1.00	1.00
Frt	1.00	1.00	0.85	1.00	1.00		1.00	1.00	0.85	1.00	1.00	0.85
Flt Protected	0.95	1.00	1.00	0.95	1.00		0.95	0.95	1.00	0.95	1.00	1.00
Satd. Flow (prot)	1640	3406	1442	1530	3398		1559	1553	1475	1388	1624	1337
Flt Permitted	0.22	1.00	1.00	0.18	1.00		0.95	0.95	1.00	0.95	1.00	1.00
Satd. Flow (perm)	374	3406	1442	289	3398		1559	1553	1475	1388	1624	1337
Peak-hour factor, PHF	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96
Adi, Flow (vph)	22	968	285	91	1121	6	565	16	220	1	2	19
RTOR Reduction (vph)	0	0	100	0	0	0	0	0	169	0	0	18
Lane Group Flow (vph)	22	968	185	91	1127	0	288	293	51	1	2	1
Confl. Peds. (#/hr)	1					1	1		1	1		1
Heavy Vehicles (%)	10%	6%	12%	18%	6%	30%	10%	28%	8%	30%	17%	19%
Turn Type	Perm	NA	Perm	pm+pt	NA		Split	NA	Perm	Split	NA	Perm
Protected Phases		2		1	6		. 4	4		. 8	8	
Permitted Phases	2		2	6					4			8
Actuated Green, G (s)	53.7	53.7	53.7	65.8	65.8		27.9	27.9	27.9	4.0	4.0	4.0
Effective Green, g (s)	53.7	53.7	53.7	65.8	65.8		27.9	27.9	27.9	4.0	4.0	4.0
Actuated g/C Ratio	0.45	0.45	0.45	0.55	0.55		0.23	0.23	0.23	0.03	0.03	0.03
Clearance Time (s)	6.9	6.9	6.9	3.0	6.9		7.7	7.7	7.7	7.7	7.7	7.7
Vehicle Extension (s)	3.0	3.0	3.0	2.5	3.0		4.5	4.5	4.5	4.5	4.5	4.5
Lane Grp Cap (vph)	167	1524	645	252	1863		362	361	342	46	54	44
v/s Ratio Prot		c0.28		0.03	c0.33		0.18	c0.19		0.00	c0.00	
v/s Ratio Perm	0.06		0.13	0.17					0.03			0.00
v/c Ratio	0.13	0.64	0.29	0.36	0.60		0.80	0.81	0.15	0.02	0.04	0.01
Uniform Delay, d1	19.5	25.6	21.0	15.6	18.3		43.4	43.6	36.6	56.1	56.1	56.1
Progression Factor	1.00	1.00	1.00	1.99	1.76		1.00	1.00	1.00	1.00	1.00	1.00
Incremental Delay, d2	1.6	2.0	1.1	0.5	1.2		12.7	14.2	0.4	0.3	0.5	0.2
Delay (s)	21.1	27.6	22.1	31.5	33.5		56.1	57.8	37.0	56.4	56.6	56.3
Level of Service	С	С	С	С	С		E	E	D	E	E	E
Approach Delay (s)		26.3			33.3			51.4			56.4	
Approach LOS		С			С			D			E	
Intersection Summary												
HCM 2000 Control Delay			35.1	Н	CM 2000	Level of S	Service		D			
HCM 2000 Volume to Capa	icity ratio		0.66									
Actuated Cycle Length (s)			120.0	S	um of lost	t time (s)			25.3			
Intersection Capacity Utilization	ation		86.6%	IC	CU Level o	of Service			E			
Analysis Period (min)			15									
a Critical Lana Crown												

c Critical Lane Group

Uppers Quarry Traffic Impact Study TMIG

				-			1	1	7	
	<i>,</i>	-	-	•		T	×	÷	*	
Lane Group	EBL	EBT	WBL	WBT	NBL	NBT	SBL	SBT	SBR	
Lane Configurations		4		- <b>4</b> >	<u>۲</u>	<b>≜</b> ⊅	ሻ	- ++	1	
Traffic Volume (vph)	110	31	34	17	16	473	82	240	44	
Future Volume (vph)	110	31	34	17	16	473	82	240	44	
Turn Type	Perm	NA	Perm	NA	Perm	NA	Perm	NA	Perm	
Protected Phases		2		6		4		8		
Permitted Phases	2		6		4		8		8	
Detector Phase	2	2	6	6	4	4	8	8	8	
Switch Phase										
Minimum Initial (s)	10.0	10.0	10.0	10.0	25.0	25.0	25.0	25.0	25.0	
Minimum Split (s)	38.1	38.1	38.1	38.1	32.0	32.0	32.0	32.0	32.0	
Total Split (s)	46.0	46.0	46.0	46.0	54.0	54.0	54.0	54.0	54.0	
Total Split (%)	46.0%	46.0%	46.0%	46.0%	54.0%	54.0%	54.0%	54.0%	54.0%	
Yellow Time (s)	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	
All-Red Time (s)	31	31	31	31	2.0	2.0	2.0	2.0	2.0	
Lost Time Adjust (s)	0.1	0.0	0.1	0.0	0.0	0.0	0.0	0.0	0.0	
Total Lost Time (s)		8.1		8.1	7.0	7.0	7.0	7.0	7.0	
		0.1		0.1	1.0	7.0	1.0	1.0	1.0	
Lead-Lag Ontimize?										
Recall Mode	C-Max	C-Max	Max	Max	None	None	None	None	None	
	0-IVIAX	57 F	IVIAA	57.5	27.4	27.4	27.4	27.4	27.4	
Act Elici Green (S)		0.59		0.59	0.27	0.27	0.27	0.27	0.07	
Actualed g/C Ratio		0.00		0.00	0.27	0.27	0.27	0.27	0.27	
V/C Nalio		10.20		2.0	0.07	24.4	0.01	0.01	U.11 E 0	
		12.2		0.0	20.9	0.0	41.0	29.5	0.0	
Queue Delay		10.0		0.0	0.0	24.4	0.0	0.0	0.0	
		12.2		3.9	20.9	34.4	41.0	29.3	0.C	
LUS		40 C		A	C	0	D	00.0	A	
Approach Delay		12.2		3.9		34.1		29.2		
Approach LUS		В		A		C		C		
Intersection Summary										
Cycle Length: 100										
Actuated Cycle Length: 10	00									
Offset: 0 (0%), Reference	d to phase 2:	EBTL, St	art of Gre	en						
Natural Cycle: 75										
Control Type: Actuated-C	oordinated									
Maximum v/c Ratio: 0.65										
Intersection Signal Delay:	25.0			Ir	ntersectio	n LOS: C				
Intersection Capacity Utili	zation 88.3%			10	CU Level	of Service	θE			
Analysis Period (min) 15										

opilito una i nuoco.	L. Duvio rioud a rilugula i allo	loud bout		
→ Ø2 (R)			< <b>↑</b> ø4	
46 s			54 s	
₹ø6			↓ Ø8	
46 s			54 s	

Synchro 10 Report

HCM Signalized Intersection Capacity Analysis 2: Davis Road & Niagara Falls Road/Beaverdams Road <2025 Background> AM Peak Hour 09-14-2021

	۶	+	$\mathbf{F}$	4	Ļ	•	•	Ť	1	*	ŧ	~
Novement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
ane Configurations		\$			\$		ľ	A1≱		ľ	<u></u>	1
raffic Volume (vph)	110	31	12	34	17	166	16	473	59	82	240	44
Future Volume (vph)	110	31	12	34	17	166	16	473	59	82	240	44
deal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
fotal Lost time (s)		8.1			8.1		7.0	7.0		7.0	7.0	7.0
ane Util. Factor		1.00			1.00		1.00	0.95		1.00	0.95	1.00
Frt .		0.99			0.90		1.00	0.98		1.00	1.00	0.85
It Protected		0.97			0.99		0.95	1.00		0.95	1.00	1.00
Satd. Flow (prot)		1662			1632		1388	3111		1787	2983	1392
It Permitted		0.66			0.94		0.60	1.00		0.33	1.00	1.00
Satd. Flow (perm)		1136			1538		870	3111		613	2983	1392
Peak-hour factor, PHF	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95
Adj. Flow (vph)	116	33	13	36	18	175	17	498	62	86	253	46
RTOR Reduction (vph)	0	2	0	0	74	0	0	13	0	0	0	33
ane Group Flow (vph)	0	160	0	0	155	0	17	547	0	86	253	13
leavy Vehicles (%)	10%	7%	7%	7%	12%	2%	30%	15%	7%	1%	21%	16%
Turn Type	Perm	NA		Perm	NA		Perm	NA		Perm	NA	Perm
Protected Phases		2			6			4			8	
Permitted Phases	2			6			4			8		8
Actuated Green, G (s)		57.5			57.5		27.4	27.4		27.4	27.4	27.4
Effective Green, g (s)		57.5			57.5		27.4	27.4		27.4	27.4	27.4
Actuated g/C Ratio		0.58			0.58		0.27	0.27		0.27	0.27	0.27
Clearance Time (s)		8.1			8.1		7.0	7.0		7.0	7.0	7.0
/ehicle Extension (s)		3.0			3.0		5.0	5.0		5.0	5.0	5.0
ane Grp Cap (vph)		653			884		238	852		167	817	381
/s Ratio Prot								c0.18			0.08	
/s Ratio Perm		c0.14			0.10		0.02			0.14		0.01
/c Ratio		0.24			0.17		0.07	0.64		0.51	0.31	0.03
Jniform Delay, d1		10.5			10.0		26.9	32.0		30.7	28.8	26.6
Progression Factor		1.00			1.00		1.00	1.00		1.00	1.00	1.00
ncremental Delay, d2		0.9			0.4		0.3	2.3		5.3	0.5	0.1
Delay (s)		11.4			10.5		27.1	34.2		35.9	29.3	26.7
evel of Service		В			В		С	С		D	С	С
Approach Delay (s)		11.4			10.5			34.0			30.4	
Approach LOS		В			В			С			С	
ntersection Summary												
ICM 2000 Control Delay			26.3	Н	CM 2000	Level of	Service		С			
ICM 2000 Volume to Capacity	ratio		0.37									
Actuated Cycle Length (s)			100.0	S	um of los	time (s)			15.1			
ntersection Capacity Utilization	1		88.3%	IC	CU Level	of Service			E			
Analysis Period (min)			15									
Critical Lane Group												

Uppers Quarry Traffic Impact Study TMIG

J. Davis Ruau & Li	unuys L	ane									00 11 20
	٠	<b>→</b>	4	+	×	1	t	1	ŧ	-	
Lane Group	EBL	EBT	WBL	WBT	WBR	NBL	NBT	SBL	SBT	SBR	
Lane Configurations	<u>۳</u>	4	<u>۲</u>	<b>↑</b>	1	<u>۲</u>	4	<u>۲</u>	<b>↑</b>	1	
Traffic Volume (vph)	140	518	36	395	233	22	139	181	94	143	
Future Volume (vph)	140	518	36	395	233	22	139	181	94	143	
Turn Type	Perm	NA	Perm	NA	Perm	Perm	NA	Perm	NA	Perm	
Protected Phases		2		6			4		8		
Permitted Phases	2		6		6	4		8		8	
Detector Phase	2	2	6	6	6	4	4	8	8	8	
Switch Phase											
Vinimum Initial (s)	22.0	22.0	22.0	22.0	22.0	15.0	15.0	15.0	15.0	15.0	
Minimum Split (s)	36.0	36.0	36.0	36.0	36.0	32.0	32.0	32.0	32.0	32.0	
Total Split (s)	46.0	46.0	46.0	46.0	46.0	44.0	44.0	44.0	44.0	44.0	
Total Split (%)	51.1%	51.1%	51.1%	51.1%	51.1%	48.9%	48.9%	48.9%	48.9%	48.9%	
Yellow Time (s)	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	
All-Red Time (s)	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	
Lost Time Adjust (s)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Total Lost Time (s)	7.0	7.0	7.0	7.0	7.0	7.0	7.0	7.0	7.0	7.0	
_ead/Lag											
_ead-Lag Optimize?											
Recall Mode	C-Max	C-Max	Мах	Max	Мах	None	None	None	None	None	
Act Effct Green (s)	53.8	53.8	53.8	53.8	53.8	22.2	22.2	22.2	22.2	22.2	
Actuated g/C Ratio	0.60	0.60	0.60	0.60	0.60	0.25	0.25	0.25	0.25	0.25	
/c Ratio	0.30	0.52	0.11	0.40	0.26	0.09	0.45	0.76	0.27	0.33	
Control Delay	12.8	14.2	11.3	12.5	2.4	23.5	29.0	49.5	27.1	5.9	
Queue Delav	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Total Delay	12.8	14.2	11.3	12.5	2.4	23.5	29.0	49.5	27.1	5.9	
OS	B	B	B	B	A	C	C	D	C	A	
Approach Delay		13.9	2	8.9		•	28.4	2	29.6		
Approach LOS		В		A			С		C		
ntersection Summary											
Cycle Length: 90											
Actuated Cycle Length: 90											
Offset: 0 (0%), Referenced	to phase 2:	EBTL, St	art of Gre	en							
Natural Cycle: 70											
Control Type: Actuated-Cod	ordinated										
Maximum v/c Ratio: 0.76											
ntersection Signal Delay: 1	6.9			Ir	ntersectio	n LOS: B					
ntersection Capacity Utiliza	tity Utilization 95.0% ICU Level of Service F										
Analysis Period (min) 15											

	≪ <b>1</b> Ø4
46 s	44 s
<b>∲</b> ♥ Ø6	↓ Ø8
46 s	44 s

Synchro 10 Report

HCM Signalized Intersection Capacity Analysis 3: Davis Road & Lundys Lane <2025 Background> AM Peak Hour 09-14-2021

	۶	-	$\mathbf{r}$	4	+	×	٠	t	۲	1	Ŧ	~
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	٦	ţ,		5	•	1	۲	1.		ň	•	1
Traffic Volume (vph)	140	518	18	36	395	233	22	139	24	181	94	143
Future Volume (vph)	140	518	18	36	395	233	22	139	24	181	94	143
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Total Lost time (s)	7.0	7.0		7.0	7.0	7.0	7.0	7.0		7.0	7.0	7.0
Lane Util. Factor	1.00	1.00		1.00	1.00	1.00	1.00	1.00		1.00	1.00	1.00
Frpb, ped/bikes	1.00	1.00		1.00	1.00	1.00	1.00	1.00		1.00	1.00	1.00
Flpb, ped/bikes	1.00	1.00		1.00	1.00	1.00	1.00	1.00		1.00	1.00	1.00
Frt	1.00	0.99		1.00	1.00	0.85	1.00	0.98		1.00	1.00	0.85
Flt Protected	0.95	1.00		0.95	1.00	1.00	0.95	1.00		0.95	1.00	1.00
Satd. Flow (prot)	1656	1825		1467	1743	1442	1444	1529		1530	1532	1392
Flt Permitted	0.48	1.00		0.37	1.00	1.00	0.69	1.00		0.64	1.00	1.00
Satd. Flow (perm)	834	1825		569	1743	1442	1052	1529		1030	1532	1392
Peak-hour factor, PHF	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94
Adj. Flow (vph)	149	551	19	38	420	248	23	148	26	193	100	152
RTOR Reduction (vph)	0	1	0	0	0	100	0	9	0	0	0	115
Lane Group Flow (vph)	149	569	0	38	420	148	23	165	0	193	100	37
Confl. Peds. (#/hr)			1	1								
Heavy Vehicles (%)	9%	3%	19%	23%	9%	12%	25%	20%	30%	18%	24%	16%
Turn Type	Perm	NA		Perm	NA	Perm	Perm	NA		Perm	NA	Perm
Protected Phases		2			6			4			8	
Permitted Phases	2			6		6	4			8		8
Actuated Green, G (s)	53.8	53.8		53.8	53.8	53.8	22.2	22.2		22.2	22.2	22.2
Effective Green, g (s)	53.8	53.8		53.8	53.8	53.8	22.2	22.2		22.2	22.2	22.2
Actuated g/C Ratio	0.60	0.60		0.60	0.60	0.60	0.25	0.25		0.25	0.25	0.25
Clearance Time (s)	7.0	7.0		7.0	7.0	7.0	7.0	7.0		7.0	7.0	7.0
Vehicle Extension (s)	4.0	4.0		4.0	4.0	4.0	2.0	2.0		2.0	2.0	2.0
Lane Grp Cap (vph)	498	1090		340	1041	861	259	377		254	377	343
v/s Ratio Prot		c0.31			0.24			0.11			0.07	
v/s Ratio Perm	0.18			0.07		0.10	0.02			c0.19		0.03
v/c Ratio	0.30	0.52		0.11	0.40	0.17	0.09	0.44		0.76	0.27	0.11
Uniform Delay, d1	8.9	10.6		7.8	9.6	8.1	26.1	28.6		31.4	27.3	26.2
Progression Factor	1.00	1.00		1.00	1.00	1.00	1.00	1.00		1.00	1.00	1.00
Incremental Delay, d2	1.5	1.8		0.7	1.2	0.4	0.1	0.3		11.0	0.1	0.1
Delay (s)	10.4	12.4		8.5	10.8	8.5	26.2	28.9		42.4	27.5	26.3
Level of Service	В	В		A	В	A	С	С		D	С	С
Approach Delay (s)		12.0			9.9			28.6			33.6	
Approach LOS		В			A			С			С	
Intersection Summary												
HCM 2000 Control Delay			17.5	H	CM 2000	Level of S	Service		В			
HCM 2000 Volume to Capaci	ty ratio		0.59									
Actuated Cycle Length (s)			90.0	S	um of losi	t time (s)			14.0			
Intersection Capacity Utilizati	on		95.0%	IC	U Level	of Service			F			
Analysis Period (min)			15									
c Critical Lane Group												

Uppers Quarry Traffic Impact Study TMIG

4: Thorold Townline Road & Thorold Stone Road 09-14-2021											
	٦	-	*	4	+	*	•	Ť	1	ŧ	
Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	SBL	SBT	
Lane Configurations	ካ		1	<u>۲</u>	- <b>†</b> †	1	<u>۲</u>	4	<u>۲</u>	- îs	
Traffic Volume (vph)	323	659	95	110	807	73	82	130	52	141	
Future Volume (vph)	323	659	95	110	807	73	82	130	52	141	
Turn Type	pm+pt	NA	Perm	pm+pt	NA	Perm	pm+pt	NA	Perm	NA	
Protected Phases	5	2		1	6		7	4		8	
Permitted Phases	2		2	6		6	4		8		
Detector Phase	5	2	2	1	6	6	7	4	8	8	
Switch Phase											
Minimum Initial (s)	8.0	10.0	10.0	8.0	10.0	10.0	8.0	10.0	10.0	10.0	
Minimum Split (s)	11.0	35.1	35.1	12.5	35.1	35.1	11.0	41.4	41.4	41.4	
Total Split (s)	30.0	49.2	49.2	17.8	37.0	37.0	11.0	53.0	42.0	42.0	
Total Split (%)	25.0%	41.0%	41.0%	14.8%	30.8%	30.8%	9.2%	44.2%	35.0%	35.0%	
Yellow Time (s)	3.0	4.1	4.1	3.0	4.1	4.1	3.0	4.1	4.1	4.1	
All-Red Time (s)	0.0	2.0	2.0	0.0	2.0	2.0	0.0	2.3	2.3	2.3	
Lost Time Adjust (s)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Total Lost Time (s)	3.0	6.1	6.1	3.0	6.1	6.1	3.0	6.4	6.4	6.4	
Lead/Lag	Lead	Lag	Lag	Lead	Lag	Lag	Lead		Lag	Lag	
Lead-Lag Optimize?	Yes	Yes	Yes	Yes	Yes	Yes	Yes		Yes	Yes	
Recall Mode	None	C-Max	C-Max	None	C-Max	C-Max	None	None	None	None	
Act Effct Green (s)	72.5	56.6	56.6	58.2	45.1	45.1	41.3	37.9	29.1	29.1	
Actuated q/C Ratio	0.60	0.47	0.47	0.48	0.38	0.38	0.34	0.32	0.24	0.24	
v/c Ratio	0.79	0.42	0.14	0.32	0.64	0.12	0.44	0.37	0.20	0.89	
Control Delay	51.1	37.5	22.0	16.4	37.3	2.5	31.7	28.6	35.6	60.2	
Queue Delay	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Total Delay	51.1	37.5	22.0	16.4	37.3	2.5	31.7	28.6	35.6	60.2	
LOS	D	D	С	В	D	А	С	С	D	E	
Approach Delay		40.2			32.4			29.6		57.0	
Approach LOS		D			С			С		E	
Intersection Summary											
Cycle Length: 120											
Actuated Cycle Length: 12	0										
Offset: 0 (0%), Referenced	to phase 2:	EBTL an	d 6:WBTL	, Start of	Green						
Natural Cycle: 100											
Control Type: Actuated-Co	ordinated										
Maximum v/c Ratio: 0.89											
Intersection Signal Delay:	38.8			Ir	ntersectio	n LOS: D					
Intersection Capacity Utiliz	ation 85.8%			10	CU Level	of Service	θE				
Analysis Period (min) 15											

Splits and Phases:	4: Thorold Townline Road &	Thorold Stone Road
--------------------	----------------------------	--------------------

<b>√</b> Ø1	📣 Ø2 (R) 🕊		
17.8 s	49.2 s	53 s	
	● ♥ Ø6 (R)	▲ Ø7	
30 s	37 s	11 s 42 s	

Synchro 10 Report

HCM Signalized Intersection Capacity Analysis 4: Thorold Townline Road & Thorold Stone Road <2025 Background> AM Peak Hour 09-14-2021

	≯	+	*	4	ł	*	•	1	1	*	Ŧ	~
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	<u>۲</u>	- <b>†</b> †	1	ሻ	- <b>†</b> †	1	٦	4		٦	ĥ	
Traffic Volume (vph)	323	659	95	110	807	73	82	130	51	52	141	205
Future Volume (vph)	323	659	95	110	807	73	82	130	51	52	141	205
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Total Lost time (s)	3.0	6.1	6.1	3.0	6.1	6.1	3.0	6.4		6.4	6.4	
Lane Util. Factor	1.00	0.95	1.00	1.00	0.95	1.00	1.00	1.00		1.00	1.00	
Frpb, ped/bikes	1.00	1.00	1.00	1.00	1.00	0.97	1.00	1.00		1.00	1.00	
Flpb, ped/bikes	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00		1.00	1.00	
Frt	1.00	1.00	0.85	1.00	1.00	0.85	1.00	0.96		1.00	0.91	
Flt Protected	0.95	1.00	1.00	0.95	1.00	1.00	0.95	1.00		0.95	1.00	
Satd. Flow (prot)	1641	3471	1369	1444	3505	1453	1492	1554		1641	1474	
Flt Permitted	0.18	1.00	1.00	0.39	1.00	1.00	0.22	1.00		0.64	1.00	
Satd. Flow (perm)	317	3471	1369	594	3505	1453	339	1554		1104	1474	
Peak-hour factor, PHF	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96
Adi, Flow (vph)	336	686	99	115	841	76	85	135	53	54	147	214
RTOR Reduction (vph)	0	0	50	0	0	48	0	13	0	0	47	0
Lane Group Flow (vph)	336	686	49	115	841	28	85	175	0	54	314	0
Confl. Peds. (#/hr)	4					4						
Heavy Vehicles (%)	10%	4%	18%	25%	3%	8%	21%	14%	25%	10%	18%	17%
Turn Type	pm+pt	NA	Perm	pm+pt	NA	Perm	pm+pt	NA		Perm	NA	
Protected Phases	5	2		1	6		7	4			8	
Permitted Phases	2		2	6		6	4			8		
Actuated Green, G (s)	69.0	56.0	56.0	54.5	44.5	44.5	38.5	38.5		29.1	29.1	
Effective Green, q (s)	69.0	56.0	56.0	54.5	44.5	44.5	38.5	38.5		29.1	29.1	
Actuated g/C Ratio	0.58	0.47	0.47	0.45	0.37	0.37	0.32	0.32		0.24	0.24	
Clearance Time (s)	3.0	6.1	6.1	3.0	6.1	6.1	3.0	6.4		6.4	6.4	
Vehicle Extension (s)	2.5	6.0	6.0	2.5	6.0	6.0	2.5	2.3		2.3	2.3	
Lane Grp Cap (vph)	419	1619	638	340	1299	538	170	498		267	357	
v/s Ratio Prot	c0.14	0.20		0.03	0.24		c0.03	0.11			c0.21	
v/s Ratio Perm	c0.32		0.04	0.13		0.02	0.13			0.05		
v/c Ratio	0.80	0.42	0.08	0.34	0.65	0.05	0.50	0.35		0.20	0.88	
Uniform Delay, d1	19.6	21.3	17.7	19.4	31.3	24.2	31.1	31.2		36.2	43.8	
Progression Factor	2 18	1.58	3.81	1 00	1 00	1 00	1 00	1 00		1 00	1 00	
Incremental Delay, d2	8.8	0.7	0.2	0.4	2.5	0.2	1.7	0.3		0.2	20.7	
Delay (s)	51.5	34.3	67.6	19.9	33.8	24.4	32.8	31.4		36.4	64.5	
Level of Service	D	С	E	B	C	С	C	С		D	E	
Approach Delay (s)	-	42.4	-	2	31.5	Ũ	Ŭ	31.9		-	60.8	
Approach LOS		D			С			С			E	
Intersection Summary												
HCM 2000 Control Dolov	LI,	CM 2000	Loval of	Sonvice		D						
HGM 2000 Control Delay	п		Level OI	Service		U						
Actuated Cycle Length (a)	0.	um of look	time (c)			10 F						
Intersection Capacity Utilization 85.8%						f Sorvior			10.0			
Analysis Period (min) 15					O Level (		,		2			
Critical Lana Crow			10									

Uppers Quarry Traffic Impact Study TMIG

5: Thorold Townline Road & Lundys Lane 09-14-20											
	٦	-	$\mathbf{\hat{z}}$	4	+	1	Ť	1	ţ	~	
Lane Group	EBL	EBT	EBR	WBL	WBT	NBL	NBT	SBL	SBT	SBR	
Lane Configurations	<u>۳</u>	<b>↑</b>	1	ሻ	4	ሻ	4	<u>۲</u>	<b>↑</b>	1	
Traffic Volume (vph)	157	521	98	38	348	71	140	22	85	56	
Future Volume (vph)	157	521	98	38	348	71	140	22	85	56	
Turn Type	Perm	NA	Perm	Perm	NA	Perm	NA	Perm	NA	Perm	
Protected Phases		2			6		4		8		
Permitted Phases	2		2	6		4		8		8	
Detector Phase	2	2	2	6	6	4	4	8	8	8	
Switch Phase											
/linimum Initial (s)	20.0	20.0	20.0	20.0	20.0	10.0	10.0	10.0	10.0	10.0	
/linimum Split (s)	29.0	29.0	29.0	29.0	29.0	35.0	35.0	35.0	35.0	35.0	
Total Split (s)	65.0	65.0	65.0	65.0	65.0	35.0	35.0	35.0	35.0	35.0	
Fotal Split (%)	65.0%	65.0%	65.0%	65.0%	65.0%	35.0%	35.0%	35.0%	35.0%	35.0%	
'ellow Time (s)	5.0	5.0	5.0	5.0	5.0	4.0	4.0	4.0	4.0	4.0	
All-Red Time (s)	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	
ost Time Adjust (s)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
otal Lost Time (s)	7.0	7.0	7.0	7.0	7.0	6.0	6.0	6.0	6.0	6.0	
.ead/Lag											
.ead-Lag Optimize?											
Recall Mode	C-Max	C-Max	C-Max	Max	Max	None	None	None	None	None	
ct Effct Green (s)	68.8	68.8	68.8	68.8	68.8	18.2	18.2	18.2	18.2	18.2	
Actuated g/C Ratio	0.69	0.69	0.69	0.69	0.69	0.18	0.18	0.18	0.18	0.18	
/c Ratio	0.29	0.45	0.10	0.08	0.34	0.35	0.63	0.15	0.31	0.22	
Control Delay	8.8	9.2	3.6	6.9	7.8	38.8	43.8	34.1	36.6	10.3	
Queue Delay	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
otal Delay	8.8	9.2	3.6	6.9	7.8	38.8	43.8	34.1	36.6	10.3	
.OS	A	A	A	A	A	D	D	С	D	В	
Approach Delay		8.4			7.7		42.4		27.3		
Approach LOS		A			A		D		С		
ntersection Summary											
Cycle Length: 100											
ctuated Cycle Length: 10	0										
Offset: 0 (0%). Referenced to phase 2:EBTL. Start of Green											
Natural Cycle: 65											
ontrol Type: Actuated-Co	ordinated										
laximum v/c Ratio: 0.63											
tersection Signal Delay:	15.4			Ir	ntersectio	n LOS: B					
tersection Capacity Utiliz	ation 79.0%			10	CU Level	of Service	e D				
nalvsis Period (min) 15											

≠ø2 (R)	<b>₫</b> ø4	
65 s	35 s	
₹ Ø6	<b>↓</b> Ø8	
65 s	35 s	

Synchro 10 Report

HCM Signalized Intersection Capacity Analysis 5: Thorold Townline Road & Lundys Lane <2025 Background> AM Peak Hour 09-14-2021

	٦	-	$\mathbf{F}$	∢	←	•	1	Ť	۲	1	ŧ	~
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	5	•	1	<u> </u>	1,		۲	ĥ		۲.	•	1
Traffic Volume (vph)	157	521	98	38	348	39	71	140	37	22	85	56
Future Volume (vph)	157	521	98	38	348	39	71	140	37	22	85	56
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Total Lost time (s)	7.0	7.0	7.0	7.0	7.0		6.0	6.0		6.0	6.0	6.0
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00		1.00	1.00		1.00	1.00	1.00
Frpb, ped/bikes	1.00	1.00	1.00	1.00	1.00		1.00	1.00		1.00	1.00	1.00
Flpb, ped/bikes	1.00	1.00	1.00	1.00	1.00		1.00	1.00		1.00	1.00	1.00
Frt	1.00	1.00	0.85	1.00	0.98		1.00	0.97		1.00	1.00	0.85
Flt Protected	0.95	1.00	1.00	0.95	1.00		0.95	1.00		0.95	1.00	1.00
Satd. Flow (prot)	1581	1810	1495	1752	1771		1612	1607		1671	1638	1252
Flt Permitted	0.50	1.00	1.00	0.41	1.00		0.70	1.00		0.51	1.00	1.00
Satd. Flow (perm)	834	1810	1495	752	1771		1184	1607		893	1638	1252
Peak-hour factor, PHF	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93
Adi, Flow (vph)	169	560	105	41	374	42	76	151	40	24	91	60
RTOR Reduction (vph)	0	0	17	0	3	0	0	11	0	0	0	49
Lane Group Flow (vph)	169	560	88	41	413	0	76	180	0	24	91	11
Confl. Peds. (#/hr)	1					1						
Heavy Vehicles (%)	14%	5%	8%	3%	6%	0%	12%	17%	5%	8%	16%	29%
Turn Type	Perm	NA	Perm	Perm	NA		Perm	NA		Perm	NA	Perm
Protected Phases		2			6			4			8	
Permitted Phases	2		2	6			4			8		8
Actuated Green, G (s)	68.8	68.8	68.8	68.8	68.8		18.2	18.2		18.2	18.2	18.2
Effective Green, a (s)	68.8	68.8	68.8	68.8	68.8		18.2	18.2		18.2	18.2	18.2
Actuated q/C Ratio	0.69	0.69	0.69	0.69	0.69		0.18	0.18		0.18	0.18	0.18
Clearance Time (s)	7.0	7.0	7.0	7.0	7.0		6.0	6.0		6.0	6.0	6.0
Vehicle Extension (s)	5.0	5.0	5.0	5.0	5.0		5.0	5.0		5.0	5.0	5.0
Lane Grp Cap (vph)	573	1245	1028	517	1218		215	292		162	298	227
v/s Ratio Prot		c0.31			0.23			c0.11			0.06	
v/s Ratio Perm	0.20		0.06	0.05			0.06			0.03		0.01
v/c Ratio	0.29	0.45	0.09	0.08	0.34		0.35	0.62		0.15	0.31	0.05
Uniform Delay, d1	6.1	7.0	5.2	5.1	6.3		35.8	37.7		34.4	35.4	33.8
Progression Factor	1.00	1.00	1.00	1.00	1.00		1.00	1.00		1.00	1.00	1.00
Incremental Delay, d2	1.3	1.2	0.2	0.3	0.8		2.1	5.5		0.9	1.2	0.2
Delay (s)	7.4	8.2	5.3	5.4	7.1		37.8	43.2		35.3	36.6	33.9
Level of Service	А	А	А	А	А		D	D		D	D	С
Approach Delay (s)		7.7			7.0			41.7			35.5	
Approach LOS		Α			А			D			D	
Intersection Summary												
HCM 2000 Control Delay			15.5	H	CM 2000	Level of S	Service		В			
HCM 2000 Volume to Capacity ratio 0.48			0.48									
Actuated Cycle Length (s) 100.0			S	um of lost	time (s)			13.0				
Intersection Capacity Utiliza	ation		79.0%	IC	U Level o	of Service			D			
Analysis Period (min)			15									
<ul> <li>Critical Lana Crown</li> </ul>												

c Critical Lane Group

Uppers Quarry Traffic Impact Study TMIG

HCM Unsignalized Intersection Capacity Analysis 6: Thorold Townline Road & Beaverdams Road

<2025 Background> AM Peak Hour 09-14-2021

	٦	-	$\mathbf{\hat{z}}$	∢	←	•	•	Ť	1	1	Ŧ	4
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		\$			\$			¢			÷	
Sign Control		Stop			Stop			Stop			Stop	
Traffic Volume (vph)	19	139	16	17	175	22	24	245	33	11	318	19
Future Volume (vph)	19	139	16	17	175	22	24	245	33	11	318	19
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Hourly flow rate (vph)	21	151	17	18	190	24	26	266	36	12	346	21
Direction, Lane #	EB 1	WB 1	NB 1	SB 1								
Volume Total (vph)	189	232	328	379								
Volume Left (vph)	21	18	26	12								
Volume Right (vph)	17	24	36	21								
Hadj (s)	0.02	-0.03	0.20	0.31								
Departure Headway (s)	6.8	6.7	6.4	6.4								
Degree Utilization, x	0.36	0.43	0.58	0.67								
Capacity (veh/h)	453	473	525	530								
Control Delay (s)	13.6	14.6	18.0	21.6								
Approach Delay (s)	13.6	14.6	18.0	21.6								
Approach LOS	В	В	С	С								
Intersection Summary												
Delay			17.7									
Level of Service			С									
Intersection Capacity Utilizat	tion		46.4%	IC	U Level o	of Service			А			
Analysis Period (min)			15									

HCM Unsignalized Intersection Capacity Analysis 7: Thorold Townline Road & Uppers Lane

<2025 Background> AM Peak Hour _____09-14-2021

	1	•	1	1	1	Ŧ
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations	¥.		1.			4
Traffic Volume (veh/h)	0	0	323	0	0	256
Future Volume (Veh/h)	0	0	323	0	0	256
Sian Control	Stop	, i	Free	, in the second s	, i	Free
Grade	0%		0%			0%
Peak Hour Factor	0.93	0.93	0.93	0.93	0.93	0.93
Hourly flow rate (yph)	0.00	0.00	347	0.00	0.00	275
Pedestrians	Ū	Ŭ	011	Ŭ	Ū	210
I ane Width (m)						
Walking Speed (m/s)						
Percent Blockage						
Pight turn flare (yeh)						
Median type			None			None
Median storage yeb			NUTE			NUTE
linetroom signal (m)						
opsireani signar (m)						
pA, platoon unblocked	600	247			247	
vC, conflicting volume	022	347			347	
VC1, stage 1 conf vol						
VC2, stage 2 cont vol	000	0.47			0.47	
vCu, unblocked vol	622	347			347	
tC, single (s)	6.4	6.2			4.1	
tC, 2 stage (s)						
tF (s)	3.5	3.3			2.2	
p0 queue free %	100	100			100	
cM capacity (veh/h)	454	701			1223	
Direction, Lane #	WB 1	NB 1	SB 1			
Volume Total	0	347	275			
Volume Left	0	0	0			
Volume Right	0	0	0			
cSH	1700	1700	1223			
Volume to Capacity	0.00	0.20	0.00			
Queue Length 95th (m)	0.0	0.0	0.0			
Control Delay (s)	0.0	0.0	0.0			
Lane LOS	A					
Approach Delay (s)	0.0	0.0	0.0			
Approach LOS	A					
Intersection Summary						
Average Delay			0.0			
Intersection Capacity Utiliz	ation		20.3%	IC	U Level o	of Service
Analysis Period (min)			15			
			15			

Uppers Quarry Traffic Impact Study TMIG

Synchro 10 Report

Uppers Quarry Traffic Impact Study TMIG

Timings       <2025 Background> PM Peak Hour         1: Davis Road & Thorold Stone Road       09-14-2021												
	٦	+	*	4	Ļ	≺	1	1	×	ţ	~	
Lane Group	EBL	EBT	EBR	WBL	WBT	NBL	NBT	NBR	SBL	SBT	SBR	
Lane Configurations	٦	- <b>†</b> †	1	ሻ	<b>≜</b> î≽	ሻ	ર્સ	1	٦	•	1	
Traffic Volume (vph)	24	1233	586	146	1164	506	5	126	4	6	28	
Future Volume (vph)	24	1233	586	146	1164	506	5	126	4	6	28	
Turn Type	Perm	NA	Perm	pm+pt	NA	Split	NA	Perm	Split	NA	Perm	
Protected Phases		2		1	6	4	4		8	8		
Permitted Phases	2		2	6				4			8	
Detector Phase	2	2	2	1	6	4	4	4	8	8	8	
Switch Phase												
Minimum Initial (s)	20.0	20.0	20.0	5.0	20.0	10.0	10.0	10.0	10.0	10.0	10.0	
Minimum Split (s)	28.9	28.9	28.9	8.0	28.9	29.7	29.7	29.7	17.7	17.7	17.7	
Total Split (S)	63.0	63.0	63.0	18.0	81.0	41.3	41.3	41.3	17.7	17.7	17.7	
Total Split (%)	45.0%	45.0%	45.0%	12.9%	57.9%	29.5%	29.5%	29.5%	12.0%	12.0%	12.0%	
Yellow Time (s)	5.4	5.4	5.4	3.0	5.4	5.7	5.7	5.7	5./	5.7	5.7	
All-Red Time (S)	1.5	1.5	1.5	0.0	1.5	2.0	2.0	2.0	2.0	2.0	2.0	
Lost Time Adjust (s)	0.0	0.0	0.0	2.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Lead/Lag	6.0 Lan	0.9	6.0 Del	J.c	0.9	1.1	1.1	1.1	1.1	1.1	1.1	
Leau/Lag	Lay Yes	Ves	Vas	Ves								
Recall Mode	C-Max	C-Max	C-Max	None	C-Max	None	None	None	None	None	None	
Act Effct Green (s)	71.1	71.1	71.1	89.9	86.0	28.8	28.8	28.8	10.0	10.0	10.0	
Actuated g/C Ratio	0.51	0.51	0.51	0.64	0.61	0.21	0.21	0.21	0.07	0.07	0.07	
v/c Ratio	0.17	0.72	0.66	0.66	0.56	0.77	0.79	0.32	0.03	0.05	0.13	
Control Delay	29.8	33.2	19.9	32.5	19.5	67.3	68.9	8.8	61.2	61.5	1.3	
Queue Delay	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Total Delay	29.8	33.2	19.9	32.5	19.5	67.3	68.9	8.8	61.2	61.5	1.3	
LOS	С	С	В	С	В	E	E	А	E	E	А	
Approach Delay		28.9			20.9		56.4			16.7		
Approach LOS		С			С		E			В		
Intersection Summary												
Cycle Length: 140												
Actuated Cycle Length: 140												
Offset: 0 (0%) Referenced to	n nhase 2	FRTL and	16·WBTI	Start of	Green							
Natural Color, Holdenbarg, Bridde Leb Fe and erner E, Ganter Frederik												
Control Type: Actuated-Coor	rdinated											
Maximum v/c Ratio: 0.79												
Intersection Signal Delay: 30	).6			Ir	ntersectio	n LOS: C						
Intersection Capacity Utilizat	ion 87.6%			10	CU Level	of Service	εE					
Analysis Period (min) 15												

Splits and Phases: 1: Davis Road & Thorold Stone Road

Ø1		<b>√</b> _{Ø4}	1 Ø8
18 s	63 s	41.3 s	17.7 s
₩ Ø6 (R)			
81s			

Uppers Quarry Traffic Impact Study TMIG

Synchro 10 Report

HCM Signalized Intersection Capacity Analysis 1: Davis Road & Thorold Stone Road <2025 Background> PM Peak Hour

	٦	-	$\mathbf{\hat{z}}$	4	←	•	•	Ť	۲	1	ŧ	~
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	ľ	<u></u>	1	ľ	A1⊅		ľ	ę	1	7	•	7
Traffic Volume (vph)	24	1233	586	146	1164	1	506	5	126	4	6	28
Future Volume (vph)	24	1233	586	146	1164	1	506	5	126	4	6	28
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Total Lost time (s)	6.9	6.9	6.9	3.0	6.9		7.7	7.7	7.7	7.7	7.7	7.7
Lane Util. Factor	1.00	0.95	1.00	1.00	0.95		0.95	0.95	1.00	1.00	1.00	1.00
Frpb, ped/bikes	1.00	1.00	1.00	1.00	1.00		1.00	1.00	1.00	1.00	1.00	0.98
Flpb, ped/bikes	1.00	1.00	1.00	1.00	1.00		1.00	1.00	1.00	1.00	1.00	1.00
Frt	1.00	1.00	0.85	1.00	1.00		1.00	1.00	0.85	1.00	1.00	0.85
Flt Protected	0.95	1.00	1.00	0.95	1.00		0.95	0.95	1.00	0.95	1.00	1.00
Satd. Flow (prot)	1433	3539	1568	1671	3539		1681	1678	1482	1805	1810	1524
Flt Permitted	0.19	1.00	1.00	0.09	1.00		0.95	0.95	1.00	0.95	1.00	1.00
Satd. Flow (perm)	294	3539	1568	163	3539		1681	1678	1482	1805	1810	1524
Peak-hour factor, PHF	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95
Adj. Flow (vph)	25	1298	617	154	1225	1	533	5	133	4	6	29
RTOR Reduction (vph)	0	0	145	0	0	0	0	0	106	0	0	28
Lane Group Flow (vph)	25	1298	472	154	1226	0	266	272	27	4	6	1
Confl. Peds. (#/hr)							1					1
Heavy Vehicles (%)	26%	2%	3%	8%	2%	0%	2%	30%	9%	0%	5%	4%
Turn Type	Perm	NA	Perm	pm+pt	NA		Split	NA	Perm	Split	NA	Perm
Protected Phases		2		1	6		. 4	4		. 8	8	
Permitted Phases	2		2	6					4			8
Actuated Green, G (s)	68.0	68.0	68.0	82.9	82.9		28.8	28.8	28.8	6.0	6.0	6.0
Effective Green, g (s)	68.0	68.0	68.0	82.9	82.9		28.8	28.8	28.8	6.0	6.0	6.0
Actuated g/C Ratio	0.49	0.49	0.49	0.59	0.59		0.21	0.21	0.21	0.04	0.04	0.04
Clearance Time (s)	6.9	6.9	6.9	3.0	6.9		7.7	7.7	7.7	7.7	7.7	7.7
Vehicle Extension (s)	3.0	3.0	3.0	3.0	3.0		4.5	4.5	4.5	4.5	4.5	4.5
Lane Grp Cap (vph)	142	1718	761	224	2095		345	345	304	77	77	65
v/s Ratio Prot		c0.37		c0.06	0.35		0.16	c0.16		0.00	c0.00	
v/s Ratio Perm	0.09		0.30	0.35					0.02			0.00
v/c Ratio	0.18	0.76	0.62	0.69	0.59		0.77	0.79	0.09	0.05	0.08	0.02
Uniform Delay, d1	20.2	29.2	26.5	22.6	17.8		52.5	52.7	45.0	64.3	64.3	64.2
Progression Factor	1.00	1.00	1.00	1.00	1.00		1.00	1.00	1.00	1.00	1.00	1.00
Incremental Delay, d2	2.7	3.1	3.8	8.5	1.2		11.4	12.6	0.2	0.5	0.7	0.2
Delay (s)	22.9	32.4	30.3	31.1	19.0		63.8	65.3	45.2	64.8	65.1	64.4
Level of Service	С	С	С	С	В		E	E	D	E	E	E
Approach Delay (s)		31.6			20.4			60.7			64.5	
Approach LOS		С			С			E			E	
Intersection Summary												
HCM 2000 Control Delay			32,9	Н	CM 2000	Level of S	Service		С			
HCM 2000 Volume to Capacity ratio 0.72												
Actuated Cycle Length (s) 140.0			140.0	S	um of losi	t time (s)			25.3			
Intersection Capacity Utilization 87.6%				IC	U Level	of Service			E			
Analysis Period (min)			15						-			

c Critical Lane Group

Uppers Quarry Traffic Impact Study TMIG

2: Davis Road & N	liagara F	alls R	load				09-14-202			
	۶	-	4	+	٠	1	1	Ŧ	∢	
Lane Group	EBL	EBT	WBL	WBT	NBL	NBT	SBL	SBT	SBR	
Lane Configurations		- <del>4</del> >		- <b>4</b> >		<b>≜î</b> ≽	ሻ	<u></u>	1	
Traffic Volume (vph)	90	32	74	44	12	409	170	471	105	
Future Volume (vph)	90	32	74	44	12	409	170	471	105	
Turn Type	Perm	NA	Perm	NA	Perm	NA	Perm	NA	Perm	
Protected Phases		2		6		4		8		
Permitted Phases	2		6		4		8		8	
Detector Phase	2	2	6	6	4	4	8	8	8	
Switch Phase	40.0			10.0						
Minimum Initial (s)	10.0	10.0	10.0	10.0	25.0	25.0	25.0	25.0	25.0	
Vinimum Split (s)	38.1	38.1	38.1	38.1	32.0	32.0	32.0	32.0	32.0	
Total Split (s)	40.0	40.0	40.0	40.0	60.0	60.0	60.0	60.0	60.0	
Total Split (%)	40.0%	40.0%	40.0%	40.0%	60.0%	60.0%	60.0%	60.0%	60.0%	
reliow Time (s)	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	
All-Red Time (S)	3.1	3.1	3.1	3.1	2.0	2.0	2.0	2.0	2.0	
LOST TIME Adjust (s)		0.0		0.0	0.0	0.0	0.0	0.0	0.0	
ood/Log		0.1		0.1	7.0	7.0	7.0	7.0	7.0	
_eau/Lag										
Leau-Lay Optimize?	C Max	C Max	Max	Max	None	None	None	None	None	
Act Effet Groop (s)	0-IVIAX	52 5	IVIAA	52 5	32 /	32.4	32 /	32.4	32.4	
Actuated a/C Ratio		0.52		0.52	0.32	0.32	0.32	0.32	0.32	
Ic Ratio		0.32		0.34	0.02	0.32	0.32	0.02	0.02	
Control Delay		15.9		13.5	19.4	25.9	44.6	27.3	4.2	
Queue Delay		0.0		0.0	0.0	0.0	0.0	0.0	0.0	
Fotal Delay		15.9		13.5	19.4	25.9	44.6	27.3	4.2	
OS		B		B	B	C	D	C	Α	
Approach Delay		15.9		13.5	-	25.7	-	28.0		
Approach LOS		В		В		C		С		
ntersection Summary										
Cycle Length: 100										
Actuated Cycle Length: 10	0									
Offset: 0 (0%), Referenced	to phase 2:	EBTL, St	art of Gre	en						
Vatural Cycle: 75										
Control Type: Actuated-Co	ordinated									
Maximum v/c Ratio: 0.72										
ntersection Signal Delay:	23.9			li	ntersectio	n LOS: C				
ntersection Capacity Utiliz	ation 76.1%			10	CU Level	of Service	e D			
Analysis Period (min) 15										

opilits and Filases.	2. Davis Rudu & Ividya	a rais nua	Ju/Deaveruallis Rodu
▲ _{Ø2 (R)}			<b>↑</b> ø4
40 s			60 s
₹ø6			↓ ∞ _{Ø8}
40 s			60 s

Synchro 10 Report

HCM Signalized Intersection Capacity Analysis 2: Davis Road & Niagara Falls Road/Beaverdams Road <2025 Background> PM Peak Hour 09-14-2021

	۶	+	*	4	+	•	•	Ť	*	×	ŧ	~
lovement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
ane Configurations		4			4		٦	<b>↑</b> 1,-		٦	- <b>†</b> †	7
raffic Volume (vph)	90	32	17	74	44	147	12	409	50	170	471	105
uture Volume (vph)	90	32	17	74	44	147	12	409	50	170	471	105
deal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
otal Lost time (s)		8.1			8.1		7.0	7.0		7.0	7.0	7.0
ane Util. Factor		1.00			1.00		1.00	0.95		1.00	0.95	1.00
rt		0.98			0.93		1.00	0.98		1.00	1.00	0.85
It Protected		0.97			0.99		0.95	1.00		0.95	1.00	1.00
atd. Flow (prot)		1717			1702		1805	3298		1770	3343	1583
It Permitted		0.67			0.87		0.41	1.00		0.42	1.00	1.00
atd. Flow (perm)		1180			1499		771	3298		773	3343	1583
eak-hour factor, PHF	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95
dj. Flow (vph)	95	34	18	78	46	155	13	431	53	179	496	111
TOR Reduction (vph)	0	3	0	0	31	0	0	14	0	0	0	75
ane Group Flow (vph)	0	144	0	0	248	0	13	470	0	179	496	36
leavy Vehicles (%)	2%	2%	30%	2%	1%	2%	0%	8%	5%	2%	8%	2%
urn Type	Perm	NA		Perm	NA		Perm	NA		Perm	NA	Perm
rotected Phases		2			6			4			8	
ermitted Phases	2			6			4			8		8
ctuated Green, G (s)		52.5			52.5		32.4	32.4		32.4	32.4	32.4
ffective Green, g (s)		52.5			52.5		32.4	32.4		32.4	32.4	32.4
ctuated g/C Ratio		0.52			0.52		0.32	0.32		0.32	0.32	0.32
Clearance Time (s)		8.1			8.1		7.0	7.0		7.0	7.0	7.0
ehicle Extension (s)		3.0			3.0		5.0	5.0		5.0	5.0	5.0
ane Grp Cap (vph)		619			786		249	1068		250	1083	512
/s Ratio Prot								0.14			0.15	
/s Ratio Perm		0.12			c0.17		0.02			c0.23		0.02
/c Ratio		0.23			0.32		0.05	0.44		0.72	0.46	0.07
Iniform Delay, d1		12.8			13.5		23.2	26.7		29.8	26.8	23.4
rogression Factor		1.00			1.00		1.00	1.00		1.00	1.00	1.00
ncremental Delay, d2		0.9			1.0		0.2	0.6		11.5	0.6	0.1
)elay (s)		13.7			14.6		23.4	27.3		41.2	27.5	23.5
evel of Service		В			В		С	С		D	С	С
pproach Delay (s)		13.7			14.6			27.2			30.0	
pproach LOS		В			В			С			С	
ntersection Summary												
ICM 2000 Control Delay			25.3	H	CM 2000	Level of	Service		С			
ICM 2000 Volume to Capacit	y ratio		0.47									
ctuated Cycle Length (s)			100.0	S	um of lost	time (s)			15.1			
ntersection Capacity Utilization	n		76.1%	IC	U Level o	of Service			D			
nalysis Period (min)			15									
Critical Lane Group												

Uppers Quarry Traffic Impact Study TMIG

Timings 3: Davis Road & Lu	ndys L	ane					<202	5 Bacl	kgroun	d> PM	Peak Ho 09-14-2
	٨	-	4	+	•	•	Ť	1	ţ	4	
Lane Group	EBL	EBT	WBL	WBT	WBR	NBL	NBT	SBL	SBT	SBR	
Lane Configurations	<u>۳</u>	f,	<u>۲</u>	<b>↑</b>	1	<u>۲</u>	4	ሻ	<b>↑</b>	1	
Traffic Volume (vph)	179	565	28	553	241	46	141	300	125	157	
Future Volume (vph)	179	565	28	553	241	46	141	300	125	157	
Turn Type	pm+pt	NA	Perm	NA	Perm	Perm	NA	pm+pt	NA	Perm	
Protected Phases	5	2		6			4	3	8		
Permitted Phases	2		6		6	4		8		8	
Detector Phase	5	2	6	6	6	4	4	3	8	8	
Switch Phase											
Minimum Initial (s)	5.0	22.0	22.0	22.0	22.0	15.0	15.0	5.0	15.0	15.0	
Minimum Split (s)	8.0	36.0	36.0	36.0	36.0	32.0	32.0	8.0	32.0	32.0	
Total Split (s)	12.0	66.0	54.0	54.0	54.0	32.0	32.0	22.0	54.0	54.0	
Total Split (%)	10.0%	55.0%	45.0%	45.0%	45.0%	26.7%	26.7%	18.3%	45.0%	45.0%	
Yellow Time (s)	3.0	5.0	5.0	5.0	5.0	5.0	5.0	3.0	5.0	5.0	
All-Red Time (s)	0.0	2.0	2.0	2.0	2.0	2.0	2.0	0.0	2.0	2.0	
Lost Time Adjust (s)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Total Lost Time (s)	3.0	7.0	7.0	7.0	7.0	7.0	7.0	3.0	7.0	7.0	
Lead/Lag	Lead		Lag	Lag	Lag	Lag	Lag	Lead			
Lead-Lag Optimize?	Yes		Yes	Yes	Yes	Yes	Yes	Yes			
Recall Mode	None	C-Max	Max	Max	Max	Max	Max	None	Max	Max	
Act Effct Green (s)	63.0	59.0	47.0	47.0	47.0	26.0	26.0	51.0	47.0	47.0	
Actuated o/C Ratio	0.52	0 49	0.39	0.39	0.39	0.22	0.22	0.42	0.39	0.39	
v/c Ratio	0.75	0.72	0.16	0.82	0.36	0.18	0.52	0.66	0.20	0.24	
Control Delay	35.1	29.4	28.8	45.2	9.00	41.4	45.5	32.0	25.0	4.3	
Oueue Delay	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Total Delay	35.1	29.4	28.8	45.2	9.1	41.4	45.5	32.0	25.0	4.3	
	D	20.4	20.0	-10.2 D	Δ	- 11.1 D	-10.0 D	02.0	20.0	Δ	
Approach Delay	U	30.7	0	34.1	~	0	44.7	0	23.0	A	
Annroach LOS		JU.1		J4.1			-++./ D		20.0		
		5		5			5		5		
Intersection Summary											
Cycle Length: 120											
Actuated Cycle Length: 120											
Offset: 0 (0%), Referenced to	o phase 2	EBTL, St	art of Gre	en							
Natural Cycle: 85											
Control Type: Actuated-Coor	rdinated										
Maximum v/c Ratio: 0.82											
ntersection Signal Delay: 31	.3			I	ntersectio	n LOS: C					
Intersection Capacity Utilizat Analysis Period (min) 15	ion 108.19	%		10	CU Level	of Service	e G				

Ø2 (R)	·	Ø3	<b>√</b> [†] ø₄	
66 s		22 s	32 s	
∕ _{Ø5}	₩ Ø6	<b>₽</b> _Ø8		
12 s !	54 s	54 s		

Synchro 10 Report

HCM Signalized Intersection Capacity Analysis 3: Davis Road & Lundys Lane <2025 Background> PM Peak Hour 09-14-2021

	٦	-	$\mathbf{\hat{z}}$	4	+	•	٠	Ť	1	1	Ŧ	~
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	<u> </u>	ĥ		<u> </u>	•	1	ň	ţ,		۲	•	1
Traffic Volume (vph)	179	565	28	28	553	241	46	141	37	300	125	157
Future Volume (vph)	179	565	28	28	553	241	46	141	37	300	125	157
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Total Lost time (s)	3.0	7.0		7.0	7.0	7.0	7.0	7.0		3.0	7.0	7.0
Lane Util. Factor	1.00	1.00		1.00	1.00	1.00	1.00	1.00		1.00	1.00	1.00
Frpb, ped/bikes	1.00	1.00		1.00	1.00	0.98	1.00	1.00		1.00	1.00	1.00
Flpb, ped/bikes	1.00	1.00		1.00	1.00	1.00	1.00	1.00		1.00	1.00	1.00
Frt	1.00	0.99		1.00	1.00	0.85	1.00	0.97		1.00	1.00	0.85
Flt Protected	0.95	1.00		0.95	1.00	1.00	0.95	1.00		0.95	1.00	1.00
Satd. Flow (prot)	1719	1811		1611	1863	1473	1736	1671		1702	1743	1553
Flt Permitted	0.16	1.00		0.29	1.00	1.00	0.67	1.00		0.48	1.00	1.00
Satd. Flow (perm)	286	1811		496	1863	1473	1226	1671		857	1743	1553
Peak-hour factor. PHF	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93
Adj. Flow (vph)	192	608	30	30	595	259	49	152	40	323	134	169
RTOR Reduction (vph)	0	2	0	0	0	144	0	8	0	0	0	103
Lane Group Flow (vph)	192	636	0	30	595	115	49	184	0	323	134	66
Confl. Peds. (#/hr)	2		1	1		2			1	1		
Heavy Vehicles (%)	5%	3%	26%	12%	2%	7%	4%	9%	12%	6%	9%	4%
Turn Type	pm+pt	NA		Perm	NA	Perm	Perm	NA		pm+pt	NA	Perm
Protected Phases	5	2			6			4		3	8	
Permitted Phases	2			6		6	4			8		8
Actuated Green, G (s)	59.0	59.0		47.0	47.0	47.0	26.0	26.0		47.0	47.0	47.0
Effective Green, g (s)	59.0	59.0		47.0	47.0	47.0	26.0	26.0		47.0	47.0	47.0
Actuated g/C Ratio	0.49	0.49		0.39	0.39	0.39	0.22	0.22		0.39	0.39	0.39
Clearance Time (s)	3.0	7.0		7.0	7.0	7.0	7.0	7.0		3.0	7.0	7.0
Vehicle Extension (s)	3.0	4.0		4.0	4.0	4.0	2.0	2.0		3.0	2.0	2.0
Lane Grp Cap (vph)	248	890		194	729	576	265	362		462	682	608
v/s Ratio Prot	c0.06	0.35			c0.32			0.11		c0.10	0.08	
v/s Ratio Perm	0.32			0.06		0.08	0.04			c0.17		0.04
v/c Ratio	0.77	0.72		0.15	0.82	0.20	0.18	0.51		0.70	0.20	0.11
Uniform Delay, d1	23.1	23.9		23.6	32.6	24.1	38.4	41.4		27.7	24.1	23.2
Progression Factor	1.00	1.00		1.10	1.08	1.84	1.00	1.00		1.00	1.00	1.00
Incremental Delay, d2	14.0	4.9		1.5	9.0	0.7	1.5	5.0		4.6	0.6	0.4
Delay (s)	37.1	28.8		27.5	44.4	45.1	39.9	46.4		32.3	24.7	23.6
Level of Service	D	С		С	D	D	D	D		С	С	С
Approach Delay (s)		30.7			44.0			45.1			28.3	
Approach LOS		С			D			D			С	
Intersection Summary												
HCM 2000 Control Delay			36.0	Н	CM 2000	Level of	Service		D			
HCM 2000 Volume to Capac	ity ratio		0.78									
Actuated Cycle Length (s)			120.0	S	um of losi	t time (s)			20.0			
Intersection Capacity Utilizat	ion		108.1%	IC	U Level	of Service			G			
Analysis Period (min)			15									
c Critical Lane Group												

Uppers Quarry Traffic Impact Study TMIG

	٦	-	$\mathbf{r}$	1	+	•	1	1	1	Ŧ	
Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	SBL	SBT	
Lane Configurations	- N	- <b>†</b> †	1	<u>۲</u>	- <b>†</b> †	1	<u>۲</u>	4	ሻ	4	
Traffic Volume (vph)	231	1036	53	61	821	35	123	135	48	158	
Future Volume (vph)	231	1036	53	61	821	35	123	135	48	158	
Turn Type	pm+pt	NA	Perm	pm+pt	NA	Perm	pm+pt	NA	pm+pt	NA	
Protected Phases	5	2		1	6		7	4	3	8	
Permitted Phases	2		2	6		6	4		8		
Detector Phase	5	2	2	1	6	6	7	4	3	8	
Switch Phase											
Minimum Initial (s)	8.0	10.0	10.0	5.0	10.0	10.0	5.0	10.0	5.0	10.0	
Minimum Split (s)	11.0	35.1	35.1	8.0	35.1	35.1	8.0	41.4	8.0	41.4	
Total Split (s)	21.0	55.0	55.0	9.6	43.6	43.6	13.4	45.9	9.5	42.0	
Total Split (%)	17.5%	45.8%	45.8%	8.0%	36.3%	36.3%	11.2%	38.3%	7.9%	35.0%	
Yellow Time (s)	3.0	4.1	4.1	3.0	4.1	4.1	3.0	4.1	3.0	4.1	
All-Red Time (s)	0.0	2.0	2.0	0.0	2.0	2.0	0.0	2.3	0.0	2.3	
Lost Time Adjust (s)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Total Lost Time (s)	3.0	6.1	6.1	3.0	6.1	6.1	3.0	6.4	3.0	6.4	
Lead/Lag	Lead	Lag	Lag	Lead	Lag	Lag	Lead	Lag	Lead	Lag	
Lead-Lag Optimize?	Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes	
Recall Mode	None	C-Max	C-Max	None	C-Max	C-Max	None	None	None	None	
Act Effct Green (s)	65.9	54.9	54.9	55.1	45.3	45.3	48.1	37.1	41.4	31.7	
Actuated g/C Ratio	0.55	0.46	0.46	0.46	0.38	0.38	0.40	0.31	0.34	0.26	
v/c Ratio	0.72	0.66	0.07	0.30	0.64	0.05	0.57	0.49	0.13	0.92	
Control Delay	29.1	29.4	0.2	18.9	35.2	0.1	32.4	32.1	21.4	60.7	
Queue Delav	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Total Delay	29.1	29.4	0.2	18.9	35.2	0.1	32.4	32.1	21.4	60.7	
LOS	C	С	А	В	D	A	С	C	С	E	
Approach Delay	-	28.2		_	32.8		-	32.2	-	56.8	
Approach LOS		C			С			С		E	
Intersection Summary											
Cycle Length: 120											
Actuated Cycle Length: 12	0										
Offset: 0 (0%), Referenced	to phase 2	EBTL and	d 6:WBTL	Start of	Green						
Natural Cycle: 100				,							
Control Type: Actuated-Co	ordinated										
Maximum v/c Ratio: 0.92											
ntersection Signal Delay:	34.5			Ir	ntersectio	n LOS: C					
intersection Capacity Utiliz	ation 84.4%			IC	CU Level	of Service	θE				
Analysis Period (min) 15											

✓ø1 ↓ Ø2 (0	र)♥	<b>1</b> Ø3	Ø4
9.6 s 55 s		9.5 s 45.	9 s
	●	<b>1</b> Ø7	<b>↓</b> Ø8
21 s	43.6 s	13.4 s	42 s

Synchro 10 Report

HCM Signalized Intersection Capacity Analysis 4: Thorold Townline Road & Thorold Stone Road <2025 Background> PM Peak Hour 09-14-2021

	۶	-	$\mathbf{\hat{v}}$	1	+	×	1	1	۲	1	ţ	~
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	۲.	<b>^</b>	1	۲.	<b>^</b>	1	۲	ĥ		۲	4Î	
Traffic Volume (vph)	231	1036	53	61	821	35	123	135	104	48	158	272
Future Volume (vph)	231	1036	53	61	821	35	123	135	104	48	158	272
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Total Lost time (s)	3.0	6.1	6.1	3.0	6.1	6.1	3.0	6.4		3.0	6.4	
Lane Util. Factor	1.00	0.95	1.00	1.00	0.95	1.00	1.00	1.00		1.00	1.00	
Frt	1.00	1.00	0.85	1.00	1.00	0.85	1.00	0.93		1.00	0.91	
Flt Protected	0.95	1.00	1.00	0.95	1.00	1.00	0.95	1.00		0.95	1.00	
Satd. Flow (prot)	1671	3574	1568	1671	3539	1538	1736	1584		1671	1644	
Flt Permitted	0.18	1.00	1.00	0.17	1.00	1.00	0.14	1.00		0.57	1.00	
Satd. Flow (perm)	314	3574	1568	305	3539	1538	251	1584		994	1644	
Peak-hour factor, PHF	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96
Adj. Flow (vph)	241	1079	55	64	855	36	128	141	108	50	165	283
RTOR Reduction (vph)	0	0	30	0	0	23	0	23	0	0	53	0
Lane Group Flow (vph)	241	1079	25	64	855	13	128	226	0	50	395	0
Heavy Vehicles (%)	8%	1%	3%	8%	2%	5%	4%	10%	15%	8%	4%	5%
Turn Type	pm+pt	NA	Perm	pm+pt	NA	Perm	pm+pt	NA		pm+pt	NA	
Protected Phases	5	2		1	6		7	4		3	8	
Permitted Phases	2		2	6		6	4			8		
Actuated Green, G (s)	62.2	53.7	53.7	50.2	44.7	44.7	45.3	37.1		37.5	32.3	
Effective Green, g (s)	62.2	53.7	53.7	50.2	44.7	44.7	45.3	37.1		37.5	32.3	
Actuated g/C Ratio	0.52	0.45	0.45	0.42	0.37	0.37	0.38	0.31		0.31	0.27	
Clearance Time (s)	3.0	6.1	6.1	3.0	6.1	6.1	3.0	6.4		3.0	6.4	
Vehicle Extension (s)	2.5	6.0	6.0	3.0	6.0	6.0	3.0	2.3		3.0	2.3	
Lane Grp Cap (vph)	326	1599	701	190	1318	572	218	489		339	442	
v/s Ratio Prot	c0.09	0.30		0.02	0.24		c0.05	0.14		0.01	c0.24	
v/s Ratio Perm	c0.29		0.02	0.13		0.01	0.17			0.04		
v/c Ratio	0.74	0.67	0.04	0.34	0.65	0.02	0.59	0.46		0.15	0.89	
Uniform Delay, d1	19.7	26.2	18.6	22.3	31.2	23.8	28.3	33.4		29.3	42.2	
Progression Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00		1.00	1.00	
Incremental Delay, d2	8.0	2.3	0.1	1.1	2.5	0.1	4.0	0.4		0.2	19.6	
Delay (s)	27.7	28.5	18.7	23.3	33.6	23.9	32.3	33.8		29.5	61.8	
Level of Service	С	С	В	С	С	С	С	С		С	E	
Approach Delay (s)		28.0			32.6			33.3			58.6	
Approach LOS		С			С			С			E	
Intersection Summary												
HCM 2000 Control Delay			34.7	H	CM 2000	Level of	Service		С			
HCM 2000 Volume to Capac	city ratio		0.79									
Actuated Cycle Length (s)			120.0	S	um of los	time (s)			18.5			
Intersection Capacity Utilizat	tion		84.4%	IC	CU Level	of Service	)		E			
Analysis Period (min)			15									
c Critical Lane Group												

Uppers Quarry Traffic Impact Study TMIG

	ic Rouu	u Lun	uyo Lu	ne							
	٦	-	$\mathbf{i}$	4	+	1	Ť	1	ŧ	~	
ane Group	EBL	EBT	EBR	WBL	WBT	NBL	NBT	SBL	SBT	SBR	
ane Configurations	ሻ	<b>↑</b>	1	ሻ	ef 👘	<u>۲</u>	ef 👘	ሻ	<b>↑</b>	1	
raffic Volume (vph)	81	527	103	44	555	113	131	52	118	130	
uture Volume (vph)	81	527	103	44	555	113	131	52	118	130	
Turn Type	Perm	NA	Perm	Perm	NA	Perm	NA	Perm	NA	Perm	
Protected Phases		2			6		4		8		
Permitted Phases	2		2	6		4		8		8	
etector Phase	2	2	2	6	6	4	4	8	8	8	
witch Phase											
finimum Initial (s)	20.0	20.0	20.0	20.0	20.0	10.0	10.0	10.0	10.0	10.0	
linimum Split (s)	29.0	29.0	29.0	29.0	29.0	35.0	35.0	35.0	35.0	35.0	
otal Split (s)	85.0	85.0	85.0	85.0	85.0	35.0	35.0	35.0	35.0	35.0	
otal Split (%)	70.8%	70.8%	70.8%	70.8%	70.8%	29.2%	29.2%	29.2%	29.2%	29.2%	
'ellow Time (s)	5.0	5.0	5.0	5.0	5.0	4.0	4.0	4.0	4.0	4.0	
II-Red Time (s)	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	
ost Time Adjust (s)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
otal Lost Time (s)	7.0	7.0	7.0	7.0	7.0	6.0	6.0	6.0	6.0	6.0	
.ead/Lag											
ead-Lag Optimize?											
Recall Mode	C-Max	C-Max	C-Max	C-Max	C-Max	None	None	None	None	None	
ct Effct Green (s)	86.6	86.6	86.6	86.6	86.6	20.4	20.4	20.4	20.4	20.4	
ctuated g/C Ratio	0.72	0.72	0.72	0.72	0.72	0.17	0.17	0.17	0.17	0.17	
/c Ratio	0.20	0.44	0.10	0.09	0.49	0.67	0.65	0.43	0.43	0.38	
Control Delay	8.4	10.9	4.0	6.8	9.4	63.3	51.8	52.5	47.7	9.2	
Queue Delay	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
otal Delay	8.4	10.9	4.0	6.8	9.4	63.3	51.8	52.5	47.7	9.2	
OS	A	В	Α	Α	Α	E	D	D	D	А	
Approach Delay		9.6			9.3		56.2		31.8		
pproach LOS		Α			Α		E		С		
ntersection Summary											
Cycle Length: 120											
ctuated Cycle Length: 12	20										
Offset: 0 (0%), Reference	to phase 2	EBTL and	d 6:WBTL	Start of	Green						
atural Cycle: 70				,							
ontrol Type: Actuated-Co	ordinated										
laximum v/c Ratio: 0.67											
tersection Signal Delay:	20.0			Ir	ntersectio	n LOS: C					
tersection Capacity Utiliz	ation 87.8%			10	CU Level	of Service	ε				
nalysis Period (min) 15											

Ø2 (R)	<b>₫</b> _{Ø4}
85 s	35 s
₩ Ø6 (R)	<b>€</b> ≥Ø8
85 s	35 s

Synchro 10 Report

HCM Signalized Intersection Capacity Analysis 5: Thorold Townline Road & Lundys Lane <2025 Background> PM Peak Hour 09-14-2021

	۶	-	$\mathbf{r}$	4	←	•	•	Ť	۲	1	Ŧ	~
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	۲	•	1	۲	¢Î		۲.	4Î		ň	•	1
Traffic Volume (vph)	81	527	103	44	555	32	113	131	50	52	118	130
Future Volume (vph)	81	527	103	44	555	32	113	131	50	52	118	130
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Total Lost time (s)	7.0	7.0	7.0	7.0	7.0		6.0	6.0		6.0	6.0	6.0
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00		1.00	1.00		1.00	1.00	1.00
Frpb, ped/bikes	1.00	1.00	1.00	1.00	1.00		1.00	1.00		1.00	1.00	1.00
Flpb, ped/bikes	1.00	1.00	1.00	1.00	1.00		1.00	1.00		1.00	1.00	1.00
Frt	1.00	1.00	0.85	1.00	0.99		1.00	0.96		1.00	1.00	0.85
Flt Protected	0.95	1.00	1.00	0.95	1.00		0.95	1.00		0.95	1.00	1.00
Satd. Flow (prot)	1625	1827	1553	1752	1833		1687	1745		1736	1776	1524
Flt Permitted	0.36	1.00	1.00	0.40	1.00		0.62	1.00		0.43	1.00	1.00
Satd. Flow (perm)	621	1827	1553	739	1833		1094	1745		794	1776	1524
Peak-hour factor, PHF	0.91	0.91	0.91	0.91	0.91	0.91	0.91	0.91	0.91	0.91	0.91	0.91
Adj. Flow (vph)	89	579	113	48	610	35	124	144	55	57	130	143
RTOR Reduction (vph)	0	0	16	0	1	0	0	12	0	0	0	119
Lane Group Flow (vph)	89	579	97	48	644	0	124	187	0	57	130	24
Confl. Peds. (#/hr)	1					1						
Heavy Vehicles (%)	11%	4%	4%	3%	2%	15%	7%	6%	0%	4%	7%	6%
Turn Type	Perm	NA	Perm	Perm	NA		Perm	NA		Perm	NA	Perm
Protected Phases		2			6			4			8	
Permitted Phases	2		2	6			4			8		8
Actuated Green, G (s)	86.6	86.6	86.6	86.6	86.6		20.4	20.4		20.4	20.4	20.4
Effective Green, g (s)	86.6	86.6	86.6	86.6	86.6		20.4	20.4		20.4	20.4	20.4
Actuated g/C Ratio	0.72	0.72	0.72	0.72	0.72		0.17	0.17		0.17	0.17	0.17
Clearance Time (s)	7.0	7.0	7.0	7.0	7.0		6.0	6.0		6.0	6.0	6.0
Vehicle Extension (s)	5.0	5.0	5.0	5.0	5.0		5.0	5.0		5.0	5.0	5.0
Lane Grp Cap (vph)	448	1318	1120	533	1322		185	296		134	301	259
v/s Ratio Prot		0.32			c0.35			0.11			0.07	
v/s Ratio Perm	0.14		0.06	0.06			c0.11			0.07		0.02
v/c Ratio	0.20	0.44	0.09	0.09	0.49		0.67	0.63		0.43	0.43	0.09
Uniform Delay, d1	5.4	6.8	5.0	5.0	7.2		46.6	46.3		44.6	44.6	42.0
Progression Factor	1.12	1.30	1.19	1.00	1.00		1.00	1.00		1.00	1.00	1.00
Incremental Delay, d2	0.7	0.8	0.1	0.3	1.3		11.8	6.0		4.5	2.1	0.3
Delay (s)	6.8	9.6	6.0	5.3	8.5		58.4	52.3		49.1	46.7	42.3
Level of Service	A	А	Α	Α	Α		E	D		D	D	D
Approach Delay (s)		8.8			8.2			54.6			45.2	
Approach LOS		А			A			D			D	
Intersection Summary												
HCM 2000 Control Delay			21.2	Н	CM 2000	Level of	Service		С			
HCM 2000 Volume to Capa	acity ratio		0.52									
Actuated Cycle Length (s)			120.0	S	um of lost	time (s)			13.0			
Intersection Capacity Utiliza	ation		87.8%	IC	CU Level o	of Service			E			
Analysis Period (min)			15									
<ul> <li>Critical Lana Croup</li> </ul>												

c Critical Lane Group

Uppers Quarry Traffic Impact Study TMIG

HCM Unsignalized Intersection Capacity Analysis 6: Thorold Townline Road & Beaverdams Road

<2025 Background> PM Peak Hour _____09-14-2021

	۶	-	$\mathbf{\hat{z}}$	4	←	•	•	Ť	1	1	Ŧ	~
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBF
Lane Configurations		\$			\$			¢			÷	
Sign Control		Stop			Stop			Stop			Stop	
Traffic Volume (vph)	27	213	16	43	192	21	32	338	26	20	229	41
Future Volume (vph)	27	213	16	43	192	21	32	338	26	20	229	41
Peak Hour Factor	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93
Hourly flow rate (vph)	29	229	17	46	206	23	34	363	28	22	246	44
Direction, Lane #	EB 1	WB 1	NB 1	SB 1								
Volume Total (vph)	275	275	425	312								
Volume Left (vph)	29	46	34	22								
Volume Right (vph)	17	23	28	44								
Hadj (s)	0.02	0.01	0.13	0.03								
Departure Headway (s)	7.5	7.5	7.0	7.3								
Degree Utilization, x	0.57	0.57	0.83	0.63								
Capacity (veh/h)	426	426	489	450								
Control Delay (s)	20.1	20.1	36.0	21.9								
Approach Delay (s)	20.1	20.1	36.0	21.9								
Approach LOS	С	С	E	С								
Intersection Summary												
Delay			25.8									
Level of Service			D									
Intersection Capacity Utilizat	tion		56.7%	IC	U Level o	of Service			В			
Analysis Period (min)			15									

HCM Unsignalized Intersection Capacity Analysis 7: Thorold Townline Road & Uppers Lane

<2025 Background> PM Peak Hour 09-14-2021

	✓	•	T.	1	×	Ŧ
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations	¥		1.			et.
Traffic Volume (veh/h)	0	0	323	0	0	297
Future Volume (Veh/h)	0	0	323	0	0	297
Sian Control	Stop		Free		-	Free
Grade	0%		0%			0%
Peak Hour Factor	0.91	0.91	0.91	0.91	0.91	0.91
Hourly flow rate (vph)	0	0	355	0	0	326
Pedestrians	Ů	Ŭ	000	, in the second se	Ŭ	020
Lane Width (m)						
Walking Speed (m/s)						
Percent Blockage						
Right turn flare (veh)						
Median type			None			None
Median storage veh)			110/10			110110
Instream signal (m)						
nX nlatoon unblocked						
vC. conflicting volume	681	355			355	
vC1_stage 1 conf vol	001	555			000	
vC2, stage 2 conf vol						
vCu, unblocked vol	681	355			355	
tC single (s)	6.4	62			4 1	
tC. 2 stage (s)	0.4	0.2			7.1	
tF (c)	3.5	33			22	
n0 queue free %	100	100			100	
cM canacity (yeh/h)	410	603			1215	
	413	033			1213	
Direction, Lane #	WB 1	NB 1	SB 1			
Volume Total	0	355	326			
Volume Left	0	0	0			
Volume Right	0	0	0			
cSH	1700	1700	1215			
Volume to Capacity	0.00	0.21	0.00			
Queue Length 95th (m)	0.0	0.0	0.0			
Control Delay (s)	0.0	0.0	0.0			
Lane LOS	A					
Approach Delay (s)	0.0	0.0	0.0			
Approach LOS	А					
Intersection Summary						
Average Delay			0.0			
Intersection Capacity Utiliz	zation		20.3%	IC	U Level o	f Service
Analysis Period (min)			15			

Uppers Quarry Traffic Impact Study TMIG

Synchro 10 Report

Uppers Quarry Traffic Impact Study TMIG

Timings		<2025 Total - Thorold Townline> AM Peak Hour										
1: Davis Road & Th	orold S	Stone F	Road								09-2	3-2021
	۶	-	$\mathbf{F}$	4	+	1	1	1	1	ţ	1	
Lane Group	EBL	EBT	EBR	WBL	WBT	NBL	NBT	NBR	SBL	SBT	SBR	
Lane Configurations	ľ	- <b>†</b> †	1	ľ	A	ľ	Ę	1	7	1	1	
Traffic Volume (vph)	21	948	274	87	1102	542	15	211	1	2	18	
Future Volume (vph)	21	948	274	87	1102	542	15	211	1	2	18	
Turn Type	Perm	NA	Perm	Perm	NA	Split	NA	Perm	Split	NA	Perm	
Protected Phases		2			6	4	4		8	8		
Permitted Phases	2		2	6				4			8	
Detector Phase	2	2	2	6	6	4	4	4	8	8	8	
Switch Phase												
Minimum Initial (s)	20.0	20.0	20.0	20.0	20.0	10.0	10.0	10.0	10.0	10.0	10.0	_
Minimum Split (s)	28.9	28.9	28.9	28.9	28.9	29.7	29.7	29.7	21.7	21.7	21.7	
Total Split (s)	58.0	58.0	58.0	58.0	58.0	40.0	40.0	40.0	22.0	22.0	22.0	
Total Split (%)	48.3%	48.3%	48.3%	48.3%	48.3%	33.3%	33.3%	33.3%	18.3%	18.3%	18.3%	
Yellow Time (s)	5.4	5.4	5.4	5.4	5.4	5.7	5.7	5.7	5./	5.7	5.7	
All-Red Time (S)	1.5	1.5	1.5	1.5	1.5	2.0	2.0	2.0	2.0	2.0	2.0	
Lost Time Adjust (s)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
	0.9	0.9	0.9	0.9	0.9	1.1	1.1	1.1	1.1	1.1	1.1	
Lead-Lag Ontimize?												
Recall Mode	C-Max	C-Max	C-Max	Max	Max	None	None	None	None	None	None	
Act Effct Green (s)	70.1	70.1	70.1	70.1	70.1	28.3	28.3	28.3	10.0	10.0	10.0	
Actuated g/C Ratio	0.58	0.58	0.58	0.58	0.58	0.24	0.24	0.24	0.08	0.08	0.08	
v/c Ratio	0.13	0.51	0.31	0.44	0.59	0.78	0.80	0.43	0.01	0.01	0.09	
Control Delay	19.3	18.3	6.0	33.5	24.8	58.2	59.7	7.2	51.0	51.0	0.9	
Queue Delay	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Total Delay	19.3	18.3	6.0	33.5	24.8	58.2	59.7	7.2	51.0	51.0	0.9	
LOS	В	В	А	С	С	E	E	А	D	D	А	
Approach Delay		15.6			25.4		44.7			7.7		
Approach LOS		В			С		D			А		
Intersection Summarv												
Cycle Length: 120												
Actuated Cycle Length: 120												
Offset: 0 (0%), Referenced to	o phase 2	EBTL. St	art of Gre	en								
Natural Cycle: 85		,										
Control Type: Actuated-Coor	rdinated											
Maximum v/c Ratio: 0.80												
Intersection Signal Delay: 26	5.1			I	ntersectio	n LOS: C						
Intersection Capacity Utilizat	ion 87.3%			10	CU Level	of Service	εE					
Analysis Period (min) 15												

Splits and Phases: 1: Davis Road & Thorold Stone Road

≠ø2 (R)	<b>◆</b> Ø4	<b>4</b> ∎ø8
58 s	40 s	22 s
<b>₩</b> Ø6		
58 s		

Uppers Quarry Traffic Impact Study TMIG

Synchro 10 Report

HCM Signalized Intersection Capacity Analysis<2025 Total - Thorold Townline> AM Peak Hour 1: Davis Road & Thorold Stone Road 09-23-2021

	٦	-	$\mathbf{F}$	4	←	•	•	Ť	۲	1	ŧ	~
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	ň	<b>^</b>	1	۲	A1⊅		۲	ę	1	۲	•	1
Traffic Volume (vph)	21	948	274	87	1102	6	542	15	211	1	2	18
Future Volume (vph)	21	948	274	87	1102	6	542	15	211	1	2	18
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Total Lost time (s)	6.9	6.9	6.9	6.9	6.9		7.7	7.7	7.7	7.7	7.7	7.7
Lane Util. Factor	1.00	0.95	1.00	1.00	0.95		0.95	0.95	1.00	1.00	1.00	1.00
Frpb, ped/bikes	1.00	1.00	1.00	1.00	1.00		1.00	1.00	0.99	1.00	1.00	0.99
Flpb, ped/bikes	1.00	1.00	1.00	1.00	1.00		1.00	1.00	1.00	1.00	1.00	1.00
Frt	1.00	1.00	0.85	1.00	1.00		1.00	1.00	0.85	1.00	1.00	0.85
Flt Protected	0.95	1.00	1.00	0.95	1.00		0.95	0.95	1.00	0.95	1.00	1.00
Satd. Flow (prot)	1640	3343	1442	1530	3336		1559	1553	1475	1388	1624	1337
Flt Permitted	0.17	1.00	1.00	0.22	1.00		0.95	0.95	1.00	0.95	1.00	1.00
Satd. Flow (perm)	289	3343	1442	358	3336		1559	1553	1475	1388	1624	1337
Peak-hour factor, PHF	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96
Adj. Flow (vph)	22	988	285	91	1148	6	565	16	220	1	2	19
RTOR Reduction (vph)	0	0	95	0	0	0	0	0	168	0	0	18
Lane Group Flow (vph)	22	988	190	91	1154	0	288	293	52	1	2	1
Confl. Peds. (#/hr)	1					1	1		1	1		1
Heavy Vehicles (%)	10%	8%	12%	18%	8%	30%	10%	28%	8%	30%	17%	19%
Turn Type	Perm	NA	Perm	Perm	NA		Split	NA	Perm	Split	NA	Perm
Protected Phases		2			6		4	4	-	8	8	
Permitted Phases	2		2	6					4			8
Actuated Green, G (s)	65.4	65.4	65.4	65.4	65.4		28.3	28.3	28.3	4.0	4.0	4.0
Effective Green, g (s)	65.4	65.4	65.4	65.4	65.4		28.3	28.3	28.3	4.0	4.0	4.0
Actuated g/C Ratio	0.55	0.55	0.55	0.55	0.55		0.24	0.24	0.24	0.03	0.03	0.03
Clearance Time (s)	6.9	6.9	6.9	6.9	6.9		7.7	7.7	7.7	7.7	7.7	7.7
Vehicle Extension (s)	3.0	3.0	3.0	3.0	3.0		4.5	4.5	4.5	4.5	4.5	4.5
Lane Grp Cap (vph)	157	1821	785	195	1818		367	366	347	46	54	44
v/s Ratio Prot		0.30			c0.35		0.18	c0.19		0.00	c0.00	
v/s Ratio Perm	0.08		0.13	0.25					0.04			0.00
v/c Ratio	0.14	0.54	0.24	0.47	0.63		0.78	0.80	0.15	0.02	0.04	0.01
Uniform Delay, d1	13.4	17.6	14.3	16.7	19.0		43.0	43.2	36.3	56.1	56.1	56.1
Progression Factor	1.00	1.00	1.00	1.35	1.27		1.00	1.00	1.00	1.00	1.00	1.00
Incremental Delay, d2	1.9	1.2	0.7	5.7	1.2		11.7	13.1	0.3	0.3	0.5	0.2
Delay (s)	15.3	18.8	15.0	28.2	25.4		54.7	56.3	36.7	56.4	56.6	56.3
Level of Service	В	В	В	С	С		D	E	D	E	E	E
Approach Delay (s)		17.9			25.6			50.3			56.4	
Approach LOS		В			С			D			E	
Intersection Summary												
HCM 2000 Control Delay			28.7	Н	CM 2000	Level of S	Service		С			
HCM 2000 Volume to Capa	acity ratio		0.66									
Actuated Cycle Length (s)	,		120.0	S	um of lost	time (s)			22.3			
Intersection Capacity Utiliza	ation		87.3%	IC	CU Level o	of Service			E			
Analysis Period (min)			15									

c Critical Lane Group

Uppers Quarry Traffic Impact Study TMIG

Timings 2 [.] Davis Road & Ni	anara F	- alls R	oad/Be	eaverd	<202 ams R	25 Tota load	al - Tho	orold T	ownline	e> AM Peak Hour 09-23-2021
2. Davis Road a Riv	<u>,</u>	-	<b>(</b>	<b>+</b>	1	1	1	ţ	~	
Lane Group	EBL	EBT	WBL	WBT	NBL	NBT	SBL	SBT	SBR	
Lane Configurations		4		4	5	<b>41</b> 2	۲	44	1	
Traffic Volume (vph)	110	31	34	17	16	473	82	240	44	
Future Volume (vph)	110	31	34	17	16	473	82	240	44	
Turn Type	Perm	NA	Perm	NA	Perm	NA	Perm	NA	Perm	
Protected Phases		2		6		4		8		
Permitted Phases	2		6		4		8		8	
Detector Phase	2	2	6	6	4	4	8	8	8	
Switch Phase										
Minimum Initial (s)	10.0	10.0	10.0	10.0	25.0	25.0	25.0	25.0	25.0	
Minimum Split (s)	38.1	38.1	38.1	38.1	32.0	32.0	32.0	32.0	32.0	
Total Split (s)	50.0	50.0	50.0	50.0	50.0	50.0	50.0	50.0	50.0	
Total Split (%)	50.0%	50.0%	50.0%	50.0%	50.0%	50.0%	50.0%	50.0%	50.0%	
Yellow Time (s)	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	
All-Red Time (s)	3.1	3.1	3.1	3.1	2.0	2.0	2.0	2.0	2.0	
Lost Time Adjust (s)		0.0		0.0	0.0	0.0	0.0	0.0	0.0	
Total Lost Time (s)		8.1		8.1	7.0	7.0	7.0	7.0	7.0	
Lead/Lag										
Lead-Lag Optimize?										
Recall Mode	C-Max	C-Max	Max	Max	None	None	None	None	None	
Act Effct Green (s)		57.5		57.5	27.4	27.4	27.4	27.4	27.4	
Actuated g/C Ratio		0.58		0.58	0.27	0.27	0.27	0.27	0.27	
v/c Ratio		0.25		0.24	0.07	0.65	0.51	0.31	0.11	
Control Delay		12.2		3.9	26.1	34.6	41.8	29.4	5.8	
Queue Delay		0.0		0.0	0.0	0.0	0.0	0.0	0.0	
Total Delay		12.2		3.9	26.1	34.6	41.8	29.4	5.8	
LOS		В		А	С	С	D	С	А	
Approach Delay		12.2		3.9		34.3		29.3		
Approach LOS		В		Α		С		С		
Intersection Summary										
Cycle Length: 100										
Actuated Cycle Length: 100										
Offset: 0 (0%), Referenced to	art of Gre									
Natural Cycle: 75										
Control Type: Actuated-Coor	rdinated									
Maximum v/c Ratio: 0.65										
Intersection Signal Delay: 25	Ir	ntersectio	n LOS: C							
Intersection Capacity Utilizat	tion 88.3%				CU Level	of Service	εE			
Analysis Period (min) 15										
Calife and Diseases C. D.	in Denal A	Manan /								
Spills and Phases: 2: Dav	puts and Phases: 2: Davis Road & Niagara Falls Road/Beaverdams Road									

→ _{Ø2 (R)}	< <b>↑</b> Ø4	
50 s	50 s	
€ Ø6		
F.A.	<b>F</b> A	

Synchro 10 Report

 HCM Signalized Intersection Capacity Analysis
 2025 Total - Thorold Townline> AM Peak Hour

 2: Davis Road & Niagara Falls Road/Beaverdams Road
 09-23-2021

	≯	-	$\mathbf{r}$	1	-	•	1	1	1	1	Ŧ	-
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		4			4		ሻ	<b>4</b> 12		5	44	1
Traffic Volume (vph)	110	31	12	34	17	166	16	473	59	82	240	44
Future Volume (vph)	110	31	12	34	17	166	16	473	59	82	240	44
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Total Lost time (s)		8.1			8.1		7.0	7.0		7.0	7.0	7.0
Lane Util. Factor		1.00			1.00		1.00	0.95		1.00	0.95	1.00
Frt		0.99			0.90		1.00	0.98		1.00	1.00	0.85
Flt Protected		0.97			0.99		0.95	1.00		0.95	1.00	1.00
Satd. Flow (prot)		1662			1632		1388	3111		1787	2983	1392
Flt Permitted		0.66			0.94		0.60	1.00		0.33	1.00	1.00
Satd. Flow (perm)		1136			1538		870	3111		613	2983	1392
Peak-hour factor, PHF	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95
Adj. Flow (vph)	116	33	13	36	18	175	17	498	62	86	253	46
RTOR Reduction (vph)	0	2	0	0	74	0	0	12	0	0	0	33
Lane Group Flow (vph)	0	160	0	0	155	0	17	548	0	86	253	13
Heavy Vehicles (%)	10%	7%	7%	7%	12%	2%	30%	15%	7%	1%	21%	16%
Turn Type	Perm	NA		Perm	NA		Perm	NA		Perm	NA	Perm
Protected Phases		2			6			4			8	
Permitted Phases	2			6			4			8		8
Actuated Green, G (s)		57.5			57.5		27.4	27.4		27.4	27.4	27.4
Effective Green, g (s)		57.5			57.5		27.4	27.4		27.4	27.4	27.4
Actuated g/C Ratio		0.58			0.58		0.27	0.27		0.27	0.27	0.27
Clearance Time (s)		8.1			8.1		7.0	7.0		7.0	7.0	7.0
Vehicle Extension (s)		3.0			3.0		5.0	5.0		5.0	5.0	5.0
Lane Grp Cap (vph)		653			884		238	852		167	817	381
v/s Ratio Prot								c0.18			0.08	
v/s Ratio Perm		c0.14			0.10		0.02			0.14		0.01
v/c Ratio		0.24			0.17		0.07	0.64		0.51	0.31	0.03
Uniform Delay, d1		10.5			10.0		26.9	32.0		30.7	28.8	26.6
Progression Factor		1.00			1.00		1.00	1.00		1.00	1.00	1.00
Incremental Delay, d2		0.9			0.4		0.3	2.3		5.3	0.5	0.1
Delay (s)		11.4			10.5		27.1	34.3		35.9	29.3	26.7
Level of Service		В			В		С	С		D	С	С
Approach Delay (s)		11.4			10.5			34.1			30.4	
Approach LOS		В			В			С			С	
Intersection Summary												
HCM 2000 Control Delay			26.3	Н	CM 2000	Level of	Service		С			
HCM 2000 Volume to Capacity	ratio		0.37									
Actuated Cycle Length (s)			100.0	S	um of los	t time (s)			15.1			
Intersection Capacity Utilization	I		88.3%	IC	U Level	of Service			E			
Analysis Period (min)			15									
c Critical Lane Group												

Uppers Quarry Traffic Impact Study TMIG

Timings 3: Davis Road & Lu	undvs L			<2025 Total - Thorold Townline> AM Peak Hour 09-23-2021							
	۶	<b>→</b>	4	+	×	1	1	1	ţ	~	
Lane Group	EBL	EBT	WBL	WBT	WBR	NBL	NBT	SBL	SBT	SBR	
Lane Configurations	ľ	¢Î	ľ	•	1	ľ	ĥ	ľ	•	1	
Traffic Volume (vph)	140	520	36	397	233	22	139	181	94	143	
Future Volume (vph)	140	520	36	397	233	22	139	181	94	143	
Turn Type	Perm	NA	Perm	NA	Perm	Perm	NA	Perm	NA	Perm	
Protected Phases		2		6			4		8		
Permitted Phases	2		6		6	4		8		8	
Detector Phase	2	2	6	6	6	4	4	8	8	8	
Switch Phase											
Minimum Initial (s)	22.0	22.0	22.0	22.0	22.0	15.0	15.0	15.0	15.0	15.0	
Minimum Split (s)	36.0	36.0	36.0	36.0	36.0	32.0	32.0	32.0	32.0	32.0	
Total Split (s)	52.0	52.0	52.0	52.0	52.0	38.0	38.0	38.0	38.0	38.0	
Total Split (%)	57.8%	57.8%	57.8%	57.8%	57.8%	42.2%	42.2%	42.2%	42.2%	42.2%	
Yellow Time (s)	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	
All-Red Time (s)	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	
Lost Time Adjust (s)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Total Lost Time (s)	7.0	7.0	7.0	7.0	7.0	7.0	7.0	7.0	7.0	7.0	
Lead/Lag											
Lead-Lag Optimize?											
Recall Mode	C-Max	C-Max	Мах	Max	Max	None	None	None	None	None	
Act Effct Green (s)	54.2	54.2	54.2	54.2	54.2	21.8	21.8	21.8	21.8	21.8	
Actuated g/C Ratio	0.60	0.60	0.60	0.60	0.60	0.24	0.24	0.24	0.24	0.24	
v/c Ratio	0.30	0.52	0.11	0.40	0.26	0.09	0.46	0.78	0.27	0.34	
Control Delay	12.4	13.8	10.9	12.1	2.3	24.1	29.8	51.7	27.6	6.1	
Queue Delav	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Total Delay	12.4	13.8	10.9	12.1	2.3	24.1	29.8	51.7	27.6	6.1	
LOS	В	В	В	В	A	С	С	D	C	A	
Approach Delay		13.5		8.6		-	29.1		30.7		
Approach LOS		В		A			С		С		
Intersection Summary											
Cycle Length: 90											
Actuated Cycle Length: 90											
Offset: 0 (0%) Referenced to phase 2 FBTL Start of Green											
Natural Cycle: 70		,									
Control Type: Actuated-Coc	ordinated										
Maximum v/c Ratio: 0.78											
Intersection Signal Delay: 1	7.0			Ir	ntersectio	n LOS: B					
Intersection Capacity Utiliza	tion 95.1%			IC	CU Level	of Service	9 F				
Analysis Period (min) 15											
Splits and Phases: 3: Day	vis Road &	Lundys L	ane								
Ø2 (R)							Ø4				

- → Ø2 (R)	<b>™</b> ø₄	
52 s	38 s	
<b>∲</b> Ø6	Ø8	
52 s	38 s	

Synchro 10 Report

 HCM Signalized Intersection Capacity Analysis<2025 Total - Thorold Townline> AM Peak Hour

 3: Davis Road & Lundys Lane

	٦	-	$\mathbf{r}$	4	+	•	٩	Ť	۲	1	Ŧ	~
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	۲.	¢Î,		۲	•	1	۲.	f,		ň	•	1
Traffic Volume (vph)	140	520	18	36	397	233	22	139	24	181	94	143
Future Volume (vph)	140	520	18	36	397	233	22	139	24	181	94	143
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Total Lost time (s)	7.0	7.0		7.0	7.0	7.0	7.0	7.0		7.0	7.0	7.0
Lane Util. Factor	1.00	1.00		1.00	1.00	1.00	1.00	1.00		1.00	1.00	1.00
Frpb, ped/bikes	1.00	1.00		1.00	1.00	1.00	1.00	1.00		1.00	1.00	1.00
Flpb, ped/bikes	1.00	1.00		1.00	1.00	1.00	1.00	1.00		1.00	1.00	1.00
Frt	1.00	1.00		1.00	1.00	0.85	1.00	0.98		1.00	1.00	0.85
Flt Protected	0.95	1.00		0.95	1.00	1.00	0.95	1.00		0.95	1.00	1.00
Satd. Flow (prot)	1656	1825		1467	1743	1442	1444	1529		1530	1532	1392
Flt Permitted	0.48	1.00		0.37	1.00	1.00	0.69	1.00		0.64	1.00	1.00
Satd. Flow (perm)	834	1825		570	1743	1442	1052	1529		1028	1532	1392
Peak-hour factor, PHF	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94
Adj. Flow (vph)	149	553	19	38	422	248	23	148	26	193	100	152
RTOR Reduction (vph)	0	1	0	0	0	99	0	8	0	0	0	115
Lane Group Flow (vph)	149	571	0	38	422	149	23	166	0	193	100	37
Confl. Peds. (#/hr)			1	1								
Heavy Vehicles (%)	9%	3%	19%	23%	9%	12%	25%	20%	30%	18%	24%	16%
Turn Type	Perm	NA		Perm	NA	Perm	Perm	NA		Perm	NA	Perm
Protected Phases		2			6			4			8	
Permitted Phases	2			6		6	4			8		8
Actuated Green, G (s)	54.2	54.2		54.2	54.2	54.2	21.8	21.8		21.8	21.8	21.8
Effective Green, g (s)	54.2	54.2		54.2	54.2	54.2	21.8	21.8		21.8	21.8	21.8
Actuated g/C Ratio	0.60	0.60		0.60	0.60	0.60	0.24	0.24		0.24	0.24	0.24
Clearance Time (s)	7.0	7.0		7.0	7.0	7.0	7.0	7.0		7.0	7.0	7.0
Vehicle Extension (s)	4.0	4.0		4.0	4.0	4.0	2.0	2.0		2.0	2.0	2.0
Lane Grp Cap (vph)	502	1099		343	1049	868	254	370		249	371	337
v/s Ratio Prot		c0.31			0.24			0.11			0.07	
v/s Ratio Perm	0.18			0.07		0.10	0.02			c0.19		0.03
v/c Ratio	0.30	0.52		0.11	0.40	0.17	0.09	0.45		0.78	0.27	0.11
Uniform Delay, d1	8.7	10.4		7.6	9.4	7.9	26.4	29.0		31.8	27.6	26.5
Progression Factor	1.00	1.00		1.00	1.00	1.00	1.00	1.00		1.00	1.00	1.00
Incremental Delay, d2	1.5	1.8		0.7	1.1	0.4	0.1	0.3		12.8	0.1	0.1
Delay (s)	10.2	12.1		8.3	10.5	8.4	26.5	29.3		44.6	27.8	26.6
Level of Service	В	В		А	В	Α	С	С		D	С	С
Approach Delay (s)		11.7			9.7			29.0			34.7	
Approach LOS		В			A			С			С	
Intersection Summary												
HCM 2000 Control Delay			17.6	Н	CM 2000	Level of S	Service		В			
HCM 2000 Volume to Capa	acity ratio		0.59									
Actuated Cycle Length (s)			90.0	S	um of los	t time (s)			14.0			
Intersection Capacity Utilization	ation		95.1%	IC	CU Level of	of Service			F			
Analysis Period (min)			15									
<ul> <li>Oritical Lana Crown</li> </ul>												

c Critical Lane Group

Uppers Quarry Traffic Impact Study TMIG

	٠	-	$\mathbf{r}$	1	-	•	1	Ť	•	Ŧ	
Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	SBL	SBT	
Lane Configurations	ሻ	- <b>†</b> †	1	ሻ	<u></u>	1	٦	4Î	ሻ	ĥ	
Traffic Volume (vph)	323	659	114	124	807	73	108	150	52	154	
Future Volume (vph)	323	659	114	124	807	73	108	150	52	154	
Turn Type	pm+pt	NA	Perm	pm+pt	NA	Perm	pm+pt	NA	Perm	NA	
Protected Phases	5	2		1	6		7	4		8	
Permitted Phases	2		2	6		6	4		8		
Detector Phase	5	2	2	1	6	6	7	4	8	8	
Switch Phase											
Vinimum Initial (s)	8.0	10.0	10.0	8.0	10.0	10.0	8.0	10.0	10.0	10.0	
Minimum Split (s)	11.0	35.1	35.1	12.5	35.1	35.1	11.0	41.4	41.4	41.4	
Total Split (s)	27.0	43.0	43.0	20.0	36.0	36.0	14.0	57.0	43.0	43.0	
Total Split (%)	22.5%	35.8%	35.8%	16.7%	30.0%	30.0%	11.7%	47.5%	35.8%	35.8%	
Yellow Time (s)	3.0	4.1	4.1	3.0	4.1	4.1	3.0	4.1	4.1	4.1	
All-Red Time (s)	0.0	2.0	2.0	0.0	2.0	2.0	0.0	2.3	2.3	2.3	
ost Time Adjust (s)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Total Lost Time (s)	3.0	6.1	6.1	3.0	6.1	6.1	3.0	6.4	6.4	6.4	
_ead/Lag	Lead	Lag	Lag	Lead	Lag	Lag	Lead		Lag	Lag	
Lead-Lag Optimize?	Yes	Yes	Yes	Yes	Yes	Yes	Yes		Yes	Yes	
Recall Mode	None	C-Max	C-Max	None	C-Max	C-Max	None	None	None	None	
Act Effct Green (s)	66.3	49.0	49.0	53.2	38.9	38.9	47.7	44.3	30.9	30.9	
Actuated g/C Ratio	0.55	0.41	0.41	0.44	0.32	0.32	0.40	0.37	0.26	0.26	
//c Ratio	0.87	0.48	0.21	0.40	0.74	0.14	0.54	0.43	0.20	0.90	
Control Delay	62.5	42.4	23.4	20.0	43.2	2.7	32.0	26.7	34.4	60.6	
Queue Delay	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Total Delay	62.5	42.4	23.4	20.0	43.2	2.7	32.0	26.7	34.4	60.6	
LOS	E	D	С	С	D	А	С	С	С	Е	
Approach Delav		46.4			37.4			28.4		57.3	
Approach LOS		D			D			С		E	
ntersection Summary											
Cycle Length: 120											
Actuated Cycle Length: 120											
Offset: 0 (0%), Referenced t	o phase 2:	EBTL and	d 6:WBTL	. Start of	Green						
Vatural Cycle: 100											
Control Type: Actuated-Coo	rdinated										
/laximum v/c Ratio: 0.90											
ntersection Signal Delay: 42	2.7			Ir	ntersection	n LOS: D					
ntersection Capacity Utilizat	tion 86.5%			10	CU Level	of Service	Ε				
Analysis Period (min) 15											

opilis and Fliases.	. Thoroid Town	
		<b>+</b>

Ø1		<b>√</b> 04	
20 s	43 s	57 s	
▶ Ø2	Ø6 (R)	★ Ø7	
27 s	36 s	14 s 43 s	

Synchro 10 Report

 HCM Signalized Intersection Capacity Analysis<2025 Total - Thorold Townline> AM Peak Hour

 4: Thorold Townline Road & Thorold Stone Road

 09-23-2021

	٦	-	$\mathbf{i}$	4	+	*	1	Ť	۲	1	Ŧ	~
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	٦	44	1	٦	44	1	ሻ	1.		5	î,	
Traffic Volume (vph)	323	659	114	124	807	73	108	150	71	52	154	205
Future Volume (vph)	323	659	114	124	807	73	108	150	71	52	154	205
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Total Lost time (s)	3.0	6.1	6.1	3.0	6.1	6.1	3.0	6.4		6.4	6.4	
Lane Util. Factor	1.00	0.95	1.00	1.00	0.95	1.00	1.00	1.00		1.00	1.00	
Frpb, ped/bikes	1.00	1.00	1.00	1.00	1.00	0.97	1.00	1.00		1.00	1.00	
Flpb, ped/bikes	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00		1.00	1.00	
Frt	1.00	1.00	0.85	1.00	1.00	0.85	1.00	0.95		1.00	0.91	
Flt Protected	0.95	1.00	1.00	0.95	1.00	1.00	0.95	1.00		0.95	1.00	
Satd. Flow (prot)	1641	3471	1252	1378	3505	1453	1318	1393		1641	1453	
Flt Permitted	0.15	1.00	1.00	0.37	1.00	1.00	0.22	1.00		0.62	1.00	
Satd. Flow (perm)	257	3471	1252	543	3505	1453	307	1393		1063	1453	
Peak-hour factor, PHF	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96
Adi, Flow (vph)	336	686	119	129	841	76	112	156	74	54	160	214
RTOR Reduction (vph)	0	0	62	0	0	51	0	16	0	0	43	0
Lane Group Flow (vph)	336	686	57	129	841	25	113	214	0	54	331	0
Confl. Peds. (#/hr)	4					4						
Heavy Vehicles (%)	10%	4%	29%	31%	3%	8%	37%	24%	42%	10%	23%	17%
Turn Type	pm+pt	NA	Perm	pm+pt	NA	Perm	pm+pt	NA		Perm	NA	
Protected Phases	5	2		1	6		7	4			8	
Permitted Phases	2		2	6		6	4			8		
Actuated Green, G (s)	63.2	49.0	49.0	50.1	38.9	38.9	44.3	44.3		30.9	30.9	
Effective Green, g (s)	63.2	49.0	49.0	50.1	38.9	38.9	44.3	44.3		30.9	30.9	
Actuated g/C Ratio	0.53	0.41	0.41	0.42	0.32	0.32	0.37	0.37		0.26	0.26	
Clearance Time (s)	3.0	6.1	6.1	3.0	6.1	6.1	3.0	6.4		6.4	6.4	
Vehicle Extension (s)	2.5	6.0	6.0	2.5	6.0	6.0	2.5	2.3		2.3	2.3	
Lane Grp Cap (vph)	381	1417	511	304	1136	471	200	514		273	374	
v/s Ratio Prot	c0.16	0.20		0.04	0.24		c0.05	0.15			c0.23	
v/s Ratio Perm	c0.31		0.05	0.14		0.02	0.16			0.05		
v/c Ratio	0.88	0.48	0.11	0.42	0.74	0.05	0.56	0.42		0.20	0.88	
Uniform Delay, d1	27.7	26.2	22.0	22.5	36.1	27.9	28.1	28.2		34.9	42.8	
Progression Factor	1.78	1.46	3.09	1.00	1.00	1.00	1.00	1.00		1.00	1.00	
Incremental Delay, d2	18.6	1.1	0.4	0.7	4.4	0.2	2.9	0.3		0.2	21.0	
Delay (s)	67.9	39.2	68.4	23.2	40.4	28.1	31.0	28.5		35.1	63.8	
Level of Service	E	D	E	С	D	С	С	С		D	E	
Approach Delay (s)		50.7			37.4			29.4			60.2	
Approach LOS		D			D			С			E	
Intersection Summary												
HCM 2000 Control Delay			44.9	Н	CM 2000	Level of	Service		D			
HCM 2000 Volume to Cap	acity ratio		0.87									
Actuated Cycle Length (s)			120.0	S	um of los	t time (s)			18.5			
Intersection Capacity Utiliz	ation		86.5%	IC	U Level	of Service	3		E			
Analysis Period (min)			15									
- Oritical Lana Origina												

c Critical Lane Group

Uppers Quarry Traffic Impact Study TMIG

Timings 5: Thorold Townline	ine	<2025 Total - Thorold Townline> AM Peak Hour 09-23-2021									
	٠	-	`	4	+	1	t	1	ţ	~	
Lane Group	EBL	EBT	EBR	WBL	WBT	NBL	NBT	SBL	SBT	SBR	
Lane Configurations	ľ	•	1	ľ	ĥ	ľ	eî Î	ľ	•	1	
Traffic Volume (vph)	159	521	98	38	348	71	140	23	85	58	
Future Volume (vph)	159	521	98	38	348	71	140	23	85	58	
Turn Type	Perm	NA	Perm	Perm	NA	Perm	NA	Perm	NA	Perm	
Protected Phases		2			6		4		8		
Permitted Phases	2		2	6		4		8		8	
Detector Phase	2	2	2	6	6	4	4	8	8	8	
Switch Phase											
Minimum Initial (s)	20.0	20.0	20.0	20.0	20.0	10.0	10.0	10.0	10.0	10.0	
Minimum Split (s)	29.0	29.0	29.0	29.0	29.0	35.0	35.0	35.0	35.0	35.0	
Total Split (s)	65.0	65.0	65.0	65.0	65.0	35.0	35.0	35.0	35.0	35.0	
Total Split (%)	65.0%	65.0%	65.0%	65.0%	65.0%	35.0%	35.0%	35.0%	35.0%	35.0%	
Yellow Time (s)	5.0	5.0	5.0	5.0	5.0	4.0	4.0	4.0	4.0	4.0	
All-Red Time (s)	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	
Lost Time Adjust (s)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Total Lost Time (s)	7.0	7.0	7.0	7.0	7.0	6.0	6.0	6.0	6.0	6.0	
Lead/Lag											
Lead-Lag Optimize?	0.14	0.14	0.14						N		
Recall Mode	C-Max	C-Max	C-Max	Max	Max	None	None	None	None	None	
Act Effect Green (s)	68.8	68.8	68.8	68.8	68.8	18.2	18.2	18.2	18.2	18.2	
Actuated g/C Ratio	0.09	0.69	0.69	0.69	0.69	0.18	0.18	0.18	0.18	0.18	
V/C Katio	0.30	0.45	0.10	0.08	0.34	0.35	0.03	0.15	0.31	0.22	
Oucus Delay	0.0	9.2	3.0	0.9	1.0	30.0	43.0	34.3	30.0	10.5	
Queue Delay	0.0	0.0	0.0	0.0	0.0	20.0	12.0	24.2	26.6	10.2	
	0.0	9.2	5.0	0.9	7.0	J0.0	43.0	34.5	JU.U	10.3 D	
Approach Delay	A	8.5	A	A	77	U	12.1	U	27.1	D	
Approach LOS		0.5			Δ		42.4 D		21.1		
Appidadii 200		Л			7				0		
Intersection Summary											
Cycle Length: 100											
Actuated Cycle Length: 100											
Offset: 0 (0%), Referenced to	phase 2	EBTL, St	art of Gre	en							
Natural Cycle: 65											
Control Type: Actuated-Coor	dinated										
Maximum v/c Ratio: 0.63											
Intersection Signal Delay: 15	.4			Ir	ntersectio	n LOS: B					
Intersection Capacity Utilizati	ion 79.9%			10	JU Level	of Service	θD				
The second se											
Analysis Period (min) 15											

↓	1 Ø4	
65 s	35 s	
₹ Ø6		
65 s	35 s	

Synchro 10 Report

 HCM Signalized Intersection Capacity Analysis<2025 Total - Thorold Townline > AM Peak Hour

 5: Thorold Townline Road & Lundys Lane

 09-23-2021

	٦	-	$\mathbf{\hat{v}}$	4	←	*	1	t	۲	1	Ŧ	~
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	ň	*	1	٢	ĥ		٢	î,		ň	•	1
Traffic Volume (vph)	159	521	98	38	348	40	71	140	37	23	85	58
Future Volume (vph)	159	521	98	38	348	40	71	140	37	23	85	58
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Total Lost time (s)	7.0	7.0	7.0	7.0	7.0		6.0	6.0		6.0	6.0	6.0
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00		1.00	1.00		1.00	1.00	1.00
Frpb. ped/bikes	1.00	1.00	1.00	1.00	1.00		1.00	1.00		1.00	1.00	1.00
Flpb, ped/bikes	1.00	1.00	1.00	1.00	1.00		1.00	1.00		1.00	1.00	1.00
Frt	1.00	1.00	0.85	1.00	0.98		1.00	0.97		1.00	1.00	0.85
Flt Protected	0.95	1.00	1.00	0.95	1.00		0.95	1.00		0.95	1.00	1.00
Satd, Flow (prot)	1581	1810	1495	1752	1771		1612	1607		1671	1638	1252
Flt Permitted	0.50	1.00	1.00	0.41	1.00		0.70	1.00		0.51	1.00	1.00
Satd, Flow (perm)	833	1810	1495	752	1771		1184	1607		893	1638	1252
Peak-hour factor PHF	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93
Adi Flow (vph)	171	560	105	41	374	43	76	151	40	25	91	62
RTOR Reduction (vph)	0	0	17	0	3	0	0	11	0	0	0	51
Lane Group Flow (vph)	171	560	88	41	414	0	76	180	0	25	91	11
Confl Peds (#/hr)	1	000	00			1		100	, in the second s	20	0.	
Heavy Vehicles (%)	14%	5%	8%	3%	6%	0%	12%	17%	5%	8%	16%	29%
Turn Type	Perm	NA	Perm	Perm	NA		Perm	NA		Perm	NA	Perm
Protected Phases		2		-	6		-	4		-	8	
Permitted Phases	2		2	6			4			8		8
Actuated Green, G (s)	68.8	68.8	68.8	68.8	68.8		18.2	18.2		18.2	18.2	18.2
Effective Green, q (s)	68.8	68.8	68.8	68.8	68.8		18.2	18.2		18.2	18.2	18.2
Actuated q/C Ratio	0.69	0.69	0.69	0.69	0.69		0.18	0.18		0.18	0.18	0.18
Clearance Time (s)	7.0	7.0	7.0	7.0	7.0		6.0	6.0		6.0	6.0	6.0
Vehicle Extension (s)	5.0	5.0	5.0	5.0	5.0		5.0	5.0		5.0	5.0	5.0
Lane Grp Cap (vph)	573	1245	1028	517	1218		215	292		162	298	227
v/s Ratio Prot		c0.31			0.23			c0.11			0.06	
v/s Ratio Perm	0.21		0.06	0.05			0.06			0.03		0.01
v/c Ratio	0.30	0.45	0.09	0.08	0.34		0.35	0.62		0.15	0.31	0.05
Uniform Delay, d1	6.1	7.0	5.2	5.1	6.4		35.8	37.7		34.4	35.4	33.8
Progression Factor	1.00	1.00	1.00	1.00	1.00		1.00	1.00		1.00	1.00	1.00
Incremental Delay, d2	1.3	1.2	0.2	0.3	0.8		2.1	5.5		0.9	1.2	0.2
Delay (s)	7.5	8.2	5.3	5.4	7.1		37.8	43.2		35.4	36.6	34.0
Level of Service	А	А	А	А	А		D	D		D	D	С
Approach Delay (s)		7.7			7.0			41.7			35.5	
Approach LOS		А			Α			D			D	
Intersection Summary												
HCM 2000 Control Delay			15.6	Н	CM 2000	Level of S	Service		В			
HCM 2000 Volume to Capa	acity ratio		0.48									
Actuated Cycle Length (s)			100.0	S	um of lost	time (s)			13.0			
Intersection Capacity Utiliza	ation		79.9%	IC	U Level o	of Service			D			
Analysis Period (min)			15									
a Critical Lana Crown												

c Critical Lane Group

Uppers Quarry Traffic Impact Study TMIG

Timings <2025 Total - Thorold Townline> AM Peak Hour 6: Thorold Townline Road & Beaverdams Road 09-23-2021										
	<u>)</u>	<u>→</u>	<ul> <li>Image: A state of the state of</li></ul>	<b>+</b>	1	t	4	ţ		
Lane Group	EBL	EBT	WBL	WBT	NBL	NBT	SBL	SBT		
Lane Configurations		4		4		4		4		
Traffic Volume (vph)	19	139	17	175	24	311	11	364		
Future Volume (vph)	19	139	17	175	24	311	11	364		
Turn Type	Perm	NA	Perm	NA	Perm	NA	Perm	NA		
Protected Phases		2		6		4		8		
Permitted Phases	2		6		4		8			
Detector Phase	2	2	6	6	4	4	8	8		
Switch Phase										
Minimum Initial (s)	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0		
Minimum Split (s)	30.5	30.5	30.5	30.5	34.0	34.0	30.5	30.5		
Total Split (s)	31.0	31.0	31.0	31.0	59.0	59.0	59.0	59.0		
Total Split (%)	34.4%	34.4%	34.4%	34.4%	65.6%	65.6%	65.6%	65.6%		
Yellow Time (s)	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0		
All-Red Time (s)	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0		
Lost Time Adjust (s)		0.0		0.0		0.0		0.0		
Total Lost Time (s)		6.0		6.0		6.0		6.0		
Lead/Lag										
Lead-Lag Optimize?										
Recall Mode	C-Max	C-Max	Max	Max	Max	Max	Max	Max		
Act Effct Green (s)		25.0		25.0		53.0		53.0		
Actuated g/C Ratio		0.28		0.28		0.59		0.59		
v/c Ratio		0.39		0.46		0.48		0.50		
Control Delay		28.5		29.8		12.7		13.1		
Queue Delay		0.0		0.0		0.0		0.0		
I otal Delay		28.5		29.8		12.7		13.1		
LOS		C		C		B		B		
Approach Delay		28.5		29.8		12.7		13.1		
Approach LOS		C		C		В		В		
Intersection Summary										
Cycle Length: 90										
Actuated Cycle Length: 90										
Offset: 0 (0%), Referenced t	to phase 2	EBTL, St	art of Gre	en						
Natural Cycle: 65										
Control Type: Actuated-Coo	rdinated									
Maximum v/c Ratio: 0.50										
Intersection Signal Delay: 18	8.4			I	ntersectio	n LOS: B				
Intersection Capacity Utiliza	tion 57.9%			10	CU Level	of Service	e B			
Analysis Period (min) 15										
Splits and Phases: 6: Tho	orold Town	line Road	& Beave	rdams Ro	ad					

J → Ø2 (R)		
31 s	59 s	
<b>₩</b> Ø6	Øs	
31 s	59 s	

Synchro 10 Report

 HCM Signalized Intersection Capacity Analysis<2025 Total - Thorold Townline > AM Peak Hour

 6: Thorold Townline Road & Beaverdams Road

	۶	-	$\mathbf{\hat{z}}$	4	+	۰.	٩.	Ť	۲	1	Ŧ	~
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		\$			\$			\$			4	
Traffic Volume (vph)	19	139	16	17	175	22	24	311	33	11	364	19
Future Volume (vph)	19	139	16	17	175	22	24	311	33	11	364	19
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Total Lost time (s)		6.0			6.0			6.0			6.0	
Lane Util. Factor		1.00			1.00			1.00			1.00	
Frpb, ped/bikes		1.00			1.00			1.00			1.00	
Flpb, ped/bikes		1.00			1.00			1.00			1.00	
Frt		0.99			0.99			0.99			0.99	
Flt Protected		0.99			1.00			1.00			1.00	
Satd. Flow (prot)		1808			1846			1462			1476	
Flt Permitted		0.95			0.97			0.96			0.99	
Satd. Flow (perm)		1723			1794			1407			1459	
Peak-hour factor, PHF	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Adj. Flow (vph)	21	151	17	18	190	24	26	338	36	12	396	21
RTOR Reduction (vph)	0	4	0	0	4	0	0	4	0	0	2	0
Lane Group Flow (vph)	0	185	0	0	228	0	0	396	0	0	427	0
Confl. Peds. (#/hr)			5	5			6					6
Heavy Vehicles (%)	5%	2%	9%	0%	1%	2%	0%	33%	0%	9%	29%	9%
Turn Type	Perm	NA		Perm	NA		Perm	NA		Perm	NA	
Protected Phases		2			6			4			8	
Permitted Phases	2			6			4			8		
Actuated Green, G (s)		25.0			25.0			53.0			53.0	
Effective Green, g (s)		25.0			25.0			53.0			53.0	
Actuated g/C Ratio		0.28			0.28			0.59			0.59	
Clearance Time (s)		6.0			6.0			6.0			6.0	
Vehicle Extension (s)		5.0			5.0			5.0			5.0	
Lane Grp Cap (vph)		478			498			828			859	
v/s Ratio Prot												
v/s Ratio Perm		0.11			c0.13			0.28			c0.29	
v/c Ratio		0.39			0.46			0.48			0.50	
Uniform Delay, d1		26.3			26.9			10.6			10.8	
Progression Factor		1.00			1.00			1.00			1.00	
Incremental Delay, d2		2.4			3.0			2.0			2.1	
Delay (s)		28.7			29.9			12.6			12.8	
Level of Service		С			С			В			В	
Approach Delay (s)		28.7			29.9			12.6			12.8	
Approach LOS		С			С			В			В	
Intersection Summary												
HCM 2000 Control Delay			18.3	Н	CM 2000	Level of S	Service		В			
HCM 2000 Volume to Capaci	ty ratio		0.48									
Actuated Cycle Length (s)	,		90.0	S	um of lost	time (s)			12.0			
Intersection Capacity Utilizati	on		57.9%	IC	U Level o	of Service			В			
Analysis Period (min)			15									

c Critical Lane Group

Uppers Quarry Traffic Impact Study TMIG

7: Thorold Townlin	e Road	& Upp	ers La	y Anar ne	ysizuz	5 TOLAT	- 11101010 10W11111e> Alvi Peak Hour 09-23-2021
	4	•	Ť	*	*	Ļ	
Movement	WBL	WBR	NBT	NBR	SBL	SBT	
Lane Configurations	Y		4Î		۲	1	
Traffic Volume (veh/h)	3	66	323	3	46	256	
Future Volume (Veh/h)	3	66	323	3	46	256	
Sign Control	Stop		Free			Free	
Grade	0%		0%			0%	
Peak Hour Factor	0.93	0.93	0.93	0.93	0.93	0.93	
Hourly flow rate (vph)	3	71	347	3	49	275	
Pedestrians							
Lane Width (m)							
Walking Speed (m/s)							
Percent Blockage							
Right turn flare (veh)							
Median type			None			None	
Median storage veh)							
Upstream signal (m)							
pX_platoon unblocked							
vC conflicting volume	722	348			350		
vC1_stage 1 conf vol		0.0			000		
vC2_stage 2 conf vol							
vCu_unblocked vol	722	348			350		
tC single (s)	6.4	7 1			49		
tC, 2 stage (s)	0.1	7.1			4.0		
tE (s)	3.5	41			29		
n0 queue free %	99	87			94		
cM capacity (veh/h)	375	537			870		
Direction Lane #	WB 1	NR 1	SB 1	SB 2			
Volume Total	74	350	19	275			
Volume Left	3	0.00	40	215			
Volume Right	71	3		0			
cSH	528	1700	870	1700			
Volume to Canacity	0 14	0.21	0.06	0.16			
Queue Length 95th (m)	30	0.0	14	0.0			
Control Delay (s)	12 0	0.0	94	0.0			
Lane LOS	-12.5 B	0.0	Δ	0.0			
Approach Delay (s)	12 9	0.0	14				
Approach LOS	B	0.0	1.1				
Intersection Summary							
Average Delay			10				
Intersection Canacity Litilize	ation		34.8%	IC		of Service	Δ
Analysis Period (min)			15	10	O Level (		<u>^</u>
			10				

Synchro 10 Report

HCM Unsignalized Inte ction Ca acity Analysian25 Total - Thorold Townline> AM Peak Hu

Timings	Timings <pre>&lt;2025 Total - Thorold Townline&gt; PM Peak Hour</pre>											
1: Davis Road & Th	orold S	Stone F	Road								09-2	3-2021
	≯	-	$\mathbf{r}$	4	+	1	Ť	1	1	ţ	~	
Lane Group	EBL	EBT	EBR	WBL	WBT	NBL	NBT	NBR	SBL	SBT	SBR	
Lane Configurations	5	44	1	5	<b>≜t</b> ₀	۲	ન	1	5	•	1	
Traffic Volume (vph)	24	1252	586	146	1183	506	5	126	4	6	28	
Future Volume (vph)	24	1252	586	146	1183	506	5	126	4	6	28	
Turn Type	Perm	NA	Perm	pm+pt	NA	Split	NA	Perm	Split	NA	Perm	
Protected Phases		2		1	6	4	4		8	8		
Permitted Phases	2		2	6				4			8	
Detector Phase	2	2	2	1	6	4	4	4	8	8	8	
Switch Phase												
Minimum Initial (s)	20.0	20.0	20.0	5.0	20.0	10.0	10.0	10.0	10.0	10.0	10.0	
Minimum Split (s)	28.9	28.9	28.9	8.0	28.9	29.7	29.7	29.7	17.7	17.7	17.7	
Total Split (s)	55.0	55.0	55.0	14.0	69.0	33.3	33.3	33.3	17.7	17.7	17.7	
Total Split (%)	45.8%	45.8%	45.8%	11.7%	57.5%	27.8%	27.8%	27.8%	14.8%	14.8%	14.8%	
Yellow Time (s)	5.4	5.4	5.4	3.0	5.4	5.7	5.7	5.7	5.7	5.7	5.7	
All-Red Time (s)	1.5	1.5	1.5	0.0	1.5	2.0	2.0	2.0	2.0	2.0	2.0	
Lost Time Adjust (s)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Total Lost Time (s)	6.9	6.9	6.9	3.0	6.9	7.7	7.7	7.7	7.7	7.7	7.7	
Lead/Lag	Lag	Lag	Lag	Lead								
Lead-Lag Optimize?	Yes	Yes	Yes	Yes	0.14							
Recall Mode	C-Max	C-Max	C-Max	None	C-Max	None	None	None	None	None	None	
Act Effct Green (s)	58.2	58.2	58.2	/4.9	/1.0	23.8	23.8	23.8	10.0	10.0	10.0	
Actuated g/C Ratio	0.48	0.48	0.48	0.62	0.59	0.20	0.20	0.20	0.08	0.08	0.08	
V/C Katio	0.19	0.78	0.07	0.74	0.00	0.80	0.82	0.33	0.03	0.04	0.12	
Control Delay	21.0	32.2	10.0	47.7	24.5	03.9	00.9	0.9	0.0	51.5	1.0	
Total Delay	27.8	32.2	16.6	47.7	24.3	63.0	65.0	8.0	51.2	51.3	1.0	
	21.0	52.2	10.0	47.7	24.5	00.0 E	00.0 E	0.5	J1.2	J1.J	1.0	
Approach Delay	U	27.2	D	U	26.0	E	53.8	A	U	13.0	A	
Approach LOS		21.2			20.9		55.0 D			13.3 B		
Intersection Summany		U			U		U			U		
Cycle Longth: 120												
Actuated Cycle Length: 120												
Offect: 0 (0%) Referenced to	nhaco 2	EBTL and		Start of	Groon							
Natural Cycle: 95	) priase 2.	LDTL and	JU.WDIL	., Start U	Green							
Control Type: Actuated-Coor	dinated											
Maximum v/c Ratio: 0.82	anatou											
Intersection Signal Delay: 31	4			Ir	ntersectio	n LOS [.] C						
Intersection Capacity Utilizati	ion 88.1%			10	CU Level	of Service	ε					
Analysis Period (min) 15												
. , , ,												

Splits and Ph	ases: 1: Davis Road & Thorold Stone Road		
<b>√</b> Ø1	🖉 🗘 🖗 🖉 2 (R)	<b>▲</b> Ø4	<b>11</b> _{Ø8}
14 s	55 s	33.3 s	17.7 s
🗲 Ø6 (R)	•		
69 s			

Synchro 10 Report

HCM Signalized Intersection Capacity Analysis<2025 Total - Thorold Townline> PM Peak Hour 1: Davis Road & Thorold Stone Road 09-23-2021

	٦	-	$\mathbf{\hat{z}}$	4	←	•	٠	Ť	۲	1	Ŧ	~
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	<u>۲</u>	- <b>††</b>	1	<u>۳</u>	<b>↑</b> 1≽		<u>۲</u>	4	1	<u>۲</u>	<b>↑</b>	1
Traffic Volume (vph)	24	1252	586	146	1183	1	506	5	126	4	6	28
Future Volume (vph)	24	1252	586	146	1183	1	506	5	126	4	6	28
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Total Lost time (s)	6.9	6.9	6.9	3.0	6.9		7.7	7.7	7.7	7.7	7.7	7.7
Lane Util. Factor	1.00	0.95	1.00	1.00	0.95		0.95	0.95	1.00	1.00	1.00	1.00
Frpb, ped/bikes	1.00	1.00	1.00	1.00	1.00		1.00	1.00	1.00	1.00	1.00	0.98
Flpb, ped/bikes	1.00	1.00	1.00	1.00	1.00		1.00	1.00	1.00	1.00	1.00	1.00
Frt	1.00	1.00	0.85	1.00	1.00		1.00	1.00	0.85	1.00	1.00	0.85
Flt Protected	0.95	1.00	1.00	0.95	1.00		0.95	0.95	1.00	0.95	1.00	1.00
Satd. Flow (prot)	1433	3505	1568	1671	3505		1681	1678	1482	1805	1810	1525
Flt Permitted	0.18	1.00	1.00	0.08	1.00		0.95	0.95	1.00	0.95	1.00	1.00
Satd. Flow (perm)	276	3505	1568	134	3505		1681	1678	1482	1805	1810	1525
Peak-hour factor, PHF	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95
Adj. Flow (vph)	25	1318	617	154	1245	1	533	5	133	4	6	29
RTOR Reduction (vph)	0	0	175	0	0	0	0	0	107	0	0	28
Lane Group Flow (vph)	25	1318	442	154	1246	0	266	272	26	4	6	1
Confl. Peds. (#/hr)							1					1
Heavy Vehicles (%)	26%	3%	3%	8%	3%	0%	2%	30%	9%	0%	5%	4%
Turn Type	Perm	NA	Perm	pm+pt	NA		Split	NA	Perm	Split	NA	Perm
Protected Phases		2		1	6		4	4		8	8	
Permitted Phases	2		2	6					4			8
Actuated Green, G (s)	55.1	55.1	55.1	67.9	67.9		23.8	23.8	23.8	6.0	6.0	6.0
Effective Green, g (s)	55.1	55.1	55.1	67.9	67.9		23.8	23.8	23.8	6.0	6.0	6.0
Actuated g/C Ratio	0.46	0.46	0.46	0.57	0.57		0.20	0.20	0.20	0.05	0.05	0.05
Clearance Time (s)	6.9	6.9	6.9	3.0	6.9		7.7	7.7	7.7	7.7	7.7	7.7
Vehicle Extension (s)	3.0	3.0	3.0	3.0	3.0		4.5	4.5	4.5	4.5	4.5	4.5
Lane Grp Cap (vph)	126	1609	719	201	1983		333	332	293	90	90	76
v/s Ratio Prot		c0.38		c0.06	0.36		0.16	c0.16		0.00	c0.00	
v/s Ratio Perm	0.09		0.28	0.37					0.02			0.00
v/c Ratio	0.20	0.82	0.62	0.77	0.63		0.80	0.82	0.09	0.04	0.07	0.02
Uniform Delay, d1	19.3	28.1	24.5	25.6	17.5		45.8	46.0	39.3	54.3	54.3	54.2
Progression Factor	1.00	1.00	1.00	1.51	1.31		1.00	1.00	1.00	1.00	1.00	1.00
Incremental Delay, d2	3.5	4.8	3.9	12.3	1.1		13.9	15.9	0.2	0.4	0.5	0.2
Delay (s)	22.8	32.9	28.4	51.0	24.2		59.7	61.9	39.5	54.6	54.9	54.4
Level of Service	С	С	С	D	С		E	E	D	D	D	D
Approach Delay (s)		31.4			27.1			56.6			54.5	
Approach LOS		С			С			E			D	
Intersection Summary												
HCM 2000 Control Delay			34.3	Н	CM 2000	Level of S	Service		С			
HCM 2000 Volume to Capa	acity ratio		0.77									
Actuated Cycle Length (s)			120.0	S	um of lost	t time (s)			25.3			
Intersection Capacity Utiliza	ation		88.1%	IC	U Level o	of Service			E			
Analysis Period (min)			15									
0.00												

c Critical Lane Group

Uppers Quarry Traffic Impact Study TMIG

Timings <2025 Total - Thorold Townline> PM Peak Hour 2: Davis Road & Niagara Falls Road/Beaverdams Road 09-23-2021										
	۰	-	1	+	•	Ť	1	ţ	~	
Lane Group	EBL	EBT	WBL	WBT	NBL	NBT	SBL	SBT	SBR	
Lane Configurations		\$		\$	ľ	<b>≜î</b> ≽	ľ	- <b>†</b> †	1	
Traffic Volume (vph)	90	32	74	44	12	409	170	471	105	
Future Volume (vph)	90	32	74	44	12	409	170	471	105	
Turn Type	Perm	NA	Perm	NA	Perm	NA	Perm	NA	Perm	
Protected Phases		2		6		4		8		
Permitted Phases	2		6		4		8		8	
Detector Phase	2	2	6	6	4	4	8	8	8	
Switch Phase										
Ainimum Initial (s)	10.0	10.0	10.0	10.0	25.0	25.0	25.0	25.0	25.0	
/linimum Split (s)	38.1	38.1	38.1	38.1	32.0	32.0	32.0	32.0	32.0	
Total Split (s)	40.0	40.0	40.0	40.0	60.0	60.0	60.0	60.0	60.0	
Fotal Split (%)	40.0%	40.0%	40.0%	40.0%	60.0%	60.0%	60.0%	60.0%	60.0%	
ellow Time (s)	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	
II-Red Time (s)	3.1	3.1	3.1	3.1	2.0	2.0	2.0	2.0	2.0	
ost Time Adjust (s)		0.0		0.0	0.0	0.0	0.0	0.0	0.0	
otal Lost Time (s)		8.1		8.1	7.0	7.0	7.0	7.0	7.0	
ead/Lag										
ead-Lag Optimize?										
Recall Mode	C-Max	C-Max	Max	Max	None	None	None	None	None	
Act Effct Green (s)		52.5		52.5	32.4	32.4	32.4	32.4	32.4	
Actuated g/C Ratio		0.52		0.52	0.32	0.32	0.32	0.32	0.32	
/c Ratio		0.24		0.34	0.05	0.45	0.72	0.46	0.19	
Control Delay		15.9		13.5	19.4	25.9	44.6	27.3	4.2	
Queue Delay		0.0		0.0	0.0	0.0	0.0	0.0	0.0	
otal Delay		15.9		13.5	19.4	25.9	44.6	27.3	4.2	
OS		В		В	В	С	D	С	A	
Approach Delay		15.9		13.5		25.7		28.0		
pproach LOS		В		В		С		С		
ntersection Summary										
Cycle Length: 100										
ctuated Cycle Length: 100										
)ffset: 0 (0%) Referenced t	to nhase 2 [.]	EBTI St	art of Gre	en						
latural Cycle: 75										
Control Type: Actuated-Con	rdinated									
Aximum v/c Ratio: 0.72										
ntersection Signal Delay: 2	3.9			Ir	ntersectio	n LOS: C				
ntersection Capacity Utiliza	tion 76.1%				CU Level	of Service	e D			
nalvsis Period (min) 15										
				1/5						

opino ana i naoco.	2. Davis Road & Niagara	da/Deaverdams road
[▲] ø2 (R)		<b>™</b> ø4
40 s		60 s
₹ø6		€ 28
40 s		60 s

Synchro 10 Report

 HCM Signalized Intersection Capacity Analysis<2025 Total - Thorold Townline> PM Peak Hour

 2: Davis Road & Niagara Falls Road/Beaverdams Road
 09-23-2021

	۶	-	$\mathbf{r}$	4	+	•	٠	Ť	۲	1	Ŧ	~
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		÷			÷		۲	<b>≜</b> 1₽		۲	<u></u>	1
Traffic Volume (vph)	90	32	17	74	44	147	12	409	50	170	471	105
Future Volume (vph)	90	32	17	74	44	147	12	409	50	170	471	105
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Total Lost time (s)		8.1			8.1		7.0	7.0		7.0	7.0	7.0
Lane Util. Factor		1.00			1.00		1.00	0.95		1.00	0.95	1.00
Frt		0.98			0.93		1.00	0.98		1.00	1.00	0.85
Flt Protected		0.97			0.99		0.95	1.00		0.95	1.00	1.00
Satd. Flow (prot)		1717			1702		1805	3298		1770	3343	1583
Flt Permitted		0.67			0.87		0.41	1.00		0.42	1.00	1.00
Satd. Flow (perm)		1180			1499		771	3298		773	3343	1583
Peak-hour factor, PHF	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95
Adj. Flow (vph)	95	34	18	78	46	155	13	431	53	179	496	111
RTOR Reduction (vph)	0	3	0	0	31	0	0	14	0	0	0	75
Lane Group Flow (vph)	0	144	0	0	248	0	13	470	0	179	496	36
Heavy Vehicles (%)	2%	2%	30%	2%	1%	2%	0%	8%	5%	2%	8%	2%
Turn Type	Perm	NA		Perm	NA		Perm	NA		Perm	NA	Perm
Protected Phases		2			6			4			8	
Permitted Phases	2			6			4			8		8
Actuated Green, G (s)		52.5			52.5		32.4	32.4		32.4	32.4	32.4
Effective Green, g (s)		52.5			52.5		32.4	32.4		32.4	32.4	32.4
Actuated g/C Ratio		0.52			0.52		0.32	0.32		0.32	0.32	0.32
Clearance Time (s)		8.1			8.1		7.0	7.0		7.0	7.0	7.0
Vehicle Extension (s)		3.0			3.0		5.0	5.0		5.0	5.0	5.0
Lane Grp Cap (vph)		619			786		249	1068		250	1083	512
v/s Ratio Prot								0.14			0.15	
v/s Ratio Perm		0.12			c0.17		0.02			c0.23		0.02
v/c Ratio		0.23			0.32		0.05	0.44		0.72	0.46	0.07
Uniform Delay, d1		12.8			13.5		23.2	26.7		29.8	26.8	23.4
Progression Factor		1.00			1.00		1.00	1.00		1.00	1.00	1.00
Incremental Delay, d2		0.9			1.0		0.2	0.6		11.5	0.6	0.1
Delay (s)		13.7			14.6		23.4	27.3		41.2	27.5	23.5
Level of Service		В			В		С	С		D	С	С
Approach Delay (s)		13.7			14.6			27.2			30.0	
Approach LOS		В			В			С			С	
Intersection Summary												
HCM 2000 Control Delay			25.3	Н	CM 2000	Level of S	Service		С			
HCM 2000 Volume to Capacit	y ratio		0.47									
Actuated Cycle Length (s)			100.0	S	um of lost	time (s)			15.1			
Intersection Capacity Utilization	on		76.1%	IC	CU Level of	of Service			D			
Analysis Period (min)			15									
c Critical Lane Group												

Uppers Quarry Traffic Impact Study TMIG

o. Davie rieda a Ed	inuys L	ane			09-23-						
	٦	-	4	+	•	1	1	1	ŧ	-	
Lane Group	EBL	EBT	WBL	WBT	WBR	NBL	NBT	SBL	SBT	SBR	
Lane Configurations	ሻ	ĥ	۲.	•	1	۳.	ĥ	ኘ	•	1	
Traffic Volume (vph)	179	567	28	555	241	46	141	300	125	157	
Future Volume (vph)	179	567	28	555	241	46	141	300	125	157	
Turn Type	pm+pt	NA	Perm	NA	Perm	Perm	NA	pm+pt	NA	Perm	
Protected Phases	5	2		6			4	3	8		
Permitted Phases	2		6		6	4		8		8	
Detector Phase	5	2	6	6	6	4	4	3	8	8	
Switch Phase											
Minimum Initial (s)	5.0	22.0	22.0	22.0	22.0	15.0	15.0	5.0	15.0	15.0	
Minimum Split (s)	8.0	36.0	36.0	36.0	36.0	32.0	32.0	8.0	32.0	32.0	
Total Split (s)	13.0	69.0	56.0	56.0	56.0	32.0	32.0	19.0	51.0	51.0	
Total Split (%)	10.8%	57.5%	46.7%	46.7%	46.7%	26.7%	26.7%	15.8%	42.5%	42.5%	
Yellow Time (s)	3.0	5.0	5.0	5.0	5.0	5.0	5.0	3.0	5.0	5.0	
All-Red Time (s)	0.0	2.0	2.0	2.0	2.0	2.0	2.0	0.0	2.0	2.0	
Lost Time Adjust (s)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Total Lost Time (s)	3.0	7.0	7.0	7.0	7.0	7.0	7.0	3.0	7.0	7.0	
Lead/Lag	Lead		Lag	Lag	Lag	Lag	Lag	Lead			
Lead-Lag Optimize?	Yes		Yes	Yes	Yes	Yes	Yes	Yes			
Recall Mode	None	C-Max	Max	Max	Max	Max	Max	None	Max	Мах	
Act Effct Green (s)	66.0	62.0	49.3	49.3	49.3	25.2	25.2	48.0	44.0	44.0	
Actuated g/C Ratio	0.55	0.52	0.41	0.41	0.41	0.21	0.21	0.40	0.37	0.37	
v/c Ratio	0.66	0.68	0.14	0.78	0.35	0.19	0.53	0.72	0.21	0.25	
Control Delay	25.5	26.2	26.7	41.9	9,6	41.6	46.3	37.4	27.2	4.7	
Queue Delay	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Total Delay	25.5	26.2	26.7	41.9	9,6	41.6	46.3	37.4	27.2	4.7	
LOS	C	0	C	D	A	D	D	D	C	A	
Approach Delay	Ū	26.1		31.9		5	45.3		26.4		
Approach LOS		C		C			D		C		
Internetien Operation							_				
Intersection Summary			_	_			_				
Cycle Length: 120											
Actuated Cycle Length: 120											
Uttset: 0 (0%), Referenced t	o phase 2	EBTL, St	art of Gre	en							
Natural Cycle: 85											
Control Type: Actuated-Coo	rdinated										
Maximum v/c Ratio: 0.78											
Intersection Signal Delay: 29	9.9			I	ntersectio	n LOS: C					
Intersection Capacity Utiliza	tion 108.25	%		10	CU Level	ot Service	ЭĠ				
Analysis Period (min) 15											

→ø2 (R)	Ø3	1 ₀₄
69 s	19 s	32 s
▶ _{Ø5} ♥ _{Ø6}	<b>₽</b> Ø8	
13 s 56 s	51 s	

Synchro 10 Report

 HCM Signalized Intersection Capacity Analysis<2025 Total - Thorold Townline> PM Peak Hour

 3: Davis Road & Lundys Lane

	٦	-	$\mathbf{\hat{z}}$	4	+	×	•	Ť	1	1	Ŧ	~
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	۲	4		۲	1	1	۲	f,		۲	1	1
Traffic Volume (vph)	179	567	28	28	555	241	46	141	37	300	125	157
Future Volume (vph)	179	567	28	28	555	241	46	141	37	300	125	157
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Total Lost time (s)	3.0	7.0		7.0	7.0	7.0	7.0	7.0		3.0	7.0	7.0
Lane Util. Factor	1.00	1.00		1.00	1.00	1.00	1.00	1.00		1.00	1.00	1.00
Frpb, ped/bikes	1.00	1.00		1.00	1.00	0.98	1.00	1.00		1.00	1.00	1.00
Flpb, ped/bikes	1.00	1.00		1.00	1.00	1.00	1.00	1.00		1.00	1.00	1.00
Frt	1.00	0.99		1.00	1.00	0.85	1.00	0.97		1.00	1.00	0.85
Flt Protected	0.95	1.00		0.95	1.00	1.00	0.95	1.00		0.95	1.00	1.00
Satd. Flow (prot)	1719	1811		1611	1863	1473	1736	1671		1702	1743	1553
Flt Permitted	0.18	1.00		0.32	1.00	1.00	0.67	1.00		0.47	1.00	1.00
Satd. Flow (perm)	322	1811		537	1863	1473	1226	1671		845	1743	1553
Peak-hour factor, PHF	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93
Adj. Flow (vph)	192	610	30	30	597	259	49	152	40	323	134	169
RTOR Reduction (vph)	0	1	0	0	0	143	0	8	0	0	0	107
Lane Group Flow (vph)	192	639	0	30	597	116	49	184	0	323	134	62
Confl. Peds. (#/hr)	2		1	1		2			1	1		
Heavy Vehicles (%)	5%	3%	26%	12%	2%	7%	4%	9%	12%	6%	9%	4%
Turn Type	pm+pt	NA		Perm	NA	Perm	Perm	NA		pm+pt	NA	Perm
Protected Phases	5	2			6			4		3	8	
Permitted Phases	2			6		6	4			8		8
Actuated Green, G (s)	62.0	62.0		49.3	49.3	49.3	25.2	25.2		44.0	44.0	44.0
Effective Green, g (s)	62.0	62.0		49.3	49.3	49.3	25.2	25.2		44.0	44.0	44.0
Actuated g/C Ratio	0.52	0.52		0.41	0.41	0.41	0.21	0.21		0.37	0.37	0.37
Clearance Time (s)	3.0	7.0		7.0	7.0	7.0	7.0	7.0		3.0	7.0	7.0
Vehicle Extension (s)	3.0	4.0		4.0	4.0	4.0	2.0	2.0		3.0	2.0	2.0
Lane Grp Cap (vph)	279	935		220	765	605	257	350		422	639	569
v/s Ratio Prot	0.06	c0.35			c0.32			0.11		c0.10	0.08	
v/s Ratio Perm	0.30			0.06		0.08	0.04			c0.18		0.04
v/c Ratio	0.69	0.68		0.14	0.78	0.19	0.19	0.53		0.77	0.21	0.11
Uniform Delay, d1	21.1	21.7		22.1	30.7	22.6	39.0	42.1		30.8	26.1	25.1
Progression Factor	1.00	1.00		1.10	1.10	2.28	1.00	1.00		1.00	1.00	1.00
Incremental Delay, d2	6.9	4.0		1.2	7.1	0.6	1.6	5.6		8.1	0.7	0.4
Delay (s)	28.0	25.7		25.5	40.8	52.1	40.7	47.7		38.9	26.8	25.5
Level of Service	С	С		С	D	D	D	D		D	С	С
Approach Delay (s)		26.2			43.6			46.2			32.7	
Approach LOS		С			D			D			С	
Intersection Summary												
HCM 2000 Control Delay			35,6	Н	CM 2000	Level of	Service		P			
HCM 2000 Volume to Cap	acity ratio		0.79									
Actuated Cycle Length (s)			120.0	S	um of los	t time (s)			20.0			
Intersection Capacity Utiliz	ation		108.2%	10	CU Level	of Service			G			
Analysis Period (min)			15									

c Critical Lane Group

Uppers Quarry Traffic Impact Study TMIG

Timings 2025 Total - Thorold Townline> PM Peak Ho 4: Thorold Townline Road & Thorold Stone Road										Peak Hou 09-23-202	
	٨	-	$\mathbf{r}$	4	+	•	•	Ť	1	ţ	
Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	SBL	SBT	
Lane Configurations	ľ	<u></u>	1	ľ	<u></u>	1	۲	4	٢	¢Î	
Traffic Volume (vph)	231	1036	72	75	821	35	142	148	48	171	
Future Volume (vph)	231	1036	72	75	821	35	142	148	48	171	
Turn Type	pm+pt	NA	Perm	pm+pt	NA	Perm	pm+pt	NA	pm+pt	NA	
Protected Phases	5	2		1	6		7	4	3	8	
Permitted Phases	2		2	6		6	4		8		
Detector Phase	5	2	2	1	6	6	7	4	3	8	
Switch Phase											
Minimum Initial (s)	8.0	10.0	10.0	5.0	10.0	10.0	5.0	10.0	5.0	10.0	
Minimum Split (s)	11.0	35.1	35.1	8.0	35.1	35.1	8.0	41.4	8.0	41.4	
Total Split (s)	21.0	54.4	54.4	9.6	43.0	43.0	13.0	46.0	10.0	43.0	
Total Split (%)	17.5%	45.3%	45.3%	8.0%	35.8%	35.8%	10.8%	38.3%	8.3%	35.8%	
Yellow Time (s)	3.0	4.1	4.1	3.0	4.1	4.1	3.0	4.1	3.0	4.1	
All-Red Time (s)	0.0	2.0	2.0	0.0	2.0	2.0	0.0	2.3	0.0	2.3	
Lost Time Adjust (s)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Total Lost Time (s)	3.0	6.1	6.1	3.0	6.1	6.1	3.0	6.4	3.0	6.4	
Lead/Lag	Lead	Lag	Lag	Lead	Lag	Lag	Lead	Lag	Lead	Lag	
Lead-Lag Optimize?	Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes	
Recall Mode	None	C-Max	C-Max	None	C-Max	C-Max	None	None	None	None	
Act Effct Green (s)	64.4	53.4	53.4	53.3	43.5	43.5	49.6	38.2	43.3	33.2	
Actuated g/C Ratio	0.54	0.44	0.44	0.44	0.36	0.36	0.41	0.32	0.36	0.28	
v/c Ratio	0.73	0.68	0.12	0.42	0.67	0.06	0.71	0.56	0.13	0.93	
Control Delay	49.3	51.1	24.5	23.2	36.8	0.2	42.0	34.0	20.9	61.9	
Queue Delay	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Total Delay	49.3	51.1	24.5	23.2	36.8	0.2	42.0	34.0	20.9	61.9	
LOS	D	D	С	С	D	A	D	С	С	E	
Approach Delay		49.4			34.4			36.8		57.9	
Approach LOS		D			С			D		E	
Intersection Summarv											
Cycle Length: 120											
Actuated Cycle Length: 120											
Offset: 0 (0%), Referenced to	o phase 2	EBTL an	d 6:WBTI	. Start of	Green						
Natural Cycle: 100	- p.1000 2.			, 500.00							
Control Type: Actuated-Coor	dinated										
Maximum v/c Ratio: 0.93											
Intersection Signal Delay: 44	.7			Ir	ntersectio	n LOS: D					
Intersection Capacity Utilizat	ion 86.1%				CU Level	of Service	ε				
Analysis Period (min) 15											

Splits and Phases:	4: Thorold Townline R	load & Thorold Stone Road
--------------------	-----------------------	---------------------------

🖌 Ø1 🕹 Ø2 (F	)	Ø3	<\$ ₫ Ø4
9.6 s 54.4 s		10 s	46 s
▶ Ø2	●	<b>▲</b> Ø7	ØS
21 s	43 s	13 s	43 s

Synchro 10 Report

 HCM Signalized Intersection Capacity Analysis<2025 Total - Thorold Townline> PM Peak Hour

 4: Thorold Townline Road & Thorold Stone Road
 09-23-2021

	≯	-	$\mathbf{r}$	•	←	•	1	Ť	1	1	Ŧ	1
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	ሻ		1	ሻ	- <b>†</b> †	1	ሻ	4Î		٦	¢Î	
Traffic Volume (vph)	231	1036	72	75	821	35	142	148	118	48	171	272
Future Volume (vph)	231	1036	72	75	821	35	142	148	118	48	171	272
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Total Lost time (s)	3.0	6.1	6.1	3.0	6.1	6.1	3.0	6.4		3.0	6.4	
Lane Util. Factor	1.00	0.95	1.00	1.00	0.95	1.00	1.00	1.00		1.00	1.00	
Frt	1.00	1.00	0.85	1.00	1.00	0.85	1.00	0.93		1.00	0.91	
Flt Protected	0.95	1.00	1.00	0.95	1.00	1.00	0.95	1.00		0.95	1.00	
Satd. Flow (prot)	1671	3574	1292	1492	3539	1538	1570	1482		1671	1613	
Flt Permitted	0.17	1.00	1.00	0.17	1.00	1.00	0.14	1.00		0.52	1.00	
Satd. Flow (perm)	296	3574	1292	262	3539	1538	235	1482		912	1613	
Peak-hour factor, PHF	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96
Adj. Flow (vph)	241	1079	75	78	855	36	148	154	123	50	178	283
RTOR Reduction (vph)	0	0	42	0	0	23	0	25	0	0	50	0
Lane Group Flow (vph)	241	1079	33	78	855	13	148	252	0	50	411	0
Heavy Vehicles (%)	8%	1%	25%	21%	2%	5%	15%	17%	23%	8%	10%	5%
Turn Type	pm+pt	NA	Perm	pm+pt	NA	Perm	pm+pt	NA		pm+pt	NA	
Protected Phases	5	2		1	6		7	4		3	8	
Permitted Phases	2		2	6		6	4			8		
Actuated Green, G (s)	60.7	52.2	52.2	48.4	42.9	42.9	46.8	38.2		39.4	33.8	
Effective Green, g (s)	60.7	52.2	52.2	48.4	42.9	42.9	46.8	38.2		39.4	33.8	
Actuated g/C Ratio	0.51	0.44	0.44	0.40	0.36	0.36	0.39	0.32		0.33	0.28	
Clearance Time (s)	3.0	6.1	6.1	3.0	6.1	6.1	3.0	6.4		3.0	6.4	
Vehicle Extension (s)	2.5	6.0	6.0	3.0	6.0	6.0	3.0	2.3		3.0	2.3	
Lane Grp Cap (vph)	319	1554	562	162	1265	549	202	471		334	454	
v/s Ratio Prot	c0.09	0.30		0.02	0.24		c0.06	0.17		0.01	c0.26	
v/s Ratio Perm	c0.29		0.03	0.17		0.01	0.22			0.04		
v/c Ratio	0.76	0.69	0.06	0.48	0.68	0.02	0.73	0.54		0.15	0.91	
Uniform Delay, d1	20.8	27.4	19.6	23.8	32.7	25.0	28.2	33.6		28.0	41.6	
Progression Factor	2.25	1.75	6.20	1.00	1.00	1.00	1.00	1.00		1.00	1.00	
Incremental Delay, d2	6.4	1.7	0.1	2.2	2.9	0.1	12.8	0.8		0.2	21.2	
Delay (s)	53.1	49.8	122.0	26.1	35.6	25.1	41.0	34.4		28.2	62.8	
Level of Service	D	D	F	С	D	С	D	С		С	E	
Approach Delay (s)		54.3			34.4			36.7			59.4	
Approach LOS		D			С			D			E	
Intersection Summary												
HCM 2000 Control Delay			47.0	H	CM 2000	Level of	Service		D			
HCM 2000 Volume to Capa	city ratio		0.82									
Actuated Cycle Length (s)			120.0	S	um of los	t time (s)			18.5			
Intersection Capacity Utiliza	tion		86.1%	IC	CU Level	of Service	Э		E			
Analysis Period (min)			15									
c Critical Lane Group												

Uppers Quarry Traffic Impact Study TMIG
Timings 5: Thorold Townline	ine	<2025 Total - Thorold Townline> PM Peak Hour 09-23-2021									
	٠	-	`	4	+	•	Ť	1	ţ	~	
Lane Group	EBL	EBT	EBR	WBL	WBT	NBL	NBT	SBL	SBT	SBR	
Lane Configurations	ľ	•	1	ľ	ĥ	ľ	ĥ	ľ	•	1	
Traffic Volume (vph)	83	527	103	44	555	113	131	53	118	132	
Future Volume (vph)	83	527	103	44	555	113	131	53	118	132	
Turn Type	Perm	NA	Perm	Perm	NA	Perm	NA	Perm	NA	Perm	
Protected Phases		2			6		4		8		
Permitted Phases	2		2	6		4		8		8	
Detector Phase	2	2	2	6	6	4	4	8	8	8	
Switch Phase											
Minimum Initial (s)	20.0	20.0	20.0	20.0	20.0	10.0	10.0	10.0	10.0	10.0	
Minimum Split (s)	29.0	29.0	29.0	29.0	29.0	35.0	35.0	35.0	35.0	35.0	
Total Split (s)	80.0	80.0	80.0	80.0	80.0	40.0	40.0	40.0	40.0	40.0	
Total Split (%)	66.7%	66.7%	66.7%	66.7%	66.7%	33.3%	33.3%	33.3%	33.3%	33.3%	
Yellow Time (s)	5.0	5.0	5.0	5.0	5.0	4.0	4.0	4.0	4.0	4.0	
All-Red Time (s)	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	
Lost Time Adjust (s)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Total Lost Time (s)	7.0	7.0	7.0	7.0	7.0	6.0	6.0	6.0	6.0	6.0	
Lead/Lag											
Lead-Lag Optimize?											
Recall Mode	C-Max	C-Max	C-Max	C-Max	C-Max	None	None	None	None	None	
Act Effct Green (s)	86.7	86.7	86.7	86.7	86.7	20.3	20.3	20.3	20.3	20.3	
Actuated g/C Ratio	0.72	0.72	0.72	0.72	0.72	0.17	0.17	0.17	0.17	0.17	
v/c Ratio	0.20	0.44	0.10	0.09	0.49	0.67	0.65	0.44	0.43	0.38	
Control Delay	7.2	9.2	3.2	6.7	9.4	63.8	51.7	53.2	47.9	9.2	
Queue Delay	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
l otal Delay	7.2	9.2	3.2	6.7	9.4	63.8	51.7	53.2	47.9	9.2	
LOS	A	A	A	A	A	E	D	D	D	A	
Approach Delay		8.1			9.2		56.4		32.0		
Approach LOS		A			A		E		U		
Intersection Summary											
Cycle Length: 120											
Actuated Cycle Length: 120											
Offset: 0 (0%), Referenced to	phase 2	EBTL and	d 6:WBTL	., Start of	Green						
Natural Cycle: 70											
Control Type: Actuated-Coor	dinated										
Maximum v/c Ratio: 0.67											
Intersection Signal Delay: 19.5 Intersection LOS: B											
Intersection Capacity Utilizati Analysis Period (min) 15	Intersection Capacity Utilization 87.8% ICU Level of Service E Analysis Period (min) 15										
Splits and Phases: 5: Thor	old Town	line Road	& Lundv	s Lane							

Ø2 (R)	1 ₀₄
80 s	40 s
₩ Ø6 (R)	<b>↓</b> Ø8
80 s	40 s

Synchro 10 Report

 HCM Signalized Intersection Capacity Analysis<2025 Total - Thorold Townline > PM Peak Hour

 5: Thorold Townline Road & Lundys Lane

 09-23-2021

	٦	-	$\mathbf{r}$	4	←	×	٠	Ť	۲	1	Ŧ	~
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	۲	1	1	۲	4Î		٦	f,		٦	1	1
Traffic Volume (vph)	83	527	103	44	555	33	113	131	50	53	118	132
Future Volume (vph)	83	527	103	44	555	33	113	131	50	53	118	132
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Total Lost time (s)	7.0	7.0	7.0	7.0	7.0		6.0	6.0		6.0	6.0	6.0
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00		1.00	1.00		1.00	1.00	1.00
Frpb, ped/bikes	1.00	1.00	1.00	1.00	1.00		1.00	1.00		1.00	1.00	1.00
Flpb, ped/bikes	1.00	1.00	1.00	1.00	1.00		1.00	1.00		1.00	1.00	1.00
Frt	1.00	1.00	0.85	1.00	0.99		1.00	0.96		1.00	1.00	0.85
Flt Protected	0.95	1.00	1.00	0.95	1.00		0.95	1.00		0.95	1.00	1.00
Satd. Flow (prot)	1625	1827	1553	1752	1832		1687	1745		1736	1776	1524
Flt Permitted	0.36	1.00	1.00	0.40	1.00		0.62	1.00		0.43	1.00	1.00
Satd. Flow (perm)	621	1827	1553	740	1832		1093	1745		792	1776	1524
Peak-hour factor, PHF	0.91	0.91	0.91	0.91	0.91	0.91	0.91	0.91	0.91	0.91	0.91	0.91
Adi, Flow (vph)	91	579	113	48	610	36	124	144	55	58	130	145
RTOR Reduction (vph)	0	0	14	0	1	0	0	13	0	0	0	120
Lane Group Flow (vph)	91	579	99	48	645	0	124	186	0	58	130	25
Confl. Peds. (#/hr)	1					1						
Heavy Vehicles (%)	11%	4%	4%	3%	2%	15%	7%	6%	0%	4%	7%	6%
Turn Type	Perm	NA	Perm	Perm	NA		Perm	NA		Perm	NA	Perm
Protected Phases		2			6			4			8	
Permitted Phases	2		2	6			4			8		8
Actuated Green, G (s)	86.7	86.7	86.7	86.7	86.7		20.3	20.3		20.3	20.3	20.3
Effective Green, g (s)	86.7	86.7	86.7	86.7	86.7		20.3	20.3		20.3	20.3	20.3
Actuated g/C Ratio	0.72	0.72	0.72	0.72	0.72		0.17	0.17		0.17	0.17	0.17
Clearance Time (s)	7.0	7.0	7.0	7.0	7.0		6.0	6.0		6.0	6.0	6.0
Vehicle Extension (s)	5.0	5.0	5.0	5.0	5.0		5.0	5.0		5.0	5.0	5.0
Lane Grp Cap (vph)	448	1320	1122	534	1323		184	295		133	300	257
v/s Ratio Prot		0.32			c0.35			0.11			0.07	
v/s Ratio Perm	0.15		0.06	0.06			c0.11			0.07		0.02
v/c Ratio	0.20	0.44	0.09	0.09	0.49		0.67	0.63		0.44	0.43	0.10
Uniform Delay, d1	5.4	6.8	4.9	4.9	7.1		46.7	46.4		44.7	44.7	42.1
Progression Factor	0.94	1.09	0.87	1.00	1.00		1.00	1.00		1.00	1.00	1.00
Incremental Delay, d2	0.7	0.8	0.1	0.3	1.3		12.0	5.8		4.7	2.1	0.3
Delay (s)	5.8	8.1	4.4	5.3	8.4		58.8	52.2		49.4	46.8	42.4
Level of Service	A	А	А	А	А		E	D		D	D	D
Approach Delay (s)		7.3			8.2			54.7			45.4	
Approach LOS		А			А			D			D	
Intersection Summary												
HCM 2000 Control Delay			20.7	Н	CM 2000	Level of	Service		С			
HCM 2000 Volume to Capa	acity ratio		0.52									
Actuated Cycle Length (s)			120.0	0 Sum of lost time (s)				13.0				
Intersection Capacity Utilization	ation		87.8%	IC	U Level	of Service			E			
Analysis Period (min)			15									
0.11 0												

c Critical Lane Group

Uppers Quarry Traffic Impact Study TMIG

Timings 6 [.] Thorold Townline	e Road	& Bea	verdar	<202 ad	<2025 Total - Thorold Townline> PM Peak Hour d 09-23-2021				
	<u>)</u>	<u>→</u>	<ul> <li>Image: A start of the start of</li></ul>	<b>+</b>	1	t	4	ţ	
Lane Group	EBL	EBT	WBL	WBT	NBL	NBT	SBL	SBT	
Lane Configurations		4		4		4		4	
Traffic Volume (vph)	27	213	43	192	32	384	20	275	
Future Volume (vph)	27	213	43	192	32	384	20	275	
Turn Type	Perm	NA	Perm	NA	Perm	NA	Perm	NA	
Protected Phases		2		6		4		8	
Permitted Phases	2		6		4		8		
Detector Phase	2	2	6	6	4	4	8	8	
Switch Phase									
Minimum Initial (s)	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	
Minimum Split (s)	32.0	32.0	32.0	32.0	35.0	35.0	35.0	35.0	
Total Split (s)	36.0	36.0	36.0	36.0	54.0	54.0	54.0	54.0	
Total Split (%)	40.0%	40.0%	40.0%	40.0%	60.0%	60.0%	60.0%	60.0%	
Yellow Time (s)	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0	
All-Red Time (s)	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	
Lost Time Adjust (s)		0.0		0.0		0.0		0.0	
Total Lost Time (s)		6.0		6.0		6.0		6.0	
Lead/Lag									
Lead-Lag Optimize?									
Recall Mode	C-Max	C-Max	Max	Max	None	None	None	None	
Act Effct Green (s)		41.7		41.7		36.3		36.3	
Actuated g/C Ratio		0.46		0.46		0.40		0.40	
v/c Ratio		0.34		0.35		0.76		0.58	
Control Delay		18.8		19.0		30.7		23.0	
Queue Delay		0.0		0.0		0.0		0.0	
Total Delay		18.8		19.0		30.7		23.0	
LOS		B		В		C		C	
Approach Delay		18.8		19.0		30.7		23.0	
Approach LOS		В		В		U		C	
Intersection Summary									
Cycle Length: 90									
Actuated Cycle Length: 90									
Offset: 0 (0%), Referenced t	to phase 2	EBTL, St	art of Gre	en					
Natural Cycle: 70									
Control Type: Actuated-Coo	rdinated								
Maximum v/c Ratio: 0.76									
Intersection Signal Delay: 24	4.0			Ir	ntersectio	n LOS: C			
Intersection Capacity Utilizat	tion 63.3%			10	CU Level	of Service	эB		
Analysis Period (min) 15									
Splits and Phases: 6: Tho	orold Town	line Road	& Beave	rdams Ro	ad				

▲ Ø2 (R)	
36 s	54 s
<b>★</b> Ø6	
36 s	54.8

Synchro 10 Report

 HCM Signalized Intersection Capacity Analysis<2025 Total - Thorold Townline > PM Peak Hour

 6: Thorold Townline Road & Beaverdams Road

	۶	<b>→</b>	$\mathbf{\hat{z}}$	4	+	۰.	٩.	t	۲	1	ŧ	~
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		4			\$			\$			4	
Traffic Volume (vph)	27	213	16	43	192	21	32	384	26	20	275	41
Future Volume (vph)	27	213	16	43	192	21	32	384	26	20	275	41
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Total Lost time (s)		6.0			6.0			6.0			6.0	
Lane Util. Factor		1.00			1.00			1.00			1.00	
Frpb, ped/bikes		1.00			1.00			1.00			1.00	
Flpb, ped/bikes		1.00			1.00			1.00			1.00	
Frt		0.99			0.99			0.99			0.98	
Flt Protected		0.99			0.99			1.00			1.00	
Satd. Flow (prot)		1831			1832			1605			1594	
Flt Permitted		0.95			0.91			0.95			0.96	
Satd. Flow (perm)		1745			1677			1534			1530	
Peak-hour factor, PHF	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93
Adj. Flow (vph)	29	229	17	46	206	23	34	413	28	22	296	44
RTOR Reduction (vph)	0	2	0	0	3	0	0	3	0	0	7	0
Lane Group Flow (vph)	0	273	0	0	272	0	0	472	0	0	355	0
Confl. Peds. (#/hr)	1		5	5		1	8		3	3		8
Heavy Vehicles (%)	10%	1%	4%	4%	1%	0%	4%	19%	0%	2%	19%	6%
Turn Type	Perm	NA		Perm	NA		Perm	NA		Perm	NA	
Protected Phases		2			6			4			8	
Permitted Phases	2			6			4			8		
Actuated Green, G (s)		41.7			41.7			36.3			36.3	
Effective Green, g (s)		41.7			41.7			36.3			36.3	
Actuated g/C Ratio		0.46			0.46			0.40			0.40	
Clearance Time (s)		6.0			6.0			6.0			6.0	
Vehicle Extension (s)		5.0			5.0			5.0			5.0	
Lane Grp Cap (vph)		808			777			618			617	
v/s Ratio Prot												
v/s Ratio Perm		0.16			c0.16			c0.31			0.23	
v/c Ratio		0.34			0.35			0.76			0.58	
Uniform Delay, d1		15.4			15.5			23.2			20.9	
Progression Factor		1.00			1.00			1.00			1.00	
Incremental Delay, d2		1.1			1.2			6.6			2.1	
Delay (s)		16.5			16.7			29.7			22.9	
Level of Service		В			В			С			С	
Approach Delay (s)		16.5			16.7			29.7			22.9	
Approach LOS		В			В			С			С	
Intersection Summary												
HCM 2000 Control Delay			22.7	Н	CM 2000	Level of S	Service		С			
HCM 2000 Volume to Capa	citv ratio		0.54									
Actuated Cycle Length (s)			90.0	S	um of lost	time (s)			12.0			
Intersection Capacity Utiliza	ation		63.3%	IC	U Level o	of Service			B			
Analysis Period (min)			15						_			

c Critical Lane Group

Uppers Quarry Traffic Impact Study TMIG

7: Thorold Townline	Interse e Road	ction C & Upp	apacit ers Lai	y Anal <u>y</u> ne	ys1202	5 I otal -	- Thoroid Townline> Pivi Peak Hour 09-23-2021
	4	•	Ť	*	1	Ļ	
Movement	WBL	WBR	NBT	NBR	SBL	SBT	
Lane Configurations	Y		4Î		۲	1	
Traffic Volume (veh/h)	3	46	323	3	46	297	
Future Volume (Veh/h)	3	46	323	3	46	297	
Sign Control	Stop		Free			Free	
Grade	0%		0%			0%	
Peak Hour Factor	0.91	0.91	0.91	0.91	0.91	0.91	
Hourly flow rate (vph)	3	51	355	3	51	326	
Pedestrians							
Lane Width (m)							
Walking Speed (m/s)							
Percent Blockage							
Right turn flare (veh)							
Median type			None			None	
Median storage veh)							
Upstream signal (m)							
pX, platoon unblocked							
vC. conflicting volume	784	356			358		
vC1, stage 1 conf vol							
vC2, stage 2 conf vol							
vCu, unblocked vol	784	356			358		
tC single (s)	6.4	7.0			49		
tC 2 stage (s)	0.1	1.0					
tF (s)	3.5	40			29		
n0 queue free %	99	91			94		
cM capacity (veh/h)	343	538			863		
Direction, Lane #	WB 1	NB 1	SB 1	SB 2			
Volume Total	54	358	51	326			
Volume Left	3	0	51	0			
Volume Right	51	3	0	0			
cSH	522	1700	863	1700			
Volume to Capacity	0.10	0.21	0.06	0.19			
Queue Lenath 95th (m)	2.8	0.0	1.5	0.0			
Control Delay (s)	12.7	0.0	9.4	0.0			
Lane LOS	В		A				
Approach Delay (s)	12.7	0.0	1.3				
Approach LOS	В						
Intersection Summary							
Average Delay			1.5				
Intersection Capacity Utiliza	tion		33.8%	IC	U Level o	of Service	A
Analysis Period (min)			15				

Synchro 10 Report

...... . . . ... ~ •• . ------.... 

Timings     <2035 Background> AM Peak       1: Davis Road & Thorold Stone Road     09-1												
	≯	+	*	4	+	•	Ť	1	*	ŧ	4	
Lane Group	EBL	EBT	EBR	WBL	WBT	NBL	NBT	NBR	SBL	SBT	SBR	
Lane Configurations	ሻ		1	ሻ	At≱	ሻ	ę	1	ኘ	•	1	
Traffic Volume (vph)	21	991	336	114	1096	649	15	257	1	2	18	
Future Volume (vph)	21	991	336	114	1096	649	15	257	1	2	18	
Turn Type	Perm	NA	Perm	pm+pt	NA	Split	NA	Perm	Split	NA	Perm	
Protected Phases		2		1	6	4	4		8	8		
Permitted Phases	2		2	6				4			8	
Detector Phase	2	2	2	1	6	4	4	4	8	8	8	
Switch Phase												
Minimum Initial (s)	20.0	20.0	20.0	8.0	20.0	10.0	10.0	10.0	10.0	10.0	10.0	
Minimum Split (s)	28.9	28.9	28.9	12.5	28.9	29.7	29.7	29.7	21.7	21.7	21.7	
Total Split (s)	46.3	46.3	46.3	13.0	59.3	39.0	39.0	39.0	21.7	21.7	21.7	
Total Split (%)	38.6%	38.6%	38.6%	10.8%	49.4%	32.5%	32.5%	32.5%	18.1%	18.1%	18.1%	
Yellow Time (s)	5.4	5.4	5.4	3.0	5.4	5.7	5.7	5.7	5.7	5.7	5.7	
All-Red Time (s)	1.5	1.5	1.5	0.0	1.5	2.0	2.0	2.0	2.0	2.0	2.0	
Lost Time Adjust (s)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Total Lost Time (s)	6.9	6.9	6.9	3.0	6.9	1.1	1.1	1.1	1.1	1.1	1.1	
Lead/Lag	Lag	Lag	Lag	Lead								
Leau-Lag Optimize?	C Mox	C Mox	C Mox	Nono	Мох	Nono	Nono	None	Nono	Nono	Nono	
Recall Wode	C-IVIAX	C-IVIAX	C-IVIAX	72.0	ER 1	20.0	20.2	20.2	10.0	10.0	10.0	
Act Elici Green (S)	0.46	0.46	0.46	12.0	00.1	0.25	0.25	0.25	0.09	0.09	0.09	
v/c Patio	0.40	0.40	0.40	0.00	0.57	0.25	0.25	0.25	0.00	0.00	0.08	
Control Delay	28.2	30.5	12.7	22.8	38.7	67.1	68.2	7 1	51.0	51.0	0.00	
	20.2	0.0	0.0	0.0	0.0	07.1	00.2	0.0	0.0	0.0	0.7	
Total Delay	28.2	30.5	12.7	33.8	38.7	67.1	68.2	7 1	51.0	51.0	0.0	
LOS	20.2 C	0.00 C	R	0.00 C	D	F	F	Δ	D	01.0 D	Δ	
Approach Delay	v	26.0	0	Ŭ	38.3	-	50.8	~	U	7.5		
Approach LOS		C			D		D			A		
Intersection Summary		-					_					
Cycle Length: 120												
Actuated Cycle Length: 120												
Offset: 0 (0%), Referenced to	phase 2	EBTL, St	art of Gre	en								
Natural Cycle: 105												_
Control Type: Actuated-Coor	dinated											
Maximum v/c Ratio: 0.89	_											_
Intersection Signal Delay: 36	.7			I	ntersection	n LOS: D	_					
Intersection Capacity Utilizati	ion 90.1%			10	U Level	ot Service	θE					_
Analysis Period (min) 15												

Splits and Phases: 1: Davis Road & Thorold Stone Road

<b>√</b> Ø1	🗸 🗸 🖉 🖉 🖉	<b>▲</b> Ø4	<b>₩</b> Ø8
13 s	46.3 s	39 s	21.7s
₹ø6			
59.3 s			

Uppers Quarry Traffic Impact Study TMIG

Synchro 10 Report

# HCM Signalized Intersection Capacity Analysis 1: Davis Road & Thorold Stone Road

<2035 Background> AM Peak Hour

	٦	-	$\mathbf{r}$	4	+	•	1	Ť	۲	1	Ŧ	~
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	ሻ	44	1	5	<b>4</b> 16		5	÷.	1	٦	•	1
Traffic Volume (vph)	21	991	336	114	1096	6	649	15	257	1	2	18
Future Volume (vph)	21	991	336	114	1096	6	649	15	257	1	2	18
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Total Lost time (s)	6.9	6.9	6.9	3.0	6.9		7.7	7.7	7.7	7.7	7.7	7.7
Lane Util. Factor	1.00	0.95	1.00	1.00	0.95		0.95	0.95	1.00	1.00	1.00	1.00
Frpb, ped/bikes	1.00	1.00	1.00	1.00	1.00		1.00	1.00	0.99	1.00	1.00	0.99
Flpb, ped/bikes	1.00	1.00	1.00	1.00	1.00		1.00	1.00	1.00	1.00	1.00	1.00
Frt	1.00	1.00	0.85	1.00	1.00		1.00	1.00	0.85	1.00	1.00	0.85
Flt Protected	0.95	1.00	1.00	0.95	1.00		0.95	0.95	1.00	0.95	1.00	1.00
Satd. Flow (prot)	1640	3406	1442	1530	3399		1559	1554	1475	1388	1624	1337
Flt Permitted	0.21	1.00	1.00	0.14	1.00		0.95	0.95	1.00	0.95	1.00	1.00
Satd. Flow (perm)	354	3406	1442	228	3399		1559	1554	1475	1388	1624	1337
Peak-hour factor PHF	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96
Adi, Flow (vph)	22	1032	350	119	1142	6	676	16	268	1	2	19
RTOR Reduction (vph)	0	0	121	0	0	0	0	0	201	0	0	18
Lane Group Flow (vph)	22	1032	229	119	1148	0	345	347	67	1	2	1
Confl. Peds. (#/hr)	1					1	1		1	1		1
Heavy Vehicles (%)	10%	6%	12%	18%	6%	30%	10%	28%	8%	30%	17%	19%
Turn Type	Perm	NA	Perm	pm+pt	NA		Split	NA	Perm	Split	NA	Perm
Protected Phases		2			6		4	4		. 8	8	
Permitted Phases	2		2	6					4			8
Actuated Green, G (s)	50.4	50.4	50.4	63.5	63.5		30.2	30.2	30.2	4.0	4.0	4.0
Effective Green, g (s)	50.4	50.4	50.4	63.5	63.5		30.2	30.2	30.2	4.0	4.0	4.0
Actuated g/C Ratio	0.42	0.42	0.42	0.53	0.53		0.25	0.25	0.25	0.03	0.03	0.03
Clearance Time (s)	6.9	6.9	6.9	3.0	6.9		7.7	7.7	7.7	7.7	7.7	7.7
Vehicle Extension (s)	3.0	3.0	3.0	2.5	3.0		4.5	4.5	4.5	4.5	4.5	4.5
Lane Grp Cap (vph)	148	1430	605	230	1798		392	391	371	46	54	44
v/s Ratio Prot		c0.30		0.04	c0.34		0.22	c0.22		0.00	c0.00	
v/s Ratio Perm	0.06		0.16	0.23					0.05			0.00
v/c Ratio	0.15	0.72	0.38	0.52	0.64		0.88	0.89	0.18	0.02	0.04	0.01
Uniform Delay, d1	21.5	29.0	24.0	18.3	20.1		43.2	43.3	35.2	56.1	56.1	56.1
Progression Factor	1.00	1.00	1.00	2.30	1.99		1.00	1.00	1.00	1.00	1.00	1.00
Incremental Delay, d2	2.1	3.2	1.8	0.9	1.1		20.8	21.7	0.4	0.3	0.5	0.2
Delay (s)	23.6	32.1	25.8	43.0	41.0		64.0	65.0	35.6	56.4	56.6	56.3
Level of Service	С	С	С	D	D		E	E	D	E	E	E
Approach Delay (s)		30.4			41.2			56.4			56.4	
Approach LOS		С			D			E			E	
Intersection Summary												
HCM 2000 Control Delay			41.2	Н	CM 2000	Level of S	Service		D			
HCM 2000 Volume to Capac	city ratio		0.74									
Actuated Cycle Length (s)			120.0	) Sum of lost time (s)					25.3			
Intersection Capacity Utilization	tion		90.1%	IC	CU Level	of Service			E			
Analysis Period (min)			15									
- Oritical Lana Origina												

c Critical Lane Group

Uppers Quarry Traffic Impact Study TMIG

	*			t			1	1	1	
		-	¥.	•	7	I		÷	*	
Lane Group	EBL	EBT	WBL	WBT	NBL	NBT	SBL	SBT	SBR	
Lane Configurations		4		- <b>4</b> >	<u>۲</u>	<b>≜</b> ⊅	ሻ	- ++	1	
Traffic Volume (vph)	110	31	29	17	25	626	82	329	44	
Future Volume (vph)	110	31	29	17	25	626	82	329	44	
Turn Type	Perm	NA	Perm	NA	Perm	NA	Perm	NA	Perm	
Protected Phases		2		6		4		8		
Permitted Phases	2		6		4		8		8	
Detector Phase	2	2	6	6	4	4	8	8	8	
Switch Phase										
Minimum Initial (s)	10.0	10.0	10.0	10.0	25.0	25.0	25.0	25.0	25.0	
Minimum Split (s)	38.1	38.1	38.1	38.1	32.0	32.0	32.0	32.0	32.0	
Total Split (s)	46.0	46.0	46.0	46.0	54.0	54.0	54.0	54.0	54.0	
Total Split (%)	46.0%	46.0%	46.0%	46.0%	54.0%	54.0%	54.0%	54.0%	54.0%	
Yellow Time (s)	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	
All-Red Time (s)	3.1	3.1	3.1	3.1	2.0	2.0	2.0	2.0	2.0	
Lost Time Adjust (s)	0.1	0.0	0.1	0.0	0.0	0.0	0.0	0.0	0.0	
Total Lost Time (s)		8.1		8.1	7.0	7.0	7.0	7.0	7.0	
		0.1		0.1	1.0	1.0	1.0	1.0	1.0	
Lead Lag Optimize?										
	C Max	C Max	Max	Max	None	None	None	Nono	None	
	C-IVIAX	E2 0	IVIAA	ED 0	20.4	20.4	20.4	20.4	20.4	
Act Elici Green (S)		0.52		0.52	0.20	0.20	0.20	0.20	0.22	
Actualed g/C Ratio		0.55		0.55	0.32	0.32	0.52	0.32	0.32	
V/C Ratio		0.27		0.25	0.10	0.70	0.00	0.30	0.10	
Control Delay		15.4		5.0	22.5	32.8	41.0	20.3	4.7	
		0.0		0.0	0.0	0.0	0.0	0.0	0.0	
I OTAI Delay		15.4		5.0	22.5	32.8	41.6	26.3	4./	
LUS		B		A	C	C	D	C	A	
Approach Delay		15.4		5.0		32.5		27.0		
Approach LOS		В		A		C		C		
Intersection Summary										
Cvcle Length: 100										
Actuated Cycle Length: 10	00									
Offset: 0 (0%), Reference	d to phase 2:	EBTL, St	art of Gre	en						
Natural Cycle: 75										
Control Type: Actuated-C	oordinated									
Maximum v/c Ratio: 0 70										
Intersection Signal Delay:	25.2			lr	ntersectio	n LOS: C				
Intersection Canacity Litili	zation 88 /1%			10		of Service	> F			
An alwais Daniad (min) 45	244011 00.4 /0			N		0014100				

Ø2 (R)		
46 s	54 s	
<b>↓</b> Ø6	↓ Ø8	
46 s	54 s	

Synchro 10 Report

HCM Signalized Intersection Capacity Analysis 2: Davis Road & Niagara Falls Road/Beaverdams Road <2035 Background> AM Peak Hour 09-14-2021

	۶	<b>→</b>	$\mathbf{\hat{z}}$	4	+	×	1	Ť	۲	1	Ŧ	~
Novement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
ane Configurations		¢			\$		1	A		۲	<u></u>	1
raffic Volume (vph)	110	31	18	29	17	166	25	626	46	82	329	44
Future Volume (vph)	110	31	18	29	17	166	25	626	46	82	329	44
deal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
otal Lost time (s)		8.1			8.1		7.0	7.0		7.0	7.0	7.0
ane Util. Factor		1.00			1.00		1.00	0.95		1.00	0.95	1.00
Frt .		0.98			0.89		1.00	0.99		1.00	1.00	0.85
It Protected		0.97			0.99		0.95	1.00		0.95	1.00	1.00
Satd. Flow (prot)		1658			1631		1388	3122		1787	2983	1392
It Permitted		0.67			0.94		0.53	1.00		0.26	1.00	1.00
Satd. Flow (perm)		1155			1549		779	3122		480	2983	1392
Peak-hour factor, PHF	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95
Adj. Flow (vph)	116	33	19	31	18	175	26	659	48	86	346	46
RTOR Reduction (vph)	0	3	0	0	82	0	0	7	0	0	0	31
ane Group Flow (vph)	0	165	0	0	142	0	26	700	0	86	346	15
leavy Vehicles (%)	10%	7%	7%	7%	12%	2%	30%	15%	7%	1%	21%	16%
Turn Type	Perm	NA		Perm	NA		Perm	NA		Perm	NA	Perm
Protected Phases		2			6			4			8	
Permitted Phases	2			6			4			8		8
Actuated Green, G (s)		52.8			52.8		32.1	32.1		32.1	32.1	32.1
Effective Green, g (s)		52.8			52.8		32.1	32.1		32.1	32.1	32.1
Actuated g/C Ratio		0.53			0.53		0.32	0.32		0.32	0.32	0.32
Clearance Time (s)		8.1			8.1		7.0	7.0		7.0	7.0	7.0
/ehicle Extension (s)		3.0			3.0		5.0	5.0		5.0	5.0	5.0
ane Grp Cap (vph)		609			817		250	1002		154	957	446
/s Ratio Prot								c0.22			0.12	
/s Ratio Perm		c0.14			0.09		0.03			0.18		0.01
/c Ratio		0.27			0.17		0.10	0.70		0.56	0.36	0.03
Jniform Delay, d1		13.0			12.3		23.8	29.7		28.1	26.1	23.3
Progression Factor		1.00			1.00		1.00	1.00		1.00	1.00	1.00
ncremental Delay, d2		1.1			0.5		0.4	2.7		7.3	0.5	0.1
Delay (s)		14.1			12.7		24.2	32.4		35.4	26.6	23.4
evel of Service		В			В		С	С		D	С	С
Approach Delay (s)		14.1			12.7			32.2			27.8	
Approach LOS		В			В			С			С	
ntersection Summary												
ICM 2000 Control Delay			26.3	Н	CM 2000	Level of	Service		С			
ICM 2000 Volume to Capacity	ratio		0.43									
Actuated Cycle Length (s)			100.0	S	um of los	t time (s)			15.1			
ntersection Capacity Utilization	1		88.4%	IC	CU Level of	of Service			E			
Analysis Period (min)			15									
Critical Lane Group												

Uppers Quarry Traffic Impact Study TMIG

Timings 3: Davis Road & Lu	undys L	ane					<203	5 Bacl	kgroun	id> AM	Peak Hou 09-14-202
	۶	+	4	ł	*	1	1	1	Ŧ	~	
Lane Group	EBL	EBT	WBL	WBT	WBR	NBL	NBT	SBL	SBT	SBR	
Lane Configurations	<u>۳</u>	f,	<u>۲</u>	<b>↑</b>	1	ሻ	4	<u>۳</u>	<b>↑</b>	1	
Traffic Volume (vph)	153	633	45	500	132	22	139	136	94	159	
Future Volume (vph)	153	633	45	500	132	22	139	136	94	159	
Turn Type	Perm	NA	Perm	NA	Perm	Perm	NA	Perm	NA	Perm	
Protected Phases		2		6			4		8		
Permitted Phases	2		6		6	4		8		8	
Detector Phase	2	2	6	6	6	4	4	8	8	8	
Switch Phase											
Minimum Initial (s)	22.0	22.0	22.0	22.0	22.0	15.0	15.0	15.0	15.0	15.0	
Minimum Split (s)	36.0	36.0	36.0	36.0	36.0	32.0	32.0	32.0	32.0	32.0	
Total Split (s)	53.0	53.0	53.0	53.0	53.0	37.0	37.0	37.0	37.0	37.0	
Total Split (%)	58.9%	58.9%	58.9%	58.9%	58.9%	41.1%	41.1%	41.1%	41.1%	41.1%	
Yellow Time (s)	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	
All-Red Time (s)	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	
ost Time Adjust (s)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Fotal Lost Time (s)	7.0	7.0	7.0	7.0	7.0	7.0	7.0	7.0	7.0	7.0	
_ead/Lag											
Lead-Lag Optimize?											
Recall Mode	C-Max	C-Max	Max	Max	Max	None	None	None	None	None	
Act Effct Green (s)	57.4	57.4	57.4	57.4	57.4	18.6	18.6	18.6	18.6	18.6	
Actuated g/C Ratio	0.64	0.64	0.64	0.64	0.64	0.21	0.21	0.21	0.21	0.21	
v/c Ratio	0.36	0.59	0.16	0.48	0.14	0.11	0.56	0.71	0.32	0.40	
Control Delay	11.6	13.1	9.6	11.2	2.0	27.9	35.6	52.0	31.8	74	
Queue Delay	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Total Delay	11.6	13.1	9.6	11.2	2.0	27.9	35.6	52.0	31.8	74	
05	0 R	R	Δ.0	R	0 	c	оо П	0 <u>-</u> .0	CC	Α	
Approach Delay	U	12.8	~	93		5	34 7	5	28.9		
Approach LOS		12.0 B		Δ			C.		20.0 C		
atomotica Ouromotica				~			Ū		Ũ		
Intersection Summary											
Cycle Length: 90											
Actuated Cycle Length: 90											
Unset: 0 (0%), Referenced	to phase 2	EBIL, St	art of Gre	en							
Natural Cycle: 70											
Control Type: Actuated-Coo	rainated										
viaximum v/c Ratio: 0.71											
ntersection Signal Delay: 1	b./	N.		li 	ntersectio	n LOS: B	0				
ntersection Capacity Utiliza	tion 101.19	//o		10	JU Level	of Service	e G				
Analysis Period (min) 15											
Splits and Phases: 3: Day	is Road &	Lundvs L	ane								
						-	۱.				

→ ø2 (R)	<b>™</b> Ø4	
53 s	37 s	
<b>◆</b> Ø6	\$ Ø8	
53 s	37 s	

Synchro 10 Report

HCM Signalized Intersection Capacity Analysis 3: Davis Road & Lundys Lane <2035 Background> AM Peak Hour 09-14-2021

	٦	-	$\mathbf{\hat{z}}$	4	+	×	٠	Ť	۲	1	Ŧ	~
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	<u></u>	ĥ		ሻ	•	1	ň	1.		5	•	1
Traffic Volume (vph)	153	633	18	45	500	132	22	139	30	136	94	159
Future Volume (vph)	153	633	18	45	500	132	22	139	30	136	94	159
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Total Lost time (s)	7.0	7.0		7.0	7.0	7.0	7.0	7.0		7.0	7.0	7.0
Lane Util. Factor	1.00	1.00		1.00	1.00	1.00	1.00	1.00		1.00	1.00	1.00
Frpb, ped/bikes	1.00	1.00		1.00	1.00	1.00	1.00	1.00		1.00	1.00	1.00
Flpb, ped/bikes	1.00	1.00		1.00	1.00	1.00	1.00	1.00		1.00	1.00	1.00
Frt	1.00	1.00		1.00	1.00	0.85	1.00	0.97		1.00	1.00	0.85
Flt Protected	0.95	1.00		0.95	1.00	1.00	0.95	1.00		0.95	1.00	1.00
Satd. Flow (prot)	1656	1828		1467	1743	1442	1444	1519		1530	1532	1392
Flt Permitted	0.41	1.00		0.31	1.00	1.00	0.69	1.00		0.61	1.00	1.00
Satd. Flow (perm)	718	1828		476	1743	1442	1052	1519		985	1532	1392
Peak-hour factor, PHF	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94
Adj. Flow (vph)	163	673	19	48	532	140	23	148	32	145	100	169
RTOR Reduction (vph)	0	1	0	0	0	51	0	10	0	0	0	134
Lane Group Flow (vph)	163	691	0	48	532	89	23	170	0	145	100	35
Confl. Peds. (#/hr)			1	1								
Heavy Vehicles (%)	9%	3%	19%	23%	9%	12%	25%	20%	30%	18%	24%	16%
Turn Type	Perm	NA		Perm	NA	Perm	Perm	NA		Perm	NA	Perm
Protected Phases		2			6			4			8	
Permitted Phases	2			6		6	4			8		8
Actuated Green, G (s)	57.4	57.4		57.4	57.4	57.4	18.6	18.6		18.6	18.6	18.6
Effective Green, g (s)	57.4	57.4		57.4	57.4	57.4	18.6	18.6		18.6	18.6	18.6
Actuated g/C Ratio	0.64	0.64		0.64	0.64	0.64	0.21	0.21		0.21	0.21	0.21
Clearance Time (s)	7.0	7.0		7.0	7.0	7.0	7.0	7.0		7.0	7.0	7.0
Vehicle Extension (s)	4.0	4.0		4.0	4.0	4.0	2.0	2.0		2.0	2.0	2.0
Lane Grp Cap (vph)	457	1165		303	1111	919	217	313		203	316	287
v/s Ratio Prot		c0.38			0.31			0.11			0.07	
v/s Ratio Perm	0.23			0.10		0.06	0.02			c0.15		0.03
v/c Ratio	0.36	0.59		0.16	0.48	0.10	0.11	0.54		0.71	0.32	0.12
Uniform Delay, d1	7.6	9.5		6.6	8.5	6.3	29.0	31.9		33.2	30.3	29.1
Progression Factor	1.00	1.00		1.00	1.00	1.00	1.00	1.00		1.00	1.00	1.00
Incremental Delay, d2	2.2	2.2		1.1	1.5	0.2	0.1	1.0		9.5	0.2	0.1
Delay (s)	9.8	11.7		7.7	10.0	6.5	29.0	32.9		42.7	30.5	29.1
Level of Service	A	В		Α	А	Α	С	С		D	С	С
Approach Delay (s)		11.4			9.2			32.5			34.2	
Approach LOS		В			А			С			С	
Intersection Summary												
HCM 2000 Control Delay			16.9	Н	CM 2000	Level of	Service		В			
HCM 2000 Volume to Capa	acity ratio		0.62									
Actuated Cycle Length (s)			90.0	S	um of los	t time (s)			14.0			
Intersection Capacity Utilization	ation		101.1%	IC	U Level	of Service			G			
Analysis Period (min)			15									
- Oritical Lana Origina												

c Critical Lane Group

Uppers Quarry Traffic Impact Study TMIG

Timings 4: Thorold Townline	Road	& Tho	<203	5 Bacl	kgroun	d> AM	Peak Hour 09-14-2021				
	۶	-	$\mathbf{r}$	4	+	•	•	t	1	ţ	
Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	SBL	SBT	
Lane Configurations	<u>۲</u>	- <b>†</b> †	1	<u>۲</u>	- <b>†</b> †	1	ሻ	4	ሻ	4	
Traffic Volume (vph)	323	767	159	203	854	73	107	160	52	209	
Future Volume (vph)	323	767	159	203	854	73	107	160	52	209	
Turn Type	pm+pt	NA	Perm	pm+pt	NA	Perm	pm+pt	NA	Perm	NA	
Protected Phases	5	2		1	6		7	4		8	
Permitted Phases	2		2	6		6	4		8		
Detector Phase	5	2	2	1	6	6	7	4	8	8	
Switch Phase											
Minimum Initial (s)	8.0	10.0	10.0	8.0	10.0	10.0	8.0	10.0	10.0	10.0	
Minimum Split (s)	11.0	35.1	35.1	12.5	35.1	35.1	11.0	41.4	41.4	41.4	
Total Split (s)	27.0	48.6	48.6	17.4	39.0	39.0	11.0	54.0	43.0	43.0	
Total Split (%)	22.5%	40.5%	40.5%	14.5%	32.5%	32.5%	9.2%	45.0%	35.8%	35.8%	
Yellow Time (s)	3.0	4.1	4.1	3.0	4.1	4.1	3.0	4.1	4.1	4.1	
All-Red Time (s)	0.0	2.0	2.0	0.0	2.0	2.0	0.0	2.3	2.3	2.3	
Lost Time Adjust (s)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Total Lost Time (s)	3.0	6.1	6.1	3.0	6.1	6.1	3.0	6.4	6.4	6.4	
_ead/Lag	Lead	Lag	Lag	Lead	Lag	Lag	Lead		Lag	Lag	
Lead-Lag Optimize?	Yes	Yes	Yes	Yes	Yes	Yes	Yes		Yes	Yes	
Recall Mode	None	C-Max	C-Max	None	C-Max	C-Max	None	None	None	None	
Act Effct Green (s)	65.2	46.1	46.1	53.6	37.5	37.5	48.8	45.4	34.4	34.4	
Actuated g/C Ratio	0.54	0.38	0.38	0.45	0.31	0.31	0.41	0.38	0.29	0.29	
//c Ratio	0.92	0.60	0.27	0.71	0.81	0.14	0.56	0.42	0.18	0.94	
Control Delay	72.0	44.9	23.9	31.0	46.4	2.6	33.5	26.6	32.9	67.9	
Queue Delay	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Fotal Delay	72.0	44.9	23.9	31.0	46.4	2.6	33.5	26.6	32.9	67.9	
LOS	E	D	С	С	D	A	С	С	С	E	
Approach Delay		49.2			40.8			28.7		64.0	
Approach LOS		D			D			C		E	
Intersection Summary											
Cycle Length: 120											
Actuated Cycle Length: 120											
Offset: 0 (0%), Referenced to	o phase 2:	EBTL an	d 6:WBTL	, Start of	Green						
Natural Cycle: 100											
Control Type: Actuated-Coor	rdinated										
Maximum v/c Ratio: 0.94											
ntersection Signal Delay: 46	5.2			lr	ntersectio	n LOS: D					
intersection Capacity Utilizat	ion 89.3%			IC	CU Level	of Service	θE				
Analysis Period (min) 15											

Splits and Phases:	4: Thorold Townline Road &	Thorold Stone Road
--------------------	----------------------------	--------------------

Ø1		
17.4 s	48.6 s	54 s
	♥ ♥ Ø6 (R)	★ Ø7
27 s	39 s	11s 43s

Synchro 10 Report

HCM Signalized Intersection Capacity Analysis 4: Thorold Townline Road & Thorold Stone Road <2035 Background> AM Peak Hour 09-14-2021

	۶	+	*	4	Ļ	*	•	1	*	1	Ŧ	~
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	ľ	<u></u>	1	ľ	<u></u>	1	ľ	¢Î		ľ	¢Î	
Traffic Volume (vph)	323	767	159	203	854	73	107	160	80	52	209	205
Future Volume (vph)	323	767	159	203	854	73	107	160	80	52	209	205
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Total Lost time (s)	3.0	6.1	6.1	3.0	6.1	6.1	3.0	6.4		6.4	6.4	
Lane Util. Factor	1.00	0.95	1.00	1.00	0.95	1.00	1.00	1.00		1.00	1.00	
Frpb, ped/bikes	1.00	1.00	1.00	1.00	1.00	0.97	1.00	1.00		1.00	1.00	
Flpb, ped/bikes	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00		1.00	1.00	
Frt	1.00	1.00	0.85	1.00	1.00	0.85	1.00	0.95		1.00	0.93	
Flt Protected	0.95	1.00	1.00	0.95	1.00	1.00	0.95	1.00		0.95	1.00	
Satd. Flow (prot)	1641	3471	1369	1444	3505	1453	1492	1535		1641	1497	
Flt Permitted	0.11	1.00	1.00	0.28	1.00	1.00	0.19	1.00		0.60	1.00	
Satd. Flow (perm)	197	3471	1369	422	3505	1453	296	1535		1043	1497	
Peak-hour factor, PHF	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96
Adj. Flow (vph)	336	799	166	211	890	76	111	167	83	54	218	214
RTOR Reduction (vph)	0	0	82	0	0	52	0	16	0	0	30	0
Lane Group Flow (vph)	336	799	84	211	890	24	111	234	0	54	402	0
Confl. Peds. (#/hr)	4					4						
Heavy Vehicles (%)	10%	4%	18%	25%	3%	8%	21%	14%	25%	10%	18%	17%
Turn Type	pm+pt	NA	Perm	pm+pt	NA	Perm	pm+pt	NA		Perm	NA	
Protected Phases	5	2		1	6		7	4			8	
Permitted Phases	2		2	6		6	4			8		
Actuated Green, G (s)	62.1	46.1	46.1	50.4	37.4	37.4	45.4	45.4		34.4	34.4	
Effective Green, g (s)	62.1	46.1	46.1	50.4	37.4	37.4	45.4	45.4		34.4	34.4	
Actuated g/C Ratio	0.52	0.38	0.38	0.42	0.31	0.31	0.38	0.38		0.29	0.29	
Clearance Time (s)	3.0	6.1	6.1	3.0	6.1	6.1	3.0	6.4		6.4	6.4	
Vehicle Extension (s)	2.5	6.0	6.0	2.5	6.0	6.0	2.5	2.3		2.3	2.3	
Lane Grp Cap (vph)	363	1333	525	287	1092	452	191	580		298	429	
v/s Ratio Prot	c0.17	0.23		0.08	0.25		c0.04	0.15			c0.27	
v/s Ratio Perm	c0.31		0.06	0.23		0.02	0.18			0.05		
v/c Ratio	0.93	0.60	0.16	0.74	0.82	0.05	0.58	0.40		0.18	0.94	
Uniform Delay, d1	33.4	29.6	24.2	24.1	38.1	28.9	27.8	27.4		32.2	41.7	
Progression Factor	1.63	1.41	3.12	1.00	1.00	1.00	1.00	1.00		1.00	1.00	
Incremental Delay, d2	24.4	1.6	0.5	8.9	6.7	0.2	3.7	0.3		0.2	27.8	
Delay (s)	78.8	43.2	76.3	32.9	44.8	29.1	31.4	27.6		32.4	69.6	
Level of Service	E	D	E	С	D	С	С	С		С	E	
Approach Delay (s)		56.6			41.7			28.8			65.4	
Approach LOS		Е			D			С			E	
Intersection Summary												
HCM 2000 Control Delay			49.6	H	CM 2000	Level of	Service		D			
HCM 2000 Volume to Capac	ity ratio		0.93									
Actuated Cycle Length (s)			120.0	S	um of lost	time (s)			18.5			
Intersection Capacity Utilizat	ion		89.3%	IC	U Level o	of Service	Э		E			
Analysis Period (min)			15									
a Critical Lana Crown												

c Critical Lane Group

Uppers Quarry Traffic Impact Study TMIG

5: Thorold Townlin	e Road	& Lun						09-14-202			
	۶	-	$\mathbf{\hat{z}}$	4	+	1	Ť	1	ŧ	4	
Lane Group	EBL	EBT	EBR	WBL	WBT	NBL	NBT	SBL	SBT	SBR	
Lane Configurations	ሻ	<b>↑</b>	1	ሻ	ef 👘	ሻ	ef 👘	ሻ	<b>↑</b>	1	
Traffic Volume (vph)	203	607	107	38	422	77	140	44	85	82	
Future Volume (vph)	203	607	107	38	422	77	140	44	85	82	
Turn Type	Perm	NA	Perm	Perm	NA	Perm	NA	Perm	NA	Perm	
Protected Phases		2			6		4		8		
Permitted Phases	2		2	6		4		8		8	
Detector Phase	2	2	2	6	6	4	4	8	8	8	
Switch Phase											
Vinimum Initial (s)	20.0	20.0	20.0	20.0	20.0	10.0	10.0	10.0	10.0	10.0	
Vinimum Split (s)	29.0	29.0	29.0	29.0	29.0	35.0	35.0	35.0	35.0	35.0	
Total Split (s)	65.0	65.0	65.0	65.0	65.0	35.0	35.0	35.0	35.0	35.0	
Total Split (%)	65.0%	65.0%	65.0%	65.0%	65.0%	35.0%	35.0%	35.0%	35.0%	35.0%	
rellow Time (s)	5.0	5.0	5.0	5.0	5.0	4.0	4.0	4.0	4.0	4.0	
All-Red Time (s)	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	
ost Time Adjust (s)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
otal Lost Time (s)	7.0	7.0	7.0	7.0	7.0	6.0	6.0	6.0	6.0	6.0	
.ead/Lag											
ead-Lag Optimize?											
Recall Mode	C-Max	C-Max	C-Max	Max	Max	None	None	None	None	None	
Act Effct Green (s)	68.8	68.8	68.8	68.8	68.8	18.2	18.2	18.2	18.2	18.2	
Actuated g/C Ratio	0.69	0.69	0.69	0.69	0.69	0.18	0.18	0.18	0.18	0.18	
//c Ratio	0.45	0.52	0.11	0.09	0.44	0.39	0.63	0.29	0.31	0.29	
Control Delay	12.0	10.4	4.0	7.1	8.9	39.8	43.8	38.2	36.6	9.6	
Queue Delay	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Total Delay	12.0	10.4	4.0	7.1	8.9	39.8	43.8	38.2	36.6	9.6	
.0S	В	В	А	А	А	D	D	D	D	А	
Approach Delay		10.0			8.8		42.6		26.4		
Approach LOS		Α			А		D		С		
ntersection Summary											
Cycle Length: 100											
Actuated Cycle Length: 100											
Offset: 0 (0%) Referenced	to phase 2	EBTI St	art of Gre	en							
Jatural Cycle: 80											
Control Type: Actuated-Cor	rdinated										
Maximum v/c Ratio: 0.63											
ntersection Signal Delay: 1	5.8			Ir	ntersectio	n LOS: B					
ntersection Capacity Utiliza	tion 88.2%			10	CU Level	of Service	ε				
Analysis Period (min) 15											

Ø2 (R)	A 04
65 s	35 s
€ Ø6	<b>↓</b> Ø8
65 s	35 s

Synchro 10 Report

HCM Signalized Intersection Capacity Analysis 5: Thorold Townline Road & Lundys Lane <2035 Background> AM Peak Hour 09-14-2021

	٦	+	*	•	ł	*	•	Ť	1	1	Ŧ	~
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	ľ	•	1	ľ	4Î		ľ	4Î		٢	•	1
Traffic Volume (vph)	203	607	107	38	422	78	77	140	37	44	85	82
Future Volume (vph)	203	607	107	38	422	78	77	140	37	44	85	82
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Total Lost time (s)	7.0	7.0	7.0	7.0	7.0		6.0	6.0		6.0	6.0	6.0
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00		1.00	1.00		1.00	1.00	1.00
Frpb, ped/bikes	1.00	1.00	1.00	1.00	1.00		1.00	1.00		1.00	1.00	1.00
Flpb, ped/bikes	1.00	1.00	1.00	1.00	1.00		1.00	1.00		1.00	1.00	1.00
Frt	1.00	1.00	0.85	1.00	0.98		1.00	0.97		1.00	1.00	0.85
Flt Protected	0.95	1.00	1.00	0.95	1.00		0.95	1.00		0.95	1.00	1.00
Satd. Flow (prot)	1582	1810	1495	1752	1760		1612	1607		1671	1638	1252
Flt Permitted	0.42	1.00	1.00	0.35	1.00		0.70	1.00		0.51	1.00	1.00
Satd. Flow (perm)	701	1810	1495	648	1760		1184	1607		893	1638	1252
Peak-hour factor, PHF	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93
Adj. Flow (vph)	218	653	115	41	454	84	83	151	40	47	91	88
RTOR Reduction (vph)	0	0	17	0	5	0	0	11	0	0	0	72
Lane Group Flow (vph)	218	653	98	41	533	0	83	180	0	47	91	16
Confl. Peds. (#/hr)	1					1						
Heavy Vehicles (%)	14%	5%	8%	3%	6%	0%	12%	17%	5%	8%	16%	29%
Turn Type	Perm	NA	Perm	Perm	NA		Perm	NA		Perm	NA	Perm
Protected Phases		2			6			4			8	
Permitted Phases	2		2	6			4			8		8
Actuated Green, G (s)	68.8	68.8	68.8	68.8	68.8		18.2	18.2		18.2	18.2	18.2
Effective Green, q (s)	68.8	68.8	68.8	68.8	68.8		18.2	18.2		18.2	18.2	18.2
Actuated g/C Ratio	0.69	0.69	0.69	0.69	0.69		0.18	0.18		0.18	0.18	0.18
Clearance Time (s)	7.0	7.0	7.0	7.0	7.0		6.0	6.0		6.0	6.0	6.0
Vehicle Extension (s)	5.0	5.0	5.0	5.0	5.0		5.0	5.0		5.0	5.0	5.0
Lane Grp Cap (vph)	482	1245	1028	445	1210		215	292		162	298	227
v/s Ratio Prot		c0.36			0.30			c0.11			0.06	
v/s Ratio Perm	0.31		0.07	0.06			0.07			0.05		0.01
v/c Ratio	0.45	0.52	0.10	0.09	0.44		0.39	0.62		0.29	0.31	0.07
Uniform Delay, d1	7.1	7.6	5.2	5.2	7.0		36.0	37.7		35.3	35.4	33.9
Progression Factor	1.00	1.00	1.00	1.00	1.00		1.00	1.00		1.00	1.00	1.00
Incremental Delay, d2	3.0	1.6	0.2	0.4	1.2		2.4	5.5		2.1	1.2	0.3
Delay (s)	10.1	9.2	5.4	5.6	8.1		38.4	43.2		37.4	36.6	34.2
Level of Service	В	А	A	A	А		D	D		D	D	C
Approach Delay (s)		9.0			8.0			41.8			35.8	-
Approach LOS		А			A			D			D	
Intersection Summary												
HCM 2000 Control Delay			16.0	Н	CM 2000	Level of S	Service		В			
HCM 2000 Volume to Capa	acity ratio		0.54									
Actuated Cycle Length (s)			100.0	S	um of lost	time (s)			13.0			
Intersection Capacity Utiliza	ation		88.2%	IC	U Level o	of Service			E			
Analysis Period (min)			15									
a Critical Lana Crown												

c Critical Lane Group

Uppers Quarry Traffic Impact Study TMIG

6: Thorold Townlin	e Road		09-14-202						
	٦	-	4	+	1	1	1	Ŧ	
Lane Group	EBL	EBT	WBL	WBT	NBL	NBT	SBL	SBT	
Lane Configurations		4		4		4		- <b>4</b> >	
Traffic Volume (vph)	19	126	52	170	24	317	11	538	
Future Volume (vph)	19	126	52	170	24	317	11	538	
Turn Type	Perm	NA	Perm	NA	Perm	NA	Perm	NA	
Protected Phases		2		6		4		8	
Permitted Phases	2		6		4		8		
Detector Phase	2	2	6	6	4	4	8	8	
Switch Phase									
Minimum Initial (s)	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	
Minimum Split (s)	30.5	30.5	30.5	30.5	34.0	34.0	30.5	30.5	
Total Split (s)	31.0	31.0	31.0	31.0	59.0	59.0	59.0	59.0	
Total Split (%)	34.4%	34.4%	34.4%	34.4%	65.6%	65.6%	65.6%	65.6%	
Yellow Time (s)	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0	
All-Red Time (s)	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	
Lost Time Adjust (s)		0.0		0.0		0.0		0.0	
Total Lost Time (s)		6.0		6.0		6.0		6.0	
Lead/Lag									
Lead-Lag Optimize?									
Recall Mode	C-Max	C-Max	Max	Max	Max	Max	Max	Max	
Act Effct Green (s)		25.0		25.0		53.0		53.0	
Actuated g/C Ratio		0.28		0.28		0.59		0.59	
v/c Ratio		0.36		0.57		0.50		0.68	
Control Delay		27.9		33.0		12.4		17.2	
Queue Delav		0.0		0.0		0.0		0.0	
Total Delay		27.9		33.0		12.4		17.2	
I OS		C		С		B		B	
Approach Delay		27.9		33.0		12 4		17.2	
Approach LOS		C		C		В		В	
Intersection Summary									
Cvcle Lenath: 90									
Actuated Cycle Length: 90									
Offset: 0 (0%) Referenced	to phase 2	EBTI St	art of Gre	en					
Natural Cycle: 70	10 prideo 21	, 00							
Control Type: Actuated-Cor	ordinated								
Maximum v/c Ratio: 0.68	anatod								
ntersection Signal Delay: 1	98			Ir	ntersectio	n I OS' B			
ntersection Canacity Utiliza	ation 66 7%			10	CULEVE	of Service	э.С		
Analysis Period (min) 15				N	00 2000	0.001100			

→ Ø2 (R)		
31 s	59 s	
<b>₩</b> Ø6		
31 s	59 s	

Synchro 10 Report

HCM Signalized Intersection Capacity Analysis 6: Thorold Townline Road & Beaverdams Road <2035 Background> AM Peak Hour 09-14-2021

	۶	-	$\mathbf{\hat{v}}$	4	-	×	٩.	Ť	۲	1	Ŧ	~
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		\$			\$			\$			÷	
Traffic Volume (vph)	19	126	16	52	170	22	24	317	83	11	538	19
Future Volume (vph)	19	126	16	52	170	22	24	317	83	11	538	19
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Total Lost time (s)		6.0			6.0			6.0			6.0	
Lane Util. Factor		1.00			1.00			1.00			1.00	
Frpb, ped/bikes		1.00			1.00			1.00			1.00	
Flpb, ped/bikes		1.00			1.00			1.00			1.00	
Frt		0.99			0.99			0.97			1.00	
Flt Protected		0.99			0.99			1.00			1.00	
Satd. Flow (prot)		1804			1838			1625			1568	
Flt Permitted		0.94			0.90			0.95			0.99	
Satd. Flow (perm)		1714			1669			1551			1554	
Peak-hour factor, PHF	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Adj. Flow (vph)	21	137	17	57	185	24	26	345	90	12	585	21
RTOR Reduction (vph)	0	4	0	0	4	0	0	10	0	0	1	0
Lane Group Flow (vph)	0	171	0	0	262	0	0	451	0	0	617	0
Confl. Peds. (#/hr)			5	5			6					6
Heavy Vehicles (%)	5%	2%	9%	0%	1%	2%	0%	18%	0%	9%	21%	9%
Turn Type	Perm	NA		Perm	NA		Perm	NA		Perm	NA	
Protected Phases		2			6			4			8	
Permitted Phases	2			6			4			8		
Actuated Green, G (s)		25.0			25.0			53.0			53.0	
Effective Green, g (s)		25.0			25.0			53.0			53.0	
Actuated g/C Ratio		0.28			0.28			0.59			0.59	
Clearance Time (s)		6.0			6.0			6.0			6.0	
Vehicle Extension (s)		5.0			5.0			5.0			5.0	
Lane Grp Cap (vph)		476			463			913			915	
v/s Ratio Prot												
v/s Ratio Perm		0.10			c0.16			0.29			c0.40	
v/c Ratio		0.36			0.57			0.49			0.67	
Uniform Delay, d1		26.1			27.9			10.7			12.6	
Progression Factor		1.00			1.00			1.00			1.00	
Incremental Delay, d2		2.1			5.0			1.9			4.0	
Delay (s)		28.2			32.8			12.6			16.6	
Level of Service		С			С			В			В	
Approach Delay (s)		28.2			32.8			12.6			16.6	
Approach LOS		С			С			В			В	
Intersection Summary												
HCM 2000 Control Delay			19.6	Н	CM 2000	Level of S	Service		В			
HCM 2000 Volume to Capacit	ty ratio		0.64									
Actuated Cycle Length (s)			90.0	S	um of los	t time (s)			12.0			
Intersection Capacity Utilization	on		66.7%	IC	U Level	of Service			С			
Analysis Period (min)			15									
c Critical Lane Group												

Uppers Quarry Traffic Impact Study TMIG

7: Thorold Townline	e Road	& Upp	ers La	ne	,		09-14-2021
	4	•	Ť	1	1	Ļ	
Movement	WBL	WBR	NBT	NBR	SBL	SBT	
Lane Configurations	Y		el el		٦	1	
Traffic Volume (veh/h)	0	0	458	0	0	419	
Future Volume (Veh/h)	0	0	458	0	0	419	
Sign Control	Stop		Free			Free	
Grade	0%		0%			0%	
Peak Hour Factor	0.93	0.93	0.93	0.93	0.93	0.93	
Hourly flow rate (vph)	0	0	492	0	0	451	
Pedestrians							
Lane Width (m)							
Walking Speed (m/s)							
Percent Blockage							
Right turn flare (veh)							
Median type			None			None	
Median storage veh)							
Upstream signal (m)							
pX, platoon unblocked							
vC, conflicting volume	943	492			492		
vC1, stage 1 conf vol							
vC2, stage 2 conf vol							
vCu, unblocked vol	943	492			492		
tC, single (s)	6.4	6.2			4.1		
tC, 2 stage (s)							
tF (s)	3.5	3.3			2.2		
p0 queue free %	100	100			100		
cM capacity (veh/h)	294	581			1082		
Direction, Lane #	WB 1	NB 1	SB 1	SB 2			
Volume Total	0	492	0	451			
Volume Left	0	0	0	0			
Volume Right	0	0	0	0			
cSH	1700	1700	1700	1700			
Volume to Capacity	0.00	0.29	0.00	0.27			
Queue Length 95th (m)	0.0	0.0	0.0	0.0			
Control Delay (s)	0.0	0.0	0.0	0.0			
Lane LOS	A						
Approach Delay (s)	0.0	0.0	0.0				
Approach LOS	A						
Intersection Summary							
Average Delay			0.0				
Intersection Capacity Utiliza	ation		27.4%	IC	U Level of	of Service	e A
Analysis Period (min)			15				

Timings     <2035 Background> PM Peak Hour       1: Davis Road & Thorold Stone Road     09-14-2021												
	۶	-	$\mathbf{r}$	4	+	1	1	1	1	ţ	~	
Lane Group	EBL	EBT	EBR	WBL	WBT	NBL	NBT	NBR	SBL	SBT	SBR	
Lane Configurations	۲	<b>^</b>	1	۲	đħ	۲	નુ	1	1	•	1	
Traffic Volume (vph)	24	1255	736	211	1223	627	5	178	4	6	28	
Future Volume (vph)	24	1255	736	211	1223	627	5	178	4	6	28	
Turn Type	Perm	NA	Perm	pm+pt	NA	Split	NA	Perm	Split	NA	Perm	
Protected Phases		2		1	6	4	4		8	8		
Permitted Phases	2		2	6				4			8	
Detector Phase	2	2	2	1	6	4	4	4	8	8	8	
Switch Phase												
Minimum Initial (s)	20.0	20.0	20.0	5.0	20.0	10.0	10.0	10.0	10.0	10.0	10.0	
Minimum Split (s)	28.9	28.9	28.9	8.0	28.9	29.7	29.7	29.7	17.7	17.7	17.7	
Total Split (s)	55.0	55.0	55.0	14.0	69.0	33.3	33.3	33.3	17.7	17.7	17.7	
Total Split (%)	45.8%	45.8%	45.8%	11.7%	57.5%	27.8%	27.8%	27.8%	14.8%	14.8%	14.8%	
Yellow Time (s)	5.4	5.4	5.4	3.0	5.4	5.7	5.7	5.7	5.7	5.7	5.7	
All-Red Time (s)	1.5	1.5	1.5	0.0	1.5	2.0	2.0	2.0	2.0	2.0	2.0	
Lost Time Adjust (s)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Total Lost Time (s)	6.9	6.9	6.9	3.0	6.9	7.7	7.7	7.7	7.7	7.7	7.7	
Lead/Lag	Lag	Lag	Lag	Lead								
Lead-Lag Optimize?	Yes	Yes	Yes	Yes								
Recall Mode	C-Max	C-Max	C-Max	None	C-Max	None	None	None	None	None	None	
Act Effct Green (s)	52.2	52.2	52.2	73.1	69.2	25.6	25.6	25.6	10.0	10.0	10.0	
Actuated g/C Ratio	0.44	0.44	0.44	0.61	0.58	0.21	0.21	0.21	0.08	0.08	0.08	_
v/c Ratio	0.22	0.86	0.85	0.85	0.63	0.92	0.94	0.40	0.03	0.04	0.12	
Control Delay	29.6	38.4	25.2	55.8	28.5	/8.2	80.8	8.3	51.2	51.3	1.0	
Queue Delay	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
l otal Delay	29.6	38.4	25.2	55.8	28.5	78.2	80.8	8.3	51.2	51.3	1.0	
LOS	C	D	C	E	C	E	F	A	D	D	A	
Approach Delay		33.5			32.5		63.9			13.9		
Approach LOS		U			U		E			В		
Intersection Summary												
Cycle Length: 120												
Actuated Cycle Length: 120												
Offset: 0 (0%), Referenced to	o phase 2	:EBTL an	d 6:WBTL	, Start of	Green							
Natural Cycle: 105												
Control Type: Actuated-Coor	rdinated											
Maximum v/c Ratio: 0.94												
Intersection Signal Delay: 38	3.7			Ir	ntersectio	n LOS: D						
Intersection Capacity Utilizat Analysis Period (min) 15	ion 92.6%	)		10	CU Level	of Service	e F					
Splits and Phases: 1: Davi	is Road &	Thorold S	Stone Roa	ad								

✓ Ø1 ↓ → Ø2 (R)	<b>↓</b> _{Ø4}	1 Jos
14 s 55 s	33.3 s	17.7 s
✓ Ø6 (R)		
69 s		

Synchro 10 Report

HCM Signalized Intersection Capacity Analysis 1: Davis Road & Thorold Stone Road <2035 Background> PM Peak Hour

	٨	-	$\mathbf{\hat{z}}$	4	+	•	•	Ť	۲	1	ŧ	~
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	<u>۲</u>	- • • •	7	ሻ	<b>≜î</b> ≽		ሻ	ę	1	٦	•	7
Traffic Volume (vph)	24	1255	736	211	1223	1	627	5	178	4	6	28
Future Volume (vph)	24	1255	736	211	1223	1	627	5	178	4	6	28
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Total Lost time (s)	6.9	6.9	6.9	3.0	6.9		7.7	7.7	7.7	7.7	7.7	7.7
Lane Util. Factor	1.00	0.95	1.00	1.00	0.95		0.95	0.95	1.00	1.00	1.00	1.00
Frpb, ped/bikes	1.00	1.00	1.00	1.00	1.00		1.00	1.00	1.00	1.00	1.00	0.98
Flpb, ped/bikes	1.00	1.00	1.00	1.00	1.00		1.00	1.00	1.00	1.00	1.00	1.00
Frt	1.00	1.00	0.85	1.00	1.00		1.00	1.00	0.85	1.00	1.00	0.85
Flt Protected	0.95	1.00	1.00	0.95	1.00		0.95	0.95	1.00	0.95	1.00	1.00
Satd. Flow (prot)	1433	3539	1568	1671	3539		1681	1680	1482	1805	1810	1525
Flt Permitted	0.18	1.00	1.00	0.08	1.00		0.95	0.95	1.00	0.95	1.00	1.00
Satd. Flow (perm)	267	3539	1568	135	3539		1681	1680	1482	1805	1810	1525
Peak-hour factor, PHF	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95
Adj. Flow (vph)	25	1321	775	222	1287	1	660	5	187	4	6	29
RTOR Reduction (vph)	0	0	239	0	0	0	0	0	147	0	0	28
Lane Group Flow (vph)	25	1321	536	222	1288	0	330	335	40	4	6	1
Confl. Peds. (#/hr)							1					1
Heavy Vehicles (%)	26%	2%	3%	8%	2%	0%	2%	30%	9%	0%	5%	4%
Turn Type	Perm	NA	Perm	pm+pt	NA		Split	NA	Perm	Split	NA	Perm
Protected Phases		2		1	6		4	4		8	8	
Permitted Phases	2		2	6					4			8
Actuated Green, G (s)	49.1	49.1	49.1	66.1	66.1		25.6	25.6	25.6	6.0	6.0	6.0
Effective Green, g (s)	49.1	49.1	49.1	66.1	66.1		25.6	25.6	25.6	6.0	6.0	6.0
Actuated g/C Ratio	0.41	0.41	0.41	0.55	0.55		0.21	0.21	0.21	0.05	0.05	0.05
Clearance Time (s)	6.9	6.9	6.9	3.0	6.9		7.7	7.7	7.7	7.7	7.7	7.7
Vehicle Extension (s)	3.0	3.0	3.0	3.0	3.0		4.5	4.5	4.5	4.5	4.5	4.5
Lane Grp Cap (vph)	109	1448	641	253	1949		358	358	316	90	90	76
v/s Ratio Prot		0.37		c0.10	0.36		0.20	c0.20		0.00	c0.00	
v/s Ratio Perm	0.09		0.34	c0.38					0.03			0.00
v/c Ratio	0.23	0.91	0.84	0.88	0.66		0.92	0.94	0.13	0.04	0.07	0.02
Uniform Delay, d1	23.1	33.4	31.8	34.6	19.0		46.2	46.4	38.2	54.3	54.3	54.2
Progression Factor	1.00	1.00	1.00	1.45	1.48		1.00	1.00	1.00	1.00	1.00	1.00
Incremental Delay, d2	4.8	10.3	12.3	17.0	1.0		29.3	31.9	0.3	0.4	0.5	0.2
Delay (s)	28.0	43.7	44.1	67.2	29.2		75.5	78.3	38.5	54.6	54.9	54.4
Level of Service	С	D	D	E	С		E	E	D	D	D	D
Approach Delay (s)		43.6			34.8			68.5			54.5	
Approach LOS		D			С			E			D	
Intersection Summary												
HCM 2000 Control Delay			45.5	Н	CM 2000	Level of S	Service		D			
HCM 2000 Volume to Capa	icity ratio		0.86									
Actuated Cycle Length (s)	·		120.0	S	um of los	t time (s)			25.3			
Intersection Capacity Utiliza	ation		92.6%	IC	U Level	of Service			F			
Analysis Period (min)			15									

c Critical Lane Group

Uppers Quarry Traffic Impact Study TMIG

Lane Group         EBL         EBT         WBL         WBT         NBL         NBT         SBL         SBT         SBR           Lane Configurations         4         4         7         4         7         4         7         4         7         4         7         4         7         4         7         4         7         4         7         4         7         4         7         7         6         4         7         4         7         7         6         4         2         6         4         8         8           Protected Phases         2         6         6         4         8         8         8         8           Permitted Phase         2         6         6         4         8         8         8         8           Permitted Phase         2         2         6         6         4         8         8         8           Writch Phase         10.0         10.0         10.0         10.0         25.0         25.0         25.0         25.0         25.0         25.0         25.0         25.0         25.0         25.0         25.0         25.0         25.0         25.0											
Lane Group         EBL         EBT         WBL         WBT         NBL         NBT         SBL         SBT         SBR           Lane Configurations		٦	-	1	+	1	Ť	1	Ŧ	~	
Lane Configurations       A       A       A       A       A       A       A       A       A       A       A       A       A       A       A       A       A       A       A       A       A       A       A       A       A       A       A       B       A       Perm       NA       Perm<	Lane Group	EBL	EBT	WBL	WBT	NBL	NBT	SBL	SBT	SBR	
Traffic Volume (vph)       90       32       60       44       26       582       170       691       105         Future Volume (vph)       90       32       60       44       26       582       170       691       105         Future Volume (vph)       90       32       60       44       26       582       170       691       105         Protected Phases       2       6       4       8       8       8         Detector Phase       2       2       6       4       8       8       8         Switch Phase       10.0       10.0       10.0       10.0       25.0       25.0       25.0       25.0       25.0         Minimum Split (s)       38.1       38.1       38.1       38.1       38.1       38.1       38.1       38.1       38.1       38.1       38.1       38.1       38.1       38.1       38.1       38.1       38.1       38.1       38.1       38.1       38.1       38.1       38.1       38.1       38.1       38.1       38.1       38.1       38.1       38.1       38.1       38.1       38.1       38.1       38.1       38.1       38.1       38.1       38.1	Lane Configurations		4		4	<u>۲</u>	<b>≜</b> ⊅	ሻ	- <b>†</b> †	1	
Future Volume (vph)         90         32         60         44         26         582         170         691         105           Tum Type         Perm         NA         Perm         NA         Perm         NA         Perm         NA         Perm         Perm         NA         Perm         Perm         NA         Perm         Perm         NA         Perm         Perm <pern<pern<pern<pern<pern<pern<pern<pern< td=""><td>Traffic Volume (vph)</td><td>90</td><td>32</td><td>60</td><td>44</td><td>26</td><td>582</td><td>170</td><td>691</td><td>105</td><td></td></pern<pern<pern<pern<pern<pern<pern<pern<>	Traffic Volume (vph)	90	32	60	44	26	582	170	691	105	
Tum Type         Perm         NA         Perm         NA         Perm         NA         Perm         NA         Perm           Protected Phases         2         6         4         8         8           Detector Phase         2         2         6         4         8         8           Switch Phase         2         2         6         6         4         8         8           Switch Phase         2         2         6         6         4         4         8         8         8           Minimum Initial (s)         10.0         10.0         10.0         25.0         25.0         25.0         25.0         25.0         25.0         25.0         25.0         25.0         25.0         25.0         25.0         25.0         25.0         25.0         25.0         25.0         25.0         25.0         25.0         25.0         25.0         25.0         25.0         25.0         25.0         25.0         25.0         25.0         25.0         25.0         25.0         25.0         25.0         25.0         25.0         25.0         25.0         25.0         25.0         25.0         25.0         25.0         25.0         25	Future Volume (vph)	90	32	60	44	26	582	170	691	105	
Protected Phases 2 6 4 8 Permitted Phases 2 6 6 4 8 8 Switch Phase 2 2 6 6 4 8 8 Switch Phase 2 2 6 6 6 4 4 8 8 8 Switch Phase 4 4 8 8 8 Switch Phase 5 Switch Phase 5	Turn Type	Perm	NA	Perm	NA	Perm	NA	Perm	NA	Perm	
Permitted Phases 2 2 6 4 8 8 8 Detector Phase 2 2 6 6 4 4 8 8 8 Detector Phase 2 2 6 6 4 4 8 8 8 Detector Phase 2 2 6 6 6 4 4 8 8 8 Detector Phase 2 2 6 6 6 4 4 8 8 8 Detector Phase 2 2 6 6 6 4 4 8 8 8 Detector Phase 2 Minimum Initial (s) 10.0 10.0 10.0 25.0 25.0 25.0 25.0 25.0 Minimum Split (s) 38.1 38.1 38.1 38.1 32.0 32.0 32.0 32.0 32.0 Total Split (s) 40.0 40.0 40.0 40.0 60.0 60.0 60.0 60.0	Protected Phases		2		6		4		8		
Detector Phase 2 2 2 6 6 4 4 4 8 8 8 8 Switch Phase Winimum Initial (s) 10.0 10.0 10.0 25.0 25.0 25.0 25.0 25.0 25.0 Minimum Split (s) 38.1 38.1 38.1 38.1 38.1 32.0 32.0 32.0 32.0 Total Split (s) 40.0 40.0 40.0 40.0 60.0 60.0 60.0 60.0	Permitted Phases	2		6		4		8		8	
Switch Phase           Minimum Initial (s)         10.0         10.0         10.0         25.0         25.0         25.0         25.0           Minimum Split (s)         38.1         38.1         38.1         38.1         32.0         32.0         32.0         32.0         32.0         32.0           Total Split (s)         40.0         40.0         40.0         60.0%         60.0%         60.0%         60.0%         60.0%         60.0%         60.0%         60.0%         60.0%         60.0%         60.0%         60.0%         60.0%         60.0%         60.0%         60.0%         60.0%         60.0%         60.0%         60.0%         60.0%         60.0%         60.0%         60.0%         60.0%         60.0%         60.0%         60.0%         60.0%         60.0%         60.0%         60.0%         60.0%         60.0%         60.0%         60.0%         60.0%         60.0%         60.0%         60.0%         60.0%         60.0%         60.0%         60.0%         60.0%         60.0%         60.0%         60.0%         60.0%         60.0%         60.0%         60.0%         60.0%         60.0%         60.0%         60.0%         60.0%         60.0%         60.0%         60.0% <th< td=""><td>Detector Phase</td><td>2</td><td>2</td><td>6</td><td>6</td><td>4</td><td>4</td><td>8</td><td>8</td><td>8</td><td></td></th<>	Detector Phase	2	2	6	6	4	4	8	8	8	
Minimum Initial (s)       10.0       10.0       10.0       25.0       25.0       25.0       25.0       25.0         Minimum Split (s)       38.1       38.1       38.1       38.1       32.0       32.0       32.0       32.0         Total Split (s)       40.0       40.0       40.0       60.0       60.0       60.0       60.0       60.0         Total Split (s)       40.0%       40.0%       40.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0	Switch Phase										
Minimum Spit (s)       38.1       38.1       38.1       38.1       38.1       38.1       38.1       38.1       38.1       38.1       38.1       38.1       38.1       38.1       38.1       38.1       38.1       38.1       38.1       38.1       38.1       38.1       38.1       38.1       38.1       38.1       38.1       38.1       38.1       38.1       38.1       38.1       38.1       38.1       38.1       38.1       38.1       38.1       38.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.	Minimum Initial (s)	10.0	10.0	10.0	10.0	25.0	25.0	25.0	25.0	25.0	
10 tal Spitt (s)       40.0       40.0       40.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.0       60.	Minimum Split (s)	38.1	38.1	38.1	38.1	32.0	32.0	32.0	32.0	32.0	
Incar Spin (%)       40.0%       40.0%       40.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%       60.0%	Total Split (s)	40.0	40.0	40.0	40.0	60.0	60.0	60.0	60.0	60.0	
Yellow Ime (s)       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0	Total Split (%)	40.0%	40.0%	40.0%	40.0%	60.0%	60.0%	60.0%	60.0%	60.0%	
All-Red Time (s)       3.1       3.1       3.1       3.1       3.1       2.0       2.0       2.0       2.0       2.0       2.0       2.0       2.0       2.0       2.0       2.0       2.0       2.0       2.0       2.0       2.0       2.0       2.0       2.0       2.0       2.0       2.0       2.0       2.0       2.0       2.0       2.0       2.0       2.0       2.0       2.0       2.0       2.0       2.0       2.0       2.0       2.0       2.0       2.0       2.0       2.0       2.0       2.0       2.0       2.0       2.0       2.0       2.0       2.0       2.0       2.0       2.0       2.0       2.0       2.0       2.0       2.0       2.0       2.0       2.0       2.0       2.0       2.0       2.0       2.0       2.0       2.0       2.0       2.0       2.0       2.0       2.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0 <td>Yellow Time (s)</td> <td>5.0</td> <td>5.0</td> <td>5.0</td> <td>5.0</td> <td>5.0</td> <td>5.0</td> <td>5.0</td> <td>5.0</td> <td>5.0</td> <td></td>	Yellow Time (s)	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	
Lost Time Adjust (s)       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0	All-Red Time (s)	3.1	3.1	3.1	3.1	2.0	2.0	2.0	2.0	2.0	
Iotal Lost Ime (s)       8.1       8.1       7.0       7.0       7.0       7.0       7.0         Lead/Lag       Lead/Lag Optimize?       Recall Mode       C-Max       C-Max       Max       Max       None	Lost Time Adjust (s)		0.0		0.0	0.0	0.0	0.0	0.0	0.0	
LeadLag Optimize? Lead-Lag Optimize? Recall Mode C-Max C-Max Max Max None None None None None Act Effct Green (s) 46.8 46.8 38.1 38.1 38.1 38.1 38.1 Actuated g/C Ratio 0.47 0.47 0.47 0.38 0.38 0.38 0.38 0.38 v/c Ratio 0.28 0.35 0.13 0.52 0.79 0.57 0.17 Control Delay 20.0 16.1 17.5 23.9 49.3 25.4 3.2 Queue Delay 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 Total Delay 20.0 16.1 17.5 23.9 49.3 25.4 3.2 Queue Delay 20.0 16.1 17.5 23.9 49.3 25.4 3.2 Approach Delay 20.0 16.1 23.7 27.2 Approach LOS B B B C D C A Approach LOS B B B C C C Intersection Summary Cycle Length: 100 Actuated Cycle 75 Control Type: Actuated-Coordinated Maximum v/c Ratio: 0.79 Intersection LOS: C Intersection Capacity Utilization 78.5% ICU Level of Service D	Total Lost Time (s)		8.1		8.1	7.0	7.0	7.0	7.0	7.0	
Lead-Lag Optimize?         Recall Mode       C-Max       Max       Max       None       None       None         Act Effic Green (s)       46.8       46.8       38.1       38.1       38.1       38.1         Act Effic Green (s)       0.47       0.47       0.38       0.38       0.38       0.38         Actuated g/C Ratio       0.28       0.35       0.13       0.52       0.79       0.57       0.17         Control Delay       20.0       16.1       17.5       23.9       49.3       25.4       3.2         Queue Delay       0.0       0.0       0.0       0.0       0.0       0.0       0.0         Total Delay       20.0       16.1       17.5       23.9       49.3       25.4       3.2         LOS       B       B       C       D       C       A         Approach Delay       20.0       16.1       23.7       27.2         Approach LOS       B       B       C       C       C         Intersection Summary       C       C       C       C       C         Vice Length: 100       Actuated Cycle Length: 100       Actuated Cycle Length: 100       Actuated Cycle: 75       C       <	Lead/Lag										
Recall Mode         C-Max         C-Max         Max         Max         None	Lead-Lag Optimize?										
Act Effect Green (s)       46.8       46.8       38.1       38.1       38.1       38.1       38.1         Actuated g/C Ratio       0.47       0.47       0.38       0.38       0.38       0.38       0.38         ver Ratio       0.28       0.35       0.13       0.52       0.79       0.57       0.17         Control Delay       20.0       16.1       17.5       23.9       49.3       25.4       3.2         Queue Delay       0.0       0.0       0.0       0.0       0.0       0.0       0.0         Total Delay       20.0       16.1       17.5       23.9       49.3       25.4       3.2         LOS       B       B       B       C       D       C       A         Approach Delay       20.0       16.1       23.7       27.2         Approach LOS       B       B       C       C       C         Intersection Summary       20.0       16.1       23.7       27.2         Cycle Length: 100       Offset: 0 (0%), Referenced to phase 2:EBTL, Start of Green       Start of Green       Start of Green         Natural Cycle: 75       Control Type: Actuated-Coordinated       Maximum v/c Ratio: 0.79       Intersection LOS: C	Recall Mode	C-Max	C-Max	Max	Max	None	None	None	None	None	
Actuated g/C Ratio 0.47 0.47 0.38 0.38 0.38 0.38 0.38 0.38 0.38 v/c Ratio 0.28 0.35 0.13 0.52 0.79 0.57 0.17 Control Delay 0.0 16.1 17.5 23.9 49.3 25.4 3.2 Queue Delay 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 10.1 Tr.5 23.9 49.3 25.4 3.2 Control Delay 20.0 16.1 17.5 23.9 49.3 25.4 3.2 Control Delay 20.0 16.1 23.7 27.2 Approach Delay 20.0 16.1 23.7 27.2 Control LOS B B C C C C C C C C C C C C C C C C C	Act Effct Green (s)		46.8		46.8	38.1	38.1	38.1	38.1	38.1	
Vic Ratio         0.28         0.35         0.13         0.52         0.79         0.57         0.17           Control Delay         20.0         16.1         17.5         23.9         49.3         25.4         3.2           Queue Delay         0.0         0.0         0.0         0.0         0.0         0.0         0.0           Total Delay         20.0         16.1         17.5         23.9         49.3         25.4         3.2           LOS         B         B         C         D         C         A           Approach Delay         20.0         16.1         23.7         27.2           Approach LOS         B         B         C         C         C           Intersection Summary         C         C         C         C           Cycle Length: 100         Acturated Cycle Length: 100         Acturated Cycle: 75         C         C           Control Type: Actuated-Coordinated         Maximum v/c Ratio: 0.79         Intersection LOS: C         Intersection LOS: C         Intersection CApacity Utilization 78.5%         ICU Level of Service D	Actuated g/C Ratio		0.47		0.47	0.38	0.38	0.38	0.38	0.38	
Control Delay         20.0         16.1         17.5         23.9         49.3         25.4         3.2           Queue Delay         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0 <td>v/c Ratio</td> <td></td> <td>0.28</td> <td></td> <td>0.35</td> <td>0.13</td> <td>0.52</td> <td>0.79</td> <td>0.57</td> <td>0.17</td> <td></td>	v/c Ratio		0.28		0.35	0.13	0.52	0.79	0.57	0.17	
Cube Delay         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0	Control Delay		20.0		16.1	17.5	23.9	49.3	25.4	3.2	
Iteration         20.0         Ite.1         17.5         23.9         49.3         25.4         3.2           LOS         B         B         B         C         D         C         A           Approach Delay         20.0         16.1         23.7         27.2         Approach LOS         B         B         C         C         Intersection Summary           Cycle Length:         100         Offset:         0(%), Referenced to phase 2:EBTL, Start of Green         Valuated Cycle:         75           Control Type:         Actuated-Coordinated         Maximum v/c Ratio:         0.79         Intersection LOS:         C           Intersection Capacity Utilization 78.5%         ICU Level of Service D         ICU Level of Service D         ICU Level of Service D	Queue Delay		0.0		0.0	0.0	0.0	0.0	0.0	0.0	
LOS         B         B         C         D         C         A           Approach LOS         16.1         23.7         27.2         Approach LOS         B         C         C           Intersection Summary         B         C         C         C         C         C         C         C         C         C         C         C         C         C         C         C         C         C         C         C         C         C         C         C         C         C         C         C         C         C         C         C         C         C         C         C         C         C         C         C         C         C         C         C         C         C         C         C         C         C         C         C         C         C         C         C         C         C         C         C         C         C         C         C         C         C         C         C         C         C         C         C         C         C         C         C         C         C         C         C         C         C         C         C         C         C	l otal Delay		20.0		16.1	17.5	23.9	49.3	25.4	3.2	
Approach Lolay         20.0         16.1         23.7         27.2           Approach LOS         B         B         C         C           Intersection Summary         C         C         C           Cycle Length: 100         Actuated Cycle Length: 100         Actuated Cycle 2.5         C           Offset: 0 (0%), Referenced to phase 2:EBTL, Start of Green         Natural Cycle: 75         Control Type: Actuated-Coordinated           Maximum v/c Ratio: 0.79         Intersection LOS: C         Intersection LOS: C         Intersection Capacity Utilization 78.5%         ICU Level of Service D	LOS		B		B	В	C	D	C	A	
Approach LOS B B C C C Intersection Summary Cycle Length: 100 Offset: 0 (0%), Referenced to phase 2:EBTL, Start of Green Natural Cycle: 75 Control Type: Actuated-Coordinated Maximum v/c Ratio: 0.79 Intersection Signal Delay: 24.1 Intersection LOS: C Intersection Capacity Utilization 78.5% ICU Level of Service D	Approach Delay		20.0		16.1		23.7		27.2		
Intersection Summary Cycle Length: 100 Actuated Cycle Length: 100 Offset: 0 (0%), Referenced to phase 2:EBTL, Start of Green Natural Cycle: 75 Control Type: Actuated-Coordinated Maximum v/c Ratio: 0.79 Intersection LOS: C Intersection Capacity Utilization 78.5% ICU Level of Service D	Approach LOS		В		В		C		C		
Cycle Length: 100 Actuated Cycle Length: 100 Offset: 0 (0%), Referenced to phase 2:EBTL, Start of Green Natural Cycle: 75 Control Type: Actuated-Coordinated Maximum v/c Ratio: 0.79 Intersection Signal Delay: 24.1 Intersection LOS: C Intersection Capacity Utilization 78.5% ICU Level of Service D	Intersection Summary										
Actuated Cycle Length: 100 Offset: 0 (0%), Referenced to phase 2:EBTL, Start of Green Natural Cycle: 75 Control Type: Actuated-Coordinated Maximum v/c Ratio: 0.79 Intersection Signal Delay: 24.1 Intersection LOS: C Intersection Capacity Utilization 78.5% ICU Level of Service D	Cycle Length: 100										
Offset: 0 (0%), Referenced to phase 2:EBTL, Start of Green         Natural Cycle: 75         Control Type: Actuated-Coordinated         Maximum v/c Ratio: 0.79         Intersection Signal Delay: 24.1         Intersection Capacity Utilization 78.5%         ICU Level of Service D	Actuated Cycle Length: 100										
Natural Cycle: 75         Control Type: Actuated-Coordinated         Maximum v/c Ratio: 0.79         Intersection Signal Delay: 24.1         Intersection Capacity Utilization 78.5%         ICU Level of Service D	Offset: 0 (0%), Referenced to	phase 2:	EBTL, St	art of Gre	en						
Control Type: Actuated-Coordinated Maximum v/c Ratio: 0.79 Intersection Signal Delay: 24.1 Intersection LOS: C Intersection Capacity Utilization 78.5% ICU Level of Service D	Natural Cycle: 75										
Maximum v/c Ratio: 0.79 Intersection Signal Delay: 24.1 Intersection LOS: C Intersection Capacity Utilization 78.5% ICU Level of Service D	Control Type: Actuated-Coord	dinated									
ntersection Signal Delay: 24.1 Intersection LOS: C ntersection Capacity Utilization 78.5% ICU Level of Service D	Vaximum v/c Ratio: 0.79										
Intersection Capacity Utilization 78.5% ICU Level of Service D	Intersection Signal Delay: 24.	1			I	ntersectio	n LOS: C				
	Intersection Capacity Utilization	on 78.5%			10	CU Level	of Service	e D			

opilis and Fliases.	2. Davis Rudu & Midya	ia raiis nu	du/Deaveruallis Rodu
[▲] ø2 (R)			<b>™</b> [†] Ø4
40 s			60 s
₹ø6			€ ▶ø8
40 s			60 s

Synchro 10 Report

HCM Signalized Intersection Capacity Analysis 2: Davis Road & Niagara Falls Road/Beaverdams Road <2035 Background> PM Peak Hour 09-14-2021

	۶	+	*	4	+	•	•	Ť	1	*	ŧ	~
Novement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
ane Configurations		\$			÷		۲	A		ľ	<u></u>	1
raffic Volume (vph)	90	32	31	60	44	147	26	582	41	170	691	105
Future Volume (vph)	90	32	31	60	44	147	26	582	41	170	691	105
deal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
fotal Lost time (s)		8.1			8.1		7.0	7.0		7.0	7.0	7.0
ane Util. Factor		1.00			1.00		1.00	0.95		1.00	0.95	1.00
-rt		0.97			0.92		1.00	0.99		1.00	1.00	0.85
It Protected		0.97			0.99		0.95	1.00		0.95	1.00	1.00
Satd. Flow (prot)		1667			1698		1805	3316		1770	3343	1583
It Permitted		0.70			0.88		0.28	1.00		0.32	1.00	1.00
Satd. Flow (perm)		1203			1520		531	3316		598	3343	1583
Peak-hour factor, PHF	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95
Adj. Flow (vph)	95	34	33	63	46	155	27	613	43	179	727	111
RTOR Reduction (vph)	0	7	0	0	40	0	0	7	0	0	0	69
ane Group Flow (vph)	0	155	0	0	224	0	27	649	0	179	727	42
leavy Vehicles (%)	2%	2%	30%	2%	1%	2%	0%	8%	5%	2%	8%	2%
Turn Type	Perm	NA		Perm	NA		Perm	NA		Perm	NA	Perm
Protected Phases		2			6			4			8	
Permitted Phases	2			6			4			8		8
Actuated Green, G (s)		46.8			46.8		38.1	38.1		38.1	38.1	38.1
Effective Green, g (s)		46.8			46.8		38.1	38.1		38.1	38.1	38.1
Actuated g/C Ratio		0.47			0.47		0.38	0.38		0.38	0.38	0.38
Clearance Time (s)		8.1			8.1		7.0	7.0		7.0	7.0	7.0
/ehicle Extension (s)		3.0			3.0		5.0	5.0		5.0	5.0	5.0
ane Grp Cap (vph)		563			711		202	1263		227	1273	603
/s Ratio Prot								0.20			0.22	
/s Ratio Perm		0.13			c0.15		0.05			c0.30		0.03
/c Ratio		0.27			0.32		0.13	0.51		0.79	0.57	0.07
Jniform Delay, d1		16.2			16.6		20.2	23.8		27.4	24.5	19.7
Progression Factor		1.00			1.00		1.00	1.00		1.00	1.00	1.00
ncremental Delay, d2		1.2			1.2		0.6	0.7		18.8	1.0	0.1
Delay (s)		17.4			17.8		20.8	24.5		46.2	25.5	19.8
evel of Service		В			В		С	С		D	С	В
Approach Delay (s)		17.4			17.8			24.4			28.5	
Approach LOS		В			В			С			С	
ntersection Summary												
ICM 2000 Control Delay			25.0	Н	CM 2000	Level of	Service		С			
ICM 2000 Volume to Capacit	y ratio		0.53									
Actuated Cycle Length (s)			100.0	S	um of lost	time (s)			15.1			
ntersection Capacity Utilization	n		78.5%	IC	CU Level of	of Service			D			
Analysis Period (min)			15									
Critical Lane Group												

Uppers Quarry Traffic Impact Study TMIG

3: Davis Road & Lu	ane	<2035 Background> PM Peak Hour 09-14-2021									
	٦	-	4	+	•	•	Ť	1	ţ	~	
ane Group	EBL	EBT	WBL	WBT	WBR	NBL	NBT	SBL	SBT	SBR	
ane Configurations	ሻ	ĥ	ሻ	•	1	ሻ	ĥ	ሻ	•	1	
Traffic Volume (vph)	208	717	42	718	216	46	141	239	125	184	
Future Volume (vph)	208	717	42	718	216	46	141	239	125	184	
Turn Type	pm+pt	NA	Perm	NA	Perm	Perm	NA	pm+pt	NA	Perm	
Protected Phases	5	2		6			4	3	8		
Permitted Phases	2		6		6	4		8		8	
Detector Phase	5	2	6	6	6	4	4	3	8	8	
Switch Phase											
Vinimum Initial (s)	5.0	22.0	22.0	22.0	22.0	15.0	15.0	5.0	15.0	15.0	
Vinimum Split (s)	8.0	36.0	36.0	36.0	36.0	32.0	32.0	8.0	32.0	32.0	
Fotal Split (s)	14.0	78.0	64.0	64.0	64.0	32.0	32.0	10.0	42.0	42.0	
Fotal Split (%)	11.7%	65.0%	53.3%	53.3%	53.3%	26.7%	26.7%	8.3%	35.0%	35.0%	
Yellow Time (s)	3.0	5.0	5.0	5.0	5.0	5.0	5.0	3.0	5.0	5.0	
All-Red Time (s)	0.0	2.0	2.0	2.0	2.0	2.0	2.0	0.0	2.0	2.0	
Lost Time Adjust (s)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Fotal Lost Time (s)	3.0	7.0	7.0	7.0	7.0	7.0	7.0	3.0	7.0	7.0	
_ead/Lag	Lead		Lag	Lag	Lag	Lag	Lag	Lead			
Lead-Lag Optimize?	Yes		Yes	Yes	Yes	Yes	Yes	Yes			
Recall Mode	None	C-Max	Max	Max	Max	Max	Max	None	Max	Max	
Act Effct Green (s)	75.0	71.0	57.0	57.0	57.0	25.0	25.0	39.0	35.0	35.0	
Actuated g/C Ratio	0.62	0.59	0.48	0.48	0.48	0.21	0.21	0.32	0.29	0.29	
//c Ratio	0.87	0.74	0.23	0.87	0.29	0.19	0.58	0.83	0.26	0.33	
Control Delay	51.7	23.2	23.4	43.1	8.7	41.6	47.3	58.5	34.4	6.0	
Queue Delay	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Fotal Delay	51.7	23.2	23.4	43.1	8.7	41.6	47.3	58.5	34.4	6.0	
LOS	D	С	С	D	Α	D	D	E	С	Α	
Approach Delay		29.4		34.7			46.2		35.3		
Approach LOS		С		С			D		D		
ntersection Summary											
Cycle Length: 120											
Actuated Cycle Length: 120											
Offset: 0 (0%), Referenced to	phase 2	EBTL. St	art of Gre	en							
Natural Cycle: 95											
Control Type: Actuated-Coor	dinated										
Maximum v/c Ratio: 0.87											
ntersection Signal Delay: 34	.0			Ir	tersection	n LOS: C					
ntersection Capacity Utilizat	ion 112.79	%		IC	CU Level	of Service	θH				
Analysis Period (min) 15											

Splits and Phases: 3: Davis Road & Lundys Lane

→ Ø2 (R)		Ø3	
78 s		10 s	32 s
	<b>4</b> <b>∞</b> Ø6	Ø8	
14 s	54 s	42 s	

Uppers Quarry Traffic Impact Study TMIG

Synchro 10 Report

HCM Signalized Intersection Capacity Analysis 3: Davis Road & Lundys Lane <2035 Background> PM Peak Hour 09-14-2021

	٦	-	$\mathbf{F}$	1	-	•	1	1	1	1	Ŧ	~
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	ሻ	ţ,		۲	•	1	ň	ţ,		ሻ	•	1
Traffic Volume (vph)	208	717	28	42	718	216	46	141	51	239	125	184
Future Volume (vph)	208	717	28	42	718	216	46	141	51	239	125	184
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Total Lost time (s)	3.0	7.0		7.0	7.0	7.0	7.0	7.0		3.0	7.0	7.0
Lane Util. Factor	1.00	1.00		1.00	1.00	1.00	1.00	1.00		1.00	1.00	1.00
Frpb, ped/bikes	1.00	1.00		1.00	1.00	0.98	1.00	0.99		1.00	1.00	1.00
Flpb, ped/bikes	1.00	1.00		1.00	1.00	1.00	1.00	1.00		1.00	1.00	1.00
Frt	1.00	0.99		1.00	1.00	0.85	1.00	0.96		1.00	1.00	0.85
Flt Protected	0.95	1.00		0.95	1.00	1.00	0.95	1.00		0.95	1.00	1.00
Satd. Flow (prot)	1719	1818		1611	1863	1473	1736	1652		1702	1743	1553
Flt Permitted	0.10	1.00		0.25	1.00	1.00	0.67	1.00		0.44	1.00	1.00
Satd. Flow (perm)	188	1818		418	1863	1473	1226	1652		790	1743	1553
Peak-hour factor, PHF	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93
Adj. Flow (vph)	224	771	30	45	772	232	49	152	55	257	134	198
RTOR Reduction (vph)	0	1	0	0	0	99	0	11	0	0	0	140
Lane Group Flow (vph)	224	800	0	45	772	133	49	196	0	257	134	58
Confl. Peds. (#/hr)	2		1	1		2			1	1		
Heavy Vehicles (%)	5%	3%	26%	12%	2%	7%	4%	9%	12%	6%	9%	4%
Turn Type	pm+pt	NA		Perm	NA	Perm	Perm	NA		pm+pt	NA	Perm
Protected Phases	5	2			6			4		3	8	
Permitted Phases	2			6		6	4			8		8
Actuated Green, G (s)	71.0	71.0		57.0	57.0	57.0	25.0	25.0		35.0	35.0	35.0
Effective Green, g (s)	71.0	71.0		57.0	57.0	57.0	25.0	25.0		35.0	35.0	35.0
Actuated g/C Ratio	0.59	0.59		0.48	0.48	0.48	0.21	0.21		0.29	0.29	0.29
Clearance Time (s)	3.0	7.0		7.0	7.0	7.0	7.0	7.0		3.0	7.0	7.0
Vehicle Extension (s)	3.0	4.0		4.0	4.0	4.0	2.0	2.0		3.0	2.0	2.0
Lane Grp Cap (vph)	251	1075		198	884	699	255	344		283	508	452
v/s Ratio Prot	c0.08	0.44			0.41			0.12		c0.05	0.08	
v/s Ratio Perm	c0.45			0.11		0.09	0.04			c0.21		0.04
v/c Ratio	0.89	0.74		0.23	0.87	0.19	0.19	0.57		0.91	0.26	0.13
Uniform Delay, d1	27.6	17.9		18.5	28.3	18.2	39.2	42.7		41.0	32.6	31.3
Progression Factor	1.00	1.00		1.07	1.15	1.81	1.00	1.00		1.00	1.00	1.00
Incremental Delay, d2	30.2	4.7		2.2	9.8	0.5	1.7	6.7		30.4	1.3	0.6
Delay (s)	57.8	22.5		22.1	42.4	33.5	40.8	49.4		71.4	33.9	31.9
Level of Service	E	С		С	D	С	D	D		E	С	С
Approach Delay (s)		30.3			39.5			47.7			49.6	
Approach LOS		С			D			D			D	
Intersection Summary												
HCM 2000 Control Delay			39.0	H	CM 2000	Level of	Service		D			
HCM 2000 Volume to Capac	city ratio		0.94									
Actuated Cycle Length (s)			120.0	Si	um of lost	time (s)			20.0			
Intersection Capacity Utilizat	tion		112.7%	IC	U Level o	of Service			Н			
Analysis Period (min)			15									
c Critical Lane Group												

Uppers Quarry Traffic Impact Study TMIG

	Road	& Tho	2035 Background> PM Peak Hour 09-14-2021								
	۶	-	$\mathbf{F}$	4	+	•	1	Ť	1	Ļ	
_ane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	SBL	SBT	
ane Configurations	ሻ	- <b>††</b>	1	<u>۲</u>	- <b>†</b> †	1	<u>۲</u>	4	<u>۲</u>	4	
Traffic Volume (vph)	231	1128	78	97	954	35	184	198	48	198	
Future Volume (vph)	231	1128	78	97	954	35	184	198	48	198	
Turn Type	pm+pt	NA	Perm	pm+pt	NA	Perm	pm+pt	NA	pm+pt	NA	
Protected Phases	5	2		1	6		7	4	3	8	
Permitted Phases	2		2	6		6	4		8		
Detector Phase	5	2	2	1	6	6	7	4	3	8	
Switch Phase											
Vinimum Initial (s)	8.0	10.0	10.0	5.0	10.0	10.0	5.0	10.0	5.0	10.0	
Vinimum Split (s)	11.0	35.1	35.1	8.0	35.1	35.1	8.0	41.4	8.0	41.4	
Total Split (s)	21.0	55.0	55.0	9.6	43.6	43.6	13.4	45.9	9.5	42.0	
Total Split (%)	17.5%	45.8%	45.8%	8.0%	36.3%	36.3%	11.2%	38.3%	7.9%	35.0%	
Yellow Time (s)	3.0	4.1	4.1	3.0	4.1	4.1	3.0	4.1	3.0	4.1	
All-Red Time (s)	0.0	2.0	2.0	0.0	2.0	2.0	0.0	2.3	0.0	2.3	
ost Time Adjust (s)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Total Lost Time (s)	3.0	6.1	6.1	3.0	6.1	6.1	3.0	6.4	3.0	6.4	
_ead/Lag	Lead	Lag	Lag	Lead	Lag	Lag	Lead	Lag	Lead	Lag	
_ead-Lag Optimize?	Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes	
Recall Mode	None	C-Max	C-Max	None	C-Max	C-Max	None	None	None	None	
Act Effct Green (s)	63.1	50.3	50.3	51.3	41.4	41.4	50.9	39.9	43.8	34.1	
Actuated g/C Ratio	0.53	0.42	0.42	0.43	0.34	0.34	0.42	0.33	0.36	0.28	
//c Ratio	0.85	0.78	0.11	0.61	0.81	0.06	0.86	0.73	0.18	0.95	
Control Delay	60.8	59.5	19.4	34.8	43.2	0.2	58.0	40.8	21.6	67.0	
Queue Delav	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Total Delay	60.8	59.5	19.4	34.8	43.2	0.2	58.0	40.8	21.6	67.0	
05	F	F	B	C	D	A	F	D	C	F	
Approach Delay	_	57.5	-		41 1		-	46.3	Ū	62.8	
Approach LOS		E			D			D		E	
ntersection Summary											
Cycle Length: 120											
Actuated Cycle Length: 120											
Offset: 0 (0%) Referenced to	nhase 2	FBTL and	16·WBTI	Start of	Green						
Natural Cycle: 100											
Control Type: Actuated-Coor	dinated										
Maximum v/c Ratio: 0.95											
ntersection Signal Delay: 51	.6			Ir	ntersectio	n LOS: D					
ntersection Capacity Utilizati	on 93.5%			10	CU Level	of Service	ə F				
Analysis Period (min) 15	000.070			K	00 2000	0.0011100					

Splits and Phases: 4: Thorold Townline Road & Thorold Stone Road

+ Ø1   ⊕+Ø	2 (R)	104	
9.6s 55s		9.5 s 45.9 s	
	Ø6 (R)	<b>↑</b> Ø7 <b>▶</b> Ø8	
21 s	43.6 s	13.4 s 42 s	

Uppers Quarry Traffic Impact Study TMIG Synchro 10 Report

HCM Signalized Intersection Capacity Analysis 4: Thorold Townline Road & Thorold Stone Road <2035 Background> PM Peak Hour 09-14-2021

	۶	-	$\mathbf{\hat{v}}$	•	+	×	1	1	۲	1	ţ	∢
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	۲	<b>†</b> †	1	٦	<b>^</b>	1	٦	¢Î		٦	4	
Traffic Volume (vph)	231	1128	78	97	954	35	184	198	187	48	198	272
Future Volume (vph)	231	1128	78	97	954	35	184	198	187	48	198	272
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Total Lost time (s)	3.0	6.1	6.1	3.0	6.1	6.1	3.0	6.4		3.0	6.4	
Lane Util. Factor	1.00	0.95	1.00	1.00	0.95	1.00	1.00	1.00		1.00	1.00	
Frt	1.00	1.00	0.85	1.00	1.00	0.85	1.00	0.93		1.00	0.91	
Flt Protected	0.95	1.00	1.00	0.95	1.00	1.00	0.95	1.00		0.95	1.00	
Satd. Flow (prot)	1671	3574	1568	1671	3539	1538	1736	1567		1671	1659	
Flt Permitted	0.10	1.00	1.00	0.11	1.00	1.00	0.12	1.00		0.35	1.00	
Satd. Flow (perm)	167	3574	1568	197	3539	1538	218	1567		622	1659	
Peak-hour factor, PHF	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96
Adj. Flow (vph)	241	1175	81	101	994	36	192	206	195	50	206	283
RTOR Reduction (vph)	0	0	47	0	0	24	0	28	0	0	42	0
Lane Group Flow (vph)	241	1175	34	101	994	12	192	373	0	50	447	0
Heavy Vehicles (%)	8%	1%	3%	8%	2%	5%	4%	10%	15%	8%	4%	5%
Turn Type	pm+pt	NA	Perm	pm+pt	NA	Perm	pm+pt	NA		pm+pt	NA	
Protected Phases	5	2		1	6		7	4		3	8	
Permitted Phases	2		2	6		6	4			8		
Actuated Green, G (s)	59.4	49.7	49.7	47.5	40.8	40.8	48.1	39.9		39.9	34.7	
Effective Green, q (s)	59.4	49.7	49.7	47.5	40.8	40.8	48.1	39.9		39.9	34.7	
Actuated g/C Ratio	0.49	0.41	0.41	0.40	0.34	0.34	0.40	0.33		0.33	0.29	
Clearance Time (s)	3.0	6.1	6.1	3.0	6.1	6.1	3.0	6.4		3.0	6.4	
Vehicle Extension (s)	2.5	6.0	6.0	3.0	6.0	6.0	3.0	2.3		3.0	2.3	
Lane Grp Cap (vph)	278	1480	649	160	1203	522	218	521		252	479	
v/s Ratio Prot	c0.11	0.33		0.04	0.28		c0.08	0.24		0.01	0.27	
v/s Ratio Perm	c0.32		0.02	0.21		0.01	c0.28			0.06		
v/c Ratio	0.87	0.79	0.05	0.63	0.83	0.02	0.88	0.72		0.20	0.93	
Uniform Delay, d1	32.1	30.7	21.0	25.9	36.3	26.3	28.5	35.1		28.1	41.5	
Progression Factor	1.60	1.84	11.66	1.00	1.00	1.00	1.00	1.00		1.00	1.00	
Incremental Delay, d2	14.9	2.6	0.1	7.9	6.6	0.1	31.2	4.2		0.4	25.2	
Delay (s)	66.3	59.1	245.4	33.8	42.9	26.4	59.7	39.2		28.5	66.7	
Level of Service	E	E	F	С	D	С	E	D		С	E	
Approach Delay (s)		70.4			41.6			45.9			63.2	
Approach LOS		E			D			D			E	
Intersection Summary												
HCM 2000 Control Delay			56.8	Н	CM 2000	Level of	Service		E			
HCM 2000 Volume to Capac	ity ratio		0.91									
Actuated Cycle Length (s)			120.0	S	um of lost	time (s)			18.5			
Intersection Capacity Utilizat	ion		93.5%	IC	U Level o	of Service	9		F			
Analysis Period (min)			15									
c Critical Lane Group												

Uppers Quarry Traffic Impact Study TMIG

5: Thorold Townline Road & Lundys Lane 09-14-2021											
	٦	<b>→</b>	$\mathbf{\hat{z}}$	4	+	•	t	1	ŧ	~	
Lane Group	EBL	EBT	EBR	WBL	WBT	NBL	NBT	SBL	SBT	SBR	
Lane Configurations	ሻ	<b>↑</b>	1	ሻ	ef 👘	ሻ	ef 👘	ሻ	<b>↑</b>	1	
Traffic Volume (vph)	114	673	117	44	711	117	142	95	118	183	
Future Volume (vph)	114	673	117	44	711	117	142	95	118	183	
Turn Type	Perm	NA	Perm	Perm	NA	Perm	NA	Perm	NA	Perm	
Protected Phases		2			6		4		8		
Permitted Phases	2		2	6		4		8		8	
Detector Phase	2	2	2	6	6	4	4	8	8	8	
Switch Phase											
Vinimum Initial (s)	20.0	20.0	20.0	20.0	20.0	10.0	10.0	10.0	10.0	10.0	
Minimum Split (s)	29.0	29.0	29.0	29.0	29.0	35.0	35.0	35.0	35.0	35.0	
Total Split (s)	85.0	85.0	85.0	85.0	85.0	35.0	35.0	35.0	35.0	35.0	
Total Split (%)	70.8%	70.8%	70.8%	70.8%	70.8%	29.2%	29.2%	29.2%	29.2%	29.2%	
Yellow Time (s)	5.0	5.0	5.0	5.0	5.0	4.0	4.0	4.0	4.0	4.0	
All-Red Time (s)	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	
ost Time Adjust (s)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Total Lost Time (s)	7.0	7.0	7.0	7.0	7.0	6.0	6.0	6.0	6.0	6.0	
_ead/Lag											
_ead-Lag Optimize?											
Recall Mode	C-Max	C-Max	C-Max	C-Max	C-Max	None	None	None	None	None	
Act Effct Green (s)	85.7	85.7	85.7	85.7	85.7	21.3	21.3	21.3	21.3	21.3	
Actuated g/C Ratio	0.71	0.71	0.71	0.71	0.71	0.18	0.18	0.18	0.18	0.18	
//c Ratio	0.41	0.57	0.11	0.12	0.65	0.66	0.66	0.77	0.41	0.46	
Control Delay	13.9	13.5	4.5	7.6	13.3	61.1	51.7	79.8	46.3	8.8	
Queue Delay	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Fotal Delay	13.9	13.5	4.5	7.6	13.3	61.1	51.7	79.8	46.3	8.8	
_OS	В	В	Α	А	В	E	D	E	D	А	
Approach Delay		12.4			13.0		55.3		37.0		
Approach LOS		В			В		E		D		
ntersection Summarv											
Cycle Length: 120											
Actuated Cycle Length: 120											
Offset: 0 (0%) Referenced t	o nhase 2	FRTL and	16·WBTI	Start of	Green						
Vatural Cycle: 90				., Start Of	0.0011						
Control Type: Actuated-Coo	rdinated										
Aaximum v/c Ratio: 0.77	anatod										
ntersection Signal Delay: 22	21			Ir	ntersectio	n LOS: C					
ntersection Canacity I Itiliza	tion 98.4%			10		of Service	⊳ F				
Analysis Period (min) 15	uon 00. <del>4</del> /0			N		0014100					

Ø2 (R)	<\$ [†] ø4	
85 s	35 s	
₩ Ø6 (R)	<b>↓</b> _{Ø8}	
85 s	35 s	

Synchro 10 Report

HCM Signalized Intersection Capacity Analysis 5: Thorold Townline Road & Lundys Lane <2035 Background> PM Peak Hour 09-14-2021

	≯	-	$\mathbf{F}$	∢	←	۰.	1	Ť	۲	1	ŧ	~
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	۲	•	1	۲.	ĥ		۲	4Î		۲.	•	1
Traffic Volume (vph)	114	673	117	44	711	63	117	142	50	95	118	183
Future Volume (vph)	114	673	117	44	711	63	117	142	50	95	118	183
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Total Lost time (s)	7.0	7.0	7.0	7.0	7.0		6.0	6.0		6.0	6.0	6.0
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00		1.00	1.00		1.00	1.00	1.00
Frpb, ped/bikes	1.00	1.00	1.00	1.00	1.00		1.00	1.00		1.00	1.00	1.00
Flpb, ped/bikes	1.00	1.00	1.00	1.00	1.00		1.00	1.00		1.00	1.00	1.00
Frt	1.00	1.00	0.85	1.00	0.99		1.00	0.96		1.00	1.00	0.85
Flt Protected	0.95	1.00	1.00	0.95	1.00		0.95	1.00		0.95	1.00	1.00
Satd. Flow (prot)	1626	1827	1553	1752	1818		1687	1748		1736	1776	1524
Flt Permitted	0.25	1.00	1.00	0.31	1.00		0.62	1.00		0.42	1.00	1.00
Satd. Flow (perm)	430	1827	1553	569	1818		1102	1748		762	1776	1524
Peak-hour factor, PHF	0.91	0.91	0.91	0.91	0.91	0.91	0.91	0.91	0.91	0.91	0.91	0.91
Adj. Flow (vph)	125	740	129	48	781	69	129	156	55	104	130	201
RTOR Reduction (vph)	0	0	15	0	2	0	0	12	0	0	0	165
Lane Group Flow (vph)	125	740	114	48	848	0	129	199	0	104	130	36
Confl. Peds. (#/hr)	1					1						
Heavy Vehicles (%)	11%	4%	4%	3%	2%	15%	7%	6%	0%	4%	7%	6%
Turn Type	Perm	NA	Perm	Perm	NA		Perm	NA		Perm	NA	Perm
Protected Phases		2			6			4			8	
Permitted Phases	2		2	6			4			8		8
Actuated Green, G (s)	85.7	85.7	85.7	85.7	85.7		21.3	21.3		21.3	21.3	21.3
Effective Green, g (s)	85.7	85.7	85.7	85.7	85.7		21.3	21.3		21.3	21.3	21.3
Actuated g/C Ratio	0.71	0.71	0.71	0.71	0.71		0.18	0.18		0.18	0.18	0.18
Clearance Time (s)	7.0	7.0	7.0	7.0	7.0		6.0	6.0		6.0	6.0	6.0
Vehicle Extension (s)	5.0	5.0	5.0	5.0	5.0		5.0	5.0		5.0	5.0	5.0
Lane Grp Cap (vph)	307	1304	1109	406	1298		195	310		135	315	270
v/s Ratio Prot		0.41			c0.47			0.11			0.07	
v/s Ratio Perm	0.29		0.07	0.08			0.12			c0.14		0.02
v/c Ratio	0.41	0.57	0.10	0.12	0.65		0.66	0.64		0.77	0.41	0.13
Uniform Delay, d1	6.9	8.2	5.3	5.4	9.2		46.0	45.8		47.0	43.8	41.6
Progression Factor	1.22	1.30	1.09	1.00	1.00		1.00	1.00		1.00	1.00	1.00
Incremental Delay, d2	2.5	1.1	0.1	0.6	2.6		10.7	6.1		26.7	1.8	0.5
Delay (s)	11.0	11.8	5.9	5.9	11.8		56.6	52.0		73.7	45.6	42.0
Level of Service	В	В	Α	A	В		E	D		E	D	D
Approach Delay (s)		11.0			11.4			53.7			50.7	
Approach LOS		В			В			D			D	
Intersection Summary												
HCM 2000 Control Delay			23.1	H	CM 2000	Level of S	Service		С			
HCM 2000 Volume to Capacity	y ratio		0.68									
Actuated Cycle Length (s)			120.0	S	um of lost	time (s)			13.0			
Intersection Capacity Utilizatio	n		98.4%	IC	CU Level o	of Service			F			
Analysis Period (min)			15									

c Critical Lane Group

Uppers Quarry Traffic Impact Study TMIG

Timings 6: Thorold Townline	Road	<203	5 Bacl	kground> PM Peak Hou 09-14-202					
	۶	-	4	+	•	t	1	Ŧ	
Lane Group	EBL	EBT	WBL	WBT	NBL	NBT	SBL	SBT	
Lane Configurations		4		4		4		4	
Traffic Volume (vph)	27	205	124	178	32	538	20	317	
Future Volume (vph)	27	205	124	178	32	538	20	317	
Turn Type	Perm	NA	Perm	NA	Perm	NA	Perm	NA	
Protected Phases		2		6		4		8	
Permitted Phases	2		6		4		8		
Detector Phase	2	2	6	6	4	4	8	8	
Switch Phase									
Vinimum Initial (s)	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	
Vinimum Split (s)	32.0	32.0	32.0	32.0	35.0	35.0	35.0	35.0	
Total Split (s)	37.0	37.0	37.0	37.0	53.0	53.0	53.0	53.0	
Total Split (%)	41.1%	41.1%	41.1%	41.1%	58.9%	58.9%	58.9%	58.9%	
(ellow Time (s)	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0	
All-Red Time (s)	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	
ost Time Adjust (s)		0.0		0.0		0.0		0.0	
fotal Lost Time (s)		6.0		6.0		6.0		6.0	
_ead/Lag									
ead-Lag Optimize?									
Recall Mode	C-Max	C-Max	Мах	Max	None	None	None	None	
Act Effct Green (s)		34.1		34.1		43.9		43.9	
Actuated g/C Ratio		0.38		0.38		0.49		0.49	
/c Ratio		0.41		0.69		0.87		0.50	
Control Delay		23.7		33.1		33.2		17.0	
Queue Delay		0.0		0.0		0.0		0.0	
Total Delay		23.7		33.1		33.2		17.0	
05		C		C		C		B	
Approach Delay		23.7		33.1		33.2		17 0	
Approach LOS		C		C		C		B	
ntersection Summary									
Cycle Length: 90									
Actuated Cycle Length: 90									
Offset: 0 (0%). Referenced to	o phase 2:	EBTL. St	art of Gre	en					
latural Cycle: 70		, 01							
Control Type: Actuated-Coor	rdinated								
Maximum v/c Ratio: 0.87									
ntersection Signal Delay: 27	.9			Ir	ntersectio	n LOS: C			
ntersection Capacity Utilizat	ion 96.3%			10	CU Level	of Service	F		
Analysis Period (min) 15				, in	20 20101	0.001110			

opino una i nacco.	0. 11101010 10001111110 110000	a bouro	
→ Ø2 (R)			▲ Ø4
37 s			53 s
₹ø6			
37 s			53 s

Synchro 10 Report

HCM Signalized Intersection Capacity Analysis 6: Thorold Townline Road & Beaverdams Road <2035 Background> PM Peak Hour 09-14-2021

	۶	-	$\mathbf{\hat{z}}$	4	←	*	٩	t	۲	1	Ŧ	~
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		\$			\$			\$			\$	
Traffic Volume (vph)	27	205	16	124	178	21	32	538	94	20	317	41
Future Volume (vph)	27	205	16	124	178	21	32	538	94	20	317	41
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Total Lost time (s)		6.0			6.0			6.0			6.0	
Lane Util. Factor		1.00			1.00			1.00			1.00	
Frpb, ped/bikes		1.00			1.00			1.00			1.00	
Flpb, ped/bikes		1.00			1.00			1.00			1.00	
Frt		0.99			0.99			0.98			0.99	
Flt Protected		0.99			0.98			1.00			1.00	
Satd. Flow (prot)		1830			1803			1710			1758	
Flt Permitted		0.93			0.73			0.97			0.95	
Satd. Flow (perm)		1720			1333			1656			1670	
Peak-hour factor, PHF	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93
Adi, Flow (vph)	29	220	17	133	191	23	34	578	101	22	341	44
RTOR Reduction (vph)	0	2	0	0	2	0	0	7	0	0	5	0
Lane Group Flow (vph)	0	264	0	0	345	0	0	706	0	0	402	0
Confl. Peds. (#/hr)	1		5	5		1	8		3	3		8
Heavy Vehicles (%)	10%	1%	4%	4%	1%	0%	4%	10%	0%	2%	6%	6%
Turn Type	Perm	NA		Perm	NA		Perm	NA		Perm	NA	
Protected Phases		2			6			4			8	
Permitted Phases	2			6			4			8		
Actuated Green, G (s)		34.1			34.1			43.9			43.9	
Effective Green, g (s)		34.1			34.1			43.9			43.9	
Actuated g/C Ratio		0.38			0.38			0.49			0.49	
Clearance Time (s)		6.0			6.0			6.0			6.0	
Vehicle Extension (s)		5.0			5.0			5.0			5.0	
Lane Grp Cap (vph)		651			505			807			814	
v/s Ratio Prot												
v/s Ratio Perm		0.15			c0.26			c0.43			0.24	
v/c Ratio		0.40			0.68			0.87			0.49	
Uniform Delay, d1		20.5			23.4			20.6			15.6	
Progression Factor		1.00			1.00			1.00			1.00	
Incremental Delay, d2		1.9			7.3			11.2			1.0	
Delay (s)		22.4			30.7			31.8			16.5	
Level of Service		С			С			С			В	
Approach Delay (s)		22.4			30.7			31.8			16.5	
Approach LOS		С			С			С			В	
Intersection Summary												
HCM 2000 Control Delay			26.6	Н	CM 2000	Level of	Service		С			
HCM 2000 Volume to Capa	acity ratio		0.79									
Actuated Cycle Length (s)			90.0	S	um of los	t time (s)			12.0			
Intersection Capacity Utilization	ation		96.3%	IC	CU Level (	of Service			F			
Analysis Period (min)			15									
a Critical Lana Croup												

c Critical Lane Group

Uppers Quarry Traffic Impact Study TMIG

							00 11 202
	4	•	1	1	1	Ŧ	
Movement	WBL	WBR	NBT	NBR	SBL	SBT	
Lane Configurations	Y		4Î		ľ	•	
Traffic Volume (veh/h)	0	0	513	0	0	468	
Future Volume (Veh/h)	0	0	513	0	0	468	
Sign Control	Stop		Free			Free	
Grade	0%		0%			0%	
Peak Hour Factor	0.91	0.91	0.91	0.91	0.91	0.91	
Hourly flow rate (vph)	0	0	564	0	0	514	
Pedestrians							
Lane Width (m)							
Walking Speed (m/s)							
Percent Blockage							
Right turn flare (veh)							
Median type			None			None	
Median storage veh)							
Upstream signal (m)							
pX, platoon unblocked							
vC, conflicting volume	1078	564			564		
vC1, stage 1 conf vol							
vC2, stage 2 conf vol							
vCu, unblocked vol	1078	564			564		
tC, single (s)	6.4	6.2			4.1		
tC, 2 stage (s)							
tF (s)	3.5	3.3			2.2		
p0 queue free %	100	100			100		
cM capacity (veh/h)	244	529			1018		
Direction Lane #	WB 1	NB 1	SB 1	SB 2			
Volume Total	0	564	0	514			
Volume Left	0	0	0	0			
Volume Right	0	0	0	0			
cSH	1700	1700	1700	1700			
Volume to Capacity	0.00	0.33	0.00	0.30			
Queue Length 95th (m)	0.0	0.0	0.0	0.0			
Control Delay (s)	0.0	0.0	0.0	0.0			
Lane LOS	A	5.5	0.0	0.0			
Approach Delay (s)	0.0	0.0	0.0				
Approach LOS	A						
Intersection Summary							
Average Delay		_	0.0				
			0.0				
Intersection Canacity Litilization	n		30.3%	IC		of Service	Δ Δ

Timings <2035 Total - Thorold Townline> AM Peak Hour										Hour		
1: Davis Road & Th	orold S	Stone F	Road								09-2	3-2021
	۶	-	$\mathbf{r}$	4	+	•	Ť	1	1	ţ	~	
Lane Group	EBL	EBT	EBR	WBL	WBT	NBL	NBT	NBR	SBL	SBT	SBR	
Lane Configurations	۲	<b>^</b>	1	۲	A1≱	۲.	ર્સ	1	1	•	1	
Traffic Volume (vph)	21	1010	336	114	1122	649	15	257	1	2	18	
Future Volume (vph)	21	1010	336	114	1122	649	15	257	1	2	18	
Turn Type	Perm	NA	Perm	Perm	NA	Split	NA	Perm	Split	NA	Perm	
Protected Phases		2			6	4	4		8	8		
Permitted Phases	2		2	6				4			8	
Detector Phase	2	2	2	6	6	4	4	4	8	8	8	
Switch Phase												
Minimum Initial (s)	20.0	20.0	20.0	20.0	20.0	10.0	10.0	10.0	10.0	10.0	10.0	
Minimum Split (s)	28.9	28.9	28.9	28.9	28.9	29.7	29.7	29.7	21.7	21.7	21.7	
Total Split (s)	58.0	58.0	58.0	58.0	58.0	40.0	40.0	40.0	22.0	22.0	22.0	
Total Split (%)	48.3%	48.3%	48.3%	48.3%	48.3%	33.3%	33.3%	33.3%	18.3%	18.3%	18.3%	
Yellow Time (s)	5.4	5.4	5.4	5.4	5.4	5.7	5.7	5.7	5.7	5.7	5.7	
All-Red Time (s)	1.5	1.5	1.5	1.5	1.5	2.0	2.0	2.0	2.0	2.0	2.0	
Lost Time Adjust (s)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	_
Total Lost Time (s)	0.9	0.9	0.9	0.9	0.9	1.1	1.1	1.1	1.1	1.1	1.1	
Lead/Lag												
Recall Mode	C Max	C Max	C Max	Max	Max	None	None	None	None	None	None	
Act Effet Croop (c)	67.6	67.6	67.6	67.6	67.6	20.7	20.7	20.7	10.0	10.0	10.0	
Actuated a/C Patio	07.0	07.0	07.0	07.0	07.0	0.26	0.26	0.26	0.08	0.08	0.08	
v/c Ratio	0.50	0.50	0.30	0.50	0.50	0.20	0.20	0.20	0.00	0.00	0.00	
Control Delay	20.4	20.0	7 1	47.1	27.7	64.3	65.3	7.0	51.0	51.0	0.00	
Oueue Delay	20.4	20.0	0.0	0.0	0.0	04.0	0.0	0.0	0.0	0.0	0.0	
Total Delay	20.4	20.0	7 1	47.1	27.7	64.3	65.3	7.0	51.0	51.0	0.9	
105	C	B	A	D	C	F	F	A	D	D	A	
Approach Delay	, in the second s	16.8		-	29.4	_	48.7		2	7.7		
Approach LOS		В			С		D			A		
Intersection Summary												
Cycle Length: 120												
Actuated Cycle Length: 120												
Offset: 0 (0%), Referenced to	o phase 2	EBTL. St	art of Gre	en								
Natural Cycle: 115		,		-								
Control Type: Actuated-Coor	rdinated											
Maximum v/c Ratio: 0.87												
Intersection Signal Delay: 29	9.4			Ir	ntersectio	n LOS: C						
Intersection Capacity Utilizat	tion 90.8%			10	CU Level	of Service	θE					
Analysis Period (min) 15												

Splits and Phases: 1: Davis Road & Thorold Stone Road

≠ø2 (R)	<b>↓</b> _{Ø4}	1 Ø8
58 s	40 s	22 s
<b>₩</b> Ø6		
58 s		

Uppers Quarry Traffic Impact Study TMIG

Synchro 10 Report

HCM Signalized Intersection Capacity Analysis<2035 Total - Thorold Townline> AM Peak Hour 1: Davis Road & Thorold Stone Road 09-23-2021

	۶	-	$\mathbf{F}$	4	←	•	•	Ť	۲	1	ŧ	~
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	2	<u></u>	1	ľ	A12		ľ	ę	1	1	•	1
Traffic Volume (vph)	21	1010	336	114	1122	6	649	15	257	1	2	18
Future Volume (vph)	21	1010	336	114	1122	6	649	15	257	1	2	18
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Total Lost time (s)	6.9	6.9	6.9	6.9	6.9		7.7	7.7	7.7	7.7	7.7	7.7
Lane Util. Factor	1.00	0.95	1.00	1.00	0.95		0.95	0.95	1.00	1.00	1.00	1.00
Frpb, ped/bikes	1.00	1.00	1.00	1.00	1.00		1.00	1.00	0.99	1.00	1.00	0.99
Flpb, ped/bikes	1.00	1.00	1.00	1.00	1.00		1.00	1.00	1.00	1.00	1.00	1.00
Frt	1.00	1.00	0.85	1.00	1.00		1.00	1.00	0.85	1.00	1.00	0.85
Flt Protected	0.95	1.00	1.00	0.95	1.00		0.95	0.95	1.00	0.95	1.00	1.00
Satd. Flow (prot)	1641	3374	1442	1530	3336		1559	1554	1475	1388	1624	1337
Flt Permitted	0.15	1.00	1.00	0.19	1.00		0.95	0.95	1.00	0.95	1.00	1.00
Satd. Flow (perm)	264	3374	1442	310	3336		1559	1554	1475	1388	1624	1337
Peak-hour factor PHF	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96
Adi Flow (vph)	22	1052	350	119	1169	6	676	16	268	1	2	19
RTOR Reduction (vph)	0	0	114	0	0	0	0	0	199	0	0	18
Lane Group Flow (vph)	22	1052	236	119	1175	0	345	347	69	1	2	1
Confl Peds (#/hr)	1	1002	200			1	1	• …	1	1	-	1
Heavy Vehicles (%)	10%	7%	12%	18%	8%	30%	10%	28%	8%	30%	17%	19%
Turn Tyne	Perm	NA	Perm	Perm	NA		Split	NA	Perm	Snlit	NA	Perm
Protected Phases	1 Unit	2	1 01111	1 Unit	6		4	4	1 01111	8	8	1 Onn
Permitted Phases	2		2	6	-				4			8
Actuated Green, G (s)	63.0	63.0	63.0	63.0	63.0		30.7	30.7	30.7	4.0	4.0	4.0
Effective Green, g (s)	63.0	63.0	63.0	63.0	63.0		30.7	30.7	30.7	4.0	4.0	4.0
Actuated g/C Ratio	0.52	0.52	0.52	0.52	0.52		0.26	0.26	0.26	0.03	0.03	0.03
Clearance Time (s)	6.9	6.9	6.9	6.9	6.9		77	77	77	77	77	77
Vehicle Extension (s)	3.0	3.0	3.0	3.0	3.0		4.5	4.5	4.5	4.5	4.5	4.5
Lane Grn Can (vnh)	138	1771	757	162	1751		398	397	377	46	54	44
v/s Ratio Prot		0.31			0.35		0.22	c0.22	0	0.00	c0.00	
v/s Ratio Perm	0.08		0.16	c0.38					0.05			0.00
v/c Ratio	0.16	0.59	0.31	0.73	0.67		0.87	0.87	0.18	0.02	0.04	0.01
Uniform Delay, d1	14.8	19.7	16.2	22.0	20.9		42.7	42.8	34.9	56.1	56.1	56.1
Progression Factor	1 00	1 00	1 00	1 44	1.34		1.00	1.00	1 00	1 00	1 00	1 00
Incremental Delay, d2	2.5	1.5	11	14.9	11		18.7	19.7	0.4	0.3	0.5	0.2
Delay (s)	17.2	21.1	17.3	46.6	29.1		61.4	62.5	35.3	56.4	56.6	56.3
Level of Service	В	С	В	D	С		E	E	D	E	E	E
Approach Delay (s)		20.1			30.7			54.5			56.4	_
Approach LOS		С			С			D			E	
Intersection Summary												
HCM 2000 Control Delay			33.0	Н	CM 2000	Level of S	Service		С			
HCM 2000 Volume to Capa	city ratio		0.75		2 2000	25.0.010			5			
Actuated Cycle Length (s)			120.0	S	um of lost	time (s)			22.3			
Intersection Capacity Utiliza	ation		90.8%	10	U Level o	of Service			5 F			
Analysis Period (min)			15		2 20.010				_			
			10									

c Critical Lane Group

Uppers Quarry Traffic Impact Study TMIG

Timings 2035 Total - Thorold Townline> AM Peak Hour 2: Davis Road & Niagara Falls Road/Beaverdams Road 09-23-2021											
	•	-	4	+	٩	1	6	ţ	~		
Lane Group	EBL	EBT	WBL	WBT	NBL	NBT	SBL	SBT	SBR		
Lane Configurations		\$		\$	1	A12	1	<b>^</b>	1		
Traffic Volume (vph)	110	31	29	17	25	626	82	329	44		
Future Volume (vph)	110	31	29	17	25	626	82	329	44		
Turn Type	Perm	NA	Perm	NA	Perm	NA	Perm	NA	Perm		
Protected Phases		2		6		4		8			
Permitted Phases	2		6		4		8		8		
Detector Phase	2	2	6	6	4	4	8	8	8		
Switch Phase											
Minimum Initial (s)	10.0	10.0	10.0	10.0	25.0	25.0	25.0	25.0	25.0		
Minimum Split (s)	38.1	38.1	38.1	38.1	32.0	32.0	32.0	32.0	32.0		
Total Split (s)	50.0	50.0	50.0	50.0	50.0	50.0	50.0	50.0	50.0		
Total Split (%)	50.0%	50.0%	50.0%	50.0%	50.0%	50.0%	50.0%	50.0%	50.0%		
Yellow Time (s)	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0		
All-Red Time (s)	3.1	3.1	3.1	3.1	2.0	2.0	2.0	2.0	2.0		
Lost Time Adjust (s)		0.0		0.0	0.0	0.0	0.0	0.0	0.0		
Total Lost Time (s)		8.1		8.1	7.0	7.0	7.0	7.0	7.0		
Lead/Lag											
Lead-Lag Optimize?											
Recall Mode	C-Max	C-Max	Max	Max	None	None	None	None	None		
Act Effct Green (s)		53.1		53.1	31.8	31.8	31.8	31.8	31.8		
Actuated g/C Ratio		0.53		0.53	0.32	0.32	0.32	0.32	0.32		
v/c Ratio		0.27		0.25	0.11	0.71	0.57	0.37	0.10		
Control Delay		15.1		6.3	22.8	33.4	42.9	26.7	4.8		
Queue Delay		0.0		0.0	0.0	0.0	0.0	0.0	0.0		
Total Delay		15.1		6.3	22.8	33.4	42.9	26.7	4.8		
LOS		В		Α	С	С	D	С	А		
Approach Delay		15.1		6.3		33.0		27.5			
Approach LOS		В		A		С		С			
Intersection Summary											
Cycle Length: 100											
Actuated Cycle Length: 100											
Offset: 0 (0%), Referenced t	to phase 2:	EBTL, St	art of Gre	en							
Natural Cycle: 75											
Control Type: Actuated-Coo	rdinated										
Maximum v/c Ratio: 0.71											
Intersection Signal Delay: 25	5.7			Ir	ntersectio	n LOS: C					
Intersection Capacity Utilization	tion 88.4%			10	CU Level	of Service	θE				
Analysis Period (min) 15											
Splits and Phases: 2. Day	is Road &	Niagara I	Falls Roa	d/Beaver	dams Roa	hd					
			0001000			••					

→ø2 (R)	< <b>1</b> ø4
50 s	50 s
<b>₩</b> Ø6	↓ Ø8
50 s	50 s

Synchro 10 Report

 HCM Signalized Intersection Capacity Analysis<2035 Total - Thorold Townline> AM Peak Hour

 2: Davis Road & Niagara Falls Road/Beaverdams Road
 09-23-2021

	≯	-	$\mathbf{i}$	•	+	•	1	1	1	1	Ŧ	-
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		4			4		5	<b>4</b> 12		5	44	1
Traffic Volume (vph)	110	31	18	29	17	166	25	626	46	82	329	44
Future Volume (vph)	110	31	18	29	17	166	25	626	46	82	329	44
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Total Lost time (s)		8.1			8.1		7.0	7.0		7.0	7.0	7.0
Lane Util. Factor		1.00			1.00		1.00	0.95		1.00	0.95	1.00
Frt		0.98			0.89		1.00	0.99		1.00	1.00	0.85
Flt Protected		0.97			0.99		0.95	1.00		0.95	1.00	1.00
Satd. Flow (prot)		1658			1631		1388	3122		1787	2983	1392
Flt Permitted		0.67			0.94		0.53	1.00		0.25	1.00	1.00
Satd. Flow (perm)		1150			1549		778	3122		476	2983	1392
Peak-hour factor, PHF	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95
Adj. Flow (vph)	116	33	19	31	18	175	26	659	48	86	346	46
RTOR Reduction (vph)	0	4	0	0	68	0	0	6	0	0	0	31
Lane Group Flow (vph)	0	164	0	0	156	0	26	701	0	86	346	15
Heavy Vehicles (%)	10%	7%	7%	7%	12%	2%	30%	15%	7%	1%	21%	16%
Turn Type	Perm	NA		Perm	NA		Perm	NA		Perm	NA	Perm
Protected Phases		2			6			4			8	
Permitted Phases	2			6			4			8		8
Actuated Green, G (s)		53.1			53.1		31.8	31.8		31.8	31.8	31.8
Effective Green, g (s)		53.1			53.1		31.8	31.8		31.8	31.8	31.8
Actuated g/C Ratio		0.53			0.53		0.32	0.32		0.32	0.32	0.32
Clearance Time (s)		8.1			8.1		7.0	7.0		7.0	7.0	7.0
Vehicle Extension (s)		3.0			3.0		5.0	5.0		5.0	5.0	5.0
Lane Grp Cap (vph)		610			822		247	992		151	948	442
v/s Ratio Prot								c0.22			0.12	
v/s Ratio Perm		c0.14			0.10		0.03			0.18		0.01
v/c Ratio		0.27			0.19		0.11	0.71		0.57	0.36	0.03
Uniform Delay, d1		12.8			12.2		24.1	30.0		28.4	26.3	23.5
Progression Factor		1.00			1.00		1.00	1.00		1.00	1.00	1.00
Incremental Delay, d2		1.1			0.5		0.4	2.9		7.9	0.5	0.1
Delay (s)		13.9			12.7		24.5	32.9		36.3	26.8	23.6
Level of Service		В			В		С	С		D	С	С
Approach Delay (s)		13.9			12.7			32.6			28.2	
Approach LOS		В			В			С			С	
Intersection Summary												
HCM 2000 Control Delay			26.6	Н	CM 2000	Level of	Service		С			
HCM 2000 Volume to Capacity	ratio		0.43									
Actuated Cycle Length (s)			100.0	S	um of los	t time (s)			15.1			
Intersection Capacity Utilization	1		88.4%	IC	U Level	of Service			E			
Analysis Period (min)			15									
c Critical Lane Group												

Uppers Quarry Traffic Impact Study TMIG

Timings <2035 Total - Thorold Townline> AM Peak Hour 3: Davis Road & Lundys Lane 09-23-2021											
	۶	<b>→</b>	4	+	×	٩	t	6	ţ	~	
Lane Group	EBL	EBT	WBL	WBT	WBR	NBL	NBT	SBL	SBT	SBR	
Lane Configurations	ľ	¢Î	ľ	•	1	ľ	ĥ	ľ	•	1	
Traffic Volume (vph)	153	635	45	502	132	22	139	136	94	159	
Future Volume (vph)	153	635	45	502	132	22	139	136	94	159	
Turn Type	Perm	NA	Perm	NA	Perm	Perm	NA	Perm	NA	Perm	
Protected Phases		2		6			4		8		
Permitted Phases	2		6		6	4		8		8	
Detector Phase	2	2	6	6	6	4	4	8	8	8	
Switch Phase											
Minimum Initial (s)	22.0	22.0	22.0	22.0	22.0	15.0	15.0	15.0	15.0	15.0	
Minimum Split (s)	36.0	36.0	36.0	36.0	36.0	32.0	32.0	32.0	32.0	32.0	
Total Split (s)	58.0	58.0	58.0	58.0	58.0	32.0	32.0	32.0	32.0	32.0	
Total Split (%)	64.4%	64.4%	64.4%	64.4%	64.4%	35.6%	35.6%	35.6%	35.6%	35.6%	
Yellow Time (s)	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	
All-Red Time (s)	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	
Lost Time Adjust (s)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Total Lost Time (s)	7.0	7.0	7.0	7.0	7.0	7.0	7.0	7.0	7.0	7.0	
Lead/Lag											
Lead-Lag Optimize?											
Recall Mode	C-Max	C-Max	Max	Max	Max	None	None	None	None	None	
Act Effct Green (s)	57.5	57.5	57.5	57.5	57.5	18.5	18.5	18.5	18.5	18.5	
Actuated g/C Ratio	0.64	0.64	0.64	0.64	0.64	0.21	0.21	0.21	0.21	0.21	
v/c Ratio	0.36	0.60	0.16	0.48	0.14	0.11	0.56	0.72	0.32	0.40	
Control Delay	11.5	13.0	9.5	11.1	1.9	28.0	36.1	52.5	32.0	7.5	
Queue Delay	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Total Delay	11.5	13.0	9.5	11.1	1.9	28.0	36.1	52.5	32.0	7.5	
LOS	В	В	А	В	А	С	D	D	С	А	
Approach Delay		12.7		9.2			35.2		29.2		
Approach LOS		В		А			D		С		
Intersection Summary											
Cycle Length: 90											
Actuated Cycle Length: 90											
Offset: 0 (0%), Referenced	to phase 2:	EBTL, St	art of Gre	en							
Natural Cycle: 70											
Control Type: Actuated-Coc	ordinated										
Maximum v/c Ratio: 0.72											
Intersection Signal Delay: 1	6.7			Ir	ntersectio	n LOS: B					
Intersection Capacity Utiliza	ation 101.29	%		10	CU Level	of Service	G				
Analysis Period (min) 15											
Splits and Phases: 3: Day	vis Road &	Lundys L	ane								
								4			

 	 	 	-	-	-	 -		- F
							A	
						 0.0	Ζ.,	

μ → Ø2 (R)	[™] ¶ø₄	
58 s	32 s	
₩ ₩ Ø6	<b>₽</b> Ø8	
58 s	32 s	

Synchro 10 Report

 HCM Signalized Intersection Capacity Analysis<2035 Total - Thorold Townline> AM Peak Hour

 3: Davis Road & Lundys Lane

	≯	-	$\mathbf{F}$	4	+	×	٠	Ť	1	1	Ŧ	4
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	5	ţ,		5	•	1	5	î,		5	•	1
Traffic Volume (vph)	153	635	18	45	502	132	22	139	30	136	94	159
Future Volume (vph)	153	635	18	45	502	132	22	139	30	136	94	159
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Total Lost time (s)	7.0	7.0		7.0	7.0	7.0	7.0	7.0		7.0	7.0	7.0
Lane Util. Factor	1.00	1.00		1.00	1.00	1.00	1.00	1.00		1.00	1.00	1.00
Frpb, ped/bikes	1.00	1.00		1.00	1.00	1.00	1.00	1.00		1.00	1.00	1.00
Flpb, ped/bikes	1.00	1.00		1.00	1.00	1.00	1.00	1.00		1.00	1.00	1.00
Frt	1.00	1.00		1.00	1.00	0.85	1.00	0.97		1.00	1.00	0.85
Flt Protected	0.95	1.00		0.95	1.00	1.00	0.95	1.00		0.95	1.00	1.00
Satd. Flow (prot)	1656	1828		1467	1743	1442	1444	1519		1530	1532	1392
Flt Permitted	0.41	1.00		0.31	1.00	1.00	0.69	1.00		0.61	1.00	1.00
Satd. Flow (perm)	716	1828		474	1743	1442	1052	1519		984	1532	1392
Peak-hour factor, PHF	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94
Adj. Flow (vph)	163	676	19	48	534	140	23	148	32	145	100	169
RTOR Reduction (vph)	0	1	0	0	0	51	0	10	0	0	0	134
Lane Group Flow (vph)	163	694	0	48	534	89	23	170	0	145	100	35
Confl. Peds. (#/hr)			1	1								
Heavy Vehicles (%)	9%	3%	19%	23%	9%	12%	25%	20%	30%	18%	24%	16%
Turn Type	Perm	NA		Perm	NA	Perm	Perm	NA		Perm	NA	Perm
Protected Phases		2			6			4			8	
Permitted Phases	2			6		6	4			8		8
Actuated Green, G (s)	57.5	57.5		57.5	57.5	57.5	18.5	18.5		18.5	18.5	18.5
Effective Green, g (s)	57.5	57.5		57.5	57.5	57.5	18.5	18.5		18.5	18.5	18.5
Actuated g/C Ratio	0.64	0.64		0.64	0.64	0.64	0.21	0.21		0.21	0.21	0.21
Clearance Time (s)	7.0	7.0		7.0	7.0	7.0	7.0	7.0		7.0	7.0	7.0
Vehicle Extension (s)	4.0	4.0		4.0	4.0	4.0	2.0	2.0		2.0	2.0	2.0
Lane Grp Cap (vph)	457	1167		302	1113	921	216	312		202	314	286
v/s Ratio Prot		c0.38			0.31			0.11			0.07	
v/s Ratio Perm	0.23			0.10		0.06	0.02			c0.15		0.02
v/c Ratio	0.36	0.59		0.16	0.48	0.10	0.11	0.55		0.72	0.32	0.12
Uniform Delay, d1	7.6	9.5		6.5	8.5	6.3	29.0	32.0		33.3	30.4	29.1
Progression Factor	1.00	1.00		1.00	1.00	1.00	1.00	1.00		1.00	1.00	1.00
Incremental Delay, d2	2.2	2.2		1.1	1.5	0.2	0.1	1.1		9.7	0.2	0.1
Delay (s)	9.8	11.7		7.7	9.9	6.5	29.1	33.0		43.0	30.6	29.2
Level of Service	A	В		А	Α	Α	С	С		D	С	С
Approach Delay (s)		11.3			9.1			32.6			34.4	
Approach LOS		В			А			С			С	
Intersection Summary												
HCM 2000 Control Delay			16.9	H	CM 2000	Level of	Service		В			
HCM 2000 Volume to Capa	acity ratio		0.62									
Actuated Cycle Length (s)			90.0	S	um of los	t time (s)			14.0			
Intersection Capacity Utilization	ation		101.2%	IC	U Level	of Service			G			
Analysis Period (min)			15									
0.111 0												

c Critical Lane Group

Uppers Quarry Traffic Impact Study TMIG

			-		-				`	1	
	•	-	¥	1	-		1	T	*	Ŧ	
Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	SBL	SBT	
Lane Configurations	<u>۲</u>	- <b>††</b>	1	ሻ	- <b>††</b>	1	<u>۲</u>	4Î	<u>۲</u>	14	
Traffic Volume (vph)	323	767	178	217	854	73	133	180	52	222	
Future Volume (vph)	323	767	178	217	854	73	133	180	52	222	
Turn Type	pm+pt	NA	Perm	pm+pt	NA	Perm	pm+pt	NA	Perm	NA	
Protected Phases	5	2		1	6		7	4		8	
Permitted Phases	2		2	6		6	4		8		
Detector Phase	5	2	2	1	6	6	7	4	8	8	
Switch Phase											
Minimum Initial (s)	8.0	10.0	10.0	8.0	10.0	10.0	8.0	10.0	10.0	10.0	
Minimum Split (s)	11.0	35.1	35.1	12.5	35.1	35.1	11.0	41.4	41.4	41.4	
Total Split (s)	28.5	44.5	44.5	20.0	36.0	36.0	11.0	55.5	44.5	44.5	
Total Split (%)	23.8%	37.1%	37.1%	16.7%	30.0%	30.0%	9.2%	46.3%	37.1%	37.1%	
Yellow Time (s)	3.0	4.1	4.1	3.0	4.1	4.1	3.0	4.1	4.1	4.1	
All-Red Time (s)	0.0	2.0	2.0	0.0	2.0	2.0	0.0	2.3	2.3	2.3	
Lost Time Adjust (s)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Total Lost Time (s)	3.0	6.1	6.1	3.0	6.1	6.1	3.0	6.4	6.4	6.4	
Lead/Lag	Lead	Lag	Lag	Lead	Lag	Lag	Lead		Lag	Lag	
Lead-Lag Optimize?	Yes	Yes	Yes	Yes	Yes	Yes	Yes		Yes	Yes	
Recall Mode	None	C-Max	C-Max	None	C-Max	C-Max	None	None	None	None	
Act Effct Green (s)	63.6	42.3	42.3	53.9	35.6	35.6	50.4	47.0	36.0	36.0	
Actuated g/C Ratio	0.53	0.35	0.35	0.45	0.30	0.30	0.42	0.39	0.30	0.30	
v/c Ratio	0.93	0.65	0.34	0.77	0.86	0.15	0.75	0.51	0.18	0.95	
Control Delay	73.6	49.4	25.7	38.2	50.7	2.8	49.0	28.1	31.8	67.7	
Queue Delay	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Total Delay	73.6	49.4	25.7	38.2	50.7	2.8	49.0	28.1	31.8	67.7	
LOS	E	D	С	D	D	А	D	С	С	E	
Approach Delay		52.2			45.3			34.9		63.8	
Approach LOS		D			D			С		E	
Intersection Summary											
Cycle Length: 120											
Actuated Cycle Length: 120											
Offset: 0 (0%), Referenced t	o phase 2:	EBTL and	d 6:WBTL	, Start of	Green						
Natural Cycle: 100											
Control Type: Actuated-Coo	rdinated										
Maximum v/c Ratio: 0.95											
ntersection Signal Delay: 49	).3			Ir	ntersection	1 LOS: D					
ntersection Capacity Utilizat	ion 90.7%			10	CU Level	of Service	Ε				
Analysis Period (min) 15											

Ø1	→ Ø2 (R)	<b>≜</b> ¶ø4	
20 s	44.5 s	55.5 s	
∕ _{Ø5}	● ● Ø6 (R)	<b>▲</b> Ø7	Ø8

	_
Uppers Quarry Traffic Impact Study	
TMIG	

Synchro 10 Report

 HCM Signalized Intersection Capacity Analysis<2035 Total - Thorold Townline> AM Peak Hour

 4: Thorold Townline Road & Thorold Stone Road

 09-23-2021

	٦	→	$\mathbf{i}$	1	+	×	•	1	1	1	Ŧ	~
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	۲	<b>^</b>	1	۲	<b>^</b>	1	ň	ţ,		٦	ţ,	
Traffic Volume (vph)	323	767	178	217	854	73	133	180	100	52	222	205
Future Volume (vph)	323	767	178	217	854	73	133	180	100	52	222	205
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Total Lost time (s)	3.0	6.1	6.1	3.0	6.1	6.1	3.0	6.4		6.4	6.4	
Lane Util. Factor	1.00	0.95	1.00	1.00	0.95	1.00	1.00	1.00		1.00	1.00	
Frpb, ped/bikes	1.00	1.00	1.00	1.00	1.00	0.97	1.00	1.00		1.00	1.00	
Flpb, ped/bikes	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00		1.00	1.00	
Frt	1.00	1.00	0.85	1.00	1.00	0.85	1.00	0.95		1.00	0.93	
Flt Protected	0.95	1.00	1.00	0.95	1.00	1.00	0.95	1.00		0.95	1.00	
Satd. Flow (prot)	1641	3471	1292	1399	3505	1453	1347	1412		1641	1474	
Flt Permitted	0.10	1.00	1.00	0.24	1.00	1.00	0.19	1.00		0.58	1.00	
Satd. Flow (perm)	179	3471	1292	359	3505	1453	272	1412		1004	1474	
Peak-hour factor, PHF	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96
Adj. Flow (vph)	336	799	185	226	890	76	139	188	104	54	231	214
RTOR Reduction (vph)	0	0	91	0	0	54	0	17	0	0	29	0
Lane Group Flow (vph)	336	799	94	226	890	22	139	275	0	54	416	0
Confl. Peds. (#/hr)	4					4						
Heavy Vehicles (%)	10%	4%	25%	29%	3%	8%	34%	22%	37%	10%	22%	17%
Turn Type	pm+pt	NA	Perm	pm+pt	NA	Perm	pm+pt	NA		Perm	NA	
Protected Phases	5	2		1	6		7	4			8	
Permitted Phases	2		2	6		6	4			8		
Actuated Green, G (s)	60.5	42.3	42.3	50.7	35.5	35.5	47.0	47.0		36.0	36.0	
Effective Green, g (s)	60.5	42.3	42.3	50.7	35.5	35.5	47.0	47.0		36.0	36.0	
Actuated g/C Ratio	0.50	0.35	0.35	0.42	0.30	0.30	0.39	0.39		0.30	0.30	
Clearance Time (s)	3.0	6.1	6.1	3.0	6.1	6.1	3.0	6.4		6.4	6.4	
Vehicle Extension (s)	2.5	6.0	6.0	2.5	6.0	6.0	2.5	2.3		2.3	2.3	
Lane Grp Cap (vph)	358	1223	455	283	1036	429	178	553		301	442	
v/s Ratio Prot	c0.17	0.23		0.10	0.25		c0.05	0.19			c0.28	
v/s Ratio Perm	c0.30		0.07	0.24		0.02	0.25			0.05		
v/c Ratio	0.94	0.65	0.21	0.80	0.86	0.05	0.78	0.50		0.18	0.94	
Uniform Delay, d1	35.2	32.7	27.1	24.7	39.9	30.2	28.7	27.6		31.1	41.0	
Progression Factor	1.43	1.38	2.71	1.00	1.00	1.00	1.00	1.00		1.00	1.00	
Incremental Delay, d2	28.7	2.3	0.9	14.1	9.2	0.2	19.0	0.4		0.2	28.4	
Delay (s)	79.1	47.4	74.4	38.8	49.1	30.5	47.6	28.0		31.2	69.4	
Level of Service	E	D	E	D	D	С	D	С		С	E	
Approach Delay (s)		59.3			46.0			34.3			65.3	
Approach LOS		E			D			С			E	
Intersection Summary												
HCM 2000 Control Delay			52.4	Н	CM 2000	Level of	Service		D			
HCM 2000 Volume to Capa	city ratio		0.95									
Actuated Cycle Length (s)	,		120.0	S	um of losi	t time (s)			18.5			
Intersection Capacity Utiliza	ation		90.7%	IC	U Level	of Service	)		E			
Analysis Period (min)			15									
c Critical Lane Group												

Uppers Quarry Traffic Impact Study TMIG

Timings 5: Thorold Townline	dys La	ne	<2035 Total - Thorold Townline> AM Peak Hour 09-23-2021								
	۶	+	*	4	ł	<	1	*	ţ	~	
Lane Group	EBL	EBT	EBR	WBL	WBT	NBL	NBT	SBL	SBT	SBR	
Lane Configurations	ľ	•	1	ľ	ĥ	ľ	ĥ	1	•	1	
Traffic Volume (vph)	205	607	107	38	422	77	140	45	85	84	
Future Volume (vph)	205	607	107	38	422	77	140	45	85	84	
Turn Type	Perm	NA	Perm	Perm	NA	Perm	NA	Perm	NA	Perm	
Protected Phases		2			6		4		8		
Permitted Phases	2		2	6		4		8		8	
Detector Phase	2	2	2	6	6	4	4	8	8	8	
Switch Phase											
Minimum Initial (s)	20.0	20.0	20.0	20.0	20.0	10.0	10.0	10.0	10.0	10.0	
Minimum Split (s)	29.0	29.0	29.0	29.0	29.0	35.0	35.0	35.0	35.0	35.0	
Total Split (s)	65.0	65.0	65.0	65.0	65.0	35.0	35.0	35.0	35.0	35.0	
Total Split (%)	65.0%	65.0%	65.0%	65.0%	65.0%	35.0%	35.0%	35.0%	35.0%	35.0%	
Yellow Time (s)	5.0	5.0	5.0	5.0	5.0	4.0	4.0	4.0	4.0	4.0	
All-Red Time (s)	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	
Lost Time Adjust (s)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Total Lost Time (s)	7.0	7.0	7.0	7.0	7.0	6.0	6.0	6.0	6.0	6.0	
Lead/Lag											
Lead-Lag Optimize?											
Recall Mode	C-Max	C-Max	C-Max	Max	Max	None	None	None	None	None	
Act Effct Green (s)	68.8	68.8	68.8	68.8	68.8	18.2	18.2	18.2	18.2	18.2	
Actuated g/C Ratio	0.69	0.69	0.69	0.69	0.69	0.18	0.18	0.18	0.18	0.18	
v/c Ratio	0.46	0.52	0.11	0.09	0.44	0.39	0.63	0.30	0.31	0.30	
Control Delay	12.1	10.4	4.0	7.1	8.9	39.8	43.8	38.3	36.6	9.6	
Queue Delay	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
I otal Delay	12.1	10.4	4.0	7.1	8.9	39.8	43.8	38.3	36.6	9.6	
LOS	В	В	A	A	A	D	D	D	D	A	
Approach Delay		10.0			8.8		42.6		26.3		
Approach LOS		A			A		D		C		
Intersection Summary											
Cycle Length: 100											
Actuated Cycle Length: 100											
Offset: 0 (0%), Referenced to	phase 2	EBTL. St	art of Gre	en							
Natural Cycle: 80		,									
Control Type: Actuated-Coor	dinated										
Maximum v/c Ratio: 0.63											
Intersection Signal Delay: 15	.8			Ir	ntersectio	n LOS: B					
Intersection Capacity Utilizati	ion 88.2%			10	CU Level	of Service	ε				
Analysis Period (min) 15											
Solits and Phases: 5: Thor	old Town	line Road	& Lundw	lano							

Splits and Phases 5: Thoroid Townline Road & Lundys Lane

opilio una i nuodo. O. morola rominino rioda a Eurayo Euro		
≠ Ø2 (R)	▲ Ø4	
65 s	35 s	
<b>√</b> Ø6	Ø8	
65 s	35 s	

Uppers Quarry Traffic Impact Study TMIG

Synchro 10 Report

 HCM Signalized Intersection Capacity Analysis<2035 Total - Thorold Townline > AM Peak Hour

 5: Thorold Townline Road & Lundys Lane

 09-23-2021

	٦	-	$\mathbf{r}$	1	+	•	1	1	1	1	Ŧ	~
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	5	•	1	<u> </u>	ĥ		<u> </u>	ĥ		ň	1	1
Traffic Volume (vph)	205	607	107	38	422	79	77	140	37	45	85	84
Future Volume (vph)	205	607	107	38	422	79	77	140	37	45	85	84
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Total Lost time (s)	7.0	7.0	7.0	7.0	7.0		6.0	6.0		6.0	6.0	6.0
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00		1.00	1.00		1.00	1.00	1.00
Frpb, ped/bikes	1.00	1.00	1.00	1.00	1.00		1.00	1.00		1.00	1.00	1.00
Flpb, ped/bikes	1.00	1.00	1.00	1.00	1.00		1.00	1.00		1.00	1.00	1.00
Frt	1.00	1.00	0.85	1.00	0.98		1.00	0.97		1.00	1.00	0.85
Flt Protected	0.95	1.00	1.00	0.95	1.00		0.95	1.00		0.95	1.00	1.00
Satd. Flow (prot)	1582	1810	1495	1752	1760		1612	1607		1671	1638	1252
Flt Permitted	0.42	1.00	1.00	0.35	1.00		0.70	1.00		0.51	1.00	1.00
Satd. Flow (perm)	700	1810	1495	648	1760		1184	1607		893	1638	1252
Peak-hour factor, PHF	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93
Adi, Flow (vph)	220	653	115	41	454	85	83	151	40	48	91	90
RTOR Reduction (vph)	0	0	17	0	5	0	0	11	0	0	0	74
Lane Group Flow (vph)	220	653	98	41	534	0	83	180	0	48	91	16
Confl. Peds. (#/hr)	1					1						
Heavy Vehicles (%)	14%	5%	8%	3%	6%	0%	12%	17%	5%	8%	16%	29%
Turn Type	Perm	NA	Perm	Perm	NA		Perm	NA		Perm	NA	Perm
Protected Phases		2			6			4			8	
Permitted Phases	2		2	6			4			8		8
Actuated Green, G (s)	68.8	68.8	68.8	68.8	68.8		18.2	18.2		18.2	18.2	18.2
Effective Green, g (s)	68.8	68.8	68.8	68.8	68.8		18.2	18.2		18.2	18.2	18.2
Actuated g/C Ratio	0.69	0.69	0.69	0.69	0.69		0.18	0.18		0.18	0.18	0.18
Clearance Time (s)	7.0	7.0	7.0	7.0	7.0		6.0	6.0		6.0	6.0	6.0
Vehicle Extension (s)	5.0	5.0	5.0	5.0	5.0		5.0	5.0		5.0	5.0	5.0
Lane Grp Cap (vph)	481	1245	1028	445	1210		215	292		162	298	227
v/s Ratio Prot		c0.36			0.30			c0.11			0.06	
v/s Ratio Perm	0.31		0.07	0.06			0.07			0.05		0.01
v/c Ratio	0.46	0.52	0.10	0.09	0.44		0.39	0.62		0.30	0.31	0.07
Uniform Delay, d1	7.1	7.6	5.2	5.2	7.0		36.0	37.7		35.4	35.4	33.9
Progression Factor	1.00	1.00	1.00	1.00	1.00		1.00	1.00		1.00	1.00	1.00
Incremental Delay, d2	3.1	1.6	0.2	0.4	1.2		2.4	5.5		2.1	1.2	0.3
Delay (s)	10.2	9.2	5.4	5.6	8.2		38.4	43.2		37.5	36.6	34.2
Level of Service	В	А	А	А	А		D	D		D	D	С
Approach Delay (s)		9.0			8.0			41.8			35.9	
Approach LOS		А			Α			D			D	
Intersection Summary												
HCM 2000 Control Delay			16.0	Н	CM 2000	Level of S	Service		В			
HCM 2000 Volume to Capaci	tv ratio		0.54									
Actuated Cycle Length (s)	,		100.0	S	um of lost	time (s)			13.0			
Intersection Capacity Utilizati	on		88.2%	IC	U Level o	of Service			E			
Analysis Period (min)			15						_			
c Critical Lane Group												

Uppers Quarry Traffic Impact Study TMIG

Timings     <2035 Total - Thorold Townline> AM Peak       6: Thorold Townline Road & Beaverdams Road     09-2									
	<u>)</u>	<u>→</u>	<ul> <li>Image: A start of the start of</li></ul>	<b>+</b>	1	t	4	ţ	
Lane Group	EBL	EBT	WBL	WBT	NBL	NBT	SBL	SBT	
Lane Configurations		4		4		4		4	
Traffic Volume (vph)	19	126	52	170	24	383	11	584	
Future Volume (vph)	19	126	52	170	24	383	11	584	
Turn Type	Perm	NA	Perm	NA	Perm	NA	Perm	NA	
Protected Phases		2		6		4		8	
Permitted Phases	2		6		4		8		
Detector Phase	2	2	6	6	4	4	8	8	
Switch Phase									
Minimum Initial (s)	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	
Minimum Split (s)	30.5	30.5	30.5	30.5	34.0	34.0	30.5	30.5	
Total Split (s)	31.0	31.0	31.0	31.0	59.0	59.0	59.0	59.0	
Total Split (%)	34.4%	34.4%	34.4%	34.4%	65.6%	65.6%	65.6%	65.6%	
Yellow Time (s)	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0	
All-Red Time (s)	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	
Lost Time Adjust (s)		0.0		0.0		0.0		0.0	
Total Lost Time (s)		6.0		6.0		6.0		6.0	
Lead/Lag									
Lead-Lag Optimize?									
Recall Mode	C-Max	C-Max	Max	Max	Max	Max	Max	Max	
Act Effct Green (s)		25.0		25.0		53.0		53.0	
Actuated g/C Ratio		0.28		0.28		0.59		0.59	
v/c Ratio		0.36		0.57		0.62		0.76	
Control Delay		27.9		33.0		15.6		20.7	
Queue Delay		0.0		0.0		0.0		0.0	
Total Delay		27.9		33.0		15.6		20.7	
LOS		С		С		В		С	
Approach Delay		27.9		33.0		15.6		20.7	
Approach LOS		С		С		В		С	
Intersection Summarv									
Cycle Length: 90									
Actuated Cycle Length: 90									
Offset: 0 (0%) Referenced t	to phase 2	EBTI St	art of Gre	en					
Natural Cycle: 75		, 00							
Control Type: Actuated-Coo	rdinated								
Maximum v/c Ratio: 0.76									
Intersection Signal Delay: 2	1.8			I	ntersectio	n LOS: C			
Intersection Capacity Utilization	tion 70.4%			10	CU Level	of Service	∍ C		
Analysis Period (min) 15					2.5.20.01				
Splits and Phases: 6: Tho	orold Town	line Road	& Beave	rdams Ro	ad				

opino una i nacco.	0. 110/010 100011110 110000		
▲ _{Ø2 (R)}		▲ Ø4	
31 s		59 s	
<b>₩</b> Ø6			
31 s		59 s	

Synchro 10 Report

 HCM Signalized Intersection Capacity Analysis<2035 Total - Thorold Townline > AM Peak Hour

 6: Thorold Townline Road & Beaverdams Road

	٦	-	$\mathbf{\hat{z}}$	4	+	۰.	•	Ť	۲	1	Ŧ	~
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		4			\$			\$			4	
Traffic Volume (vph)	19	126	16	52	170	22	24	383	83	11	584	19
Future Volume (vph)	19	126	16	52	170	22	24	383	83	11	584	19
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Total Lost time (s)		6.0			6.0			6.0			6.0	
Lane Util. Factor		1.00			1.00			1.00			1.00	
Frpb, ped/bikes		1.00			1.00			1.00			1.00	
Flpb, ped/bikes		1.00			1.00			1.00			1.00	
Frt		0.99			0.99			0.98			1.00	
Flt Protected		0.99			0.99			1.00			1.00	
Satd. Flow (prot)		1804			1838			1500			1509	
Flt Permitted		0.94			0.90			0.95			0.99	
Satd. Flow (perm)		1714			1669			1435			1494	
Peak-hour factor, PHF	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Adj. Flow (vph)	21	137	17	57	185	24	26	416	90	12	635	21
RTOR Reduction (vph)	0	4	0	0	4	0	0	8	0	0	1	0
Lane Group Flow (vph)	0	171	0	0	262	0	0	524	0	0	667	0
Confl. Peds. (#/hr)			5	5			6					6
Heavy Vehicles (%)	5%	2%	9%	0%	1%	2%	0%	30%	0%	9%	26%	9%
Turn Type	Perm	NA		Perm	NA		Perm	NA		Perm	NA	
Protected Phases		2			6			4			8	
Permitted Phases	2			6			4			8		
Actuated Green, G (s)		25.0			25.0			53.0			53.0	
Effective Green, g (s)		25.0			25.0			53.0			53.0	
Actuated g/C Ratio		0.28			0.28			0.59			0.59	
Clearance Time (s)		6.0			6.0			6.0			6.0	
Vehicle Extension (s)		5.0			5.0			5.0			5.0	
Lane Grp Cap (vph)		476			463			845			879	
v/s Ratio Prot												
v/s Ratio Perm		0.10			c0.16			0.37			c0.45	
v/c Ratio		0.36			0.57			0.62			0.76	
Uniform Delay, d1		26.1			27.9			12.0			13.7	
Progression Factor		1.00			1.00			1.00			1.00	
Incremental Delay, d2		2.1			5.0			3.4			6.1	
Delay (s)		28.2			32.8			15.4			19.8	
Level of Service		С			С			В			В	
Approach Delay (s)		28.2			32.8			15.4			19.8	
Approach LOS		С			С			В			В	
Intersection Summary												
HCM 2000 Control Delay			21.4	Н	CM 2000	Level of	Service		С			
HCM 2000 Volume to Capac	city ratio		0.70									
Actuated Cycle Length (s)	·		90.0	S	um of lost	time (s)			12.0			
Intersection Capacity Utilization	tion		70.4%	IC	U Level o	of Service			С			
Analysis Period (min)			15									

c Critical Lane Group

Uppers Quarry Traffic Impact Study TMIG

HCM Unsignalized 7: Thorold Townlin	Interse e Road	ction C & Upp	apacit ers Lai	y Anal <u>y</u> ne	ys1203	5 Total -	- Thorold Townline> AM Peak Hour 09-23-2021
	4	•	Ť	1	1	ţ	
Movement	WBL	WBR	NBT	NBR	SBL	SBT	
Lane Configurations	Y		¢Î		ľ	•	
Traffic Volume (veh/h)	3	66	458	3	46	419	
Future Volume (Veh/h)	3	66	458	3	46	419	
Sign Control	Stop		Free			Free	
Grade	0%		0%			0%	
Peak Hour Factor	0.93	0.93	0.93	0.93	0.93	0.93	
Hourly flow rate (vph)	3	71	492	3	49	451	
Pedestrians							
Lane Width (m)							
Walking Speed (m/s)							
Percent Blockage							
Right turn flare (veh)							
Median type			None			None	
Median storage veh)							
Upstream signal (m)							
pX, platoon unblocked							
vC, conflicting volume	1042	494			495		
vC1, stage 1 conf vol							
vC2, stage 2 conf vol							
vCu, unblocked vol	1042	494			495		
tC, single (s)	6.4	7.1			4.9		
tC, 2 stage (s)							
tF (s)	3.5	4.1			2.9		
p0 queue free %	99	84			94		
cM capacity (veh/h)	240	436			754		
Direction, Lane #	WB 1	NB 1	SB 1	SB 2			
Volume Total	74	495	49	451			
Volume Left	3	0	49	0			
Volume Right	71	3	0	0			
cSH	422	1700	754	1700			
Volume to Capacity	0.18	0.29	0.06	0.27			
Queue Length 95th (m)	5.0	0.0	1.7	0.0			
Control Delay (s)	15.3	0.0	10.1	0.0			
Lane LOS	С		В				
Approach Delay (s)	15.3	0.0	1.0				
Approach LOS	С						
Intersection Summary							
Average Delay			1.5				
Intersection Capacity Utiliza	ation		41.9%	IC	U Level o	of Service	A
Analysis Period (min)			15				

Timings <a>&lt;2035 Total - Thorold Townline&gt; PM Peak Hour</a>												
1: Davis Road & Th	orold S	Stone F	Road								09-2	3-2021
	≯	-	$\mathbf{r}$	4	+	1	Ť	1	1	ţ	4	
Lane Group	EBL	EBT	EBR	WBL	WBT	NBL	NBT	NBR	SBL	SBT	SBR	
Lane Configurations	٦	<b>^</b>	1	ሻ	<b>†</b> 12	5	ę	1	5	•	1	
Traffic Volume (vph)	24	1274	736	211	1242	627	5	178	4	6	28	
Future Volume (vph)	24	1274	736	211	1242	627	5	178	4	6	28	
Turn Type	Perm	NA	Perm	pm+pt	NA	Split	NA	Perm	Split	NA	Perm	
Protected Phases		2		1	6	4	4		8	8		
Permitted Phases	2		2	6				4			8	
Detector Phase	2	2	2	1	6	4	4	4	8	8	8	
Switch Phase												
Minimum Initial (s)	20.0	20.0	20.0	5.0	20.0	10.0	10.0	10.0	10.0	10.0	10.0	
Minimum Split (s)	28.9	28.9	28.9	8.0	28.9	29.7	29.7	29.7	17.7	17.7	17.7	
Total Split (s)	55.0	55.0	55.0	14.0	69.0	33.3	33.3	33.3	17.7	17.7	17.7	
Total Split (%)	45.8%	45.8%	45.8%	11.7%	57.5%	27.8%	27.8%	27.8%	14.8%	14.8%	14.8%	
Yellow Time (s)	5.4	5.4	5.4	3.0	5.4	5.7	5.7	5.7	5.7	5.7	5.7	
All-Red Time (s)	1.5	1.5	1.5	0.0	1.5	2.0	2.0	2.0	2.0	2.0	2.0	
Lost Time Adjust (s)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Total Lost Time (s)	6.9	6.9	6.9	3.0	6.9	7.7	7.7	7.7	7.7	7.7	7.7	
Lead/Lag	Lag	Lag	Lag	Lead								_
Lead-Lag Optimize?	Yes	Yes	Yes	Yes	0.14							
Recall Mode	C-Max	C-Max	C-Max	None	C-Max	None	None	None	None	None	None	_
Act Effct Green (s)	52.2	52.2	52.2	/3.1	69.2	25.6	25.6	25.6	10.0	10.0	10.0	
Actuated g/C Ratio	0.44	0.44	0.44	0.61	0.58	0.21	0.21	0.21	0.08	0.08	0.08	_
V/C Ratio	0.23	0.88	0.86	0.85	0.65	0.92	0.94	0.40	0.03	0.04	0.12	
Control Delay	30.3	40.0	25.9	53.4	29.3	/8.2	80.8	8.3	51.2	51.3	1.0	
Queue Delay	20.2	40.0	25.0	52.4	20.2	79.0	0.0	0.0	0.0 51.0	0.0 51.2	0.0	
	30.3	40.0	20.9	55.4 D	29.5	70.Z	00.0 E	0.5	J1.2	51.5 D	1.0	
LUG Approach Dolov	U	24.9	U	U	22.0	E	62 O	A	U	12.0	A	
Approach LOS		04.0 C			JZ.0		03.9 E			13.9 B		
Appidacii 200		U			U		L			D		
Intersection Summary												
Cycle Length: 120												
Actuated Cycle Length: 120					-							_
Offset: 0 (0%), Referenced to	phase 2	EBTL and	d 6:WBTL	., Start of	Green							
Natural Cycle: 115	P ( 1											_
Control Type: Actuated-Coor	anated											
Intersection Cignel Delaw 20	2				toroot'r	~ I OC. D						
Intersection Signal Delay: 39	.5 ion 02 10/			11	THE AVE	of Sonvice	. E					
Analysis Period (min) 15	1011 93.1%			I	JU Level	UI SEI VICE	; r'					
Analysis Fellou (IIIII) 15												

Splits and Phases: 1: Davis Road & Thorold Stone Road		
🖸 Ø1 🔮 🖗 Ø2 (R)	<b>▲</b> Ø4	1 Ø8
14 s 55 s	33.3 s	17.7 s
₩ Ø6 (R)		
60 a		

Synchro 10 Report

HCM Signalized Intersection Capacity Analysis<2035 Total - Thorold Townline> PM Peak Hour 1: Davis Road & Thorold Stone Road 09-23-2021

	٦	-	$\mathbf{r}$	4	+	•	•	Ť	۲	1	ŧ	~
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	<u>۲</u>	- <b>††</b>	1	<u>۳</u>			<u>۲</u>	4	1	<u>۲</u>	<b>↑</b>	1
Traffic Volume (vph)	24	1274	736	211	1242	1	627	5	178	4	6	28
Future Volume (vph)	24	1274	736	211	1242	1	627	5	178	4	6	28
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Total Lost time (s)	6.9	6.9	6.9	3.0	6.9		7.7	7.7	7.7	7.7	7.7	7.7
Lane Util. Factor	1.00	0.95	1.00	1.00	0.95		0.95	0.95	1.00	1.00	1.00	1.00
Frpb, ped/bikes	1.00	1.00	1.00	1.00	1.00		1.00	1.00	1.00	1.00	1.00	0.98
Flpb, ped/bikes	1.00	1.00	1.00	1.00	1.00		1.00	1.00	1.00	1.00	1.00	1.00
Frt	1.00	1.00	0.85	1.00	1.00		1.00	1.00	0.85	1.00	1.00	0.85
Flt Protected	0.95	1.00	1.00	0.95	1.00		0.95	0.95	1.00	0.95	1.00	1.00
Satd. Flow (prot)	1433	3505	1568	1671	3505		1681	1680	1482	1805	1810	1525
Flt Permitted	0.17	1.00	1.00	0.08	1.00		0.95	0.95	1.00	0.95	1.00	1.00
Satd. Flow (perm)	256	3505	1568	135	3505		1681	1680	1482	1805	1810	1525
Peak-hour factor, PHF	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95
Adj. Flow (vph)	25	1341	775	222	1307	1	660	5	187	4	6	29
RTOR Reduction (vph)	0	0	235	0	0	0	0	0	147	0	0	28
Lane Group Flow (vph)	25	1341	540	222	1308	0	330	335	40	4	6	1
Confl. Peds. (#/hr)							1					1
Heavy Vehicles (%)	26%	3%	3%	8%	3%	0%	2%	30%	9%	0%	5%	4%
Turn Type	Perm	NA	Perm	pm+pt	NA		Split	NA	Perm	Split	NA	Perm
Protected Phases		2			6		. 4	4		. 8	8	
Permitted Phases	2		2	6					4			8
Actuated Green, G (s)	49.1	49.1	49.1	66.1	66.1		25.6	25.6	25.6	6.0	6.0	6.0
Effective Green, g (s)	49.1	49.1	49.1	66.1	66.1		25.6	25.6	25.6	6.0	6.0	6.0
Actuated g/C Ratio	0.41	0.41	0.41	0.55	0.55		0.21	0.21	0.21	0.05	0.05	0.05
Clearance Time (s)	6.9	6.9	6.9	3.0	6.9		7.7	7.7	7.7	7.7	7.7	7.7
Vehicle Extension (s)	3.0	3.0	3.0	3.0	3.0		4.5	4.5	4.5	4.5	4.5	4.5
Lane Grp Cap (vph)	104	1434	641	253	1930		358	358	316	90	90	76
v/s Ratio Prot		c0.38		c0.10	0.37		0.20	c0.20		0.00	c0.00	
v/s Ratio Perm	0.10		0.34	0.38					0.03			0.00
v/c Ratio	0.24	0.94	0.84	0.88	0.68		0.92	0.94	0.13	0.04	0.07	0.02
Uniform Delay, d1	23.2	33.9	32.0	34.7	19.3		46.2	46.4	38.2	54.3	54.3	54.2
Progression Factor	1.00	1.00	1.00	1.45	1.50		1.00	1.00	1.00	1.00	1.00	1.00
Incremental Delay, d2	5.4	12.6	12.7	14.6	0.9		29.3	31.9	0.3	0.4	0.5	0.2
Delay (s)	28.6	46.6	44.7	65.1	30.0		75.5	78.3	38.5	54.6	54.9	54.4
Level of Service	С	D	D	E	С		E	E	D	D	D	D
Approach Delay (s)		45.7			35.1			68.5			54.5	
Approach LOS		D			D			E			D	
Intersection Summary												
HCM 2000 Control Delay			46.4	н	CM 2000	Level of S	Service		D			
HCM 2000 Volume to Cana	acity ratio		0.87		2.0.2000				5			
Actuated Cycle Length (s)			120.0	S	um of los	t time (s)			25.3			
Intersection Capacity Utiliza	ation		93.1%	10	CU Level	of Service			_0.0			
Analysis Period (min)			15									
			10									

c Critical Lane Group

Uppers Quarry Traffic Impact Study TMIG

Timings       <2035 Total - Thorold Townline> PM Peak Hour         2: Davis Road & Niagara Falls Road/Beaverdams Road       09-23-2021										
	•ر	-	4	+	•	t	1	ţ	~	
Lane Group	EBL	EBT	WBL	WBT	NBL	NBT	SBL	SBT	SBR	
Lane Configurations		\$		\$	ľ	¢۴	1	<b>^</b>	1	
Traffic Volume (vph)	90	32	60	44	26	582	170	691	105	
Future Volume (vph)	90	32	60	44	26	582	170	691	105	
Turn Type	Perm	NA	Perm	NA	Perm	NA	Perm	NA	Perm	
Protected Phases		2		6		4		8		
Permitted Phases	2		6		4		8		8	
Detector Phase	2	2	6	6	4	4	8	8	8	
Switch Phase										
Vinimum Initial (s)	10.0	10.0	10.0	10.0	25.0	25.0	25.0	25.0	25.0	
Vinimum Split (s)	38.1	38.1	38.1	38.1	32.0	32.0	32.0	32.0	32.0	
Fotal Split (s)	40.0	40.0	40.0	40.0	60.0	60.0	60.0	60.0	60.0	
Total Split (%)	40.0%	40.0%	40.0%	40.0%	60.0%	60.0%	60.0%	60.0%	60.0%	
Yellow Time (s)	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	
All-Red Time (s)	3.1	3.1	3.1	3.1	2.0	2.0	2.0	2.0	2.0	
ost Time Adjust (s)		0.0		0.0	0.0	0.0	0.0	0.0	0.0	
Fotal Lost Time (s)		8.1		8.1	7.0	7.0	7.0	7.0	7.0	
_ead/Lag										
.ead-Lag Optimize?										
Recall Mode	C-Max	C-Max	Max	Max	None	None	None	None	None	
Act Effct Green (s)		46.8		46.8	38.1	38.1	38.1	38.1	38.1	
Actuated g/C Ratio		0.47		0.47	0.38	0.38	0.38	0.38	0.38	
//c Ratio		0.28		0.35	0.13	0.52	0.79	0.57	0.17	
Control Delay		20.0		16.1	17.5	23.9	49.3	25.4	3.2	
Queue Delay		0.0		0.0	0.0	0.0	0.0	0.0	0.0	
Total Delay		20.0		16.1	17.5	23.9	49.3	25.4	3.2	
.0S		В		В	В	С	D	С	A	
Approach Delay		20.0		16.1		23.7		27.2		
Approach LOS		В		В		С		С		
ntersection Summary										
Cycle Length: 100										
Actuated Cycle Length: 100										
Offset: 0 (0%). Referenced to	phase 2	EBTL, St	art of Gre	en						
latural Cycle: 75	- F.1000 E.	, 00								
Control Type: Actuated-Coord	dinated									
faximum v/c Ratio: 0.79										
ntersection Signal Delay: 24	.1			Ir	ntersectio	n LOS: C				
ntersection Capacity Utilizati	on 78.5%				CU Level	of Service	e D			
analysis Period (min) 15										

Ø2 (R)	< <b>↑</b> _{Ø4}
40 s	60 s
<b>₩</b> Ø6	€ Ø8
40 s	60 s

Synchro 10 Report

 HCM Signalized Intersection Capacity Analysis<2035 Total - Thorold Townline> PM Peak Hour

 2: Davis Road & Niagara Falls Road/Beaverdams Road
 09-23-2021

	۶	-	$\mathbf{F}$	4	+	×	٠	1	۲	1	Ŧ	~
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		4			\$		۲.	<b>≜1</b> }		۲.	44	1
Traffic Volume (vph)	90	32	31	60	44	147	26	582	41	170	691	105
Future Volume (vph)	90	32	31	60	44	147	26	582	41	170	691	105
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Total Lost time (s)		8.1			8.1		7.0	7.0		7.0	7.0	7.0
Lane Util. Factor		1.00			1.00		1.00	0.95		1.00	0.95	1.00
Frt		0.97			0.92		1.00	0.99		1.00	1.00	0.85
Flt Protected		0.97			0.99		0.95	1.00		0.95	1.00	1.00
Satd. Flow (prot)		1667			1698		1805	3316		1770	3343	1583
Flt Permitted		0.70			0.88		0.28	1.00		0.32	1.00	1.00
Satd. Flow (perm)		1203			1520		531	3316		598	3343	1583
Peak-hour factor, PHF	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95
Adj. Flow (vph)	95	34	33	63	46	155	27	613	43	179	727	111
RTOR Reduction (vph)	0	7	0	0	40	0	0	7	0	0	0	69
Lane Group Flow (vph)	0	155	0	0	224	0	27	649	0	179	727	42
Heavy Vehicles (%)	2%	2%	30%	2%	1%	2%	0%	8%	5%	2%	8%	2%
Turn Type	Perm	NA		Perm	NA		Perm	NA		Perm	NA	Perm
Protected Phases		2			6			4			8	
Permitted Phases	2			6			4			8		8
Actuated Green, G (s)		46.8			46.8		38.1	38.1		38.1	38.1	38.1
Effective Green, g (s)		46.8			46.8		38.1	38.1		38.1	38.1	38.1
Actuated g/C Ratio		0.47			0.47		0.38	0.38		0.38	0.38	0.38
Clearance Time (s)		8.1			8.1		7.0	7.0		7.0	7.0	7.0
Vehicle Extension (s)		3.0			3.0		5.0	5.0		5.0	5.0	5.0
Lane Grp Cap (vph)		563			711		202	1263		227	1273	603
v/s Ratio Prot								0.20			0.22	
v/s Ratio Perm		0.13			c0.15		0.05			c0.30		0.03
v/c Ratio		0.27			0.32		0.13	0.51		0.79	0.57	0.07
Uniform Delay, d1		16.2			16.6		20.2	23.8		27.4	24.5	19.7
Progression Factor		1.00			1.00		1.00	1.00		1.00	1.00	1.00
Incremental Delay, d2		1.2			1.2		0.6	0.7		18.8	1.0	0.1
Delay (s)		17.4			17.8		20.8	24.5		46.2	25.5	19.8
Level of Service		В			В		С	С		D	С	В
Approach Delay (s)		17.4			17.8			24.4			28.5	
Approach LOS		В			В			С			С	
Intersection Summary												
HCM 2000 Control Delay			25.0	Н	CM 2000	Level of	Service		С			
HCM 2000 Volume to Capacity	y ratio		0.53									
Actuated Cycle Length (s)			100.0	S	um of lost	t time (s)			15.1			
Intersection Capacity Utilizatio	n		78.5%	IC	CU Level o	of Service			D			
Analysis Period (min)			15									
c Critical Lane Group												

Uppers Quarry Traffic Impact Study TMIG

Timings <2035 Total - Thorold Townline> PM Peak Hour 3: Davis Road & Lundys Lane 09-23-202											
	۶	-	4	+	٠	•	t	4	ţ	~	
Lane Group	EBL	EBT	WBL	WBT	WBR	NBL	NBT	SBL	SBT	SBR	
Lane Configurations	ľ	¢Î	ľ	•	1	ľ	eî 🕺	ľ	•	1	
Traffic Volume (vph)	208	719	42	720	216	46	141	239	125	184	
Future Volume (vph)	208	719	42	720	216	46	141	239	125	184	
Turn Type	pm+pt	NA	Perm	NA	Perm	Perm	NA	pm+pt	NA	Perm	
Protected Phases	5	2		6			4	3	8		
Permitted Phases	2		6		6	4		8		8	
Detector Phase	5	2	6	6	6	4	4	3	8	8	
Switch Phase											
Minimum Initial (s)	5.0	22.0	22.0	22.0	22.0	15.0	15.0	5.0	15.0	15.0	
Minimum Split (s)	8.0	36.0	36.0	36.0	36.0	32.0	32.0	8.0	32.0	32.0	
Total Split (s)	14.0	78.0	64.0	64.0	64.0	32.0	32.0	10.0	42.0	42.0	
Total Split (%)	11.7%	65.0%	53.3%	53.3%	53.3%	26.7%	26.7%	8.3%	35.0%	35.0%	
Yellow Time (s)	3.0	5.0	5.0	5.0	5.0	5.0	5.0	3.0	5.0	5.0	
All-Red Time (s)	0.0	2.0	2.0	2.0	2.0	2.0	2.0	0.0	2.0	2.0	
Lost Time Adjust (s)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Total Lost Time (s)	3.0	7.0	7.0	7.0	7.0	7.0	7.0	3.0	7.0	7.0	
Lead/Lag	Lead		Lag	Lag	Lag	Lag	Lag	Lead			
Lead-Lag Optimize?	Yes		Yes	Yes	Yes	Yes	Yes	Yes			
Recall Mode	None	C-Max	Max	Max	Max	Max	Max	None	Max	Max	
Act Effct Green (s)	75.0	71.0	57.0	57.0	57.0	25.0	25.0	39.0	35.0	35.0	
Actuated g/C Ratio	0.62	0.59	0.48	0.48	0.48	0.21	0.21	0.32	0.29	0.29	
v/c Ratio	0.88	0.75	0.23	0.88	0.29	0.19	0.58	0.83	0.26	0.33	
Control Delay	52.6	23.3	23.4	43.3	8.7	41.6	47.3	58.5	34.4	6.0	
Queue Delay	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Total Delay	52.6	23.3	23.4	43.3	8.7	41.6	47.3	58.5	34.4	6.0	
LOS	D	С	С	D	A	D	D	E	С	A	
Approach Delay		29.7		34.8			46.2		35.3		
Approach LOS		С		С			D		D		
Intersection Summary											
Cycle Length: 120											
Actuated Cycle Length: 120											
Offset: 0 (0%). Referenced to	o phase 2	EBTL. St	art of Gre	en							
Natural Cycle 95											
Control Type: Actuated-Coor	rdinated										
Maximum v/c Ratio: 0.88											
Intersection Signal Delay: 34	1.1			Ir	ntersectio	n LOS: C					
Intersection Capacity Utilizat	tion 112.8°	%		10	CU Level	of Service	эH				
Analysis Period (min) 15											
,											

Splits and Phases: 3: Davis Road & Lundys Lane

→ Ø2 (R)		Ø3	1 ₀₄
78 s		10 s	32 s
		\$ Ø8	
14 s	64 s	42 s	

Uppers Quarry Traffic Impact Study TMIG

Synchro 10 Report

HCM Signalized Intersection Capacity Analysis<2035 Total - Thorold Townline> PM Peak Hour 3: Davis Road & Lundys Lane 09-23-2021

	٦	-	$\mathbf{\hat{z}}$	4	←	•	1	Ť	1	1	Ŧ	~
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	٢	ĥ		٦	•	1	٢	ţ,		۲	•	1
Traffic Volume (vph)	208	719	28	42	720	216	46	141	51	239	125	184
Future Volume (vph)	208	719	28	42	720	216	46	141	51	239	125	184
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Total Lost time (s)	3.0	7.0		7.0	7.0	7.0	7.0	7.0		3.0	7.0	7.0
Lane Util. Factor	1.00	1.00		1.00	1.00	1.00	1.00	1.00		1.00	1.00	1.00
Frpb, ped/bikes	1.00	1.00		1.00	1.00	0.98	1.00	0.99		1.00	1.00	1.00
Flpb, ped/bikes	1.00	1.00		1.00	1.00	1.00	1.00	1.00		1.00	1.00	1.00
Frt	1.00	0.99		1.00	1.00	0.85	1.00	0.96		1.00	1.00	0.85
Flt Protected	0.95	1.00		0.95	1.00	1.00	0.95	1.00		0.95	1.00	1.00
Satd. Flow (prot)	1719	1818		1611	1863	1473	1736	1652		1702	1743	1553
Flt Permitted	0.10	1.00		0.24	1.00	1.00	0.67	1.00		0.44	1.00	1.00
Satd. Flow (perm)	185	1818		415	1863	1473	1226	1652		790	1743	1553
Peak-hour factor, PHF	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93
Adj. Flow (vph)	224	773	30	45	774	232	49	152	55	257	134	198
RTOR Reduction (vph)	0	1	0	0	0	99	0	11	0	0	0	140
Lane Group Flow (vph)	224	802	0	45	774	133	49	196	0	257	134	58
Confl. Peds. (#/hr)	2		1	1		2			1	1		
Heavy Vehicles (%)	5%	3%	26%	12%	2%	7%	4%	9%	12%	6%	9%	4%
Turn Type	pm+pt	NA		Perm	NA	Perm	Perm	NA		pm+pt	NA	Perm
Protected Phases	5	2			6			4		3	8	
Permitted Phases	2			6		6	4			8		8
Actuated Green, G (s)	71.0	71.0		57.0	57.0	57.0	25.0	25.0		35.0	35.0	35.0
Effective Green, g (s)	71.0	71.0		57.0	57.0	57.0	25.0	25.0		35.0	35.0	35.0
Actuated g/C Ratio	0.59	0.59		0.48	0.48	0.48	0.21	0.21		0.29	0.29	0.29
Clearance Time (s)	3.0	7.0		7.0	7.0	7.0	7.0	7.0		3.0	7.0	7.0
Vehicle Extension (s)	3.0	4.0		4.0	4.0	4.0	2.0	2.0		3.0	2.0	2.0
Lane Grp Cap (vph)	250	1075		197	884	699	255	344		283	508	452
v/s Ratio Prot	c0.08	0.44			0.42			0.12		c0.05	0.08	
v/s Ratio Perm	c0.45			0.11		0.09	0.04			c0.21		0.04
v/c Ratio	0.90	0.75		0.23	0.88	0.19	0.19	0.57		0.91	0.26	0.13
Uniform Delay, d1	28.1	17.9		18.6	28.3	18.2	39.2	42.7		41.0	32.6	31.3
Progression Factor	1.00	1.00		1.07	1.15	1.80	1.00	1.00		1.00	1.00	1.00
Incremental Delay, d2	30.8	4.7		2.2	9.9	0.5	1.7	6.7		30.4	1.3	0.6
Delay (s)	58.9	22.6		22.0	42.5	33.2	40.8	49.4		71.4	33.9	31.9
Level of Service	E	С		С	D	С	D	D		E	С	С
Approach Delay (s)		30.5			39.6			47.7			49.6	
Approach LOS		С			D			D			D	
Intersection Summary												
HCM 2000 Control Delay			39.1	Н	CM 2000	Level of	Service		D			
HCM 2000 Volume to Cap	acity ratio		0.95									
Actuated Cycle Length (s)			120.0	S	um of los	t time (s)			20.0			
Intersection Capacity Utiliz	ation		112.8%	IC	U Level	of Service			Н			
Analysis Period (min)			15									
0.11 0												

c Critical Lane Group

Uppers Quarry Traffic Impact Study TMIG

Timings <2035 Total - Thorold Townline> PM Peak Hour 4: Thorold Townline Road & Thorold Stone Road 09-23-2021											
	٠	-	$\mathbf{r}$	4	+	•	•	t	1	ŧ	
Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	SBL	SBT	
Lane Configurations	ľ	<u></u>	1	ľ	<b>^</b>	1	ľ	eî Î	ľ	eî	
Traffic Volume (vph)	231	1128	97	111	954	35	203	211	48	211	
Future Volume (vph)	231	1128	97	111	954	35	203	211	48	211	
Turn Type	pm+pt	NA	Perm	pm+pt	NA	Perm	pm+pt	NA	pm+pt	NA	
Protected Phases	5	2		1	6		7	4	3	8	
Permitted Phases	2		2	6		6	4		8		
etector Phase	5	2	2	1	6	6	7	4	3	8	
Switch Phase											
linimum Initial (s)	8.0	10.0	10.0	5.0	10.0	10.0	5.0	10.0	5.0	10.0	
linimum Split (s)	11.0	35.1	35.1	8.0	35.1	35.1	8.0	41.4	8.0	41.4	
otal Split (s)	19.0	50.0	50.0	10.0	41.0	41.0	17.0	51.0	9.0	43.0	
otal Split (%)	15.8%	41.7%	41.7%	8.3%	34.2%	34.2%	14.2%	42.5%	7.5%	35.8%	
'ellow Time (s)	3.0	4.1	4.1	3.0	4.1	4.1	3.0	4.1	3.0	4.1	
II-Red Time (s)	0.0	2.0	2.0	0.0	2.0	2.0	0.0	2.3	0.0	2.3	
ost Time Adjust (s)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
otal Lost Time (s)	3.0	6.1	6.1	3.0	6.1	6.1	3.0	6.4	3.0	6.4	
ead/Lag	Lead	Lag	Lag	Lead	Lag	Lag	Lead	Lag	Lead	Lag	
ead-Lag Optimize?	Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes	
Recall Mode	None	C-Max	C-Max	None	C-Max	C-Max	None	None	None	None	
ct Effct Green (s)	58.2	44.9	44.9	47.4	37.1	37.1	55.8	45.2	44.9	35.6	
ctuated g/C Ratio	0.48	0.37	0.37	0.40	0.31	0.31	0.46	0.38	0.37	0.30	
/c Ratio	0.89	0.88	0.17	0.76	0.91	0.06	0.81	0.72	0.16	0.96	
Control Delay	67.6	66.7	24.5	53.9	53.3	0.2	47.5	36.8	19.0	68.5	
lueue Delay	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
otal Delay	67.6	66.7	24.5	53.9	53.3	0.2	47.5	36.8	19.0	68.5	
OS	E	E	С	D	D	A	D	D	В	E	
pproach Delay		64.0			51.7			40.3		64.0	
pproach LOS		E			D			D		E	
ntersection Summary											
Cycle Length: 120											
ctuated Cycle Length: 120											
Iffset: 0 (0%) Referenced to	n nhase 2 [.]	FRTL an	16·WRTI	Start of	Green						
atural Cycle: 100	o pridoo 2.			., etaitei	0.001						
Control Type: Actuated-Coordinated											
laximum v/c Ratio: 0.96											
tersection Signal Delay: 56	6.4			Ir	ntersectio	n LOS: E					
tersection Capacity Utilizat	ion 95.3%				CU Level	of Service	e F				
nalysis Period (min) 15							·				
nlite and Dhasaasi 4: The		line Deed	9 Thereb		) and						

Splits and Phases: 4: Thorold Townline Road & Thorold Stone Road

🖌 Ø1 🚽	• Ø2 ( <b>R</b> )	Ø3 Ø4	
10 s 50 s	S	9 s 51 s	
	● 🔷 Ø6 (R)	▲ Ø7	
19 s	41 s	17 s 43 s	

Uppers Quarry Traffic Impact Study TMIG Synchro 10 Report

 HCM Signalized Intersection Capacity Analysis<2035 Total - Thorold Townline> PM Peak Hour

 4: Thorold Townline Road & Thorold Stone Road
 09-23-2021

	≯	-	$\mathbf{r}$	4	←	•	1	Ť	1	1	Ŧ	~
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	ľ		1	ľ	<u></u>	1	ľ	4Î		ľ	et	
Traffic Volume (vph)	231	1128	97	111	954	35	203	211	201	48	211	272
Future Volume (vph)	231	1128	97	111	954	35	203	211	201	48	211	272
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Total Lost time (s)	3.0	6.1	6.1	3.0	6.1	6.1	3.0	6.4		3.0	6.4	
Lane Util. Factor	1.00	0.95	1.00	1.00	0.95	1.00	1.00	1.00		1.00	1.00	
Frt	1.00	1.00	0.85	1.00	1.00	0.85	1.00	0.93		1.00	0.92	
Flt Protected	0.95	1.00	1.00	0.95	1.00	1.00	0.95	1.00		0.95	1.00	
Satd. Flow (prot)	1671	3574	1357	1543	3539	1538	1626	1506		1671	1630	
Flt Permitted	0.10	1.00	1.00	0.11	1.00	1.00	0.12	1.00		0.40	1.00	
Satd. Flow (perm)	178	3574	1357	178	3539	1538	211	1506		702	1630	
Peak-hour factor, PHF	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96
Adj. Flow (vph)	241	1175	101	116	994	36	211	220	209	50	220	283
RTOR Reduction (vph)	0	0	64	0	0	25	0	28	0	0	39	0
Lane Group Flow (vph)	241	1175	37	116	994	11	211	401	0	50	464	0
Heavy Vehicles (%)	8%	1%	19%	17%	2%	5%	11%	15%	19%	8%	9%	5%
Turn Type	pm+pt	NA	Perm	pm+pt	NA	Perm	pm+pt	NA		pm+pt	NA	
Protected Phases	5	2		1	6		7	4		3	8	
Permitted Phases	2		2	6		6	4			8		
Actuated Green, G (s)	54.5	44.3	44.3	43.7	36.5	36.5	53.0	45.2		41.0	36.2	
Effective Green, g (s)	54.5	44.3	44.3	43.7	36.5	36.5	53.0	45.2		41.0	36.2	
Actuated g/C Ratio	0.45	0.37	0.37	0.36	0.30	0.30	0.44	0.38		0.34	0.30	
Clearance Time (s)	3.0	6.1	6.1	3.0	6.1	6.1	3.0	6.4		3.0	6.4	
Vehicle Extension (s)	2.5	6.0	6.0	3.0	6.0	6.0	3.0	2.3		3.0	2.3	
Lane Grp Cap (vph)	267	1319	500	146	1076	467	255	567		278	491	
v/s Ratio Prot	c0.11	0.33		0.05	0.28		c0.09	0.27		0.01	c0.28	
v/s Ratio Perm	c0.30		0.03	0.24		0.01	0.27			0.05		
v/c Ratio	0.90	0.89	0.07	0.79	0.92	0.02	0.83	0.71		0.18	0.94	
Uniform Delay, d1	33.0	35.6	24.6	29.6	40.4	29.3	26.2	31.8		27.1	40.9	
Progression Factor	1.70	1.75	6.38	1.00	1.00	1.00	1.00	1.00		1.00	1.00	
Incremental Delay, d2	19.7	5.5	0.2	25.0	14.3	0.1	19.3	3.6		0.3	27.0	
Delay (s)	76.0	67.7	156.8	54.6	54.7	29.4	45.5	35.3		27.4	67.9	
Level of Service	E	E	F	D	D	С	D	D		С	E	
Approach Delay (s)		75.0			53.9			38.7			64.3	
Approach LOS		E			D			D			E	
Intersection Summary					<b>.</b>							
HCM 2000 Control Delay 61.2				H	CM 2000	Level of	Service		E			_
HCM 2000 Volume to Capacity ratio 0.9												
Actuated Cycle Length (s) 120.0				S	um of los	t time (s)			18.5			
Intersection Capacity Utilization 95.3%					U Level	of Service	e		F			
Analysis Period (min)			15									
c Critical Lane Group												

Uppers Quarry Traffic Impact Study TMIG

Timings 5: Thorold Townline	ne	<2035 Total - Thorold Townline> PM Peak Hour 09-23-2021									
	۶	-	•	4	+	•	Ť	1	ţ	~	
Lane Group	EBL	EBT	EBR	WBL	WBT	NBL	NBT	SBL	SBT	SBR	
Lane Configurations	ľ	•	1	ľ	ĥ	ľ	ĥ	ľ	•	1	
Traffic Volume (vph)	116	673	117	44	711	117	142	96	118	185	
Future Volume (vph)	116	673	117	44	711	117	142	96	118	185	
Turn Type	Perm	NA	Perm	Perm	NA	Perm	NA	Perm	NA	Perm	
Protected Phases		2			6		4		8		
Permitted Phases	2		2	6		4		8		8	
Detector Phase	2	2	2	6	6	4	4	8	8	8	
Switch Phase											
Minimum Initial (s)	20.0	20.0	20.0	20.0	20.0	10.0	10.0	10.0	10.0	10.0	
Minimum Split (s)	29.0	29.0	29.0	29.0	29.0	35.0	35.0	35.0	35.0	35.0	
Total Split (s)	85.0	85.0	85.0	85.0	85.0	35.0	35.0	35.0	35.0	35.0	
Total Split (%)	70.8%	70.8%	70.8%	70.8%	70.8%	29.2%	29.2%	29.2%	29.2%	29.2%	
Yellow Time (s)	5.0	5.0	5.0	5.0	5.0	4.0	4.0	4.0	4.0	4.0	
All-Red Time (s)	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	
Lost Time Adjust (s)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Total Lost Time (s)	7.0	7.0	7.0	7.0	7.0	6.0	6.0	6.0	6.0	6.0	
Lead/Lag											
Lead-Lag Optimize?											
Recall Mode	C-Max	C-Max	C-Max	C-Max	C-Max	None	None	None	None	None	
Act Effct Green (s)	85.6	85.6	85.6	85.6	85.6	21.4	21.4	21.4	21.4	21.4	
Actuated g/C Ratio	0.71	0.71	0.71	0.71	0.71	0.18	0.18	0.18	0.18	0.18	
v/c Ratio	0.42	0.57	0.11	0.12	0.66	0.66	0.65	0.77	0.41	0.46	
Control Delay	14.2	13.6	4.5	7.7	13.3	60.7	51.5	80.1	46.2	8.7	
Queue Delay	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Total Delay	14.2	13.6	4.5	7.7	13.3	60.7	51.5	80.1	46.2	8.7	
LOS	В	В	A	A	В	E	D	F	D	A	
Approach Delay		12.5			13.0		55.0		37.0		
Approach LOS		В			В		E		D		
Intersection Summary											
Cycle Length: 120											
Actuated Cycle Length: 120											
Offset: 0 (0%). Referenced to	phase 2	EBTL and	d 6:WBTL	. Start of	Green						
Antural Cycle: 90											
Control Type: Actuated-Coor	dinated										
Maximum v/c Ratio: 0.77											
Intersection Signal Delay: 22	.1			Ir	ntersectio	n LOS: C					
Intersection Capacity Utilizati	on 98.5%			10	CU Level	of Service	ə F				
Analysis Period (min) 15											
Calite and Dhasasy E: There											

Splits and Phases: 5: Thorold Townline Road & Lundys Lane

≠ Ø2 (R)	1 Ø4	
85 s	35 s	
₩ Ø6 (R)	<b>↓</b> Ø8	
85 s	35 s	

Uppers Quarry Traffic Impact Study TMIG

Synchro 10 Report

HCM Signalized Intersection Capacity Analysis<2035 Total - Thorold Townline> PM Peak Hour 5: Thorold Townline Road & Lundys Lane 09-23-2021

	٦	-	$\mathbf{r}$	4	+	•	٠	Ť	1	1	Ŧ	~
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	ň	•	1	5	ĥ		ň	î,		۲	•	1
Traffic Volume (vph)	116	673	117	44	711	64	117	142	50	96	118	185
Future Volume (vph)	116	673	117	44	711	64	117	142	50	96	118	185
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Total Lost time (s)	7.0	7.0	7.0	7.0	7.0		6.0	6.0		6.0	6.0	6.0
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00		1.00	1.00		1.00	1.00	1.00
Frpb, ped/bikes	1.00	1.00	1.00	1.00	1.00		1.00	1.00		1.00	1.00	1.00
Flpb, ped/bikes	1.00	1.00	1.00	1.00	1.00		1.00	1.00		1.00	1.00	1.00
Frt	1.00	1.00	0.85	1.00	0.99		1.00	0.96		1.00	1.00	0.85
Flt Protected	0.95	1.00	1.00	0.95	1.00		0.95	1.00		0.95	1.00	1.00
Satd. Flow (prot)	1626	1827	1553	1752	1817		1687	1748		1736	1776	1524
Flt Permitted	0.25	1.00	1.00	0.31	1.00		0.62	1.00		0.42	1.00	1.00
Satd. Flow (perm)	428	1827	1553	568	1817		1103	1748		764	1776	1524
Peak-hour factor, PHF	0.91	0.91	0.91	0.91	0.91	0.91	0.91	0.91	0.91	0.91	0.91	0.91
Adi, Flow (vph)	127	740	129	48	781	70	129	156	55	105	130	203
RTOR Reduction (vph)	0	0	15	0	2	0	0	12	0	0	0	167
Lane Group Flow (vph)	127	740	114	48	849	0	129	199	0	105	130	36
Confl. Peds. (#/hr)	1					1						
Heavy Vehicles (%)	11%	4%	4%	3%	2%	15%	7%	6%	0%	4%	7%	6%
Turn Type	Perm	NA	Perm	Perm	NA		Perm	NA		Perm	NA	Perm
Protected Phases		2			6			4			8	
Permitted Phases	2		2	6			4			8		8
Actuated Green, G (s)	85.6	85.6	85.6	85.6	85.6		21.4	21.4		21.4	21.4	21.4
Effective Green, g (s)	85.6	85.6	85.6	85.6	85.6		21.4	21.4		21.4	21.4	21.4
Actuated g/C Ratio	0.71	0.71	0.71	0.71	0.71		0.18	0.18		0.18	0.18	0.18
Clearance Time (s)	7.0	7.0	7.0	7.0	7.0		6.0	6.0		6.0	6.0	6.0
Vehicle Extension (s)	5.0	5.0	5.0	5.0	5.0		5.0	5.0		5.0	5.0	5.0
Lane Grp Cap (vph)	305	1303	1107	405	1296		196	311		136	316	271
v/s Ratio Prot		0.41			c0.47			0.11			0.07	
v/s Ratio Perm	0.30		0.07	0.08			0.12			c0.14		0.02
v/c Ratio	0.42	0.57	0.10	0.12	0.65		0.66	0.64		0.77	0.41	0.13
Uniform Delay, d1	7.0	8.3	5.3	5.4	9.3		45.9	45.7		47.0	43.7	41.5
Progression Factor	1.23	1.30	1.08	1.00	1.00		1.00	1.00		1.00	1.00	1.00
Incremental Delay, d2	2.6	1.1	0.1	0.6	2.6		10.3	6.1		26.7	1.8	0.5
Delay (s)	11.2	11.9	5.9	6.0	11.8		56.2	51.8		73.7	45.5	42.0
Level of Service	В	В	А	А	В		E	D		E	D	D
Approach Delay (s)		11.0			11.5			53.5			50.6	
Approach LOS		В			В			D			D	
Intersection Summary												
HCM 2000 Control Delay			23.1	Н	CM 2000	Level of S	Service		С			
HCM 2000 Volume to Capa	acity ratio		0.68									
Actuated Cycle Length (s)	· _		120.0	S	um of los	t time (s)			13.0			
Intersection Capacity Utilization	ation		98.5%	IC	U Level	of Service			F			
Analysis Period (min)			15									

c Critical Lane Group

Uppers Quarry Traffic Impact Study TMIG

Timings 6 [.] Thorold Townline	e Road	& Bea	verdar	ns Ro	<2035 Total - Thorold Townline> PM Peak Hour 09-23-2021						
	•	-	<pre>voidal</pre>	<b>+</b>	1	t	4	ţ			
Lane Group	EBL	EBT	WBL	WBT	NBL	NBT	SBL	SBT			
Lane Configurations		\$		\$		\$		\$			
Traffic Volume (vph)	27	205	124	178	32	584	20	363			
Future Volume (vph)	27	205	124	178	32	584	20	363			
Turn Type	Perm	NA	Perm	NA	Perm	NA	Perm	NA			
Protected Phases		2		6		4		8			
Permitted Phases	2		6		4		8				
Detector Phase	2	2	6	6	4	4	8	8			
Switch Phase											
Minimum Initial (s)	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0			
Minimum Split (s)	32.0	32.0	32.0	32.0	35.0	35.0	35.0	35.0			
Total Split (s)	34.0	34.0	34.0	34.0	56.0	56.0	56.0	56.0			
Total Split (%)	37.8%	37.8%	37.8%	37.8%	62.2%	62.2%	62.2%	62.2%			
Yellow Time (s)	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0			
All-Red Time (s)	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0			
Lost Time Adjust (s)		0.0		0.0		0.0		0.0			
Total Lost Time (s)		6.0		6.0		6.0		6.0			
Lead/Lag											
Lead-Lag Optimize?											
Recall Mode	C-Max	C-Max	Max	Max	None	None	None	None			
Act Effct Green (s)		30.2		30.2		47.8		47.8			
Actuated g/C Ratio		0.34		0.34		0.53		0.53			
v/c Ratio		0.46		0.79		0.90		0.55			
Control Delay		27.1		43.4		33.9		16.2			
Queue Delay		0.0		0.0		0.0		0.0			
Total Delay		27.1		43.4		33.9		16.2			
LOS		С		D		С		В			
Approach Delay		27.1		43.4		33.9		16.2			
Approach LOS		С		D		С		В			
Intersection Summary											
Cycle Length: 90											
Actuated Cycle Length: 90											
Offset: 0 (0%), Referenced t	to phase 2	EBTL. St	art of Gre	en							
Natural Cycle: 80											
Control Type: Actuated-Coo	rdinated										
Maximum v/c Ratio: 0.90											
Intersection Signal Delay: 30	0.3			Ir	ntersectio	n LOS: C					
Intersection Capacity Utilizat	tion 99.4%			10	CU Level	of Service	ə F				
Analysis Period (min) 15											
Cality and Dharasay C. The		line Deed	0 D								

opilio una i nuoco. o. moroia romini		
Ø2 (R)	<b>™</b> ¶ø4	
34 s	56 s	
<b>₩</b> Ø6	₩Ø8	
34 s	56 s	

Synchro 10 Report

 HCM Signalized Intersection Capacity Analysis<2035 Total - Thorold Townline> PM Peak Hour

 6: Thorold Townline Road & Beaverdams Road
 09-23-2021

	≯	-	$\mathbf{\hat{v}}$	4	+	•	•	Ť	۲	1	Ŧ	~
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		44			4			\$			\$	
Traffic Volume (vph)	27	205	16	124	178	21	32	584	94	20	363	41
Future Volume (vph)	27	205	16	124	178	21	32	584	94	20	363	41
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Total Lost time (s)		6.0			6.0			6.0			6.0	
Lane Util. Factor		1.00			1.00			1.00			1.00	
Frpb, ped/bikes		1.00			1.00			1.00			1.00	
Flpb, ped/bikes		1.00			1.00			1.00			1.00	
Frt		0.99			0.99			0.98			0.99	
Flt Protected		0.99			0.98			1.00			1.00	
Satd. Flow (prot)		1830			1803			1636			1630	
Flt Permitted		0.94			0.71			0.97			0.95	
Satd. Flow (perm)		1727			1296			1585			1553	
Peak-hour factor, PHF	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93
Adi, Flow (vph)	29	220	17	133	191	23	34	628	101	22	390	44
RTOR Reduction (vph)	0	3	0	0	3	0	0	7	0	0	5	0
Lane Group Flow (vph)	0	263	0	0	344	0	0	756	0	0	451	0
Confl. Peds. (#/hr)	1		5	5		1	8		3	3		8
Heavy Vehicles (%)	10%	1%	4%	4%	1%	0%	4%	16%	0%	2%	16%	6%
Turn Type	Perm	NA		Perm	NA		Perm	NA		Perm	NA	
Protected Phases		2			6			4			8	
Permitted Phases	2			6			4			8		
Actuated Green, G (s)		30.2			30.2			47.8			47.8	
Effective Green, g (s)		30.2			30.2			47.8			47.8	
Actuated g/C Ratio		0.34			0.34			0.53			0.53	
Clearance Time (s)		6.0			6.0			6.0			6.0	
Vehicle Extension (s)		5.0			5.0			5.0			5.0	
Lane Grp Cap (vph)		579			434			841			824	
v/s Ratio Prot												
v/s Ratio Perm		0.15			c0.27			c0.48			0.29	
v/c Ratio		0.45			0.79			0.90			0.55	
Uniform Delay, d1		23.4			27.1			18.9			14.0	
Progression Factor		1.00			1.00			1.00			1.00	
Incremental Delay, d2		2.6			13.9			13.2			1.3	
Delay (s)		26.0			40.9			32.1			15.3	
Level of Service		С			D			С			В	
Approach Delay (s)		26.0			40.9			32.1			15.3	
Approach LOS		С			D			С			В	
Intersection Summary												
HCM 2000 Control Delay			28.7	Н	CM 2000	Level of	Service		С			
HCM 2000 Volume to Capac	city ratio		0.86									
Actuated Cycle Length (s)			90.0	S	um of lost	time (s)			12.0			
Intersection Capacity Utilization	tion		99.4%	IC	U Level o	of Service			F			
Analysis Period (min)			15									
0.11 0												

c Critical Lane Group

Uppers Quarry Traffic Impact Study TMIG

HCM Unsignalized 7: Thorold Townlin	Interse e Road	ction C & Upp	apacit ers Lai	y Anal <u>y</u> ne	ys1203	5 Total ·	- Thorold Townline> PM Peak Hour 09-23-2021
-	4	•	t	1	1	ţ	
Movement	WBL	WBR	NBT	NBR	SBL	SBT	
Lane Configurations	Y		4Î		۲	•	
Traffic Volume (veh/h)	3	46	513	3	46	468	
Future Volume (Veh/h)	3	46	513	3	46	468	
Sign Control	Stop		Free			Free	
Grade	0%		0%			0%	
Peak Hour Factor	0.91	0.91	0.91	0.91	0.91	0.91	
Hourly flow rate (vph)	3	51	564	3	51	514	
Pedestrians							
Lane Width (m)							
Walking Speed (m/s)							
Percent Blockage							
Right turn flare (veh)							
Median type			None			None	
Median storage veh)							
Upstream signal (m)							
pX, platoon unblocked							
vC, conflicting volume	1182	566			567		
vC1, stage 1 conf vol							
vC2, stage 2 conf vol							
vCu, unblocked vol	1182	566			567		
tC, single (s)	6.4	7.0			4.9		
tC, 2 stage (s)							
tF (s)	3.5	4.0			2.9		
p0 queue free %	98	87			93		
cM capacity (veh/h)	196	398			702		
Direction, Lane #	WB 1	NB 1	SB 1	SB 2			
Volume Total	54	567	51	514			
Volume Left	3	0	51	0			
Volume Right	51	3	0	0			
cSH	377	1700	702	1700			
Volume to Capacity	0.14	0.33	0.07	0.30			
Queue Length 95th (m)	4.0	0.0	1.9	0.0			
Control Delay (s)	16.1	0.0	10.5	0.0			
Lane LOS	С		В				
Approach Delay (s)	16.1	0.0	1.0				
Approach LOS	С						
Intersection Summary							
Average Delay			1.2				
Intersection Capacity Utiliza	ation		43.8%	IC	U Level o	of Service	A
Analysis Period (min)			15				



# **APPENDIX D**

**Queueing Analysis** 

## Queuing and Blocking Report

#### <2018 Existing> AM Peak Hour 09-14-2021

Intersection: 1: Davis Road & Thorold Stone Road

Movement	EB	EB	EB	WB	WB	WB	NB	NB	NB	SB	
Directions Served	L	Т	Т	L	Т	TR	L	LT	R	Т	
Maximum Queue (m)	20.2	77.9	71.5	39.1	101.0	105.9	57.3	65.4	9.1	6.2	
Average Queue (m)	3.5	35.6	19.8	13.7	35.5	39.9	34.2	37.1	0.3	0.4	
95th Queue (m)	12.0	62.1	49.6	29.6	73.1	81.6	54.6	58.1	6.4	3.3	
Link Distance (m)		367.0	367.0		315.3	315.3	1000.6	1000.6		265.6	
Upstream Blk Time (%)											
Queuing Penalty (veh)											
Storage Bay Dist (m)	105.0			70.0					80.0		
Storage Blk Time (%)			0		1			0			
Queuing Penalty (veh)			0		1			0			

Intersection: 2: Davis Road & Niagara Falls Road/Beaverdams Road

Movement	EB	WB	NB	NB	NB	SB	SB	SB
Directions Served	LTR	LTR	L	Т	TR	L	Т	Т
Maximum Queue (m)	34.2	35.7	8.5	46.7	61.4	32.3	55.3	41.7
Average Queue (m)	13.1	12.0	0.8	21.4	25.1	13.5	23.0	7.3
95th Queue (m)	27.2	24.8	4.6	40.3	47.3	26.5	43.1	25.7
Link Distance (m)	244.6	305.1		296.6	296.6		1000.6	1000.6
Upstream Blk Time (%)								
Queuing Penalty (veh)								
Storage Bay Dist (m)			80.0			140.0		
Storage Blk Time (%)								
Queuing Penalty (veh)								

## Intersection: 3: Davis Road & Lundys Lane

Movement	EB	EB	WB	WB	WB	NB	NB	SB	SB	SB	
Directions Served	L	TR	L	Т	R	L	TR	L	Т	R	
Maximum Queue (m)	31.8	46.1	22.2	58.4	15.5	26.7	69.2	41.0	57.0	31.6	
Average Queue (m)	12.8	20.6	6.0	19.5	3.1	6.1	32.2	15.8	19.0	8.3	
95th Queue (m)	26.6	39.4	17.4	44.6	10.6	18.5	57.7	32.9	42.6	21.4	
Link Distance (m)		266.3		1923.8			458.7		610.8		
Upstream Blk Time (%)											
Queuing Penalty (veh)											
Storage Bay Dist (m)	85.0		65.0		80.0	55.0		90.0		100.0	
Storage Blk Time (%)				0			2		0		
Queuing Penalty (veh)				0			0		0		

Uppers Quarry Traffic Impact Study TMIG SimTraffic Report Page 1

## Queuing and Blocking Report

# <2018 Existing> AM Peak Hour 09-14-2021

#### Intersection: 4: Thorold Townline Road & Thorold Stone Road

Movement	EB	EB	EB	EB	WB	WB	WB	WB	NB	NB	SB	SB
Directions Served	L	Т	Т	R	L	Т	Т	R	L	TR	L	TR
Maximum Queue (m)	97.9	57.2	58.9	19.9	19.2	91.7	81.7	20.9	40.5	74.9	32.7	97.7
Average Queue (m)	49.6	18.2	23.2	2.8	4.6	55.6	45.3	7.5	14.7	26.4	10.8	47.3
95th Queue (m)	81.8	42.4	47.2	11.7	14.7	82.7	74.6	17.7	33.7	52.7	26.1	86.5
Link Distance (m)		279.0	279.0			338.6	338.6			1028.0		311.8
Upstream Blk Time (%)												
Queuing Penalty (veh)												
Storage Bay Dist (m)	100.0			50.0	85.0			90.0	80.0		75.0	
Storage Blk Time (%)	0		1			0	0			0		3
Queuing Penalty (veh)	1		0			0	0			0		2

Intersection: 5: Thorold Townline Road & Lundys Lane

Movement	EB	EB	EB	WB	WB	NB	NB	SB	SB
Directions Served	L	Т	R	L	TR	L	TR	L	TR
Maximum Queue (m)	24.3	66.5	24.8	14.1	51.9	35.5	70.2	16.1	52.3
Average Queue (m)	8.0	25.0	6.6	4.2	19.8	13.5	30.3	3.3	21.4
95th Queue (m)	18.9	51.7	17.9	12.1	42.1	29.9	58.6	11.7	43.3
Link Distance (m)		1923.8			479.5		741.7		1500.1
Upstream Blk Time (%)									
Queuing Penalty (veh)									
Storage Bay Dist (m)	90.0		20.0	55.0		25.0		25.0	
Storage Blk Time (%)		9	0		0	4	17	0	9
Queuing Penalty (veh)		13	2		0	7	11	0	1

#### Intersection: 6: Thorold Townline Road & Beaverdams Road

Movement	EB	WB	NB	SB
Directions Served	LTR	LTR	LTR	LTR
Maximum Queue (m)	25.4	17.6	45.1	29.7
Average Queue (m)	12.2	9.8	20.8	14.7
95th Queue (m)	20.6	16.3	35.5	24.9
Link Distance (m)	192.4	256.5	1091.4	1028.0
Upstream Blk Time (%)				
Queuing Penalty (veh)				
Storage Bay Dist (m)				
Storage Blk Time (%)				
Queuing Penalty (veh)				

Uppers Quarry Traffic Impact Study TMIG SimTraffic Report Page 2

# Queuing and Blocking Report

<2018 Existing> AM Peak Hour 09-14-2021

Intersection: 7: Thorold Townline Road & Uppers Lane

Movement	WB
Directions Served	LR
Maximum Queue (m)	1.4
Average Queue (m)	0.1
95th Queue (m)	1.6
Link Distance (m)	1027.2
Upstream Blk Time (%)	
Queuing Penalty (veh)	
Storage Bay Dist (m)	
Storage Blk Time (%)	
Queuing Penalty (veh)	
addating i briancy (rom)	

Network Summary

Network wide Queuing Penalty: 39

Uppers Quarry Traffic Impact Study TMIG SimTraffic Report Page 3

## Queuing and Blocking Report

#### <2018 Existing> PM Peak Hour 09-14-2021

Intersection: 1: Davis Road & Thorold Stone Road

Movement	EB	EB	EB	EB	WB	WB	WB	NB	NB	SB	SB	
Directions Served	L	Т	Т	R	L	Т	TR	L	LT	L	Т	
Maximum Queue (m)	26.4	111.1	100.0	36.5	54.0	89.4	94.7	59.4	65.0	8.1	9.3	
Average Queue (m)	5.0	55.4	42.3	1.2	21.1	39.7	42.5	34.6	37.6	0.8	1.8	
95th Queue (m)	16.4	93.4	82.9	18.3	45.6	75.5	80.1	54.1	59.3	4.4	7.1	
Link Distance (m)		367.0	367.0			315.3	315.3	1000.6	1000.6		265.6	
Upstream Blk Time (%)												
Queuing Penalty (veh)												
Storage Bay Dist (m)	105.0			50.0	70.0					30.0		
Storage Blk Time (%)		0	4		0	2						
Queuing Penalty (veh)		0	18		1	1						

Intersection: 2: Davis Road & Niagara Falls Road/Beaverdams Road

Movement	EB	WB	NB	NB	NB	SB	SB	SB
Directions Served	LTR	LTR	L	Т	TR	L	Т	Т
Maximum Queue (m)	28.3	50.6	8.6	41.1	53.2	58.1	51.4	34.1
Average Queue (m)	13.0	17.5	0.9	19.2	24.3	28.2	26.5	12.0
95th Queue (m)	25.0	35.4	4.9	35.4	44.0	47.0	45.6	30.2
Link Distance (m)	244.6	305.1		296.6	296.6		1000.6	1000.6
Upstream Blk Time (%)								
Queuing Penalty (veh)								
Storage Bay Dist (m)			80.0			140.0		
Storage Blk Time (%)								
Queuing Penalty (veh)								

## Intersection: 3: Davis Road & Lundys Lane

Movement	EB	EB	WB	WB	WB	NB	NB	SB	SB	SB	
Directions Served	L	TR	L	Т	R	L	TR	L	Т	R	
Maximum Queue (m)	41.0	88.8	21.4	92.8	20.0	26.1	43.8	28.7	45.0	31.2	
Average Queue (m)	17.6	43.0	6.1	44.1	5.8	7.9	18.7	10.8	12.6	6.8	
95th Queue (m)	33.9	73.7	16.8	77.5	14.1	19.8	36.4	23.3	30.8	19.0	
Link Distance (m)		266.3		1923.8			458.7		610.8		
Upstream Blk Time (%)											
Queuing Penalty (veh)											
Storage Bay Dist (m)	85.0		65.0		80.0	55.0		90.0		100.0	
Storage Blk Time (%)		0		2			0				
Queuing Penalty (veh)		0		2			0				

Queuing and Blocking Report

# <2018 Existing> PM Peak Hour 09-14-2021

## Intersection: 4: Thorold Townline Road & Thorold Stone Road

Movement	EB	EB	EB	EB	B24	WB	WB	WB	WB	NB	NB	SB
Directions Served	L	Т	Т	R	Т	L	Т	Т	R	L	TR	L
Maximum Queue (m)	87.1	83.3	90.0	9.2	66.2	19.4	88.4	78.1	14.4	30.0	51.3	35.6
Average Queue (m)	37.1	37.3	42.7	2.4	2.2	5.9	53.4	40.2	3.4	12.6	18.4	9.8
95th Queue (m)	67.1	75.6	83.1	8.3	46.6	15.4	80.9	70.1	10.7	27.0	41.3	24.6
Link Distance (m)		279.0	279.0		315.3		338.6	338.6			1028.0	
Upstream Blk Time (%)					0							
Queuing Penalty (veh)					1							
Storage Bay Dist (m)	100.0			50.0		85.0			90.0	80.0		75.0
Storage Blk Time (%)	0	0	5				0	0				
Queuing Penalty (veh)	1	0	2				0	0				

Intersection: 4: Thorold Townline Road & Thorold Stone Road

Movement	SB
Directions Served	TR
Maximum Queue (m)	142.5
Average Queue (m)	68.0
95th Queue (m)	121.3
Link Distance (m)	311.8
Upstream Blk Time (%)	
Queuing Penalty (veh)	
Storage Bay Dist (m)	
Storage Blk Time (%)	9
Queuing Penalty (veh)	4

## Intersection: 5: Thorold Townline Road & Lundys Lane

Movement	EB	EB	EB	WB	WB	NB	NB	SB	SB
Directions Served	L	Т	R	L	TR	L	TR	L	TR
Maximum Queue (m)	27.3	79.7	40.6	21.2	63.8	57.0	67.2	17.2	54.9
Average Queue (m)	7.3	31.3	7.2	6.2	26.6	19.6	28.0	4.9	22.1
95th Queue (m)	19.8	65.8	22.9	15.7	49.5	42.3	52.5	13.7	44.6
Link Distance (m)		1923.8			479.5		741.7		1500.1
Upstream Blk Time (%)									
Queuing Penalty (veh)									
Storage Bay Dist (m)	90.0		20.0	55.0		25.0		25.0	
Storage Blk Time (%)		12	0		0	8	14	0	10
Queuing Penalty (veh)		16	1		0	15	14	0	2

Uppers Quarry Traffic Impact Study TMIG

SimTraffic Report Page 1 Uppers Quarry Traffic Impact Study TMIG SimTraffic Report Page 2
<2018 Existing> PM Peak Hour 09-14-2021

Intersection: 6: Thorold Townline Road & Beaverdams Road

Movement	EB	WB	NB	SB
Directions Served	LTR	LTR	LTR	LTR
Maximum Queue (m)	51.1	23.6	41.4	31.0
Average Queue (m)	19.6	10.5	18.5	15.4
95th Queue (m)	35.2	18.8	32.2	25.9
Link Distance (m)	192.4	256.5	1091.4	1028.0
Upstream Blk Time (%)				
Queuing Penalty (veh)				
Storage Bay Dist (m)				
Storage Blk Time (%)				
Queuing Penalty (veh)				

Intersection: 7: Thorold Townline Road & Uppers Lane

Movement	WB
Directions Served	LR
Maximum Queue (m)	3.9
Average Queue (m)	0.2
95th Queue (m)	1.8
Link Distance (m)	1027.2
Upstream Blk Time (%)	
Queuing Penalty (veh)	
Storage Bay Dist (m)	
Storage Blk Time (%)	
Queuing Penalty (veh)	

Network Summary

Network wide Queuing Penalty: 78

Uppers Quarry Traffic Impact Study TMIG

#### <2025 Background> AM Peak Hour 09-14-2021

Intersection: 1: Davis Road & Thorold Stone Road

Movement	EB	EB	EB	WB	WB	WB	NB	NB	NB	SB	SB	
Directions Served	L	Т	Т	L	Т	TR	L	LT	R	L	Т	
Maximum Queue (m)	13.7	93.5	128.0	37.0	108.8	115.9	96.5	100.8	42.6	3.4	7.4	
Average Queue (m)	2.8	52.7	42.4	15.8	62.4	64.1	53.9	58.9	1.7	0.2	0.8	
95th Queue (m)	9.7	84.7	92.0	29.8	101.3	104.0	85.2	90.5	17.1	1.6	4.6	
Link Distance (m)		367.0	367.0		315.3	315.3	1000.6	1000.6			265.6	
Upstream Blk Time (%)												
Queuing Penalty (veh)												
Storage Bay Dist (m)	105.0			70.0					80.0	30.0		
Storage Blk Time (%)		0	3		6			2				
Queuing Penalty (veh)		0	7		5			4				

Intersection: 2: Davis Road & Niagara Falls Road/Beaverdams Road

Movement	EB	WB	NB	NB	NB	SB	SB	SB
Directions Served	LTR	LTR	L	Т	TR	L	Т	Т
Maximum Queue (m)	45.6	38.0	21.7	69.8	79.9	31.4	61.0	43.7
Average Queue (m)	17.6	14.2	3.4	35.8	42.6	15.8	30.0	13.8
95th Queue (m)	35.4	28.0	13.5	58.6	69.2	28.3	52.0	36.1
Link Distance (m)	244.6	305.1		296.6	296.6		1000.6	1000.6
Upstream Blk Time (%)								
Queuing Penalty (veh)								
Storage Bay Dist (m)			80.0			140.0		
Storage Blk Time (%)				0				
Queuing Penalty (veh)				0				

## Intersection: 3: Davis Road & Lundys Lane

Movement	EB	EB	WB	WB	WB	NB	NB	SB	SB	SB	
Directions Served	L	TR	L	Т	R	L	TR	L	Т	R	
Maximum Queue (m)	58.7	87.9	34.6	80.2	34.8	25.2	69.0	93.8	56.5	34.1	
Average Queue (m)	24.1	40.3	9.7	35.9	15.1	4.4	28.7	40.8	17.1	12.8	
95th Queue (m)	49.2	73.0	23.9	68.0	28.6	15.1	54.6	75.2	42.1	26.0	
Link Distance (m)		266.3		1920.7			458.7		610.8		
Upstream Blk Time (%)											
Queuing Penalty (veh)											
Storage Bay Dist (m)	85.0		65.0		80.0	55.0		90.0		100.0	
Storage Blk Time (%)		0		1			1	0			
Queuing Penalty (veh)		0		3			0	1			

Queuing and Blocking Report

#### <2025 Background> AM Peak Hour 09-14-2021

#### Intersection: 4: Thorold Townline Road & Thorold Stone Road

Movement	EB	EB	EB	EB	B24	WB	WB	WB	WB	NB	NB	SB
Directions Served	L	Т	Т	R	Т	L	Т	Т	R	L	TR	L
Maximum Queue (m)	101.8	84.4	86.3	38.6	64.0	38.9	106.9	96.9	25.2	51.1	73.2	31.8
Average Queue (m)	62.6	47.7	51.4	14.9	2.1	18.1	68.4	59.3	9.1	18.3	27.0	11.0
95th Queue (m)	96.3	72.9	75.6	30.8	45.1	34.2	103.5	93.4	20.7	40.5	57.4	26.2
Link Distance (m)		279.0	279.0		315.3		338.6	338.6			1028.0	
Upstream Blk Time (%)					0							
Queuing Penalty (veh)					0							
Storage Bay Dist (m)	100.0			50.0		85.0			90.0	80.0		75.0
Storage Blk Time (%)	1		12	0			4	1			0	
Queuing Penalty (veh)	2		12	0			5	1			0	

Intersection: 4: Thorold Townline Road & Thorold Stone Road

Movement	SB
Directions Served	TR
Maximum Queue (m)	142.4
Average Queue (m)	78.7
95th Queue (m)	136.5
Link Distance (m)	311.8
Upstream Blk Time (%)	
Queuing Penalty (veh)	
Storage Bay Dist (m)	
Storage Blk Time (%)	13
Queuing Penalty (veh)	7

## Intersection: 5: Thorold Townline Road & Lundys Lane

Movement	EB	EB	EB	WB	WB	NB	NB	SB	SB	SB	
Directions Served	L	Т	R	L	TR	L	TR	L	Т	R	
Maximum Queue (m)	43.1	66.4	41.2	17.2	58.1	54.9	80.3	16.9	43.0	21.7	
Average Queue (m)	19.5	29.3	6.2	5.6	21.9	15.5	31.0	4.7	16.2	7.6	
95th Queue (m)	35.9	58.6	21.9	14.5	44.9	36.6	60.9	13.3	34.9	18.8	
Link Distance (m)		1920.7			479.5		741.7		1500.2		
Upstream Blk Time (%)											
Queuing Penalty (veh)											
Storage Bay Dist (m)	90.0		20.0	55.0		25.0		25.0		30.0	
Storage Blk Time (%)		10	0		0	5	16	0	5	0	
Queuing Penalty (veh)		26	1		0	9	11	0	4	0	

Uppers Quarry Traffic Impact Study TMIG SimTraffic Report Page 1 Uppers Quarry Traffic Impact Study TMIG

<2025 Background> AM Peak Hour 09-14-2021

Intersection: 6: Thorold Townline Road & Beaverdams Road

Movement	EB	WB	NB	SB
Directions Served	LTR	LTR	LTR	LTR
Maximum Queue (m)	34.0	23.1	52.0	69.8
Average Queue (m)	15.9	11.4	25.4	31.5
95th Queue (m)	26.9	20.1	41.5	58.2
Link Distance (m)	192.4	256.5	1091.4	1028.0
Upstream Blk Time (%)				
Queuing Penalty (veh)				
Storage Bay Dist (m)				
Storage Blk Time (%)				
Queuing Penalty (veh)				

Intersection: 7: Thorold Townline Road & Uppers Lane

Movement
Directions Served
Maximum Queue (m)
Average Queue (m)
95th Queue (m)
Link Distance (m)
Upstream Blk Time (%)
Queuing Penalty (veh)
Storage Bay Dist (m)
Storage Blk Time (%)
Queuing Penalty (veh)

Network Summary

Network wide Queuing Penalty: 99

Uppers Quarry Traffic Impact Study TMIG

#### <2025 Background> PM Peak Hour 09-14-2021

Intersection: 1: Davis Road & Thorold Stone Road

Movement	EB	EB	EB	EB	WB	WB	WB	NB	NB	SB	SB	
Directions Served	L	Т	Т	R	L	Т	TR	L	LT	L	Т	
Maximum Queue (m)	22.7	121.4	118.5	66.4	67.1	104.2	112.2	92.6	89.2	7.6	14.8	
Average Queue (m)	5.0	77.0	64.7	3.7	26.0	48.5	50.4	52.7	54.9	0.8	2.5	
95th Queue (m)	15.3	118.8	110.0	30.4	51.2	87.9	93.4	78.0	80.7	4.2	9.5	
Link Distance (m)		367.0	367.0			315.3	315.3	1000.6	1000.6		265.6	
Upstream Blk Time (%)												
Queuing Penalty (veh)												
Storage Bay Dist (m)	105.0			50.0	70.0					30.0		
Storage Blk Time (%)		2	11	0	1	3			1			
Queuing Penalty (veh)		0	64	0	4	4			2			

Intersection: 2: Davis Road & Niagara Falls Road/Beaverdams Road

Movement	EB	WB	NB	NB	NB	SB	SB	SB	SB	
Directions Served	LTR	LTR	L	Т	TR	L	Т	Т	R	
Maximum Queue (m)	41.9	59.9	13.6	55.7	61.5	64.0	79.1	257.8	7.8	
Average Queue (m)	16.1	24.1	3.1	26.5	33.2	29.6	42.6	32.9	0.3	
95th Queue (m)	33.9	46.8	9.6	48.4	56.0	52.0	68.9	169.0	4.0	
Link Distance (m)	244.6	305.1		296.6	296.6		1000.6	1000.6		
Upstream Blk Time (%)										
Queuing Penalty (veh)										
Storage Bay Dist (m)			80.0			140.0			180.0	
Storage Blk Time (%)										
Queuing Penalty (veh)										

## Intersection: 3: Davis Road & Lundys Lane

Movement	EB	EB	WB	WB	WB	NB	NB	SB	SB	SB	
Directions Served	L	TR	L	Т	R	L	TR	L	Т	R	
Maximum Queue (m)	86.8	121.0	53.8	140.7	68.0	32.9	76.4	115.7	70.1	43.4	
Average Queue (m)	37.0	61.0	8.1	86.2	20.9	11.9	37.0	57.8	24.1	16.9	
95th Queue (m)	72.7	103.7	32.6	129.5	51.5	25.7	64.9	94.4	52.4	36.7	
Link Distance (m)		266.3		1920.7			458.7		610.8		
Upstream Blk Time (%)											
Queuing Penalty (veh)											
Storage Bay Dist (m)	85.0		65.0		80.0	55.0		90.0		100.0	
Storage Blk Time (%)	2	3		18			4	2	0		
Queuing Penalty (veh)	14	5		48			2	5	0		
Queuing Penalty (veh)	14	5		48			2	5	0		

Queuing and Blocking Report

#### <2025 Background> PM Peak Hour 09-14-2021

#### Intersection: 4: Thorold Townline Road & Thorold Stone Road

Movement	EB	EB	EB	EB	B24	B24	WB	WB	WB	WB	NB	NB
Directions Served	L	Т	Т	R	Т	Т	L	Т	Т	R	L	TR
Maximum Queue (m)	76.9	123.9	129.9	16.9	62.7	62.8	29.6	109.0	92.6	14.4	45.4	85.4
Average Queue (m)	38.8	55.4	59.1	5.4	2.1	2.1	11.8	65.5	55.0	3.5	19.8	38.6
95th Queue (m)	64.6	108.6	111.8	13.5	44.2	44.3	24.9	95.8	85.6	10.4	38.8	74.3
Link Distance (m)		279.0	279.0		315.3	315.3		338.6	338.6			1028.0
Upstream Blk Time (%)					0	0						
Queuing Penalty (veh)					0	0						
Storage Bay Dist (m)	100.0			50.0			85.0			90.0	80.0	
Storage Blk Time (%)		2	15					2	0			0
Queuing Penalty (veh)		4	8					1	0			1

Intersection: 4: Thorold Townline Road & Thorold Stone Road

Movement	SB	SB
Directions Served	L	TR
Maximum Queue (m)	86.6	169.6
Average Queue (m)	10.4	90.4
95th Queue (m)	44.6	153.0
Link Distance (m)		311.8
Upstream Blk Time (%)		
Queuing Penalty (veh)		
Storage Bay Dist (m)	75.0	
Storage Blk Time (%)		19
Queuing Penalty (veh)		9

## Intersection: 5: Thorold Townline Road & Lundys Lane

Movement	EB	EB	EB	WB	WB	NB	NB	SB	SB	SB	
Directions Served	L	Т	R	L	TR	L	TR	L	Т	R	
Maximum Queue (m)	38.4	59.7	28.3	19.4	80.5	53.4	57.4	30.7	54.0	28.1	
Average Queue (m)	13.4	25.9	4.2	5.6	36.7	25.1	31.4	14.7	24.4	14.6	
95th Queue (m)	30.5	50.5	16.0	15.2	67.1	43.9	54.1	27.3	43.1	24.2	
Link Distance (m)		1920.7			479.5		741.7		1500.2		
Upstream Blk Time (%)											
Queuing Penalty (veh)											
Storage Bay Dist (m)	90.0		20.0	55.0		25.0		25.0		30.0	
Storage Blk Time (%)		9	0		2	15	19	3	11	0	
Queuing Penalty (veh)		16	0		1	27	21	7	20	0	

Uppers Quarry Traffic Impact Study TMIG

SimTraffic Report Page 1 Uppers Quarry Traffic Impact Study TMIG

<2025 Background> PM Peak Hour 09-14-2021

Intersection: 6: Thorold Townline Road & Beaverdams Road

Movement	EB	WB	NB	SB
Directions Served	LTR	LTR	LTR	LTR
Maximum Queue (m)	48.3	29.6	71.0	49.9
Average Queue (m)	23.8	14.0	33.2	23.2
95th Queue (m)	40.5	24.0	56.9	38.4
Link Distance (m)	192.4	256.5	1091.4	1028.0
Upstream Blk Time (%)				
Queuing Penalty (veh)				
Storage Bay Dist (m)				
Storage Blk Time (%)				
Queuing Penalty (veh)				

Intersection: 7: Thorold Townline Road & Uppers Lane

Movement
Directions Served
Maximum Queue (m)
Average Queue (m)
95th Queue (m)
Link Distance (m)
Upstream Blk Time (%)
Queuing Penalty (veh)
Storage Bay Dist (m)
Storage Blk Time (%)
Queuing Penalty (veh)

Network Summary

Network wide Queuing Penalty: 264

Uppers Quarry Traffic Impact Study TMIG

#### <2025 Total - Thorold Townline> AM Peak Hour 09-23-2021

Intersection: 1: Davis Road & Thorold Stone Road

Movement	EB	EB	EB	WB	WB	WB	NB	NB	NB	SB	SB	
Directions Served	L	Т	Т	L	Т	TR	L	LT	R	L	Т	
Maximum Queue (m)	16.2	73.6	68.6	50.1	93.7	104.7	92.0	90.5	26.7	1.9	4.5	
Average Queue (m)	3.3	43.0	29.3	19.8	58.3	61.7	58.1	60.5	1.2	0.1	0.3	
95th Queue (m)	10.6	69.2	59.4	40.6	93.0	95.2	83.4	85.7	14.0	1.0	2.4	
Link Distance (m)		367.0	367.0		315.3	315.3	1000.6	1000.6			265.6	
Upstream Blk Time (%)												
Queuing Penalty (veh)												
Storage Bay Dist (m)	105.0			70.0					80.0	30.0		
Storage Blk Time (%)			1		5			2				
Queuing Penalty (veh)			3		4			4				

Intersection: 2: Davis Road & Niagara Falls Road/Beaverdams Road

Movement	EB	WB	NB	NB	NB	SB	SB	SB
Directions Served	LTR	LTR	L	Т	TR	L	Т	Т
Maximum Queue (m)	42.7	53.2	21.9	67.7	82.0	39.0	65.4	38.1
Average Queue (m)	16.5	19.2	4.0	37.4	44.5	16.3	27.3	11.7
95th Queue (m)	34.3	40.2	14.3	63.3	73.5	32.4	48.6	31.1
Link Distance (m)	244.6	305.1		296.6	296.6		1000.6	1000.6
Upstream Blk Time (%)								
Queuing Penalty (veh)								
Storage Bay Dist (m)			80.0			140.0		
Storage Blk Time (%)				0				
Queuing Penalty (veh)				0				

## Intersection: 3: Davis Road & Lundys Lane

Movement	EB	EB	WB	WB	WB	NB	NB	SB	SB	SB	
Directions Served	L	TR	L	Т	R	L	TR	L	Т	R	
Maximum Queue (m)	58.0	89.4	30.1	80.2	33.4	24.7	63.7	102.6	78.3	36.2	
Average Queue (m)	23.4	39.8	8.6	33.2	15.6	6.7	28.6	47.4	20.2	12.9	
95th Queue (m)	45.8	72.2	22.3	66.7	28.9	18.4	53.2	95.1	59.4	28.7	
Link Distance (m)		266.3		1920.7			458.7		610.8		
Upstream Blk Time (%)											
Queuing Penalty (veh)											
Storage Bay Dist (m)	85.0		65.0		80.0	55.0		90.0		100.0	
Storage Blk Time (%)		0		1			1	4			
Queuing Penalty (veh)		0		2			0	9			
Queuing Penalty (veh) Storage Bay Dist (m) Storage Blk Time (%) Queuing Penalty (veh)	85.0	0	65.0	1 2	80.0	55.0	1 0	90.0 4 9		100.0	

Uppers Quarry Traffic Impact Study TMIG

SimTraffic Report Page 1

## Queuing and Blocking Report

#### <2025 Total - Thorold Townline> AM Peak Hour 09-23-2021

### Intersection: 4: Thorold Townline Road & Thorold Stone Road

Movement	EB	EB	EB	EB	WB	WB	WB	WB	NB	NB	SB	SB
Directions Served	L	Т	Т	R	L	Т	Т	R	L	TR	L	TR
Maximum Queue (m)	123.3	89.7	95.5	40.6	62.4	120.8	114.2	28.0	62.6	97.5	36.4	147.8
Average Queue (m)	65.8	52.4	57.5	16.9	26.1	76.9	67.8	8.9	24.2	35.6	11.0	80.0
95th Queue (m)	101.6	80.8	86.0	32.1	51.0	113.0	104.4	20.1	50.2	72.1	27.4	134.4
Link Distance (m)		279.0	279.0			338.6	338.6			1028.0		311.8
Upstream Blk Time (%)												
Queuing Penalty (veh)												
Storage Bay Dist (m)	100.0			50.0	85.0			90.0	80.0		75.0	
Storage Blk Time (%)	1	0	16	0	0	7	2			1		12
Queuing Penalty (veh)	4	0	19	0	1	9	2			1		6

#### Intersection: 5: Thorold Townline Road & Lundys Lane

Movement	EB	EB	EB	WB	WB	NB	NB	SB	SB	SB	
Directions Served	L	Т	R	L	TR	L	TR	L	Т	R	
Maximum Queue (m)	50.2	69.5	26.9	16.6	58.3	47.4	70.4	28.6	38.9	23.2	
Average Queue (m)	21.7	32.3	4.6	5.4	25.2	14.8	29.4	6.5	16.2	8.4	
95th Queue (m)	41.2	61.8	16.3	13.5	49.8	34.4	56.5	19.6	33.4	19.6	
Link Distance (m)		1920.7			479.5		741.7		1500.2		
Upstream Blk Time (%)											
Queuing Penalty (veh)											
Storage Bay Dist (m)	90.0		20.0	55.0		25.0		25.0		30.0	
Storage Blk Time (%)		13	0		0	6	14	1	5	0	
Queuing Penalty (veh)		33	0		0	10	10	1	4	0	

## Intersection: 6: Thorold Townline Road & Beaverdams Road

Uppers Quarry Traffic Impact Study TMIG

## <2025 Total - Thorold Townline> AM Peak Hour 09-23-2021

## Intersection: 7: Thorold Townline Road & Uppers Lane

Movement	WB	SB
Directions Served	LR	L
Maximum Queue (m)	40.0	32.0
Average Queue (m)	15.6	7.1
95th Queue (m)	28.6	22.6
Link Distance (m)	1027.2	
Upstream Blk Time (%)		
Queuing Penalty (veh)		
Storage Bay Dist (m)		15.0
Storage Blk Time (%)		2
Queuing Penalty (veh)		6

## Network Summary

Network wide Queuing Penalty: 129

Uppers Quarry Traffic Impact Study TMIG

#### <2025 Total - Thorold Townline> PM Peak Hour 09-23-2021

Intersection: 1: Davis Road & Thorold Stone Road

Movement	EB	EB	EB	EB	WB	WB	WB	NB	NB	NB	SB	SB
Directions Served	L	Т	Т	R	L	Т	TR	L	LT	R	L	T
Maximum Queue (m)	19.9	138.6	131.1	79.5	47.0	106.2	112.4	76.4	79.7	14.7	6.0	13.2
Average Queue (m)	4.8	73.0	62.8	5.7	22.7	60.6	64.1	48.8	52.8	0.9	1.0	2.2
95th Queue (m)	15.0	116.5	108.9	45.6	41.8	96.5	101.1	68.7	72.3	10.0	4.1	8.3
Link Distance (m)		367.0	367.0			315.3	315.3	1000.6	1000.6			265.6
Upstream Blk Time (%)												
Queuing Penalty (veh)												
Storage Bay Dist (m)	105.0			50.0	70.0					80.0	30.0	
Storage Blk Time (%)		2	12	0		5			0			
Queuing Penalty (veh)		0	70	0		7			0			

Intersection: 2: Davis Road & Niagara Falls Road/Beaverdams Road

Movement	EB	WB	NB	NB	NB	SB	SB	SB	SB	
Directions Served	LTR	LTR	L	Т	TR	L	Т	Т	R	
Maximum Queue (m)	33.3	61.1	13.8	51.4	59.5	55.2	74.9	55.5	6.7	
Average Queue (m)	15.8	23.2	2.7	25.0	31.4	27.1	43.1	25.0	0.2	
95th Queue (m)	30.6	47.5	9.3	46.4	53.8	47.6	66.6	50.8	3.4	
Link Distance (m)	244.6	305.1		296.6	296.6		1000.6	1000.6		
Upstream Blk Time (%)										
Queuing Penalty (veh)										
Storage Bay Dist (m)			80.0			140.0			180.0	
Storage Blk Time (%)										
Queuing Penalty (veh)										

## Intersection: 3: Davis Road & Lundys Lane

EB	EB	WB	WB	WB	NB	NB	SB	SB	SB	
L	TR	L	Т	R	L	TR	L	Т	R	
69.8	119.3	20.8	156.5	65.6	28.4	73.3	118.4	66.7	45.6	
30.0	63.4	6.0	85.6	19.2	11.3	36.2	64.9	22.3	15.7	
56.6	104.9	16.6	133.8	42.9	23.1	63.0	103.9	48.9	34.2	
	266.3		1920.7			458.7		610.8		
85.0		65.0		80.0	55.0		90.0		100.0	
0	3		17			3	3	0		
2	5		45			1	9	0		
	L 69.8 30.0 56.6 85.0 0 2	EB EB   L TR   59.8 119.3   30.0 63.4   56.6 104.9   266.3   35.0   0 3   2 5	EB EB Wb   L TR L   69.8 119.3 20.8   30.0 63.4 6.0   56.6 104.9 16.6   266.3 266.3   85.0 65.0   0 3   2 5	EB EB WB WB WB   L TR L T 59.8 119.3 20.8 156.5 50.0 63.4 6.0 85.6 56.6 104.9 16.6 133.8 206.3 1920.7   385.0 65.0 0 3 17 2 5 45	EB EB WB WB WB WB   L TR L T R   59.8 119.3 20.8 156.5 65.6   30.0 63.4 6.0 85.6 19.2   56.6 104.9 16.6 133.8 42.9   266.3 1920.7 1920.7   385.0 65.0 80.0   0 3 17   2 5 45	EB EB WB WB WB NB   L TR L T R L   59.8 119.3 20.8 156.5 65.6 28.4   30.0 63.4 6.0 85.6 19.2 11.3   56.6 104.9 16.6 133.8 42.9 23.1   266.3 1920.7 1920.7 1920.7   385.0 65.0 80.0 55.0   0 3 17 2 5 45	EB EB WB WB WB NB NB NB   L TR L T R L T R L T R L T R L T R L T R L T R L T R L T R L T R L T R L T R L T R L T R L T R L T R L T R L T R L T R L T R L T R L T R L T R L T R L T R L T R L T R L T R L T R L T R L T R L T	EB EB VB VB VB VB NB NB<	EB EB WB WB WB NB NB NB SB SB<	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$

Queuing and Blocking Report

<2025 Total - Thorold Townline> PM Peak Hour 09-23-2021

#### Intersection: 4: Thorold Townline Road & Thorold Stone Road

Movement	EB	EB	EB	EB	B24	B24	WB	WB	WB	WB	NB	NB
Directions Served	L	Т	Т	R	Т	Т	L	Т	Т	R	L	TR
Maximum Queue (m)	91.7	134.1	132.0	24.7	128.9	129.8	37.8	118.1	107.4	19.8	72.0	104.0
Average Queue (m)	45.9	87.5	90.0	11.1	6.4	4.3	15.3	69.2	59.0	5.4	27.8	46.9
95th Queue (m)	79.3	125.7	126.2	23.5	80.6	65.8	31.0	103.7	93.8	14.0	56.7	90.1
Link Distance (m)		279.0	279.0		315.3	315.3		338.6	338.6			1028.0
Upstream Blk Time (%)					0	0						
Queuing Penalty (veh)					0	2						
Storage Bay Dist (m)	100.0			50.0			85.0			90.0	80.0	
Storage Blk Time (%)	0	6	32					4	1		0	2
Queuing Penalty (veh)	2	13	23					3	0		1	2

Intersection: 4: Thorold Townline Road & Thorold Stone Road

Movement	SB	SB
Directions Served	L	TR
Maximum Queue (m)	54.7	152.9
Average Queue (m)	8.5	94.7
95th Queue (m)	33.0	146.4
Link Distance (m)		311.8
Upstream Blk Time (%)		
Queuing Penalty (veh)		
Storage Bay Dist (m)	75.0	
Storage Blk Time (%)		21
Queuing Penalty (veh)		10

#### Intersection: 5: Thorold Townline Road & Lundys Lane

Movement	EB	EB	EB	WB	WB	NB	NB	SB	SB	SB	
Directions Served	L	Т	R	L	TR	L	TR	L	Т	R	
Maximum Queue (m)	42.6	71.4	51.6	21.7	92.9	55.8	71.0	40.1	56.4	37.0	
Average Queue (m)	15.5	27.4	5.8	6.3	43.8	23.9	32.3	15.2	24.9	15.1	
95th Queue (m)	32.8	60.1	25.7	15.6	78.1	44.3	58.8	31.1	46.9	30.0	
Link Distance (m)		1920.7			479.5		741.7		1500.2		
Upstream Blk Time (%)											
Queuing Penalty (veh)											
Storage Bay Dist (m)	90.0		20.0	55.0		25.0		25.0		30.0	
Storage Blk Time (%)		10	0		4	14	17	4	10	1	
Queuing Penalty (veh)		18	1		2	26	19	11	18	1	

Uppers Quarry Traffic Impact Study TMIG SimTraffic Report Page 1 Uppers Quarry Traffic Impact Study TMIG

<2025 Total - Thorold Townline> PM Peak Hour 09-23-2021

Intersection: 6: Thorold Townline Road & Beaverdams Road

Movement	EB	WB	NB	SB
Directions Served	LTR	LTR	LTR	LTR
Maximum Queue (m)	71.7	59.1	146.5	110.1
Average Queue (m)	27.2	24.0	63.3	49.2
95th Queue (m)	57.5	49.0	113.0	90.9
Link Distance (m)	192.4	256.5	1091.4	1028.0
Upstream Blk Time (%)				
Queuing Penalty (veh)				
Storage Bay Dist (m)				
Storage Blk Time (%)				
Queuing Penalty (veh)				

Intersection: 7: Thorold Townline Road & Uppers Lane

Movement	WB	NB	SB
Directions Served	LR	TR	L
Maximum Queue (m)	26.3	1.3	25.3
Average Queue (m)	12.1	0.0	4.7
95th Queue (m)	22.9	0.9	18.6
Link Distance (m)	1027.2	1500.2	
Upstream Blk Time (%)			
Queuing Penalty (veh)			
Storage Bay Dist (m)			15.0
Storage Blk Time (%)			1
Queuing Penalty (veh)			3

Network Summary

Network wide Queuing Penalty: 296

Uppers Quarry Traffic Impact Study TMIG

#### <2035 Background> AM Peak Hour 09-14-2021

Intersection: 1: Davis Road & Thorold Stone Road

Movement	EB	EB	EB	EB	WB	WB	WB	NB	NB	NB	SB	SB
Directions Served	L	Т	Т	R	L	Т	TR	L	LT	R	L	Т
Maximum Queue (m)	16.4	94.8	144.2	36.2	46.9	115.2	118.0	120.3	123.3	75.4	1.0	6.0
Average Queue (m)	4.1	59.6	51.6	1.2	21.1	75.5	79.6	71.2	76.0	5.9	0.0	0.7
95th Queue (m)	11.8	87.3	118.8	19.1	38.8	106.8	109.5	112.7	116.9	42.6	0.8	4.1
Link Distance (m)		367.0	367.0			315.3	315.3	1000.6	1000.6			265.6
Upstream Blk Time (%)			0									
Queuing Penalty (veh)			0									
Storage Bay Dist (m)	105.0			50.0	70.0					80.0	30.0	
Storage Blk Time (%)		0	5	0		9			8			
Queuing Penalty (veh)		0	15	0		10			21			

Intersection: 2: Davis Road & Niagara Falls Road/Beaverdams Road

Movement	EB	WB	NB	NB	NB	SB	SB	SB
Directions Served	LTR	LTR	L	Т	TR	L	Т	Т
Maximum Queue (m)	45.1	55.7	24.8	81.7	82.4	33.2	63.8	51.5
Average Queue (m)	19.3	21.1	6.5	43.9	47.6	15.8	32.3	17.6
95th Queue (m)	38.5	44.4	18.2	72.4	75.3	29.6	54.1	42.1
Link Distance (m)	244.6	305.1		296.6	296.6		1000.6	1000.6
Upstream Blk Time (%)								
Queuing Penalty (veh)								
Storage Bay Dist (m)			80.0			140.0		
Storage Blk Time (%)				0				
Queuing Penalty (veh)				0				

## Intersection: 3: Davis Road & Lundys Lane

Movement	EB	EB	WB	WB	WB	NB	NB	SB	SB	SB	
Directions Served	L	TR	L	Т	R	L	TR	L	Т	R	
Maximum Queue (m)	58.7	90.3	31.3	85.3	26.0	26.3	65.4	68.4	61.2	46.0	
Average Queue (m)	25.3	43.8	12.2	38.1	9.3	6.7	29.9	29.9	17.3	16.8	
95th Queue (m)	49.1	75.9	26.7	68.8	20.6	19.0	54.9	56.9	41.6	35.1	
Link Distance (m)		266.3		1920.7			458.7		610.8		
Upstream Blk Time (%)											
Queuing Penalty (veh)											
Storage Bay Dist (m)	85.0		65.0		80.0	55.0		90.0		100.0	
Storage Blk Time (%)		0		1			1	0	0		
Queuing Penalty (veh)		0		2			0	1	0		

Queuing and Blocking Report

#### <2035 Background> AM Peak Hour 09-14-2021

#### Intersection: 4: Thorold Townline Road & Thorold Stone Road

Movement	EB	EB	EB	EB	B24	B24	WB	WB	WB	WB	NB	NB
Directions Served	L	Т	Т	R	Т	Т	L	Т	Т	R	L	TR
Maximum Queue (m)	125.9	105.8	109.0	45.6	65.6	325.7	113.2	154.1	144.6	26.6	61.6	86.1
Average Queue (m)	72.8	62.0	64.8	20.9	2.2	12.9	51.5	81.1	70.8	9.3	23.4	32.2
95th Queue (m)	116.8	92.6	94.7	37.8	46.2	117.6	106.0	136.6	118.0	19.7	47.8	66.1
Link Distance (m)		279.0	279.0		315.3	315.3		338.6	338.6			1028.0
Upstream Blk Time (%)					0	0						
Queuing Penalty (veh)					0	2						
Storage Bay Dist (m)	100.0			50.0			85.0			90.0	80.0	
Storage Blk Time (%)	4	1	26	0			5	6	1		0	0
Queuing Penalty (veh)	15	2	41	0			23	11	1		1	1

Intersection: 4: Thorold Townline Road & Thorold Stone Road

Movement	SB	SB
Directions Served	L	TR
Maximum Queue (m)	89.2	197.2
Average Queue (m)	13.3	119.1
95th Queue (m)	54.1	192.3
Link Distance (m)		311.8
Upstream Blk Time (%)		
Queuing Penalty (veh)		
Storage Bay Dist (m)	75.0	
Storage Blk Time (%)		33
Queuing Penalty (veh)		17

#### Intersection: 5: Thorold Townline Road & Lundys Lane

Movement	EB	EB	EB	WB	WB	NB	NB	SB	SB	SB	
Directions Served	L	Т	R	L	TR	L	TR	L	Т	R	
Maximum Queue (m)	75.3	86.3	50.4	19.5	77.5	59.1	78.7	37.8	50.6	35.8	
Average Queue (m)	31.6	37.8	6.6	5.4	34.8	16.6	25.9	10.9	17.9	11.4	
95th Queue (m)	59.6	72.4	24.2	14.0	66.1	36.5	54.1	26.6	37.6	27.4	
Link Distance (m)		1920.7			479.5		741.7		1500.2		
Upstream Blk Time (%)											
Queuing Penalty (veh)											
Storage Bay Dist (m)	90.0		20.0	55.0		25.0		25.0		30.0	
Storage Blk Time (%)	0	14	0		2	6	14	2	6	1	
Queuing Penalty (veh)	0	43	1		1	10	11	4	7	1	

Uppers Quarry Traffic Impact Study TMIG SimTraffic Report Page 1 Uppers Quarry Traffic Impact Study TMIG

<2035 Background> AM Peak Hour 09-14-2021

Intersection: 6: Thorold Townline Road & Beaverdams Road

Movement	EB	WB	NB	SB
Directions Served	LTR	LTR	LTR	LTR
Maximum Queue (m)	54.0	72.8	102.5	119.0
Average Queue (m)	24.5	34.3	43.5	56.4
95th Queue (m)	44.8	59.6	84.6	99.1
Link Distance (m)	192.4	256.5	1091.4	1028.0
Upstream Blk Time (%)				
Queuing Penalty (veh)				
Storage Bay Dist (m)				
Storage Blk Time (%)				
Queuing Penalty (veh)				

Intersection: 7: Thorold Townline Road & Uppers Lane

Movement
Directions Served
Maximum Queue (m)
Average Queue (m)
95th Queue (m)
Link Distance (m)
Upstream Blk Time (%)
Queuing Penalty (veh)
Storage Bay Dist (m)
Storage Blk Time (%)
Queuing Penalty (veh)

Network Summary

Network wide Queuing Penalty: 242

Uppers Quarry Traffic Impact Study TMIG

#### <2035 Background> PM Peak Hour 09-14-2021

Intersection: 1: Davis Road & Thorold Stone Road

Movement	EB	EB	EB	EB	WB	WB	WB	NB	NB	NB	SB	SB
Directions Served	L	Т	Т	R	L	Т	TR	L	LT	R	L	Т
Maximum Queue (m)	24.7	146.4	150.1	111.5	72.5	111.3	112.8	114.9	116.3	87.8	3.9	11.8
Average Queue (m)	4.8	85.3	75.6	17.7	34.7	70.6	73.8	78.0	80.3	5.9	0.5	2.3
95th Queue (m)	15.3	130.8	128.5	72.7	60.8	98.6	101.3	109.9	112.3	39.9	2.8	8.2
Link Distance (m)		367.0	367.0			315.3	315.3	1000.6	1000.6			265.6
Upstream Blk Time (%)												
Queuing Penalty (veh)												
Storage Bay Dist (m)	105.0			50.0	70.0					80.0	30.0	
Storage Blk Time (%)		4	17	1	0	7			12			
Queuing Penalty (veh)		1	122	7	3	14			22			

Intersection: 2: Davis Road & Niagara Falls Road/Beaverdams Road

Movement	EB	WB	NB	NB	NB	SB	SB	SB
Directions Served	LTR	LTR	L	Т	TR	L	Т	Т
Maximum Queue (m)	50.9	62.2	19.3	65.8	71.4	60.2	88.2	80.5
Average Queue (m)	19.1	29.5	6.0	31.0	36.2	26.7	52.0	35.9
95th Queue (m)	38.5	55.6	15.4	56.8	62.9	47.7	79.1	69.7
Link Distance (m)	244.6	305.1		296.6	296.6		1000.6	1000.6
Upstream Blk Time (%)								
Queuing Penalty (veh)								
Storage Bay Dist (m)			80.0			140.0		
Storage Blk Time (%)				0				
Queuing Penalty (veh)				0				

## Intersection: 3: Davis Road & Lundys Lane

Movement	EB	EB	WB	WB	WB	NB	NB	SB	SB	SB	B9	B27
Directions Served	L	TR	L	Т	R	L	TR	L	Т	R	Т	T
Maximum Queue (m)	119.8	170.0	113.5	239.1	107.4	37.0	84.6	169.3	301.6	127.4	30.4	54.3
Average Queue (m)	66.9	81.2	20.1	121.2	33.4	12.2	41.5	131.7	136.3	32.7	10.8	10.2
95th Queue (m)	140.2	143.4	78.6	219.8	111.5	26.9	71.5	211.1	438.3	80.7	72.3	80.2
Link Distance (m)		266.3		1920.7			458.7		610.8		119.0	466.3
Upstream Blk Time (%)									5		4	
Queuing Penalty (veh)									42		34	
Storage Bay Dist (m)	85.0		65.0		80.0	55.0		90.0		100.0		
Storage Blk Time (%)	25	5		26		0	5	60		0		
Queuing Penalty (veh)	187	10		67		0	2	186		0		

Queuing and Blocking Report

#### <2035 Background> PM Peak Hour 09-14-2021

#### Intersection: 4: Thorold Townline Road & Thorold Stone Road

Movement	EB	EB	EB	EB	B24	B24	WB	WB	WB	WB	NB	NB
Directions Served	L	Т	Т	R	Т	Т	L	Т	Т	R	L	TR
Maximum Queue (m)	83.9	144.4	147.4	50.2	187.9	261.7	42.2	131.8	125.5	18.0	91.9	142.3
Average Queue (m)	46.8	105.5	109.2	11.2	8.3	13.1	19.8	89.0	79.7	4.8	35.6	72.4
95th Queue (m)	78.6	139.6	143.1	32.3	91.4	118.7	36.0	126.2	117.5	13.3	75.9	130.0
Link Distance (m)		279.0	279.0		315.3	315.3		338.6	338.6			1028.0
Upstream Blk Time (%)					0	0						
Queuing Penalty (veh)					0	3						
Storage Bay Dist (m)	100.0			50.0			85.0			90.0	80.0	
Storage Blk Time (%)	0	13	38					13	4		0	7
Queuing Penalty (veh)	0	30	30					13	2		1	14

Intersection: 4: Thorold Townline Road & Thorold Stone Road

Movement	SB	SB
Directions Served	L	TR
Maximum Queue (m)	114.0	277.2
Average Queue (m)	34.4	167.8
95th Queue (m)	135.9	290.4
Link Distance (m)		311.8
Upstream Blk Time (%)		2
Queuing Penalty (veh)		0
Storage Bay Dist (m)	75.0	
Storage Blk Time (%)		54
Queuing Penalty (veh)		26

#### Intersection: 5: Thorold Townline Road & Lundys Lane

Movement	EB	EB	EB	WB	WB	NB	NB	SB	SB	SB	
Directions Served	L	Т	R	L	TR	L	TR	L	Т	R	
Maximum Queue (m)	73.4	87.0	49.6	24.7	110.3	61.2	93.1	59.0	67.8	57.2	
Average Queue (m)	29.5	43.2	5.9	6.7	60.3	29.8	39.2	24.4	26.2	27.3	
95th Queue (m)	60.3	73.8	23.4	17.3	101.3	52.3	67.9	46.4	53.1	50.1	
Link Distance (m)		1920.7			479.5		741.7		1500.2		
Upstream Blk Time (%)											
Queuing Penalty (veh)											
Storage Bay Dist (m)	90.0		20.0	55.0		25.0		25.0		30.0	
Storage Blk Time (%)	0	15	0		9	29	24	16	10	8	
Queuing Penalty (veh)	2	35	0		4	56	28	49	26	17	

Uppers Quarry Traffic Impact Study TMIG SimTraffic Report Page 1 Uppers Quarry Traffic Impact Study TMIG

<2035 Background> PM Peak Hour 09-14-2021

Intersection: 6: Thorold Townline Road & Beaverdams Road

Movement	EB	WB	NB	SB
Directions Served	LTR	LTR	LTR	LTR
Maximum Queue (m)	70.8	118.0	244.0	165.9
Average Queue (m)	33.5	49.5	121.0	66.4
95th Queue (m)	64.7	94.3	219.0	132.8
Link Distance (m)	192.4	256.5	1091.4	1028.0
Upstream Blk Time (%)				
Queuing Penalty (veh)				
Storage Bay Dist (m)				
Storage Blk Time (%)				
Queuing Penalty (veh)				

Intersection: 7: Thorold Townline Road & Uppers Lane

Movement
Directions Served
Maximum Queue (m)
Average Queue (m)
95th Queue (m)
Link Distance (m)
Upstream Blk Time (%)
Queuing Penalty (veh)
Storage Bay Dist (m)
Storage Blk Time (%)
Queuing Penalty (veh)

Network Summary

Network wide Queuing Penalty: 1034

Uppers Quarry Traffic Impact Study TMIG

#### <2035 Total - Thorold Townline> AM Peak Hour 09-23-2021

Intersection: 1: Davis Road & Thorold Stone Road

Movement	EB	EB	EB	WB	WB	WB	NB	NB	NB	SB	SB	
Directions Served	L	Т	Т	L	Т	TR	L	LT	R	L	Т	
Maximum Queue (m)	18.4	84.8	73.3	89.9	122.7	107.3	101.0	106.7	49.8	1.9	7.6	
Average Queue (m)	3.7	47.1	33.0	43.9	74.0	74.8	67.8	70.9	3.6	0.1	0.6	
95th Queue (m)	12.5	75.9	63.6	103.5	104.7	102.0	95.5	97.6	23.8	1.3	4.4	
Link Distance (m)		367.0	367.0		315.3	315.3	1000.6	1000.6			265.6	
Upstream Blk Time (%)												
Queuing Penalty (veh)												
Storage Bay Dist (m)	105.0			70.0					80.0	30.0		
Storage Blk Time (%)			2	13	9			3				
Queuing Penalty (veh)			6	75	11			9				

Intersection: 2: Davis Road & Niagara Falls Road/Beaverdams Road

Movement	EB	WB	NB	NB	NB	SB	SB	SB
Directions Served	LTR	LTR	L	Т	TR	L	Т	Т
Maximum Queue (m)	41.9	54.6	30.4	78.2	85.3	36.7	82.0	66.4
Average Queue (m)	19.5	19.5	7.0	43.7	47.1	16.0	36.9	19.8
95th Queue (m)	36.6	41.8	21.4	68.7	75.7	31.3	65.4	47.6
Link Distance (m)	244.6	305.1		296.6	296.6		1000.6	1000.6
Upstream Blk Time (%)								
Queuing Penalty (veh)								
Storage Bay Dist (m)			80.0			140.0		
Storage Blk Time (%)				0				
Queuing Penalty (veh)				0				

## Intersection: 3: Davis Road & Lundys Lane

Movement	EB	EB	WB	WB	WB	NB	NB	SB	SB	SB	
Directions Served	L	TR	L	Т	R	L	TR	L	Т	R	
Maximum Queue (m)	50.4	86.7	33.7	79.4	25.0	26.2	65.6	84.2	69.5	62.4	
Average Queue (m)	23.1	40.3	11.4	38.2	9.6	5.8	28.6	36.3	20.4	18.3	
95th Queue (m)	42.3	74.5	26.1	71.1	20.8	17.7	54.3	69.7	49.5	41.4	
Link Distance (m)		266.3		1920.7			458.7		610.8		
Upstream Blk Time (%)											
Queuing Penalty (veh)											
Storage Bay Dist (m)	85.0		65.0		80.0	55.0		90.0		100.0	
Storage Blk Time (%)		0		1			2	1	0		
Queuing Penalty (veh)		0		2			0	2	0		
Queuing Penalty (veh)		0		2			0	2	0		

Queuing and Blocking Report

<2035 Total - Thorold Townline> AM Peak Hour 09-23-2021

#### Intersection: 4: Thorold Townline Road & Thorold Stone Road

Movement	EB	EB	EB	EB	B24	B24	WB	WB	WB	WB	NB	NB
Directions Served	L	Т	Т	R	Т	Т	L	Т	Т	R	L	TR
Maximum Queue (m)	149.6	110.0	110.2	76.5	62.4	64.6	126.0	151.1	140.4	20.8	76.6	101.2
Average Queue (m)	73.8	67.8	70.9	27.2	2.1	2.2	56.8	102.1	95.3	8.6	33.0	44.7
95th Queue (m)	116.7	98.3	100.9	53.6	44.0	45.5	103.8	145.3	138.0	17.9	66.1	88.7
Link Distance (m)		279.0	279.0		315.3	315.3		338.6	338.6			1028.0
Upstream Blk Time (%)						0						
Queuing Penalty (veh)						1						
Storage Bay Dist (m)	100.0			50.0			85.0			90.0	80.0	
Storage Blk Time (%)	3	1	31	1			5	27	16		0	2
Queuing Penalty (veh)	13	2	55	5			20	58	11		0	3

Intersection: 4: Thorold Townline Road & Thorold Stone Road

Movement	SB	SB
Directions Served	L	TR
Maximum Queue (m)	146.5	276.7
Average Queue (m)	32.7	147.4
95th Queue (m)	123.0	270.7
Link Distance (m)		311.8
Upstream Blk Time (%)		2
Queuing Penalty (veh)		0
Storage Bay Dist (m)	75.0	
Storage Blk Time (%)		43
Queuing Penalty (veh)		22

#### Intersection: 5: Thorold Townline Road & Lundys Lane

Movement	EB	EB	EB	WB	WB	NB	NB	SB	SB	SB	
Directions Served	L	Т	R	L	TR	L	TR	L	Т	R	
Maximum Queue (m)	68.9	98.4	51.3	21.6	77.7	51.2	60.1	26.6	39.3	36.5	
Average Queue (m)	33.6	36.0	8.7	6.3	36.3	14.7	28.6	10.0	16.4	12.8	
95th Queue (m)	61.1	73.1	34.1	16.0	65.8	34.2	50.7	21.8	35.5	27.3	
Link Distance (m)		1920.7			479.5		741.7		1500.2		
Upstream Blk Time (%)											
Queuing Penalty (veh)											
Storage Bay Dist (m)	90.0		20.0	55.0		25.0		25.0		30.0	
Storage Blk Time (%)	0	14	0		1	4	16	1	5	1	
Queuing Penalty (veh)	0	44	1		1	7	12	2	6	1	

Uppers Quarry Traffic Impact Study TMIG SimTraffic Report Page 1 Uppers Quarry Traffic Impact Study TMIG

#### <2035 Total - Thorold Townline> AM Peak Hour 09-23-2021

Intersection: 6: Thorold Townline Road & Beaverdams Road

Movement	EB	WB	NB	SB
Directions Served	LTR	LTR	LTR	LTR
Maximum Queue (m)	51.3	65.6	188.7	149.3
Average Queue (m)	25.0	32.8	68.5	68.7
95th Queue (m)	44.4	58.3	148.1	121.6
Link Distance (m)	192.4	256.5	1091.4	1028.0
Upstream Blk Time (%)				
Queuing Penalty (veh)				
Storage Bay Dist (m)				
Storage Blk Time (%)				
Queuing Penalty (veh)				

Intersection: 7: Thorold Townline Road & Uppers Lane

Movement	WB	NB	SB
Directions Served	LR	TR	L
Maximum Queue (m)	29.2	4.3	31.2
Average Queue (m)	14.7	0.1	8.4
95th Queue (m)	25.3	2.3	23.1
Link Distance (m)	1027.2	1500.2	
Upstream Blk Time (%)			
Queuing Penalty (veh)			
Storage Bay Dist (m)			15.0
Storage Blk Time (%)			3
Queuing Penalty (veh)			11

Network Summary

Network wide Queuing Penalty: 382

Uppers Quarry Traffic Impact Study TMIG

#### <2035 Total - Thorold Townline> PM Peak Hour 09-23-2021

Intersection: 1: Davis Road & Thorold Stone Road

Movement	EB	EB	EB	EB	WB	WB	WB	NB	NB	NB	SB	SB
Directions Served	L	Т	Т	R	L	Т	TR	L	LT	R	L	T
Maximum Queue (m)	19.4	194.8	191.0	103.4	68.8	116.8	115.4	157.8	168.8	122.0	10.0	10.3
Average Queue (m)	4.7	92.0	80.5	16.4	36.2	75.7	77.7	94.7	97.9	18.3	1.2	2.0
95th Queue (m)	14.5	161.4	143.6	71.5	61.6	102.2	103.8	141.5	146.4	86.4	5.9	7.3
Link Distance (m)		367.0	367.0			315.3	315.3	1000.6	1000.6			265.6
Upstream Blk Time (%)		0	0									
Queuing Penalty (veh)		0	0									
Storage Bay Dist (m)	105.0			50.0	70.0					80.0	30.0	
Storage Blk Time (%)		5	20	1	0	9			28			
Queuing Penalty (veh)		1	146	7	3	19			51			

Intersection: 2: Davis Road & Niagara Falls Road/Beaverdams Road

Movement	EB	WB	NB	NB	NB	SB	SB	SB	SB	
Directions Served	LTR	LTR	L	Т	TR	L	Т	Т	R	
Maximum Queue (m)	52.2	67.3	18.7	66.7	76.4	62.4	93.7	83.5	6.7	
Average Queue (m)	20.3	28.9	6.1	32.6	38.2	29.9	51.3	33.8	0.2	
95th Queue (m)	40.2	57.6	15.0	58.1	65.1	53.2	79.2	66.8	3.4	
Link Distance (m)	244.6	305.1		296.6	296.6		1000.6	1000.6		
Upstream Blk Time (%)										
Queuing Penalty (veh)										
Storage Bay Dist (m)			80.0			140.0			180.0	
Storage Blk Time (%)				0						
Queuing Penalty (veh)				0						

## Intersection: 3: Davis Road & Lundys Lane

Movement	EB	EB	WB	WB	WB	NB	NB	SB	SB	SB	
Directions Served	L	TR	L	Т	R	L	TR	L	Т	R	
Maximum Queue (m)	82.6	143.3	82.6	191.2	86.9	27.8	81.9	173.1	248.3	81.8	
Average Queue (m)	40.8	67.8	13.4	109.6	27.0	12.1	39.5	108.8	75.5	28.7	
95th Queue (m)	71.9	115.4	51.7	196.5	90.1	23.2	69.2	190.9	265.3	60.5	
Link Distance (m)		266.3		1920.7			458.7		610.8		
Upstream Blk Time (%)											
Queuing Penalty (veh)											
Storage Bay Dist (m)	85.0		65.0		80.0	55.0		90.0		100.0	
Storage Blk Time (%)	1	4		23			4	45	0		
Queuing Penalty (veh)	7	8		59			2	138	0		

Queuing and Blocking Report

<2035 Total - Thorold Townline> PM Peak Hour 09-23-2021

#### Intersection: 4: Thorold Townline Road & Thorold Stone Road

Maximum	50	<b>FD</b>		FD	D04	D04				W/D	ND	ND
wovement	EB	EB	EB	EB	BZ4	BZ4	WB	<b>WB</b>	VVB	VVB	INB	INB
Directions Served	L	Т	Т	R	Т	Т	L	Т	Т	R	L	TR
Maximum Queue (m)	93.2	147.9	158.6	125.3	63.9	64.2	92.1	157.7	148.1	20.6	69.2	119.9
Average Queue (m)	51.7	113.6	116.7	21.1	4.2	6.3	26.9	100.5	91.3	4.9	35.1	68.9
95th Queue (m)	83.2	146.9	150.0	72.3	63.7	79.0	60.1	143.8	135.1	13.9	62.4	113.2
Link Distance (m)		279.0	279.0		315.3	315.3		338.6	338.6			1028.0
Upstream Blk Time (%)					0	0						
Queuing Penalty (veh)					0	0						
Storage Bay Dist (m)	100.0			50.0			85.0			90.0	80.0	
Storage Blk Time (%)	0	20	43				0	21	10		0	6
Queuing Penalty (veh)	0	47	42				0	24	4		0	12

Intersection: 4: Thorold Townline Road & Thorold Stone Road

Movement	SB	SB
Directions Served	L	TR
Maximum Queue (m)	174.9	304.0
Average Queue (m)	56.7	202.6
95th Queue (m)	182.7	346.1
Link Distance (m)		311.8
Upstream Blk Time (%)		13
Queuing Penalty (veh)		0
Storage Bay Dist (m)	75.0	
Storage Blk Time (%)		61
Queuing Penalty (veh)		29

#### Intersection: 5: Thorold Townline Road & Lundys Lane

Movement	EB	EB	EB	WB	WB	NB	NB	SB	SB	SB	
Directions Served	L	Т	R	L	TR	L	TR	L	Т	R	
Maximum Queue (m)	90.0	86.4	40.5	23.0	125.6	60.9	82.2	66.0	80.4	61.0	
Average Queue (m)	36.2	46.5	6.9	7.0	66.8	31.0	36.8	24.3	29.1	25.9	
95th Queue (m)	76.0	79.6	27.4	17.4	109.9	55.0	66.4	48.1	61.9	51.6	
Link Distance (m)		1920.7			479.5		741.7		1500.2		
Upstream Blk Time (%)											
Queuing Penalty (veh)											
Storage Bay Dist (m)	90.0		20.0	55.0		25.0		25.0		30.0	
Storage Blk Time (%)	2	16	0		11	29	23	16	11	7	
Queuing Penalty (veh)	13	38	1		5	56	26	49	30	15	

Uppers Quarry Traffic Impact Study TMIG SimTraffic Report Page 1 Uppers Quarry Traffic Impact Study TMIG

#### <2035 Total - Thorold Townline> PM Peak Hour 09-23-2021

Intersection: 6: Thorold Townline Road & Beaverdams Road

Movement	EB	WB	NB	SB
Directions Served	LTR	LTR	LTR	LTR
Maximum Queue (m)	71.1	112.1	309.2	234.7
Average Queue (m)	34.8	54.9	133.7	100.0
95th Queue (m)	65.3	98.2	253.9	215.5
Link Distance (m)	192.4	256.5	1091.4	1028.0
Upstream Blk Time (%)				
Queuing Penalty (veh)				
Storage Bay Dist (m)				
Storage Blk Time (%)				
Queuing Penalty (veh)				

Intersection: 7: Thorold Townline Road & Uppers Lane

Movement	WB	NB	SB
Directions Served	LR	TR	L
Maximum Queue (m)	31.2	3.1	24.3
Average Queue (m)	12.0	0.1	7.3
95th Queue (m)	26.2	2.2	20.6
Link Distance (m)	1027.2	1500.2	
Upstream Blk Time (%)			
Queuing Penalty (veh)			
Storage Bay Dist (m)			15.0
Storage Blk Time (%)			2
Queuing Penalty (veh)			11

Network Summary

Network wide Queuing Penalty: 843

Uppers Quarry Traffic Impact Study TMIG

# **APPENDIX E**

Conceptual Site Access Design and Operations



PAVEMENT MARKING LEGEND							
IDENTIFICATION TYPE COLOUR WIDTH (cm)							
1	SOLID	WHITE	10				
2	3-3-3 BROKEN	WHITE	10				

## NOTES:

1) MEASUREMENTS IN METRES AND/OR MILLIMETRES UNLESS OTHERWISE SHOWN.

2) THIS DRAWING REPRESENTS A CONCEPTUAL DESIGN ONLY AND DOES NOT CONSIDER DETAILED TOPOGRAPHIC INFORMATION INCLUDING GRADING AND UTILITY LOCATIONS.

3) LANE DIMENSIONS AS SHOWN REPRESENT THE MINIMUM CRITERIA AS PER THE 2017 TRANSPORTATION OF CANADA (TAC) GEOMETRIC DESIGN GUIDELING FOR CANADIAN ROADS. FINAL DIMENSIONS AND LAYOUT / LOCATION OF AUXILIARY LANES TO BE DETERMINED THROUGH DETAILED DESIGN AND CONSULTATION WITH MUNICIPAL STAFF.

PAVEMENT MARKING DENOTATION:

⊗ PERMANENT



UPPERS QUARRY - THOROLD TOWNLINE ROAD UPPERS LANE CONCEPTUAL INTERSECTION DESIGN OPTION 1: SOUTHBOUND SLIP AROUND LANE



PROJECT No: 16137

DATE: SEPT. 2021 SCALE: N.T.S.







## INBOUND LEFT TURN - OUTBOUND RIGHT TURN

# INBOUND LEFT TURN - OUTBOUND RIGHT TURN





UPPERS QUARRY - THOROLD TOWNLINE ROAD UPPERS LANE VEHICLE MOVEMENT DIAGRAM QUARRY TRUCK INBOUND AND OUTBOUND MANOEUVRES 1) MEASUREMENTS IN METRES AND/OR MILLIMETRES UNLESS OTHERWISE SHOWN.

2) THIS DRAWING REPRESENTS A CONCEPTUAL DESIGN ONLY AND DOES NOT CONSIDER DETAILED TOPOGRAPHIC INFORMATION INCLUDING GRADING AND UTILITY LOCATIONS.

3) WHILE THE PREFERRED AGGREGATE HAUL ROUTE IS TO THE NORTH VIA THOROLD TOWNLINE (THUS THE PROVISION OF A NORTHBOUND ACCELERATION LANE AND SOUTHBOUND LEFT-TURN LANE IN THE CONCEPTUAL DESIGN), OTHER FORMS OF SITE TRAFFIC MAY ACCESS THE QUARRY FROM THE SOUTH. A DEDICATED NORTHBOUND RIGHT TURN LANE HAS BEEN INCLUDED IN THE CONCEPTUAL DESIGN TO ACCOMMODATE NON-AGGREGATE SITE TRAFFIC WITHOUT IMPEDING NORTHBOUND THROUGH TRAFFIC.



PROJECT No: 16137 SCALE: 1:500



DATE: SEPT. 2021



# **APPENDIX F**

Sightline Assessment

-7/1-C

Stopping sight distance is the sum of the distance travelled during the perception and reaction time and the braking distance.

SSD = 0.278Vt + 0.039 
$$\frac{V^2}{a}$$
 (2.5.2)

Where:

SSD = Stopping sight distance (m)

t = Brake reaction time, 2.5 s

- V = Design speed (km/h)
- a = Deceleration rate (m/s²)

**Table 2.5.2** gives the minimum stopping sight distances on level grade, on wet pavement, for a range of design speeds. These values are used for vertical curve design, intersection geometry and the placement of traffic control devices. The stopping sight distances quoted in **Table 2.5.2** may need to be increased for a variety of reasons related to grade and vehicle type as noted below.

Table 2.5.2: Stopping Sight Distance on level roadways for Automobiles⁵⁴

Design speed	Brake reaction	Braking distance	Stopping sight distance			
(km/h)	distance (m)	on level (m)	Calculated (m)	Design (m)		
20	13.9	4.6	18.5	20		
30	20.9	10.3	31.2	35		
40	27.8	18.4	46.2	50		
50	34.8	28.7	63.5	65		
60	41.7	41.3	83.0	85		
70	48.7	56.2	104.9	105		
80	55.6	73.4	129.0	130		
90	62.6	92.9	155.5	160		
100	69.5	114.7	184.2	185		
110	110 76.5		215.3	220		
120	120 83.4		248.6	250		
130	130 90.4		284.2	285		

Note: Brake reaction distance predicated on a time of 2.5 s; deceleration rate of 3.4 m/s² used to determine calculated sight distance.

## The Effect of Grade

Braking distances will increase on downgrades and decrease on upgrades. When the roadway is on a grade, formula 2.5.1 for braking distance is modified as follows:

$$d_b = \frac{V^2}{254 [(a/9.81) + G]}$$
 (2.5.3)

Where:

d_b = Braking distance (m)

V = Design speed (km/h)

a = Deceleration rate (m/s²)

G = Grade (m/m) (G is positive if vehicles uphill and negative if downhill)

It has been noted that many drivers, particularly those in automobiles, do not compensate completely (i.e., by acceleration or deceleration) for the changes in speed caused by grade. It should also be noted that in many cases the sight distance available on downgrades is greater than on upgrades, which can help to provide the necessary corrections for grade. The following **Table 2.5.3** summarizes the stopping sight distances on grades for a variety of design speeds.

	Stopping Sight Distance (m)								
Design Speed (km/h)	Dov	vngrades	; (%)	Upgrades (%)					
	3	6	9	3	6	9			
20	20	20	20	19	18	18			
30	32	35	35	31	30	29			
40	50	50	53	45	44	43			
50	66	70	74	61	59	58			
60	87	92	97	80	77	75			
70	110	116	124	100	97	93			
80	136	144	154	123	118	114			
90	164	174	187	148	141	136			
100	194	207	223	174	167	160			
110	227	243	262	203	194	186			
120	263	281	304	234	223	214			
130	302	323	350	267	254	243			

## Table 2.5.3: Stopping Sight Distance on Grades⁵⁵

Limiting the sight distance to the stopping sight distance may preclude drivers from performing unusual, evasive maneuvers. Similarly, stopping sight distance may not provide drivers with enough visibility to allow them to piece together warning signals and decide on a course of action. Because decision sight distance allows drivers to maneuver their vehicles or vary their operating speed rather than stop, decision sight distance is much greater than stopping sight distance for a given design speed.

Designers should use decision sight distance wherever information may be perceived incorrectly, decisions are required, or control actions are required. Examples of situations where it could be desirable to provide decision sight distance include:

- Complex interchanges and intersections
- Locations where unusual or unexpected maneuvers occur
- Locations where significant changes to the roadway cross section are made
- Areas where there are multiple demands on the driver's decision-making capabilities from road elements, traffic control devices, advertising, traffic, etc.
- Construction zones

**Table 2.5.6** shows the range of values for decision sight distance. The decision sight distance increases with the complexity of the evasive action that is taken by the driver and with the complexity of the surroundings. The values for decision sight distance given in the table were developed from empirical data. When using these sight distances, the designer should consider eye and object heights appropriate for specific applications. Refer to **Section 2.4.3.3** Driver Eye Height and **Section 2.5.2.1** Object Height for additional information.

	Decision Sight Distance for Avoidance Maneuver (m)								
Design Speed (km/h)	A	В	С	D	E				
50	75	160	145	160	200				
60	95	205	175	205	235				
70	125	250	200	240	275				
80	155	300	230	275	315				
90	185	360	275	320	360				
100	225	415	315	365	405				
110	265	455	335	390	435				
120+	305	505	375	415	470				

## Table 2.5.6: Decision Sight Distance⁶⁸